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ACCOUNT OF THE OPERATIONS OF THE  
GREAT TRIGONOMETRICAL SURVEY OF INDIA

VOLUME XVI.

DETAILS  
OF  
THE TIDAL OBSERVATIONS

TAKEN DURING THE PERIOD FROM 1873 TO 1892

AND

A DESCRIPTION OF THE  
METHODS OF REDUCTION

BY

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NOTE.

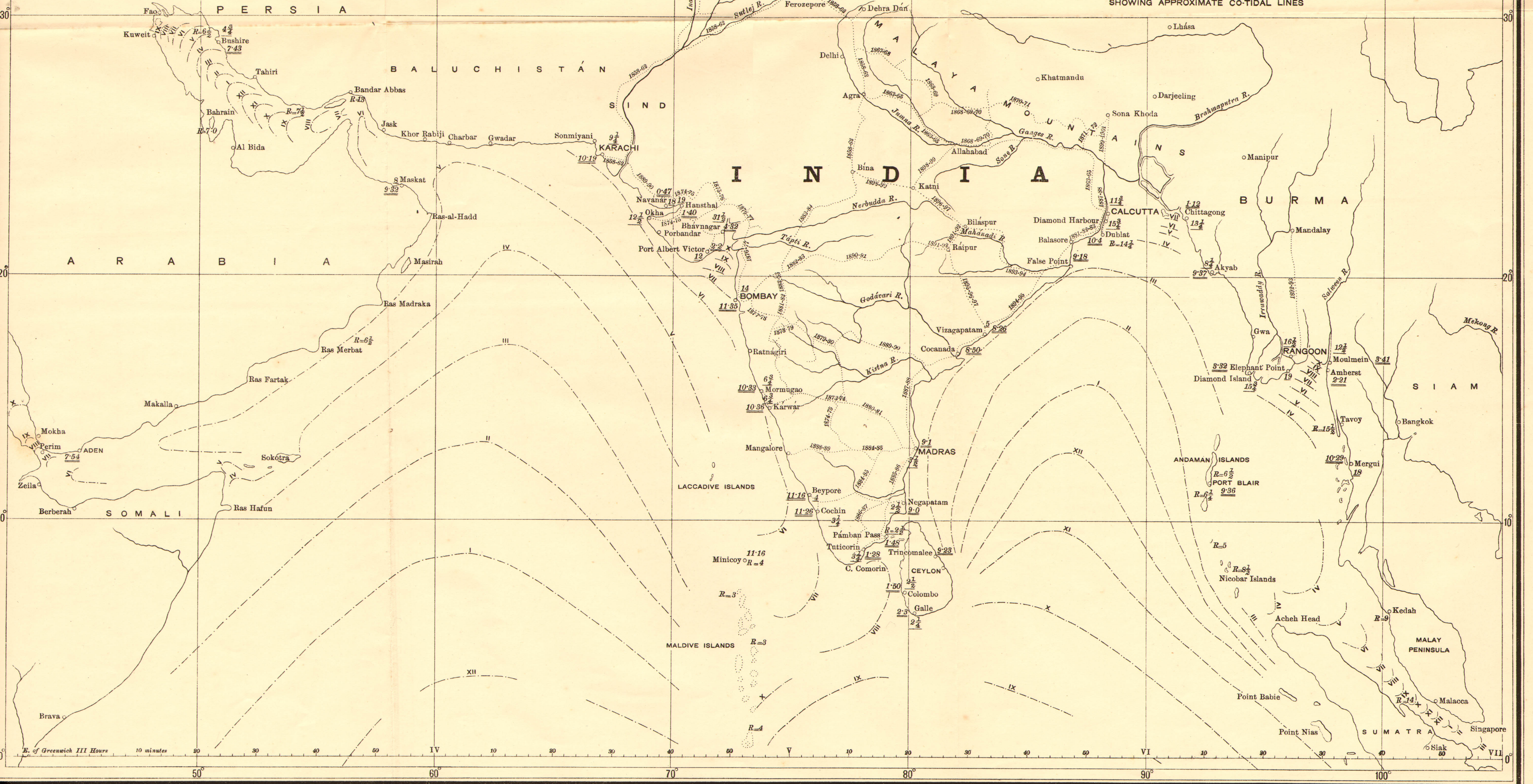
MEAN ESTABLISHMENTS determined from Survey of India Department observations are shown outside the coast-line in Italic figures doubly underlined.

APPROXIMATE CO-TIDAL LINES are shown by the dot-bar lines in the sea; and the Greenwich time of the tide is shown by the Roman Numeral preceding the co-tidal line.

THE MEAN RANGE OF GREATEST ORDINARY SPRINGS in feet is shown by the Italic figures within and along the coast-line; and by the symbol 'R=' in the sea. The values underlined have been obtained from Survey of India Department observations.

THE LEVELLING OPERATIONS are shown by dotted lines over which the dates of the operations have been printed in Italics.

CHART  
(ON MERCATOR'S PROJECTION)  
OF THE  
TIDAL AND LEVELLING OPERATIONS  
OF THE  
SURVEY OF INDIA DEPARTMENT  
1858-1892  
SHOWING APPROXIMATE CO-TIDAL LINES



E. of Greenwich III Hours 10 minutes 80 30 40 50 IV 10 20 30 40 50 V 10 20 30 40 50 VI 10 20 30 40 50 VII 10 20 30 40 50



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## P R E F A C E.



The present volume—the sixteenth—of the *Account of the Operations of the Great Trigonometrical Survey of India*, is devoted to the Indian Tidal Observations, and has been written and arranged by Mr. John Eccles, M.A.

The observations, with which this volume deals, were taken during the period from 1873 to 1892: the printing and preparation of the volume have been protracted over a longer time than was anticipated, owing to the stock of type at the Survey Office in Dehra Dún being very limited.

Tidal Observations were originally commenced in India with a view to investigating the secular changes, which were believed to be occurring, more particularly on the coast of Káthiáwár, in the relative level of land and sea. About the same time as the question of these secular changes was raised in India, a committee of the British Association for the Advancement of Science—presided over by Sir William Thomson—initiated a system of tidal investigations, which it was anticipated would secure scientific results of the highest value. Colonel J. T. Walker, R.E., F.R.S., recommended to the Government of India, that the committee's system should be followed, pointing out that, if this were done, the results would not only serve the purpose for which they were originally contemplated, but would materially contribute towards the attainment of a better knowledge of the laws of tides, which it was expected would lead to an evaluation of the mass of the moon, to information regarding the rigidity of the earth, to an approximation of the depth of the sea from the observed velocities of tide-waves, to the retardation of the earth's rotation due to tidal friction, and to various practical benefits accruing to navigation from accurate predictions of the height of the tide at any given time, and the publication of Tide Tables.

The officer selected by Colonel Walker to take charge of the Indian Tidal Operations was Lieutenant A. W. Baird, R.E., (now Colonel A. W. Baird, C.S.I., R.E., F.R.S.). Lieutenant Baird was deputed to Europe to study the practical details of the method of tidal registration and of the harmonic analysis of observations. On his return to India in 1877 he opened the first tidal observatories and trained the original staff of observers and computers. He remained in charge of the Indian Tidal work until 1886, when he was appointed Master of Her Majesty's Mint at Calcutta. The methods of observation and computation introduced by Lieutenant Baird have been continued without modification to the present day.

Colonel Baird's successor was Colonel John Hill, R.E., who held charge of the Indian Tidal Operations from 1886 to the date of his retirement from the service of Government in 1895.

On three occasions, namely in 1881, 1882 and 1888 during the absence of Colonels Baird and Hill, the control of the Tidal work devolved on Colonel Malcolm W. Rogers, R.E., afterwards Assistant Surveyor General at Calcutta.

From 1873 to 1885 Mr. T. H. Rendell was the Tidal Assistant for the inspection of observatories. He was succeeded in 1885 by Mr. G. P. Belcham, who retained this post until his retirement in 1900.

In 1877 Mr. E. J. Connor was appointed to supervise the Tidal computations, and this important duty he has continued to perform until the present date, 1901.

The tidal observatories with which this volume deals are:—

Site of Observatory	Years of Observation
1. Aden ... ..	1879 to 1892 = 13 years
2. Kurrachee (Karachi) ... ..	1881 „ 1892 = 11 „
3. Navánár ... ..	1874 „ 1875 = 1 year
4. Hansthal Point ... ..	1874 „ 1875 = 1 „
5. Okha Point and Bet Harbour ... ..	1874 „ 1875 = 1 „
6. Port Albert Victor (Káthiwadar) ... ..	1881 „ 1882 = 1 „
7. Bhávnagar ... ..	1889 „ 1892 = 3 years
8. Bombay (Apollo Bandar) ... ..	1878 „ 1892 = 14 „
9. Bombay (Prince's Dock) ... ..	1888 „ 1892 = 4 „
10. Marmugáo (Goa) ... ..	1884 „ 1889 = 5 „
11. Kárwár ... ..	1878 „ 1883 = 5 „
12. Beypore ... ..	1878 „ 1884 = 6 „
13. Cochin ... ..	1886 „ 1892 = 6 „
14. Tuticorin ... ..	1888 „ 1892 = 4 „
15. Minicoy ... ..	1891 „ 1892 = 1 year
16. Galle ... ..	1884 „ 1890 = 6 years
17. Colombo ... ..	1884 „ 1890 = 6 „
18. Trincomalee ... ..	1890 „ 1892 = 2 „
19. Pámban Pass ... ..	1878 „ 1882 = 4 „
20. Negapatam ... ..	1881 „ 1888 = 6 „ *
21. Madras ... ..	1880 „ 1890 = 10 „
22. Cocanada ... ..	1886 „ 1891 = 5 „
23. Vizagapatam ... ..	1879 „ 1885 = 6 „
24. False Point ... ..	1881 „ 1885 = 4 „
25. Dublat (Saugor Island) ... ..	1881 „ 1886 = 5 „
26. Diamond Harbour ... ..	1881 „ 1886 = 5 „
27. Kidderpore (Calcutta) ... ..	1881 „ 1892 = 11 „
28. Chittagong ... ..	1886 „ 1891 = 5 „
29. Akyab ... ..	1887 „ 1892 = 5 „
30. Elephant Point, Open Coast Station (at Old Site) ... ..	1880 „ 1881 = 1 year
30A. Elephant Point, Riverain Station (at New Site) ... ..	1884 „ 1888 = 5 years
31. Rangoon ... ..	1880 „ 1892 = 12 „
32. Amherst ... ..	1880 „ 1886 = 6 „
33. Moulmein ... ..	1880 „ 1886 = 6 „
34. Mergui ... ..	1889 „ 1892 = 3 „
35. Port Blair ... ..	1880 „ 1892 = 12 „

\* The year 1884-85 has been excluded.

Since this volume was written in 1892, new tidal observatories have been opened, mostly at the advice of Professor G. H. Darwin, F.R.S. Observations taken at Indian observatories, subsequent to the year 1892, will be recorded in a future volume of this series. In the following table is given a complete list of all Indian tidal observatories with the periods of observation.

Site of Observatory	Automatic or Personal Observations	Date of Commencement of Observations	Date of Closing of Observations	Number of Years of Observations	REMARKS	
1. Suez ... ..	Automatic	1897	Still working	3		
2. Perim ... ..	Do.	1898	Do.	2		
3. Aden ... ..	Do.	1879	Do.	20		
4. Maskat ... ..	Do.	1893	1898	5		
5. Bushire ... ..	Do.	1892	Still working	7		
6. Kurrachee (Karachi) ... ..	Do.	1881	Do.	19		
7. Hansthal ... ..	Do.	1874	1875	1		
8. Navánár ... ..	Do.	1874	1875	1		
9. Okha Point ... ..	Do.	1874	1875	1		
10. Porbandar ... ..	Personal	1893	1894	2		
10A. Porbandar ... ..	Automatic	1898	Still working	2		
11. Port Albert Victor (Káthiwadar) ... ..	Personal	1881	1882	1		
11A. Port Albert Victor (Káthiwadar) ... ..	Automatic	1900	Still working	...		
12. Bhávnagar ... ..	Do.	1889	1894	5		
13. Bombay (Apollo Bandar) ... ..	Do.	1878	Still working	22		
14. Bombay (Prince's Dock) ... ..	Do.	1888	Do.	12		
15. Mormugáo (Goa) ... ..	Do.	1884	1889	5		
16. Kárwár ... ..	Do.	1878	1883	5		
17. Bepore ... ..	Do.	1878	1884	6		
18. Cochin ... ..	Do.	1886	1892	6		
19. Tuticorin ... ..	Do.	1888	1893	5		
20. Minicoy ... ..	Do.	1891	1896	5		
21. Galle ... ..	Do.	1884	1890	6		
22. Colombo ... ..	Do.	1884	1890	6		
23. Trincomalee ... ..	Do.	1890	1896	6		
24. Pámban Pass ... ..	Do.	1878	1882	4		
25. Negapatam ... ..	Do.	1881	1888	6		
					The year 1884-85 has been excluded.	
26. Madras ... ..	Do.	{ 1880 Re-started 1895	1890	10	} 15	
27. Cocanada ... ..	Do.	1886	1891	5		
28. Vizagapatam ... ..	Do.	1879	1885	6		
29. False Point ... ..	Do.	1881	1885	4		
30. Dublat (Saugor Island) ... ..	Do.	1881	1886	5		
31. Diamond Harbour ... ..	Do.	1881	1886	5		
32. Kidderpore ... ..	Do.	1881	Still working	19		
33. Chittagong ... ..	Do.	1886	1891	5		
34. Akyab ... ..	Do.	1887	1892	5		
35. Diamond Island ... ..	Do.	1895	1899	5		
36. Elephant Point ... ..	Do.	{ 1880 Re-started 1884	1881	1		} 6
37. Rangoon ... ..	Do.	1880	1888	5		
38. Amherst ... ..	Do.	1880	Still working	20		
39. Moulmein ... ..	Do.	1880	1886	6		
40. Mergui ... ..	Do.	1880	1886	6		
41. Port Blair ... ..	Do.	1889	1894	5		
		1880	Still working	20		

Thirty-five tides are evaluated in this volume, viz:—

- 8 Semi-diurnal Lunar Tides,
- 5 Diurnal Lunar Tides,
- 3 Long-Period Lunar Tides,
- 3 Semi-diurnal Solar Tides,
- 2 Diurnal Solar Tides,
- 2 Long-Period Solar Tides,
- 5 Compound Tides,
- 7 Over-Tides.

In addition, an endeavour has recently been made by Mr. Eccles, on a method devised by Professor Darwin, to evaluate the Latitude-variation Tide and the 19-yearly Nodal Tide at Bombay. Mr. Eccles' results have been sent to Professor Darwin for his opinion.

From the commencement of the tidal operations it was arranged by Colonel Walker and Lieutenant Baird, that each observatory should be furnished with a complete equipment of meteorological instruments, and daily records of temperature, pressure and wind have been taken at every station. These records are available for future investigation, but no effective use has hitherto been made of them. Some attempts have been made in India to trace a connection between errors of tidal prediction and the effects of wind and pressure, but so far without success. Great difficulties beset these investigations: irregular tides falsifying predictions, may be produced on a coast by the occurrence in mid-ocean of storms, which are too distant to affect the barometer or anemometer of the tidal station; or the effects of storms may be transmitted through the air and the water at widely different velocities, and may thus be recorded on the tidal and meteorological instruments at widely differing times.

The several tidal stations on the coast of India have been connected with each other by trans-continental lines of spirit-levelling, executed with the utmost precision, the details and results of which will be embodied in a subsequent volume of this series. As, however, it has been found necessary, for the aid of engineering projects, to reduce the levels in every part of India to one common datum, the closing errors of the lines of spirit-levelling have been dispersed, and the corrected values of the levels have been published in pamphlets. The dispersion of errors, which has hitherto been carried out, must be regarded as preliminary only, and the method of adjustment, which is to be finally adopted, cannot yet be decided. In the preliminary dispersion the determinations of mean sea-level at Indian tidal stations have been *assumed* to be errorless: the closing errors, that appear at the ends of lines of levels, carried from tidal station to tidal station, have been *assumed* to be due to the spirit-levelling operations only, and the values of the heights of intermediate stations have been corrected accordingly. The possible fallibility of these assumptions is recognised. Each succeeding year's tidal observations give additional data; new and more correct values of mean sea-level, than those which have been adopted, are annually being deduced. As, moreover, the several lines of levels cross and recross each other, now forming a network, the method of dispersing each closing error, as it appears, over its own immediate line, can only be regarded as a temporary expedient, and the system of successive distributions must at some future date be replaced by a simultaneous reduction: the probability of error in the determinations of mean sea-level will then have to be considered.

The height of the tidal station at False Point, as derived from the direct determination of mean sea-level in the Bay of Bengal, was 1.72 feet *lower* than the value given by a line of spirit-levelling, 2223 miles long, which had emanated from the mean sea-level at Karachi,—the mean sea-level in the Bay of Bengal being thus apparently 1.72 feet *higher* than that at Karachi. On the line of levels, 1065 miles in length, which connects Bombay with Vizagapatam, a closing error of 1.363 feet appeared, the direct determination of mean sea-level at Vizagapatam being *higher* than the value derived by levelling from Bombay.

This volume has been written to give, firstly, an account of the tidal observations that have been taken, secondly, an explanation of the methods of computation, and thirdly, an abstract of the results, that have been obtained. The letter-press contains the theory of tides, as expounded by Professor Darwin, and no original investigations have been attempted. The co-tidal chart attached to this volume was prepared by Colonel J. Hill, R.E., from whom also Mr. Eccles has received valuable assistance. Chapters I and II contain historical sketches, and were compiled by Mr. Eccles from the Encyclopædia Britannica and from the records of the Government of India. Chapters III to V are based on the Manual of Tidal Observations, written by Major A. W. Baird, R.E., in 1886. Chapter III is devoted to a description of the tidal instruments and of a tidal observatory; in Chapter IV are explained the principles, that govern the selection of a site for a tidal station, the methods of erecting and adjusting the instruments, and the duties of the observer and

inspecting officer; in Chapter V it is explained how the tidal diagrams are prepared. Chapters VI and VII are devoted to the harmonic analysis of tides, and have been compiled by Mr. Eccles from Professor Darwin's Reports to the British Association for the Advancement of Science. Chapter VIII deals with tidal prediction, and has been compiled from the writings of Mr. E. Roberts, F.R.A.S., under whose directions the tide tables for the Indian ports from 1880 to the present date have been produced: Part I of this chapter has been derived from an article by Mr. Roberts, which appeared in the 'Engineer' of December 19th, 1879, and Part II was written by Mr. Roberts at Mr. Eccles' request for this volume.

In conclusion I must acknowledge, on behalf of many successive officers of the Survey of India Department, our great indebtedness to Professor George Howard Darwin, M.A., L.L.D., F.R.S., F.R.A.S., Plumian Professor of Astronomy and Experimental Philosophy, Cambridge, for the valuable assistance which we have uniformly received from him during the progress of the tidal operations in India, and for the many benefits which we have derived from his published writings on tides. Without the cordial co-operation and sympathy of this eminent mathematician the success, that has attended the Indian Tidal work, could not have been achieved.

S. G. BURRARD, MAJOR, R.E.,

*Superintendent Trigonometrical Surveys.*

*Delra Dún, February, 1901.*



## PART I.

## PAGE

- 20 line 22 from bottom      *for* band      *read* bend
- 163 A black vertical line should be inserted against 7'78 in row 131, column 19<sup>b</sup>.
- 164 The black vertical line against 14'86 in row 166, column 21<sup>b</sup>, should be against 15'00 in column 20<sup>b</sup>.
- 253 The black vertical line against 11'70 in row 111, column 1<sup>b</sup>, should be against 13'86 in the same column.
- 294 to 297 In all the places V<sub>o</sub> should be in italic type.
- 298 to 315 In all the places      *for* dh      *read* δh

## PART II.

- 78 line 5 from top      *for* Kadavcár      *read* Kadaveár
- 82 „ 2 „      „ Lat. 13° 5' N.      „ Lat. 13° 6' N.





# TIDAL OBSERVATIONS

## PART I.

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DESCRIPTION OF THE INSTRUMENTAL EQUIPMENT

AND OF

THE OPERATIONS GENERALLY

WITH

DETAILS OF THE SYSTEM OF OBSERVING

AND OF

REDUCING THE OBSERVATIONS.



## CHAPTER I.

## INTRODUCTORY.

## 1.

*Brief Historical Sketch.*

The ordinary phenomena of the rise and fall of the waters of the sea approximately twice a day, of the dependence of the times of high water on the passages of the moon and sun across the meridian, and of the heights of the tide on the relative position of the sun and moon with regard to the earth, are familiar to most people at the present day. It is, however, only of comparatively late years in the world's history that anything definite has been known of the true cause of the various changes in the sea-level, and it is only quite recently that systematic observations have been made on them. The ancients seem to have known very little about the tides, probably from their voyages having been made for the most part in the Mediterranean Sea where there is no sensible tide except at the ends of deep bays. Homer is supposed to have referred to them in the 12th book of the *Odyssey* where he speaks of Charybdis rising and retiring thrice a day, and Herodotus and Diodorus Siculus speak of the tides in the Red Sea. The first person who appears to have had an idea as to their cause was Pytheas, a navigator of Marseille, who lived about 330 B. C. and made some voyages in the northern seas of Europe. It is stated of him, by Plutarch, that he ascribed the phenomena of the tides to the moon. The Greeks can have been little acquainted with the tides, for it is recorded that the army of Alexander the Great was startled on first seeing them near the Persian Gulf. Besides, Aristotle in all his works only speaks of the tides three times; he mentions the great tides in the north of Europe, and states that the tides were ascribed by some (probably Pytheas) to the moon and that the tide in a great sea exceeds that in a small one. Among the Romans, as might be expected from the extent of their conquests, more frequent reference is made to the phenomena of the tides: Cæsar mentions them in *De Bello Gallico*, Book iv, and Strabo, following in the wake of Posidonius who appears to have had a very clear idea of the subject, divides the phenomena into daily, monthly, and annual. He observes that the sea rises as the moon approaches the meridian whether above or below the horizon and falls again as she rises or falls, that the tides increase at new and full moon, and are greatest at the summer solstice. Pliny explains the phenomena at some length, and ascribes them to the sun and moon dragging the waters along with them. Seneca and Macrobius also speak of the tides, and describe their motions with some degree of accuracy.

The next one who did anything more than merely collect the opinions of his predecessors was Kepler. In accounting for the tides he seems to have been aware of the principle of gravitation, but

not of the law. He says that all bodies attract each other, and that the waters of the ocean would all go to the moon were they not retained by the attraction of the earth. He then proceeds to explain that their elevation under the moon and on the opposite side is owing to the earth being less attracted by the moon than the nearer waters, but more than the waters which are more remote. Galileo objected to this theory and expressed regret that so acute a man as Kepler should have produced a theory which appeared to him to reintroduce the occult qualities of the ancient philosophers.

Such is a brief statement of what had been done prior to 1687 when Newton laid the foundation of all that has since been added to the theory of the tides by bringing his grand generalization of universal gravitation to bear on the subject. In the 19th corollary of the 66th proposition of Book i of the *Principia*, he introduces the conception of a canal circling the earth, and considers the influence of a satellite on the waters of the canal. It is, however, in Book iii, propositions 26 and 27, that he first determines the tidal force due to the sun and moon which are supposed to move in the equator, while the sea is supposed to cover the whole earth and to assume at each instant a figure of equilibrium. Considering only the action of the sun, he assumes this figure to be an ellipsoid of revolution with its major-axis directed towards the sun. The action of the moon produces a similar ellipsoid but of greater ellipticity, and the superposition of these two ellipsoids gives the principal variations of tide. This hypothesis, however, gave results discordant from the actual state of the tides, and in 1738 the Academy of Sciences of Paris offered as a subject for a prize, the theory of the tides. The authors of four essays received prizes; *viz.*, Daniel Bernoulli, Euler, Maclaurin and Cavalleri. Bernoulli's essay contained an extended development of the conception of the two ellipsoids, and under the name of the *equilibrium theory* is commonly associated with his name. The theory of the tidal movements of an ocean was therefore, as Laplace remarks, almost untouched when in 1774 he first undertook the subject. In the *Mécanique Céleste* he gives an investigation of the tides of an ocean covering the whole earth, but the theory although very comprehensive is far from representing the actual state of the case. Observation shows, in fact, that the irregular distribution of land and water and the variable depth of the ocean produce an irregularity in the oscillations of the sea of such complexity, that a rigorous solution of the problem is altogether beyond the power of analysis. Laplace, however, rested his discussion of tidal observation on the principle that—*The state of oscillation of a system of bodies in which the primitive conditions of movement have disappeared through friction is copieriodic with the forces acting on the system.* Hence if the sea is solicited by a periodic force, expressed as a coefficient multiplied by the cosine of an angle which increases proportionately with the time, there results a partial tide, also expressed by the cosine of an angle which increases at the same rate; but the phase of the angle and the coefficient of the cosine in the expression for the height may be very different from those occurring in the corresponding term of the equilibrium theory. The coefficients and the constants or epochs of the angles in the expressions for the tide are only derivable from observation. The action of the sun and moon is expressible in a converging series of similar cosines; whence arise the same number of partial tides, and these by the principle of superposition may be added together to give the total tide at any port. In order to unite the several constants of the partial tides, Laplace considers each tide as being produced by a fictitious satellite moving uniformly on the equator. Sir William Thomson and others have followed Laplace in this, but the method which is now adopted is due to Professor G. H. Darwin. The difference of treatment is in reality only a matter of phraseology, and the proper motion of each one of Laplace's *astres fictifs* is at once derivable from the *argument*, or angle under the sign of cosine, which Darwin associates with the partial tides.

Subsequently to Laplace the most important workers in the field were Sir John Lubbock (senior), Whewell, Airy and G. H. Darwin. The work of Lubbock and Whewell is chiefly remarkable for the coordination and analysis of enormous masses of data at various ports, and the construction of trustworthy tide-tables and co-tidal maps. Airy contributed an important review of the whole tidal theory. He also studied profoundly the theory of waves in canals, and explained the effects of frictional

resistances on the progress of tidal and other waves. Darwin's principal contribution to the theory of the tides is contained in a Report to the British Association of a Committee for the Harmonic Analysis of Tidal Observations in 1883. In this paper he cuts himself free from the trammels of the *astres fictifs*, and exhibits each partial tide as depending directly on some periodic term in the development of the tide-generating potential of the moon and sun. He further applies the analytical method of harmonic analysis to the evaluation of the various constants, and reduces the expression for the height of the tide to a form adapted for arithmetical calculation.

## 2.

### *Early Observations.*

One of the earliest sets of tidal observations was that taken at Brest between 1800 and 1806, followed, at the request of Laplace, by another set extending five years longer. It was with the results of these that Laplace compared his theory. About the year 1830 the construction of a self-registering tide-gauge gave a great impulse to tidal observations: continuous records of the tidal heights at numerous ports all over the globe were obtained, and tide-tables and co-tidal charts constructed.

The earliest observations taken in India appear to be those executed by James Kyd at the Kidderpore dock on the Hooghly between the years 1806 and 1827, and continued two more years on Saugor Island, the results being published in a series of diagrams. The next appear to be those of Colonel DeHavilland at Madras in 1821, but after the publication by Dr. Whewell of some suggestions in the Journal of the Asiatic Society of Bengal in 1833, where he expressed a hope that tidal observations would be made extensively in India, some observations were made at various places on the coast. More numerous, however, were the observations made by the Survey, Irrigation and Marine Departments in connection with their various works where a properly determined datum on which to found heights is essential. As a general rule they were personal observations, taken with a pole, sometimes only of high and low water, and at others of the heights of the tide at intervals of a quarter of an hour to an hour, but seldom extending for more than a month. The first time that a self-registering tide-gauge was used in India was in 1855 when, in connection with the triangulation, Lieutenant J. F. Tennant, R.E., of the Great Trigonometrical Survey, took observations at Kurrachee by means of a small instrument indicating variations of level to the one-hundredth part of a foot. At Kurrachee, personal observations were begun by Mr. W. Parkes, M.I.C.E., in 1857 and were continued by Mr. Price, M.I.C.E., Superintendent of the Kurrachee Harbour works, with very few interruptions till 1868, when a small self-registering instrument was erected by which the tidal curves were drawn graphically on a scale one-twelfth of the natural size: this continued working till December 1880. Mr. Parkes constructed tide-tables for Kurrachee from these observations; and also for Bombay from personal observations taken there. In 1871 Major B. R. Branfill of the Great Trigonometrical Survey, employed a self-registering tide-gauge at Tuticorin in connection with his triangulation: the observations extended from 12th May 1871 to 24th June 1872, and were reduced by the method of harmonic analysis. A small self-registering tide-gauge was set up at Aden in 1876, but the observations were not very carefully taken and were not very valuable. Besides these, the Marine and Irrigation Departments used self-registering tide-gauges at various places on the Hooghly in connection with their respective works of sounding and canal-making.

## CHAPTER II.

## ESTABLISHMENT OF TIDAL OPERATIONS IN INDIA.

## 1.

*Observations in the Gulf of Cutch.*

The events which led to the establishment of tide-gauges in the Gulf of Cutch are briefly as follows:—On the 18th August 1866, an article appeared in the *Bombay Saturday Review* in which two distinct questions were discussed:—*1stly* the encroachments of land on sea, or sea on land, as evidenced especially by the Gulf of Cambay and the coast of Káthiáwár; and *2ndly* the alternate rising and sinking of land as evidenced by the Ran of Cutch.

The attention of the Government of Bombay was drawn to this article and the matter was referred to T. Oldham, Esq., Superintendent of the Geological Survey of India, for his opinion. The main points of his reply were embodied in a Government resolution as follows:—“With regard to the Gulf of Cambay, the Government will be glad to adopt the suggestions of the Bombay Geographical Society and have the survey of the coast made, and the soundings taken in such detail as the Society may approve. But as to the more interesting question presented with the Ran of Cutch, it does not appear to the Governor-in-Council that watching the line of coast now or learning its past history will give the requisite information as to the raising or depression of the land \* \* \* The mean level of the sea, in the scientific acceptance of that phrase, is the only reliable datum to which observations for changes of land level should be referred \* \* \* There should therefore be a course of accurate tidal observations taken through two lunations at a point on the south coast of Káthiáwár, and also at a point as far into the Ran as possible, to which the tide has free access. These should be referred to bench-marks made in permanent masonry pillars close to high-water mark, and these marks should be connected to the nearest principal stations of the Great Trigonometrical Survey by careful levelling \* \* \* Captain C. T. Haig, R.E., should be asked whether observations for mean-sea level have been taken in this neighbourhood sufficient for the above objects and, if not, what expense would be incurred to make them and whether he would be good enough to undertake the duty.” In regard to this resolution and with reference to the scientific acceptance of the term ‘mean-sea level’ Lieut.-Colonel J. T. Walker, R.E., Superintendent of the Great Trigonometrical Survey, remarks:—“At the present time the scientific acceptance of that phrase is two-fold: it may imply either the mean of all the high and low waters, or the mean of all the heights recorded for as long a period as possible, at short and equal intervals. The first is the old acceptance of the term mean-sea level and it was the custom for many years to restrict tidal observations to the times of high and low water. But strictly speaking the mean of all the heights at indefinitely small intervals is the true mean-sea level, and this is the datum to which the

“recent Ordnance Survey Levels of England, Scotland and Wales have been referred, though the preceding levels of Ireland were referred to the mean of high and low water. The two data occasionally differ very materially; for instance, the mean-sea level at Liverpool which has been adopted from all the heights as the datum of the Ordnance Survey levels is 4.39 inches below the mean of high and low water \* \* \* while at Cardigan and Dundee the differences were found to exceed 6 inches.”

Colonel Walker and Captain Haig agreed that “The tidal observations must be carried over a much longer period than two lunations to give results of sufficient accuracy to serve the purposes of measuring the changes of level that may take place in a period of ten years”—the period which, it was contemplated by Mr. Oldham, should elapse before undertaking a second set of observations. They also agreed that it would be necessary to connect the tidal stations with the bench-marks by spirit-levelling, as the variations of height were known to be small, *viz.*, not more than a foot or two in a century. Colonel Walker also considered that the tidal observations should be taken with a self-registering tide-gauge capable of registering very small variations. These ideas were approved of, and as there were no gauges of sufficient accuracy in India, suitable ones were ordered from Adie of London, which in due time arrived. In the meantime correspondence in regard to the details was carried on, and in 1870 Lieutenant H. Trotter, R.E., was ordered to enter on the preliminary investigations of testing the gauges by setting them up at Bombay and generally putting the instruments in adjustment for use in the next season: it was not, however, until 1872 that the operations really commenced.

On 27th November 1872, Lieutenant A. W. Baird, R.E., who had been placed in charge of the Tidal and Levelling Operations in the Bombay Presidency, was ordered to proceed on a reconnaissance of the Gulf of Cutch for the selection of sites for the tidal observations, one being required as far into the Ran as possible, to which the tide has free access, another near Bet Island and a third as nearly as possible equidistant from the others. The stations were all to be, if possible, on the south side of the Gulf, but if not, the north side was to be examined; failing to find any of these sites, the south coast of Káthiáwár was to be examined.

The stations selected were:—Hansthal, about sixteen miles from Jodiya at the head of the Gulf, with seventy-two feet of water within one-hundred feet of the shore at low water: Navánár, on the Cutch Coast about ten miles from Mundra, with nineteen feet of water at low tide: Okha Point, opposite the Island of Bet, with twenty-three feet of water at low tide: so that with the exception of Navánár on the Cutch Coast, the actual positions of the selected sites almost coincided with those required. The instruments were set up on land close to high-water mark, the floats working in cylinders connected with deep water by means of pipes. The observations were commenced at Okha on 27th December 1873, at Hansthal on 13th February 1874, and at Navánár on 24th April 1874, and were continued till May 1875 when the observatories were dismantled.

In connection with the observations Captain Baird remarks:—“The party may be fairly congratulated on the general success of the project in having secured at Okha and Hansthal Tidal Stations complete sets of tidal combined with meteorological observations which will compare favourably with what has been done both in England and in America, and in having so far succeeded at Navánár Tidal Station that the observations taken will be sufficient to evaluate, by differentiating with both Okha and Hansthal which were working simultaneously, the principal data required. The levelling operations combined with the tidal observations complete the work necessary for one part of the project and fix the level of about thirty miles of the Ran of Cutch for the season 1874-75, and a repetition of the work some twenty years hence will effectually settle the question of secular depression in this peculiar region.” The cause of the discontinuity in the observations at Navánár was the silting up of the foreshore to such an extent in two months that a place, where there was twenty feet of water at low tide in April, was high and dry in July at low-tides, and some twenty-five or thirty feet inshore from low-water mark.

The reductions of these observations were for the most part done in England by Captain Baird and Mr. E. Roberts of the Nautical Almanac Office, who had made the whole of the tidal reductions for the British Association. When the work was completed Captain Baird returned to India stopping at Aden, under instructions from the India Office, to examine and set to rights a small self-registering tide-gauge which was working there. He found the previous records useless and advised that the instrument itself should be discarded and a new set of instruments substituted.

## 2.

### *Systematic Observations.*

In a resolution of the Government of India, dated 4th July 1877, the Governor General-in-Council observes:—"That the great scientific advantages of a systematic record of tidal observations on Indian coasts have frequently been urged upon and admitted by the Government of India. Hitherto the efforts in the direction of such a record have been desultory and, in many cases, wanting in intelligent guidance and careful selection of the points where the observations should be recorded. Additional importance has recently been given to the subject by the institution of a Marine Survey Department, for whose operations accurate tidal observations are a necessity without which no permanent record of the changes of ground in the different harbours of the coast can be kept up. The advantages to be expected from well considered and carefully conducted observations of the tides are mainly the following:—1. They enable standards to be fixed for the purposes of survey; 2. They afford data for the calculation of the rise and fall of the tides and thus subserve the purposes of navigation; 3. They are of scientific interest apart from their practical usefulness as stated above.

"The first two of these are of strictly local bearing: an accurate survey of a port is essential to the safety of the shipping frequenting it, and correct tide-tables are necessary for the convenience of navigators and for engineering purposes within the port itself.

"The Governor General-in-Council is of opinion that, in view of these considerations, every port where a tide-gauge is set up should pay for its establishment and maintenance from port funds. The third object, the scientific results to be expected from the record, will be sufficiently provided for by the appointment by the Government of India of one of its own officers to supervise and control the local observations and to arrange for their utilization to the utmost possible extent \* \* \* His Excellency-in-Council accordingly resolves to intrust the general superintendence and control of tidal observations upon Indian Coasts to Captain Baird, R.E., Deputy Superintendent in the Great Trigonometrical Survey Department, who will be guided in his operations by the orders and advice of the head of that department."

It was thus decided that the ports were to pay for the instruments and also for the cost of conducting the operations; but in the case of ports too poor to pay for the instruments, the use of those belonging to the Survey Department was granted on loan. The places at which gauges should be set up were settled by Captain Baird, in consultation with the Surveyor General, Colonel Walker, R.E., and Captain Taylor, Superintendent of Marine Survey. It was further decided that some of the ports should be permanent stations, that is, that the registration should be carried on continuously for at least nineteen years, while four or five years' observations would be sufficient at minor stations for all practical purposes. The arrangements for procuring and setting up the instruments were made by Captain Baird, with the various local Governments, and by October 1878 gauges were set up at Bombay, Kárwár, Vizagapatam, Pámban near Cape Comorin, and Beypore near Calicut; the establishment of a gauge at Madras was kept back by delay on the part of the port authorities there.



## CHAPTER III.

## DESCRIPTION OF THE INSTRUMENTS AND THE OBSERVATORY.

## 1.

*Self-Registering Tide-Gauge.*

The object aimed at in any complete system of tidal observations, is to obtain the height of the tide, above some fixed mark or datum, for every instant of time during a more or less extended period which has been fixed as far as regards Indian observations at not less than five years. This object is attained graphically by causing the rise and fall of the water to communicate its motion, by mechanical means, to a pencil which traces a line on paper wound round a drum turned by clock-work once in twenty-four hours. The height of the fixed mark or datum being indicated by a line on the paper, the distance of the pencil from the line, reduced to the proper scale, will be the height of the water above the datum at the time indicated by the position of the pencil.

An instrument such as above briefly described is called a Self-registering Tide-gauge, and of these, various forms have from time to time been constructed: the best form is, according to the opinion of Sir William Thomson, one in which the drum is inclined to the vertical, as this enables the friction between the pencil and the paper to be nicely regulated. The pattern almost exclusively used in India is that known as Newman's pattern in which the drum is horizontal, the only exception being a small gauge at Prince's Dock, Bombay, where the drum is vertical.

The description of the gauge in common use, or Newman's pattern, is given below, while that of the Prince's Dock Gauge will be found elsewhere in the volume.

The motion due to the rise and fall of the water is directly communicated to a float partially immersed in it; and that the float may be freed as far as possible from wave-action, it is surrounded by a cylinder made of thin iron plate to which the admission of the water is so regulated, that there is no sensible retardation between its rise and fall in the cylinder and outside.

The iron cylinder, *A*, (see Plate I) is made in lengths of from four to eight or even ten feet, with angle iron flanges at each end for bolting the lengths together: the bottom of the cylinder is generally closed with an iron plate, and the top reaches to the floor of the observatory, or sometimes one or two feet above it. The diameter of the cylinder of the ordinary pattern in use is twenty-four inches.

If the cylinder rests on the ground, the best inlet for the water is through holes, near the bottom of the cylinder, below the lowest level of spring-tides, but at the same time well clear of the ground on which the cylinder rests: if it does not rest on the ground, the bottom of the cylinder is the best place for the holes.

It sometimes happens that the cylinder cannot be fixed in deep water, and when this is the case a pipe connection between the sea and the cylinder is necessary. The piping used is ordinary gas-pipe in lengths of about fourteen to twenty-two feet with an internal diameter of two or three inches. The size of the pipe should be regulated by the double consideration that it must not be large enough to allow of irregular movements of the water being transmitted through it, nor small enough to cause any retardation of the rise and fall of the water in the cylinder; as regards the latter condition, the following computation justifies the adoption of the diameter given above.

Calculation to show the relative level of the water inside a cylinder of 24 inches diameter and that of the sea, the connection being made with a 2-inch pipe 300 feet long which has two bends of 90° each.

From Beardmore's *Manual of Hydrology*, Table 8,

$$\text{The discharge for a 2-inch pipe} = \sqrt{\frac{26 \cdot 69 l}{h}} \text{ cubic feet per minute,}$$

where

$$l = \text{the length of the pipe in feet,}$$

$$h = \text{the head of water in feet.}$$

Now, assuming the water in the sea to have risen 1 inch higher than in the cylinder, there is a head of 1 inch, and

$$\sqrt{\frac{l}{h}} = \sqrt{\frac{300 \times 12}{1}} = 60,$$

therefore, the discharge is 768 cubic inches per minute, supposing that there are no bends in the pipe.

Also the quantity of water required to raise the level of the cylinder 1 inch is  $12^3 \times \frac{22}{7}$  cubic inches nearly, that is, about 453 cubic inches, so that a head of one inch would discharge the quantity required in less than  $\frac{3}{8}$  of a minute.

But when there are bends in the pipe, the head required to overcome them varies with the angles of the bends and the velocity of the water through the pipe.

The area of the connecting pipe in section is equal to  $\frac{22}{7}$  square inches nearly, so that the length of pipe which would contain a volume of water sufficient to raise the water in the cylinder 1 inch, is  $453 \div \frac{22}{7}$  inches or 12 feet nearly; and if this amount is to be discharged into the cylinder in  $\frac{3}{8}$  of a minute, the velocity of the water must be 20 feet per minute, or a little more at the beginning and at a little less at the end to allow for the variation of the head.

Now by Beardmore's *Manual of Hydrology*, Table 9, for a mean velocity of 20 feet per minute and two bends of 90° each, a head of  $\cdot 0048 \times 2$  inches or  $\frac{1}{100}$  of an inch very nearly is required and even if a velocity of 25 feet per minute is allowed for, the head is only  $\cdot 0075 \times 2$  inches or  $\frac{1}{70}$  of an inch nearly, so that the bends need hardly be taken into account.

Now suppose that there is an 18 feet rise and fall of the tide at springs, *i.e.*, a mean of about 3 feet an hour, then the water will rise  $\cdot 36$  of an inch in  $\frac{3}{8}$  of a minute.

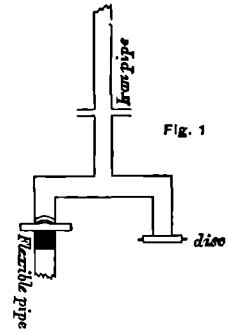
Combining the above arguments, it follows that if the sea-level was an inch higher than the water in the cylinder, the latter would be raised to this height in  $\frac{3}{8}$  of a minute by which time the sea would be  $\cdot 36$  of an inch higher. But the tide rising increases the head, and the water would tend on that account to flow quicker: also the sea-level would only be raised 1 inch in 14 minutes so that the difference of level under the conditions specified may be considered as inappreciable.

The piping used at the stations in the Gulf of Cutch was arranged as follows:—

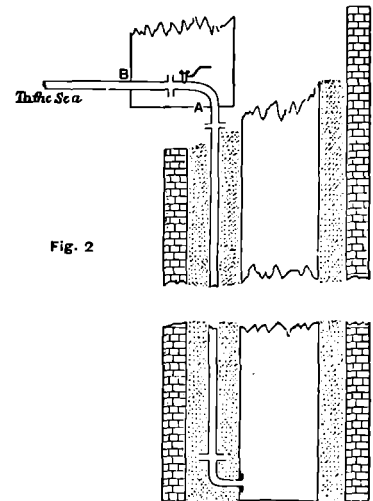
The lengths of the piping were fitted with cast-iron flanges made to screw on each end so that the pipes were easily joined together and the connections made perfectly air-tight. The piping was connected with the cylinder, at about nine inches above the bottom, by a small bend (see fig. 2) and was then brought up vertically outside the cylinder to a height of one or two feet below the lowest high-water. At this

point there was another bend fitted with a stop-cock, for the purpose explained a little further on, and from this bend the pipe was taken down along the slope of the shore to the low-water line, where lengths of flexible suction-pipe were joined on and taken out to deep water. This piping was formed by covering a helix of copper wire two inches in diameter, with a coating of india-rubber and canvas and was made in lengths of fifty or sixty feet and fitted with screw couplings. At the end of the outer length, a cylindrical copper rose about fifteen inches in length and two inches in diameter was screwed on: it had some one hundred and fifty holes of three-tenths of an inch bored in it, and was supported above the ground on a tripod fixed in deep water. The object of the copper rose was to prevent the pipe from becoming accidentally choked by sea-weed.

A T-shaped connecting piece (see fig. 1) was fitted to the end of the iron pipe and a length of the flexible piping could be fitted to either of its two outer extremities, the other being closed with a brass disc. When the flexible piping had to be removed for cleaning, the brass disc was unscrewed and a length of spare flexible piping with a rose attached, screwed on and taken out to deep water temporarily: the original pipe was then taken off and cleaned, the disc being screwed on for the time in its place and, when the cleaning was finished, the pipe and the disc were replaced in their original position so that there is no interruption of the record. This contrivance has been found to be superfluous.



In connections of this sort there is a decided tendency for air to collect in the piping, causing a retardation of the flow of water in and out of the cylinder. It was to remedy this defect that the stop-cock, alluded to above, was placed at the upper bend of the iron pipe as in fig. 2. As the stop-cock was below high-water mark it is clear that when it was opened, at the time of any high water, the air was expelled and the levels of the water inside and outside the cylinder became identical. It was occasionally found necessary to keep the stop-cock open for four or five hours while the water was above the cock. A water-tight box was made in halves and fitted over and under the stop-cock as in fig. 2, holes having been cut to admit the pipes and carefully caulked up after the box had been fitted over the pipe.



At other stations a system similar to the above in all essentials, though differing in detail as for instance placing the piping inside the cylinder instead of outside, was employed. It is not meant to lay this method down as the best possible but only as an indication of what a pipe connection should be: the circumstances at each place will be the best guide to the system to be employed, but it must above all things be borne in mind that a pipe connection is the last resort and that every endeavour should be made to place the cylinder in deep water.

The float is a cylindrical copper vessel one foot in diameter and nine inches deep, and is of such a density that it will just sink if unsupported. The band, *B*, (see Plates I and II) is a copper ribbon, about an inch wide, perforated with holes, *b*, about two and a half inches apart. It is attached by means of thumb-screws and a plate to a pillar which carries three small rollers so arranged that they bear on their upper surface a disc attached by three uprights to a plate soldered to the float. The pillar passes through the disc, its lower end being pivoted into the plate, so that the arrangement, as shown in fig. 1, Plate IV, forms a kind of swivel and prevents the band from being twisted.

The band passes over a stud-wheel, *C*, (see Plates I and II) which is of brass about nine and a half inches in diameter with a rim an inch wide: it has studs, *c*, of the same diameter as the holes, *b*,

in the band, placed in the rim at intervals of about two and a half inches, so that when the band is passed round the wheel, the studs exactly fit into the holes, thus ensuring the revolution of the wheel as the float rises and falls. The band is cut to such a length that it passes over the stud-wheel and about six feet beyond, when the float is in its lowest position in the cylinder. A weight is attached to the free end of the band as a counterpoise to the float, and from the bottom of this weight a copper chain is suspended which should be equal in weight, length for length, to the copper band. The other end of the chain is attached to an eyelet below the float so as to form with the band a sort of endless chain passing over the stud-wheel and reaching to the bottom of the cylinder. This contrivance is introduced in order that the pull on the float shall be constant, otherwise a systematic error would be introduced between rising and falling water. The counterpoise weight should be such as to give a decided preponderance, of say three or four pounds on the float side, and when once adjusted, it should not be altered without carefully noting the fact for future reference. When the whole system of float, band and counterpoise weight is hanging in position, there is about four inches space between the float and the cylinder on the one side, and the counterpoise weight and the cylinder on the other.

The bed-plate of the gauge, *Q*, (see Plates I, II and III) is of cast-iron, about seven feet long, one foot broad and three-quarters of an inch thick, the upper surface being carefully planed. Underneath this plate and cast in the same piece with it, is a web, *R*, four inches deep, which extends to within an inch of the edge of the upper plate all round, and has diagonals or stiffeners. The web rests on a wooden trestle, *S*, the top of which is five feet long, one foot broad and two inches thick, its legs being splayed and firmly braced. The trestle is placed longitudinally in the observatory, and touches the top of the float cylinder at one end.

The axle, *D*, (see Plates I and II) of the stud-wheel is supported on two uprights, *E*, *E'*, fixed to the bed-plate. It is about eight inches long, and carries at its other end a toothed wheel, *F*, which is in gearing with another toothed wheel, *F'*. The latter is fixed on an axle which is supported by two arms, *f*, (see Plate I) fastened to, *O'*, (see Plates I and II) one of the uprights which support the drum. These toothed wheels, *F*, *F'*, are constructed in couples so as to enable the working scale of the tidal diagrams to be varied at pleasure from the natural or full scale to that of  $\frac{1}{8}$ th according to the range of the tide. Six couples are supplied with each gauge, giving scales of  $\frac{1}{1}$ ,  $\frac{1}{2}$ ,  $\frac{1}{3}$ ,  $\frac{1}{4}$ ,  $\frac{1}{6}$  and  $\frac{1}{8}$ , and as the drum is five feet long, any tide of which the range does not exceed thirty feet can be safely registered. At Bhávnagar where the range is over thirty-six feet, a  $\frac{1}{10}$  scale is employed. In practice that couple is selected which enables the tidal curves to be exhibited on the largest scale possible.

The axle which carries the toothed wheel, *F'*, also carries the chain-wheel, *G*, (see Plates I and II) round which the chain, *g*, (see Plates I, II and IV) regulating the motion of the pencil-holder, *H*, winds, so that the motion of the water is communicated to the pencil. The chain-wheel, *G*, is about five inches in diameter, and its rim is grooved so that the chain winds round it without over-lapping.

At about ten inches from each end of the bed-plate there are brass uprights, *O*, *O'*, (see Plates I, II and III) fixed each carrying a pair of friction rollers, *o*, the pins on which the rollers turn being screwed into the uprights some five inches above the bed-plate.

The drum, *L*, (see Plates I, II and III) is composed of sheet-brass and made as nearly as possible into a true circular cylinder, five feet three inches in length and exactly twenty-four inches in circumference, and axles, *M*, (see Plates I and III) project from each end and rest on the friction rollers. One axle being elongated, passes through an oblong slot in the upright, *O*, and carries a toothed wheel, *N*, to gear with the driving clock, *P*, (see Plates I, II and III). The position of the drum is horizontal, and the paper on which the tidal curve is registered, is wrapped round it, being held in position by the clips, *w*, (see Plates II and III) and the edges pasted together along the length of the drum. Two grooves, *v*,

(see Plates I and III) about one-sixteenth of an inch deep and exactly five feet apart are cut round the drum, one near each end, and a third is cut midway between them. The groove at the clock end is generally adopted as the *zero-line* of the gauge, and when the paper is fixed on the drum, the zero, middle and end lines are indicated on it by rubbing over the grooves with a hard pencil. The paper is nearly five feet three inches long, and extends well beyond the extreme grooves.

Parallel to the length of the drum and fixed above it to the brass supports,  $O, O'$ , there are two bars,  $I$ , (see Plates I, II, III and IV) of solid brass drawn to angle shape: between these a slide,  $\sigma$ , (see Plate IV) moves and carries the pencil-holder,  $H$ , so as to keep it always over the centre line of the drum. The pencil-slide,  $\sigma$ , is a double T-shape and moves along the bars, being pushed towards one of them by a spring,  $s$ , (see Figs. 2 and 4, Plate IV) the spring being shown dotted in the former, so that there is no lateral motion; the upper flanges of the parallel bars are gripped between the springs,  $s'$ , (see Plate IV) and the upper plate of the slide for extra smoothness of motion. The bars,  $I$ , are prevented from buckling or having lateral motion by two arched stiffeners,  $J$ , (see Plates I and II) which are screwed to the outer sides of the bars and allow the slide and pencil-holder to pass through them.

The flexible chain,  $g$ , is fastened at one end to the chain-wheel,  $G$ , and carried round it: the other end is attached to a swivel,  $l$ , (see Figs. 2 and 3, Plate IV) on a cylindrical capstan-headed screw,  $y$ , (see Figs. 2 and 3), working into the body of the slide,  $\sigma$ , and by means of the screw,  $y$ , the slide can be moved along the bars, and the pencil adjusted for height to the zero of the gauge. At the other end of the pencil-slide there is a wire loop,  $l'$ , (see Figs. 2 and 3). A silver wire,  $K$ , (see Plates I and III) is tied to the loop,  $l'$ , and after passing over a rimmed pulley,  $k$ , at the end of the bars close to the clock and thence over another pulley,  $k'$ , on the bed-plate, (see Plate III), it has a weight of about five pounds attached to its other end, to ensure the pencil-slide moving when the water falls; a sufficient space must of course be allowed for its drop as the pencil moves between the bars. The pencil-holder,  $H$ , is a small tube which screws into the slide,  $\sigma$ , and is adjusted so that it almost touches the paper on the drum. It is made to contain common leads which are pressed down on the paper from above by a weight of two or three ounces, placed in a cup provided for the purpose.

The driving clock,  $P$ , is furnished with an English lever escapement and gold hair-spring. The movements are boxed in by moveable brass slides, and the oil-cups protected by bushes. The drum is driven by means of a toothed wheel of the clock gearing with another,  $N$ , on the axle of the drum. The arrangement for connecting and disconnecting the clock and the drum is as follows:—A clamping-screw,  $p$ , (see Plates I and III) with a milled head is connected with an interior arbor, so that when the screw is clamped, the driving toothed wheel of the clock is not moveable on the arbor, but when the screw is released the wheel can turn freely, and thus permit the drum to be placed in any position required, when the clamping of the screw will again bring the two toothed wheels into gear with the rest of the wheel-work of the clock.

In order to prevent any back-lash which may exist between the gearing of the clock and the drum, a cord carrying a weight,  $T$ , (see Plate I) of about five pounds is attached to, and encircles a barrel,  $U$ , (see Plates I and III) on the axle of the drum, thence passing over a pulley,  $t$ , (see Plate III) on the bed-plate. This barrel carries a pawl which drops on to a ratchet-wheel on the drum, neither of these being shown on the plates: it also carries a crown-wheel,  $W$ , (see Plates I and III), which gears with a bevel-pinion,  $X$ , (see Plate III). This pinion turns freely in a socket fastened to the upright,  $O$ , which supports the clock end of the drum. The outer end of the pinion is square, and the key which winds the clock fits it. In winding the pinion, the barrel is also turned, thus winding up the weight which prevents the back-lash, while any backward motion is stopped by the pawl and ratchet on the drum.

## 2.

*Self-Registering Aneroid.*

In the self-registering aneroid (see Plate V) there are seven vacuum-chambers or boxes, *A*, coupled together: the top one is attached to a screw, *B*, used for setting the metallic registering pointer; and a fork, *C*, with hardened steel bearings, is fixed to the lowest one. By means of knife-edges, a lever, *D*, rests on these bearings and connects the balancing-spring, *E*, with the vacuum-boxes, being pivoted on other knife-edges, *F*, midway between the attaching points. The vacuum-boxes and balancing-spring are placed on a brass frame, *G*.

The balancing-spring, *E*, is a spiral one hooked at the bottom to the lever, *D*, and at the top to a screw, *H*, which works in the upper part of the frame, *G*: the spring in connection with the lever prevents lost motion and by means of the screw its pull is so adjusted, that the reading of the instrument corresponds to that of the mercurial barometer under the particular atmospheric conditions existing at the time of its first adjustment. This adjustment, made by the maker, ought not to be altered unless the instrument has to be taken to pieces.

The movement produced by the variation of the atmospheric pressure on the boxes is multiplied by the lever, *D*, and further by the lever, *I*, supported on two uprights, *J*, and counterpoised. These two levers are connected together by a steel rod, *K*, pointed at both ends and pivoted in conical holes out of which it is prevented from slipping by means of forks.

A third lever, *L*, projects from the clock, *O*; it is the same length as the lever, *I*, and attached to it by a jointed piece, *M*, whose length is half the height of the recording barrel, *N*. The piece, *M*, is moveable, and at its centre a metallic pointer, *P*, is fixed for the purpose of marking on the prepared paper on the barrel: the pointer can be adjusted to press more or less heavily as required. Attached to the back of the lever, *L*, there is a sliding piece, *Q*, which is moved by the clock-work three times an hour, by means of a bent piece, *R*, the spring, *S*, preventing lost motion. The movement of the piece, *Q*, affects the lever, *L*, so as to twist the joint, *M*, and press the pointer, *P*, against the paper.

To the brass frame, *G*, on which the vacuum-boxes are placed, is fixed a steel tube, *T*, and on this the revolving drum, *U*, pivots, being maintained in position by a nut, *n*, screwing in the top of the tube. The tube is hollow to admit of a turnscrew being inserted to set the recording pencil to agree with the mercurial barometer.

At the bottom of the revolving drum, *U*, there is a crown-wheel, *V*, which gears by means of a pinion, *W*, with the clock. The drum revolves in eight and a half days. The recording barrel, *N*, on which the specially prepared paper supplied by the maker is fixed, rests by its own weight on the revolving drum and has a knob, *Y*, on the top with a hole through it of the same size and for the same purpose as the hollow in the steel tube. The several pieces are fitted on a substantial brass plate, *Z*, about twenty-one inches long and six inches wide, screwed on to a board an inch thick, and the whole instrument is fixed in a neat case, with a glass front, the top and front being made to open on hinges.

## 3.

*Self-Registering Anemometer.*

The self-registering anemometer as shown in Plate VI is fitted with Robinson's cups, *A*, (see Fig. 1) and steering-vanes, *B*, and has a long protecting tube, *C*, to prevent dust or rain blowing into the bearings. This tube is screwed on to the hollow chamber, *D*, in which is placed the mechanism shown on a larger scale in Fig. 2.

The instrument differs from the ordinary pattern in as much as the steering-vanes are made as large as possible, with a sharper angle than usual, and the screw which works the wheel of the indicating shaft has a quicker thread, so that smaller changes in the direction of the wind may be recorded on the drum, *O*, (see Figs. 3 and 4). The movement of the cups and vanes is communicated by means of the mechanism shown in Fig. 2 to the marking helices, *h, h*, by the two pairs of crown-wheels, *E, E'*, (see Figs. 3 and 4) which also are much larger than the usual pattern so as to produce easier gearing. The cylinders carrying the helices are counterpoised by weights, *w, w*, (see Fig. 4).

The screw, *F*, (see Figs. 3 and 4) enables the helices to be lifted off the drum so that the diagram may be fixed on the latter, the adjustment for time being made by means of the pencil, *p*, fitted with a spring so that it may be pressed down on the diagram.

The clock, *H*, (see Figs. 3 and 4) has a lever escapement with a gold hair-spring : it is driven by a weight, *I*, and is fitted with a dial, *K*, (see Fig. 3) showing minutes.

The driving-barrel of the clock movement is drilled through the centre and a shaft passes through the hole and bears on its outer end a pinion, *i, i*, (see Fig. 4) gearing with a wheel, *L*, on the axle of the drum, and on the other end, outside the clock, a milled-headed screw, *S*, (see Figs. 3 and 4). This arrangement allows the registering drum to be easily set, for, by loosening the screw the centre spindle becomes free, and after setting the drum to correct time the screw is again clamped.

To prevent back-lash in the drum, the double pinion, *i, i*, is made in two parts : one part is fixed on the spindle and the other is loose, but attached to the fixed part by means of a circular wire spring not shown in the plate. This spring is pressed back when gearing the double pinion and causes the tooth of the wheel, *L*, which is in gear, to be clamped on both sides and prevents lost motion.

## 4.

### *Tidal Observatory.*

The form of the observatory has been somewhat modified from time to time as additional experience has been gained from the working at various stations. The pattern now generally adopted as most convenient is shown in such detail in Plate VII, that it need not be further described. It is built of wood and so constructed as to be readily taken to pieces for removal to another station when required.

The internal fittings consist of a cupboard fixed on the wall to hold various documents and stores and to support the self-registering aneroid ; a shelf near the top of the observatory for the recording-gear of the self-registering anemometer, and a table on which to spread out the tidal diagrams.

## 5.

### *Graduated Staff.*

A staff graduated to inches, is fixed vertically outside the observatory in such a position as to be easily read, so that a comparison of the level of the water outside and inside the cylinder can be readily made.

## 6.

### *Bench-marks of Reference.*

Two or three embedded bench-marks are laid down in the vicinity of each observatory : they are similar to those in general use on the principal lines of levelling of the Great Trigonometrical Survey,

and are connected with these lines by rigorous levelling, according to the system adopted by the Survey Department. The details of the levelling connecting the bench-marks and bed-plate made at each inspection are recorded on the printed forms of the Department, and are carefully preserved for future reference if necessary.

## 7.

### *Self-Registering Tide-Gauge in use at Prince's Dock, Bombay.*

The gauge was constructed by Messrs. L  g   and Co. in 1879, under the supervision of Mr. E. Roberts, of the Nautical Almanac Office, in accordance with suggestions made by Mr. G. E. Ormiston, late Engineer to the Bombay Port Trust, and Captain A. W. Baird, R.E.

The observatory is situated on the centre pier of the Prince's Dock, and occupies the interior of the base and first floor of the light-house. The gauge is in communication with the deep water outside the dock, a well for the cylinder and a connection with the sea having been arranged for in building the dock. It was necessary to set up the gauge on the first floor because the dynamo for the electric light is on the ground floor, and this would have affected the clock, had the gauge been erected near it. A general description of the gauge is first given, to exhibit its construction and mode of operation, followed by a detailed account of each part. The letters refer to Plate VIII.

A vertical cylinder is placed in communication with the sea, by suspending it in a masonry well twelve feet in diameter, from which a nearly horizontal shaft twenty-four feet long reaches deep water; this renders the water affecting the gauge undisturbed, while its surface fairly represents the level of the surface of the water outside.

Resting on the water in the cylinder is a float which rises and falls with it, and to the float is attached a copper band, *b*, which passes over a wheel, *s*, called the stud-wheel. The rise or fall of the float communicates motion to the stud-wheel, and the stud-wheel in turn, by means of a toothed-wheel, *t*, on its own axle, communicates motion to another toothed-wheel, *t'*. On the same axle as the latter, and consequently moving with it, is a sheaved-wheel, *p*, called the pencil-wire wheel, round which a fine wire is wound; one end of this wire is secured to the circumference of the wheel, while the other hangs free and is fastened to a pencil-traveller, to which it communicates vertical motion. The pencil passes through the pencil-traveller horizontally and records the vertical motion of the latter on paper moving over a vertical, cylindrical drum, *B*: the drum revolves once in twenty-four hours by means of clock-work and the pencil is lightly pressed by a spring against its cylindrical surface. The paper is continually stretched over the portion of the drum under and about the path of the pencil-traveller, and is drawn off a second vertical drum, *C*, on which a considerable length is rolled. A third vertical drum, *A*, actuated by the same clock-work, rolls up the paper as it leaves the surface of the drum, *B*. Another pencil, *z*, pressed against the paper near the pencil-traveller guides and on a level with the zero of the traveller, marks a line on the paper, to which the heights of tide recorded by the pencil are referred. Projecting pins at one hour intervals, near the top and bottom of the drum, make pin-holes in the paper as it passes under the pencil-traveller, so that, from vertical straight lines joining these, the time of any recorded level of the water may be estimated. These pins also ensure that the paper moves with the drum. Any deviation of the pencil-traveller from a vertical path is prevented by parallel guides, *g, g*, on which a scale of feet is engraved, so that an indicator on the pencil-traveller shews the height of the tide above the zero of the scale. The upper ends of the spindles of the three drums turn in bearings in an upper horizontal plate, *u*, and the lower ends in bearings in a horizontal bed-plate, *v*. The upper horizontal plate carries the clock-face and the bearings of the stud-wheel, pencil-wire wheel, and toothed-wheels,



and has the upper ends of the guides fitted to it: the horizontal bed-plate is supported by two cast-iron trestles, *D, D*, and the rigidity of the frame secured by a cast-iron bracket to which the trestles are bolted. The gauge is protected by a panelled case with glass front and back, capable of being easily taken off.

In the detailed account of the various parts which follows, the principal parts are described in the order in which they were mentioned in the general outline, and the details are described along with the principal parts to which they belong.

The cylinder does not materially differ from that used with Newman's pattern of tide-gauge, and the float is identical with the pattern used with that gauge.

The band, *b*, is a copper ribbon, three-quarters of an inch wide and between forty and fifty feet long, the great length being due to the position of the gauge on the first floor of the light-house: the cylinder only extends to the level of the ground floor, and the band is protected by a wooden trough from the mouth of the cylinder up to and through the first floor. The band is fastened to the float in the same manner as is adopted with Newman's pattern of tide-gauge. It extends vertically upwards from its fastening to the float until it reaches the circumference of a sheaved guide-wheel, *o*, eight and a quarter inches in diameter. From this guide-wheel, which merely keeps it clear of the bed-plate, the band passes upwards and over the stud-wheel, *s*. It is pierced by oval holes to engage with the studs on the circumference of the stud-wheel. From the stud-wheel it passes vertically downwards through a hole in the bed-plate and is rolled up on the circumference of a sheaved-wheel, *r*, also eight and a quarter inches in diameter, on whose axle is a fusee, *f*, actuated by a cord which is led clear of the gauge by a pulley on the bed-plate and a block on an iron arm, and supports the counterpoise weight, *c*, the object of this being to ensure the band being always kept taut. The stud-wheel, *s*, is a sheaved-wheel eight inches in diameter. The band just fits between its flanges; the studs, about a quarter of an inch long and an eighth of an inch in diameter, and exactly two inches from centre to centre, are given a curved taper which allows the band to engage and disengage with perfect facility.

On the axle of the stud-wheel is a toothed-wheel, *t*, one inch in diameter, gearing with another toothed-wheel, *t'*, six inches in diameter.

On the axle of the latter is a sheaved-wheel, *p*, four inches in diameter, on which the pencil-traveller wire, a very fine brass wire, is wound and from which the free end of the wire depends. It will be seen that this combination of wheels results in the pencil having one-twelfth the motion of the float, *i.e.*, that the gauge works at a scale of one-twelfth the natural scale.

The pencil-traveller is an oblong block of metal an inch and a half long, having a small staple screwed into its upper end: it hangs by the pencil-traveller wire, which is knotted to the staple: a spring of bent wire is fastened to the upper part of the traveller and presses an ordinary lead, through a horizontal hole in the traveller, against the paper. The front of the traveller carries an indicator, *i*, level with the centre of the pencil-point, for the purpose of reading a graduated scale of feet engraved on the guides.

The guides, *g, g*, are formed by means of a slot passing vertically down the centre of a long brass plate, which is set up in front of the instrument between the upper horizontal plate and the bed-plate. The pencil-traveller works behind the plate, and the indicator passes through the slot, and moves along the face of the guides; the graduation zero, with which the indicator on the pencil-traveller is level, when the surface of the water is level with the zero of the gauge, is about four inches above the bed-plate, and from zero the scale is graduated downwards to read exceptionally low tides. Two side-plates are fitted to the guides and graduated like the latter: their straight edges nearly touch the paper and are used by the clerk to rule lines on the diagram equi-distant from the position of the pencil at prescribed hours: against these the date and hour are written, and they serve to fix the time-lines drawn through the pin-holes; they also act as a check on the regularity of the clerk.

The paper as marked by the pencil is extended over, and moves with, the drum, *B*, a cylinder twenty-four inches long and exactly twenty-four inches in circumference of its circular section. The upper inch of this drum is not covered by the paper: it is graduated for time into twenty-four hours, each of which measures one inch and is divided into ten-minute, and then into two-minute, graduations: a metal pointer fixed to the upper horizontal plate indicates a position on the drum two hours distant from the pencil-point and is called the time-index. This cannot be seen on the plate as it is hidden by the guides. Vertically under each hour graduation are two pin-points arranged to pierce the paper near its upper and lower edges and to mark it for time, as well as to ensure its moving with the drum. To the lower face of the drum is fixed a toothed-wheel, which gears into and drives a corresponding wheel under the drum, *A*. The drum, *B*, is directly driven by the clock, and revolves in the direction of the hands of a watch: the other drums of course revolve in the contrary direction. The paper is drawn off the drum, *C*, by the drum, *B*, and the friction to be overcome in rotating, *B*, suffices to keep the paper stretched. To press it against the pin-points, two rollers are used, their axle, *a*, being set up between the upper horizontal plate and the bed-plate. This axle is also used to carry a zero-marker, *z*, which by a lead pressed on the paper marks a line exactly level with the zero of the scale on the guides.

The drum, *A*, rolls up the paper after it has received the record. It rests simply by its own weight on the toothed-wheel driven by that under the drum, *B*. This wheel tends to rotate it just fast enough to accommodate the paper from *B* when *A* is empty, its diameter then being four inches. As *A* increases its diameter with accumulated paper, it slips on the revolving wheel beneath it, and so compensates its tendency to pull the diagram off *B* too fast. The drum, *C*, is similar to *A*, but only two inches in diameter, and is driven merely by the pull-off action exerted on the paper by the pins on the drum, *B*, of which six at the top and as many at the bottom are holding the paper at once. Both the drums, *A* and *C*, are twenty-two and a quarter inches long. The paper is continuous and one foot nine and a half inches broad, unmarked by time or height lines; about a thousand feet, or enough for fifteen months' record, are put on at a time. The completed record is cut off once a month.

The upper horizontal plate, *u*, is of iron, its form is clearly indicated in Plate VIII and the bed-plate, *r*, is also of iron, about nine inches wide and two feet six inches long: its greatest depth, about one inch, is at its centre and it tapers towards each end.

The clock, *x*, an ordinary pendulum clock is fixed underneath the bed-plate. The driving weight, an iron cylinder about one foot long and six inches in diameter, hangs below the floor by the cord, *w*, which passes over a pulley and under the bed-plate to the fusee it actuates. To prevent the weight from turning, an iron staple is fixed on its side and passes up and down an iron rod, set vertically downward, from the under side of the floor. The pendulum weight, *y*, is about one foot long and two inches in diameter, with a double milled-headed screw for adjusting the length of the pendulum: the pendulum hangs from a flat spring fixed on an inverted **V**-support. The hands must not be touched in setting the clock, for this would upset the agreement of the time-index and the clock hand.

## CHAPTER IV.

## SELECTION AND MAINTENANCE OF A TIDAL OBSERVATORY.

## 1.

*Directions for starting a Tidal Observatory.*

The choice of a site for the erection of a tide-gauge depends so much on local circumstances, that a careful reconnaissance of the fore-shore is a necessary preliminary to the selection of the best of the generally limited number of suitable positions.

The gauge should be placed so as to obtain a fair representation of the tidal oscillations of the surrounding area: to secure this it is necessary (1) that the sea should have direct communication with the gauge and not approach it through tortuous channels; (2) that the spot chosen should be sheltered from heavy weather, and (3) that there should be deep water at low-tide close to it. A good position is the end of a pier or jetty, or the wall of a dock; but it must be pointed out that a position in a cove or a minor bay at the head of a large bay, though it may apparently answer the above requirements, is not a good one for a tidal observatory, as experience shows that, at stations where the range is small (as in the south of India) the tidal curves in such a spot often present a zig-zag appearance all along the rise and fall. The irregularities are certainly not caused by lumpy water, because it has frequently been noticed that they were being registered inside the float-cylinder at times when the surface of the water outside was perfectly smooth, and no swell or ripple was apparent to the eye. The peculiarity may be seen in the curves at Kárwár and Beypore, though the scale of the illustrations is so small that it is not very marked: it has not yet been met with in tidal rivers.

When a station has been selected near deep water, and a pier, jetty or dock wall is available for the purpose, the observatory is built on it and the cylinder fixed in the water. But if nothing in the nature of a pier is available, and one cannot be specially constructed in deep water except at a prohibitory cost, the observatory must be erected on the shore, the cylinder sunk in the ground, or in a masonry well, and connected, as described in Chapter III, with the sea by piping.

The graduated staff is set up and the bench-marks are laid down as described in the preceding chapter. The trestle is put in position, longitudinally in the observatory and touching the float-cylinder at one end, and the tide-gauge placed on it in such a position that the centre of the float, the band and the counterpoise weight shall all be in a diametral plane of the float-cylinder, and also so that the float and the counterpoise weight shall each be about four inches from the sides of the cylinder. The trestle is then wedged up until its top is nearly level and its legs are firmly screwed to the floor. After this the bed-plate is levelled, longitudinally and transversely, by driving wedges in between the web and the top of the trestle.

The extreme range of the tide having been found roughly, either by observations on the staff or from local information, the various parts of the instrument are tested to see that they work freely and that there is enough drop, at extreme tides, for the counterpoise weight attached to the pencil-slide. The wheels to govern the scale of the diagram are then placed in gear with the float-wheel, a trial diagram put on and the instrument approximately adjusted so that at half-tide the pencil will be at the centre of the drum.

Sometimes the zero of the gauge, referred to at page 13 and accurately defined at the beginning of the next chapter, is made to correspond with some particular level which has been taken as the datum for local surveys, and the instrument is adjusted accordingly. For example, when soundings are being taken in the vicinity and the times noted, the gauge readings at those times may be made to indicate the amounts to be subtracted from the soundings to find the distances of the bed of the sea below the datum.

Whatever be the approximate adjustments, careful measurements must next be taken to determine the distance of the water below the surface of the bed-plate when the pencil is on the zero of the gauge. In making these zero-measurements, as they are called, a special apparatus is employed.

A flat strip of brass with a right-angled band is fixed by two or three countersunk screws to the top of a box-wood scale, divided into tenths, hundredths and five-hundredths of a foot, so that when the flat piece of brass lies on the bed-plate, the scale hangs vertically down, and care is taken that the under surface which rests on the bed-plate corresponds exactly to the zero mark of the box-wood scale. A small circular wooden disc, three inches in diameter and half an inch thick, is attached, by means of a brass clip fixed on the top of the disc, to a Chesterman's tape. The clip is made of two brass plates about two and a half inches long and one inch broad, one fixed vertically at the centre of the disc and the other attached to it by four screws at its corners, so as to be removed at pleasure. The tape is held between the plates, a line being drawn across the tape to show exactly how it is to be placed relatively to the top of the brass clip. The disc is slightly loaded with lead so that, when hanging from the tape, its under surface is quite horizontal. The distance from the bottom surface of the disc to the top of the clip is exactly three inches. The tape itself is marked at every foot from five feet to thirty feet by applying it to a standard, the disc being held suspended all the time, so as to have the tape in tension under the same conditions as when in use.

The measurements are taken as follows:—The scale is placed in position over the float-cylinder and the disc is lowered into the cylinder, care being taken to keep the tape close against the scale. When the disc is seen to be close to the surface of the water, warning is given to an assistant, and the lowering is continued very carefully until actual contact with the water is noticed by the disc causing a tremor on the surface. At the moment of contact a signal is made to the assistant who marks on the diagram the position of the pencil, and the distance in feet is read off the tape while the tenths, hundredths and thousandths are read off the scale. This distance is entered in a book, called the inspection book, in one column; the measurement of the position of the pencil above the zero-line on the

drum is then carefully made, and entered in the next column. The latter entry is multiplied by the denominator of the fraction indicating the working scale of the gauge and entered in a third column. The sum of the entries in the first and third columns gives a value of the distance of the water from the bed-plate when the pencil is on the zero-line, or, in other words, the distance of the zero of the gauge from the bed-plate.

Sets of measurements, each set consisting generally of twenty measurements, have to be taken both during a rising and a falling tide when the water is well on the rise or fall, and the mean of the two sets is the adopted value of the zero below the bed-plate: this eliminates the influence of the lost motion or back-lash between the toothed-wheels connecting the stud-wheel and the chain-wheel, and also the error arising from looseness of the pencil in the pencil-holder. If the value of the distance of the zero below the bed-plate agrees with the true zero previously fixed upon in regard to the datum, there is nothing more to be done; but if not the chain must be lengthened or shortened by means of the milled-headed screw until the agreement is complete. Reference lines are then painted on the band at the level of the top of the bed-plate when the pencil is at each of the three grooves in the drum, and the gauge may then be started.

The float-end of the bed-plate should now be connected by careful spirit-levelling with the benchmarks and with the graduated staff and, if necessary, the graduation of the latter altered so that its zero may correspond with that of the gauge.

It merely remains to set up and start the meteorological instruments, and the tidal observatory is in complete working order.

## 2.

### *Duties of the Clerk in charge of the Observatory.*

Printed instructions are given to the clerk in charge concerning his work which is carried out as follows:—The observatory is visited each day at 7 and 10 A.M. and at 4 and 6 P.M., except on Sundays when two visits are considered sufficient; and also twice a month, as a rule, to change the diagram.

The tide-gauge clock is wound up twice a week and the back-lash weight every evening. At each visit to the observatory, the position of the pencil on the drum is marked with a circle of ink round the pencil at the exact hour, and the date of the month written alongside, so that, should the drum not be truly circular, the diagram can be redivided by means of these hour marks. The preceding day's curve is inked in with one of the coloured inks supplied, and simultaneous readings of the position of the pencil on the diagram and of the bed-plate on the float-band are taken once daily

and entered in the daily report of which a specimen is given below, so as to make sure that the band has not been displaced. The height of the water for each hour of the preceding twenty-four hours is carefully measured off and entered in the report.

No. 2357.

*Daily Report of Bhavnagar Tidal Observatory, G. T. Survey of India, dated 16th May, 1892.*

S. R. Tide-gauge No. 2 working on the $\frac{1}{10}$ scale.	Wound up Clock at	Opened Stop-cock for a few minutes at H. water at	Took off Sheet No. 172 at 11-26 A.M. Put on Sheet No. 173 at 11-32 A.M.	POSITION OF PENCIL ON DRUM.				The Band read 34 at Bed-plate. Pencil read 34 on Drum at 5 hours 57 minutes P.M. Rising Tide.	Clock fast or slow of mean time by T. Office	Back-lash weight wound up at																	
	7-9 A.M.			7 A.M.	10 A.M.	4 P.M.	6 P.M.				Correct	6-1 P.M.															
		Left open from 5-0 to 8-10 A.M. 5-30 to 9-40 P.M.		Feet.	Feet.	Feet.	Feet.																				
				3'036	2'060	2'178	3'404																				
S. R. Aneroid Barometer No. A.	Wound up Clock at	Took off Sheet No. 338 at 12-5 P.M. Put on Sheet No. 339 at 12-7 P.M.	7 A.M.	10 A.M.	4 P.M.	6 P.M.	Thermometer attached to S. R. Barometer. Do. Mercurial Barometer.	7 A.M.	Mini- mum.	10 A.M.	4 P.M.	Maxi- mum.	6 P.M.														
	7-22 A.M.		Inches.	Inches.	Inches.	Inches.		81°5	80°5	91°5	100°5	101°0	99°0														
			29'938	29'966	29'942	29'926		82'5	...	94'0	100'0	...	97'0														
Mercurial Barometer No. 1726		readings at	29'926	29'994	29'858	29'860	Reset: Minimum and Maximum Thermometers at 6-0 P.M.																				
Anemometer No. B.	Wound up Clock at	Took off Sheet No. 2349 at 10 A.M. Put on Sheet No. 2350 at 10-1 A.M.				Number of miles in last 24 hours. 414 General direction of wind. Changeable																					
	7-1 A.M.																										
Position of the Pencil for each of the 24 hours from midday yesterday to midday to-day.	Feet above Zero.	The Zero-line marked on the diagram = .006 foot below the Zero cut on the Drum.																									
	Hour.	Neon	0'942	0'834	1'236	1'900	2'726	3'346	3'584	3'634	3'494	2'960	2'502	2'000	1'538	1'196	1'134	1'574	2'116	2'634	2'982	3'036	2'886	2'432	2'060	1'586	...
The rainfall from noon yesterday to noon to-day = Nil inches.				REMARKS. Graduated Staff = 34'30 } Pencil on Drum = 3'400 } at 5-57 P.M. Rising Tide.																							

\* The state of the sea should be recorded, such as boisterous or calm, heavy rollers coming in from South-west, water at Tide-gauge, calm or rough or very rough, as the case may be.

Compared by

Port Officer.

(Sd.) KANJI KUBAR,

Clerk in Charge.

The clock of the tide-gauge is compared daily with the gun or time-ball, or with a watch previously taken to the telegraph office, where Madras time can be correctly obtained at 4 P.M., and local time is deduced by applying a correction for longitude. The clock is corrected if it is over thirty seconds wrong, and the error is noted in the report with a remark as to whether or not it has been corrected. Any stoppage of the clock is noted on the diagram and also in the report. The reading of the pencil on the diagram and the height of the water at the same moment on the graduated staff, is taken once a day and entered in the report. If there is an unmistakable difference of two-tenths of a foot when the water is calm, the cylinder is flushed out and the communication holes examined. On the day after the diagram is put on and again on the day it is taken off, the zero, mid and end lines are marked by rubbing a hard pencil over the grooves cut in the drum so as to make a line half an inch long at the hours

of 10 A.M., 2 P.M. and midnight. A part of the paper not marked by any curve should, if possible, be selected and the date entered against each set of marks. The diagram, as a rule, is changed once a fortnight, generally every second Monday, when the tide has well turned so as to make sure of getting the highest and lowest tides recorded.

The change of diagram is made as follows:—The new diagram is numbered and dated, and a narrow slip is cut out in readiness for setting the zero-line; it is damped all over with clean water and paste applied to the overlap. The hour and date when the work was stopped is noted in ink on the old diagram and the pencil-holder is taken off. The diagram on the drum is cut carefully along the 12 o'clock line, the back-lash weight removed, the clips unscrewed and the diagram taken off, carefully rolled up and put aside. The drum and the clock are disconnected and the new diagram put on, making the 12 o'clock line of the paper agree with that marked on the drum and the zero of the diagram with that of the drum by means of the small slits cut out of the paper. The clips are screwed down and the drum turned round by hand till the outer edge of the diagram comes in contact with the 12 o'clock line and the height-lines meet. The pencil-holder is then fixed and the clock and drum clamped, care being taken that the pencil is over the part of the diagram which corresponds, as nearly as possible in time, with the time of the clock. The back-lash weight is carefully and slowly put on and the hour of commencing work noted on the diagram. It only remains to fix the position of the drum exactly for time. Any convenient hour, say noon, is selected and at one minute before, the connecting-screw of the clock and drum is unclamped; then when the second hand shows the exact hour, the drum is turned till the pencil is exactly over the hour-line of the diagram and the connecting-screw clamped very firmly, otherwise the clock may fail to drive the drum.

The stoppage of the clock, or in fact anything unusual, is noted on the diagram and in the daily report. If the clock stops, the weight is removed from the pencil-cup and the pencil slightly raised; the connecting-screw is unclamped, the drum held so that the back-lash weight does not run down, and revolved by hand so as to bring the pencil as nearly as possible over that part of the diagram which corresponds to about five minutes in advance of the correct time: the pencil-weight is replaced and the clock started and stopped again at an exact hour. The pencil is then adjusted to that hour and the clock and drum clamped. When the reference watch indicates that hour the gauge is started.

If by any chance the band comes off the stud-wheel, it is carefully replaced by turning the wheel until the pencil is on the mid-line of the diagram, and fitting the corresponding or 2·5 hole in the band which is marked with paint on the stud similarly marked; as the marks were made when the 2·5 line marked on the float-band was brought to agree precisely with the bed-plate, the pencil, when the wheel is released, assumes its proper position. If the chain between the pencil-slide and the float-end breaks, the pencil-holder is removed, the counterpoise weight detached and the two pieces of the chain taken out and re-riveted. The ends are then attached to the wheel and slide as before and the stud-wheel turned by hand till the 2·5 line is on a level with the bed-plate. If the deviation of the pencil from the mid-line on the drum is small, it is set right by the adjusting screw attached to the pencil-slide; but if the deviation is greater than the range of the screw, one of the toothed-wheels is taken off, and the chain wheel turned slightly; it is then replaced and the final adjustment made with the adjusting screw. During the whole operation, great care must be taken that the band does not kink.

If there is a stop-cock, it is opened every day, at high water or as near it as is convenient, but not if the level of the water is nearly the same as the height of the stop-cock.

The aneroid and mercurial barometers and the thermometers are read at 7 and 10 A.M., and at 4 and 6 P.M. If the clock of the aneroid stops, the hand is turned gently round till it points to the proper time as shown by the tide-gauge clock. The barrel is then turned till the pencil points to the proper time on the diagram and the instrument started. Great care is necessary, otherwise the gold

thread in Adie's pattern, or the marker in Légé's may be broken. In the former, the setting is not attempted when the clock hands are between five minutes to an hour and ten minutes past, as the pencil marker suspended to the gold thread is, at these times, either pressing on or close to the barrel; in the latter it is best done at five minutes past a full hour.

The aneroid clock is wound up every Monday morning and is regulated by stopping for a few minutes, if fast, or pushing the minute hand forward, if slow, but it is not altered if the error is only one or two minutes. The diagrams are carefully numbered and changed every Monday morning and the sheets inked in as they are taken off and put away.

The clock of the anemometer is wound up every morning by pulling the cord with the small weight so as to raise the heavy driving weight close up to the bed-plate. The diagrams are changed daily at 7 A.M. : they are inked in daily, dated and numbered, and the hours at which they were put on and taken off recorded on them and in the report. The number of miles of wind for the last twenty-four hours, obtained by counting the number of velocity lines and multiplying by ten, is also entered in the report. The daily reports on the forms supplied (see page 22) are made up in duplicate and one copy sent by post to the Tidal office. Anything unusual is marked on the diagram and noted on the back of the report, and if anything very urgent is required, the port-officer telegraphs to the officer in charge of the Tidal party.

### 3.

#### *Inspection of a Tidal Observatory.*

As a rule an inspection is made once a year, but if any interruption has taken place, such as the removal of the instruments for safety on account of a cyclone, as has occurred more than once, or on account of the settlement of the observatory which may necessitate a temporary suspension of the observations pending repairs, an inspection should be made as soon as possible after the information has been received. Before making an inspection, the accuracy of the one-foot graduations of the Chesterman's tape with which the zero-measurements are made is tested, and a tape is not used continuously for more than a couple of months without being retested and, if necessary, corrected.

The inspecting officer takes with him an inspection box which contains a copy of the Handbook on Tidal Observations, and of the current Tide-Tables for Indian Ports, besides the scales, measuring tape and other instruments required at an inspection; and he is accompanied by a mechanic to dismantle, clean, repair if necessary, and refit the instruments. He writes a report in the observatory inspection book, kept for the purpose, at the time of the inspection and a copy of it is forwarded to the Tidal office. It is usually divided under the following heads:—

General Remarks.

Bench-marks.

Details of Levelling.

Self-registering Tide-gauge.

Details of Determination of Working Zero.

Auxiliary Instruments.

In the general remarks, an account of the working of all the instruments since the last inspection is given, and attention drawn to the manner in which the clerk in charge performs his duties, and to anything else requiring special notice. At the actual inspection, the first thing done is to ascertain if any settlement of the tide-gauge has taken place, by connecting the float-end of the bed-plate by careful spirit-levelling with the bench-mark of reference, which in turn is connected with the other bench-marks



and with the graduated staff to test the accuracy of the zero of the latter. The results and the details of the levelling are entered in the report, mention also being made as to the condition in which the bench-marks and the staff were found, and as to whether the bed-plate was level both longitudinally and transversely.

A set of zero-measurements (as described on page 20), is then taken at rising and falling tide and entered in the inspection report as having been made *before cleaning* the gauge. If it is thought desirable to take more measurements, another pair of sets is taken before proceeding with the inspection. Concurrently with the zero-measurements, a comparison of the reading of the pencil on the drum with the reading of the bed-plate on the float-band and with the reading of the graduated staff is made both at a rising and a falling tide and entered in the report. Before cleaning the gauge, its clock is compared with the telegraph or gun-time as a check on the previous recent comparisons entered by the observatory clerk in his daily reports.

The balance of the gauge is then tested by gently turning the stud-wheel so as to raise the float completely out of the water and taking the reading of a spring-balance hooked for the purpose to one of the holes on the counterpoise side. The reading of the spring-balance gives the preponderance of the float which ought to be about three or four pounds, but when once adjusted this should require no alteration, as a change would affect the value of the zero. Should the preponderance be found to have increased, it points either to a flaw in the float sufficient to have admitted an influx of water, or to a break in the counterpoise chain on the side of the counterpoise weight. After testing the balance and before cleaning the gauge, the 2·5 line of reference painted on the band is brought to the level of the bed-plate, and if the pencil is not on the mid-line of the drum the discrepancy is measured and noted.

The float and band are then raised into the observatory for examination and measurement, and the time of stopping the gauge noted. The total length of the band, and the distances of the 2·5 and 0 lines painted on it from its junction with the float are measured, to guard against such a case as occurred during the inspection of a tidal observatory in 1887 when it was found that the readings of the band and pencil agreed, but the measurements for the determination of the working zero differed largely from what they ought to have been. The measurements and examination of the band disclosed that it had been broken close to the float, and it was found that the observatory clerk had tried to conceal the breakage by attaching the float to the band at the place where the breakage had occurred. The float is carefully examined and repaired or renewed if any water is found in it. In such a case, it is interesting to ascertain the quantity of water which has found its way into the float, as it may have been sufficient to alter the balance of the instrument and raise the working zero. An instance of this occurred at the Dublat Observatory in 1882 where water entered the float in sufficient quantity to raise the working zero 0·14 of a foot.

The dismantling of the gauge is completed and the several parts thoroughly cleaned and oiled where necessary, special mention being made in the report as to whether the driving clock required cleaning or not: the reference lines on the band are however not yet obliterated. When the several parts of the gauge have been cleaned, they are carefully refitted, the band being replaced so that when its painted 2·5 line of reference is level with the bed-plate, the pencil shall be at, or close to, the mid-line on the drum. The working of the band on the stud-wheel, while the pencil is being moved along the drum from its zero to the highest line on the diagram, is tested at low-water, so as to reduce as much as possible the chance of the band kinking. The working should be smooth, each hole of the band fitting over its stud freely, and if any hole is found too tight it is enlarged slightly with a file. The bed-plate is made level both longitudinally and transversely and, if this operation is found by spirit-levelling to have altered the level of the bed-plate relatively to that of the bench-mark of reference, the alteration of level is recorded. The refitted gauge is still unadjusted, and to ascertain the amount of adjustment required, zero-measurements are taken at rising and falling tides and recorded in the report as having

been made *after cleaning* the gauge. If a combination of the result of these measurements with the final level of the bed-plate makes the distance below the bench-mark of reference of the working zero differ from the distance of the true zero below the same bench-mark by a quantity appreciable on the scale of the diagram, the position of the pencil is adjusted until the working zero coincides with the true zero. It is usual to take, and record as having been made *after cleaning* the gauge, one more pair of sets of zero-measurements as a final test of the perfect adjustment of the instrument.

The gauge being in adjustment, the reference lines painted on the band at the last inspection are compared with the pencil readings on the drum, and if the former are found out of position they are obliterated and new ones substituted for them, care being taken that their *upper edges* correspond to the pencil readings.

The dismantling, cleaning and refitting of the self-registering aneroid and anemometer proceed at the same time as the similar duties in connection with the gauge. The aneroid is compared with the mercurial barometer, and its clock rated. The position of the pencil-marker on the diagram is adjusted, if necessary, by the screw so as to agree with the reading shown on the dial. The diagrams are examined to see if the marker is working freely, and if they show straight lines without rises at 10 o'clock and depressions at 4 o'clock, the marker is cleaned. The thermometers attached to the aneroid and mercurial barometers are compared, and the clerk is made to read the barometers and thermometers and to set the maximum and minimum thermometers. The diagrams are examined to ascertain that they have been inked in properly. The direction of the vane of the anemometer with regard to the wind and the marking of the direction on the barrel are tested, and the upper part of the instrument oiled, the cups being so marked that they cannot be put on wrongly. The clock is looked at to see if new catgut or anything else is required. The diagrams are examined and if the helices are marking faintly, their bearings, which should be quite free, are looked at, and their edges cleaned cautiously with a piece of fine sand-paper.

Before ending his inspection, the inspecting officer sees the observatory clerk make an accurate comparison of the tide-gauge clock, (which like all the other clocks in the observatory must keep *local time*) with the telegraph or gun-time, and enters the comparison in the report. He also sees that the clerk, in addition to being able to rate the clock, knows how to bring it to correct time when it is fast or slow, according to his printed instructions. A comparison of the reading of the pencil on the drum with that of the band at the bed-plate and with the level of the water on the graduated staff, is made and recorded after the gauge has been readjusted.

The inspecting officer also sees that a conspicuous note is contained in the observatory report book, for the information not only of the observatory clerk but also of the local official appointed to supervise him and superintend the working of the observatory, to the effect that whenever any interruption in the working of the tide-gauge takes place, owing, *e.g.* to the stoppage of the driving clock, hourly readings should be taken on the diagram by day and night during the interruption. If for any reason these readings cannot be taken, then hourly readings of the graduated staff should be taken by day and night and entered in the daily reports. Should this amount of frequency be unattainable, then it is indispensable that readings of high and low water should be taken day and night and entered in the daily reports. If the cause of the interruption be of so serious a nature as to render necessary the removal of the instruments from the observatory, the promptest information should be sent to the officer in charge of the tidal operations, to enable him to arrange for an inspection at the earliest possible date. The inspecting officer ends his inspection by taking a note of whatever diagrams, ink, books, pencils or other necessaries are required to be sent to the observatory.

## CHAPTER V.

## PREPARATION OF THE TIDAL DIAGRAMS.

## 1.

*Correction of the Time-lines.*

The tidal diagrams are examined and prepared for the reduction of the observations in the following manner:—Time-lines in red ink are drawn through each set of points which have been marked by the observatory clerk, showing the position of the pencil at the exact hours of 7 A.M., 10 A.M., 4 P.M. and 6 P.M., and these lines are the bases for drawing similar lines at the intermediate hours of the day. The daily reports are next examined to see if there are any clock errors amounting to three minutes or more: if there are, then crosses in red ink are made on the tidal diagrams to show the exact position of each hour. If the clock is fast, the cross is placed in *advance* of the vertical hour-line and if slow, *behind* it. The limit of three minutes' error has been adopted because one-twentieth of an inch is the smallest distance which can be conveniently and accurately laid down in measuring along the curve, and one-twentieth of an inch, on the scale of the tidal diagrams, is equivalent to three minutes.

## 2.

*Breaks in the Curves.*

Whenever a break in the curves occurs, owing to an interruption in the working of the tide-gauge, readings of the height of the water by day and night are taken at every hour, or (if such frequency is unattainable) at every high and low-water during the interruption as mentioned in the preceding chapter. These readings are plotted on the tidal diagrams and are connected by dotted lines which represent the tidal curves for the period of suspension of the automatic registrations.

## 3.

*Definitions of the Zero-lines and the Adopted Level of the Bed-plate.*

The true zero is that which has been adopted in determining the datum-line for heights in the tide-tables, and its relative level with regard to the bench-mark of reference is fixed. As a rule, the zero corresponds to that originally adopted when the gauge was started, and its distance below the bed-plate was determined when the level of the bed-plate with regard to the bench-mark was fixed.

The working zero is the level of the water with reference to the bed-plate when the pencil is on the zero-groove cut on the drum. In starting the instrument, the working zero corresponds to the true zero, but from various causes the instrument may get out of adjustment and its working zero may alter. The position of the working zero on the diagram is always marked by rubbing a hard pencil over the groove in the drum. At the close of an inspection, the working zero is made to agree closely with the true zero.

The accepted value of the true zero is the distance of the true zero from the bed-plate, which was determined when the bed-plate was fixed as regards its relative level with the bench-mark of reference.

The adopted level of the bed-plate means the level of the bed-plate with reference to the bench-mark of reference, which has been adopted in determining the true zero; as a rule this will correspond to the level obtained when the observations commenced.

#### 4.

##### *Rules for fixing the True Zero on the Diagrams.*

The inspection book is first examined to see if the bed-plate has altered in level relatively to the bench-mark of reference, and if there is any difference from the adopted level exceeding  $\cdot 02$  of a foot, a correction is applied. The measurements for the determination of the working zero at the various inspections are next examined. If no alteration has been made in the adjustment of the gauge during an inspection, the whole of the sets of measurements are grouped, and the mean value taken to represent the distance of the working zero from the bed-plate at the inspection. If an adjustment has been made during an inspection, then the measurements for the determination of zero before and after adjustment are grouped separately, and the respective means used in connection with the preceding and following diagrams. In treating the diagrams for any period between two inspections, the distance of the working zero from the bed-plate is taken as the mean of the values taken at the inspections. The following are the cases which may occur and the ways of adjusting for them:—

I. *Bed-plate settled below adopted level.*—The true zero is placed above the working zero at a distance proportional to the amount of the settlement in accordance with the scale of the diagram; hence the measurements from the true zero will be less than from the working zero.

II. *Bed-plate raised above adopted level.*—The true zero is placed below the working zero.

III. *Bed-plate unaltered and working zero at a greater distance from the bed-plate than accepted value for true zero.*—The true zero is placed above the working zero.

IV. *Bed-plate unaltered and working zero at a less distance from bed-plate than accepted value for true zero.*—The true zero is placed below the working zero.

V. *Bed-plate settled and working zero at greater distance from bed-plate than true zero.*—The true zero is placed above the working zero at a distance equal to the sum of the corrections.

VI. *Bed-plate settled and working zero at less distance from bed-plate than true zero.*—If the correction for the settlement is the greater of the two, the true zero is placed above the working zero; but if the correction on account of the difference in the zero-measurements is the greater, then the true zero is placed below the working zero, the amount of alteration in each case being the difference of the two corrections.

VII. *Bed-plate raised and distance of working zero from bed-plate less than true zero.*—The true zero is placed below the working zero at a distance equal to the sum of the two corrections.



## CHAPTER VI.

INVESTIGATION OF THEORETICAL EXPRESSIONS FOR THE REDUCTION OF TIDAL OBSERVATIONS  
BY HARMONIC ANALYSIS.

## 1.

*General Explanation of Tides.*

The general idea of the existence of tides may perhaps be best gathered by considering a planet, the earth, covered with water and attended by a satellite, the moon. The latter revolves round the former in an orbit nearly circular, but it will be simpler to consider the moon as fixed and the earth revolving round her. The moon then attracts every particle of the earth and ocean, and by the law of gravitation the force acting on any particle is directly proportional to the masses of the particle and of the moon, and inversely proportional to the square of the distance between the particle and the moon's centre. At the same time, as the earth is moving in a nearly circular orbit round the moon, each particle is tending to recede from the moon with a force, sometimes known as centrifugal force, jointly proportional to the square of the angular velocity of the earth round the moon and the distance between the particle and the moon's centre. These two radial forces, *viz.*, the attraction and the centrifugal force, balance each other at the earth's centre: also at a point nearer to the moon than the earth's centre, the former is greater, and the latter less, than it is at the centre, so that the attraction overbalances the centrifugal force. The difference of these two is the tide-generating force, and its action on a particle of water nearer to the moon than the earth's centre is to lessen the effect of gravity and allow the sea level to rise. The same effect is produced on the side of the earth remote from the moon owing to the centrifugal force overbalancing the attraction. Thus then it could be shown, in such an ideal case, that the form which the water would assume would be a prolate spheroid, with its major axis pointing towards the moon.

In the actual case, however, owing to the unequal distribution of land and water and the rotation of the earth, it must not be assumed that this is the case. For, suppose that the ocean consisted of a canal round the equator, and that an earthquake or any other cause were to generate a great wave in the canal, this wave would travel along it with a velocity dependent on the depth. If the canal were about thirteen miles deep, the velocity of the wave would be about one thousand miles an hour, and with a depth about equal to the supposed average depth of the existing seas, the velocity would be about half as great. Now, the moon's tide-generating force may be conceived as making a wave in the canal, and continually outstripping the wave it generates, for the moon travels round the equator at the rate of about one thousand miles an hour, and the sea is less than thirteen miles deep. The resultant oscillation of the ocean must therefore be the summation of a series of partial waves, generated at each instant by the moon and always falling behind her; the aggregate wave, being the same at each instant, must travel one thousand miles an hour so as to keep up with the moon.

Now, it is a general law of frictionless oscillation that, if a periodic force acts on a system, which, if left to itself, would oscillate in a period less than that of the force, the maximum excursion on one side of the equilibrium position occurs simultaneously with the maximum force in the direction of the excursion; but, if a periodic force acts on a system, which, if left to itself, would oscillate in a period greater than that of the force, the maximum excursion on one side of the equilibrium position occurs simultaneously with the maximum force in the direction opposite to that of the excursion. The latter is the case under consideration, for the period of a free wave in the shallow canal is greater than that of the moon's tide-generating action. Hence, when the system is left to settle into steady oscillation, it is low water under and opposite to the moon, so that the form of the water will be nearly an oblate spheroid with the minor axis pointing to the moon.

This conclusion about the tides of an equatorial canal is probably more nearly true of the tides of a globe partially covered with land, than the one in which the ocean is supposed at each moment to assume the prolate figure of equilibrium. In fact, observation shows that, speaking generally, it is more nearly low water than high water when the moon is on the meridian. Thus then an observer on the earth will have low water twice in a lunar day somewhere about the time the moon is on the meridian, either above or below the horizon, and high water halfway between the low waters. These are the 'semi-diurnal tides.'

If the sun be now introduced, there will be another similar tide of about half the height, depending on solar time and giving low water somewhere about noon and midnight. The superposition of this tide on the former, modified by friction and by the interference of land, gives the actually observed aggregate tide: hence it is clear that about new and full moon there must be spring tides, and at first and third quarters of the moon neap tides; and that, as the sum of the lunar and solar tide-generating forces is about three times their difference, the range of spring tides should be about three times that of neap tides, but a direct verification of this from tidal statistics is not readily obtained, owing to the difficulty of selecting tides exhibiting the effects of the disturbances caused by the sun and the moon under the circumstances in question.

Hitherto the luminaries have been supposed to move on the equator; but supposing that the moon does not, it is clear that the moon's zenith distance at upper transit is in general different from her nadir distance at lower transit. But the tide-generating force is greater, the smaller the zenith or nadir distance, and therefore the forces are different at successive transits. Thus there is a tendency for two successive lunar tides to be of unequal heights, and the resulting inequality of height is called a 'diurnal tide.' This tendency vanishes when the moon is on the equator, and as this occurs each fortnight, the lunar diurnal tide is evanescent once a fortnight. Similarly, in summer and winter the successive solar tides are generally of unequal height, while in spring and autumn this difference is inconspicuous; the various combinations of these inequalities give rise to the 'long-period tides.'

In Laplace's theory of the tides on a globe covered with ocean to a uniform depth, the diurnal tide is everywhere non-existent. But this hypothesis differs much from the reality, and in fact, at some ports the diurnal tide is so large that it overpowers the semi-diurnal, and during two portions of each lunation, there is only one great high water and one great low water in each twenty-four hours, whilst in other parts of the lunation the usual semi-diurnal tide is observed.

No existing theory of tides at all adequately represents the oscillations of the water, and this might be expected, owing to the very unequal distribution of land; it is only by a careful examination of the actual heights of the water at each station that satisfactory results can be arrived at. The comparison between tidal observations and tidal theories, and the formation of tables predicting the tidal oscillations of the sea have been carried out in two different ways, which may be called the 'synthetic' and the 'analytic.'

The semi-diurnal rise and fall of the tide, with the weekly alternation of spring and neap, would naturally suggest to the investigator to make his formula conform to the apparent simplicity of the phenomenon. He would seek to represent the height of the water by either one or two periodic functions with a variable amplitude; such a representation is the aim of the synthetic method. That method has been followed by all the great investigators of the past,—Newton, Bernoulli, Maclaurin, Laplace, Lubbock, Whewell, Airy. Since at European ports the two tides which follow one another on any one day are nearly equal, or, in other words, there is scarcely a sensible diurnal tide, these investigators bestowed comparatively little attention on the diurnal tides. If these be neglected, the synthetic method is simple, for a single function suffices to represent the tide. In non-European ports, however, the diurnal tide is sometimes so large as to mask the semi-diurnal and to make only a single instead of a double high water in twenty-four hours. To represent this diurnal tide in the synthetic method, it is necessary to introduce at least one more function. There should also be a third function representing the tides of long period. The expression for the tide-generating forces due to either sun or moon would consist of three terms, involving the declinations and hour-angles of the planet. One of these terms for each goes through its period approximately twice a day, the second once a day, and the third varies slowly. The mathematical basis of the synthetic method consists of a synthesis of the mathematical formulæ, so that the semi-diurnal term for the moon is fused with that for the sun, and the same process is carried out with the diurnal and the slowly varying terms. A mass of tidal observations at a place where the diurnal tide is small, soon shows that the fusion of two simple harmonic or periodic functions is insufficient to represent the state of the tide even if, as in all the older observations, it consists merely of heights and times of high and low water; the calculated heights and times of high and low water are found to need corrections for the variations of declinations, of motion in right ascension, and of the parallaxes of both bodies.

But, when continuously recording tide-gauges were set up, far more extended data than those of the older observations became accessible to the investigator, and more and more corrections were found to be expedient to adapt the formulæ to the facts. A systematic method of utilizing all the data became also a desideratum. This state of matters led Sir William Thomson (now Lord Kelvin) to suggest the analytic method. It is true that the dynamical foundations of that method have always lain below the surface of the synthetic method, and have constantly been appealed to for the theoretical determination of corrections: nevertheless the explicit adoption of the analytic method must be regarded as a great advance. In this method, the tidal force, or potential due to each disturbing body, is considered to be developed into a series of terms, each consisting of a constant (determined by the elements of the orbits and the obliquity of the ecliptic) multiplied by a simple harmonic function of the time. Thus in place of the terms of the synthetic method for the three classes of tides, there is an indefinitely long series of terms for each of the three classes. The loss of simplicity in the expression for the forces is far more than counterbalanced by the gain of facility for the discussion of the oscillations of the water. This facility arises from the great dynamical principle of forced oscillations, alluded to in the historical sketch given in Chapter I. Applying this principle, each individual term of the harmonic development of the tide-generating forces corresponds to an oscillation of the sea of the same period as the term, but the amplitude and phase of that oscillation must depend on a net-work of causes of almost inextricable complication. The analytic method, then, represents the tide at any port by a series of simple harmonic terms, whose period is determined from theoretical considerations, but whose amplitude and phase are found from observation. Fortunately the series representing the tidal forces converges with such rapidity, that it is necessary to consider only a moderate number of harmonic terms in the series.

One explanation is expedient before proceeding with the harmonic development. There are certain terms in the tide-generating forces of the moon, depending on the longitude of the moon's nodes, which complete their revolution in 18.6 years. Now, it has been found practically convenient in the application of the harmonic method, to follow the synthetic plan to the extent of classifying together



terms whose periods differ only in consequence of the movement of the moon's node, and at the same time to conceive that there is a small variability in the intensity of the generating forces.

## 2.

### *Tide-generating Potential due to the Moon.*

If a planet is attended by a single satellite, the motion of any body in relation to the planet's surface is found by the process described as reducing the planet's centre to rest. The planet's centre will be at rest, if every body in the system has impressed on it a velocity equal and opposite to that of the planet's centre; and this is accomplished by impressing on every body an acceleration equal and opposite to that of the planet's centre.

Let  $E$  be the mass of the planet,  
 $M$  „ mass of the satellite,  
 $r$  „ radius vector of the satellite measured from the planet's centre,  
 $\rho$  „ radius vector, measured from the same point, of the particle whose motion we wish to determine,  
 and  $z$  „ angle between  $r$  and  $\rho$ .

The satellite moves in an elliptic orbit about the planet, and the acceleration, relatively to the planet's centre, of the satellite is  $\mu \frac{E+M}{r^2}$  towards the planet along the radius vector  $r$ , where  $\mu$  is the attraction between unit masses at unit distance apart.

Now, the centre of inertia of the planet and satellite remains fixed in space, and the centre of the planet describes an orbit round that centre of inertia, similar to that described by the satellite round the planet, but with linear dimensions reduced in the ratio  $M$  to  $E+M$ . Hence the acceleration of the planet's centre is  $\mu \frac{M}{r^2}$  towards the centre of inertia of the two bodies. Thus, in order to reduce the planet's centre to rest, it is necessary to apply to each particle of the system an acceleration  $\mu \frac{M}{r^2}$  parallel to  $r$  and directed from the satellite to the planet.

Now, let a set of rectangular axes fixed in the planet be taken, and let  $M_1r$ ,  $M_2r$ ,  $M_3r$  be the co-ordinates of the satellite referred to them, and let  $\rho\xi$ ,  $\rho\eta$ ,  $\rho\zeta$  be the co-ordinates of the particle P whose radius vector is  $\rho$ .

Then the component accelerations for reducing the planet's centre to rest are

$$-\mu \frac{M \cdot M_1}{r^2}, \quad -\mu \frac{M \cdot M_2}{r^2}, \quad -\mu \frac{M \cdot M_3}{r^2};$$

and since these are the differential co-efficients with regard to  $\rho\xi$ ,  $\rho\eta$ ,  $\rho\zeta$  of the function

$$-\mu \frac{M\rho}{r^2} (M_1 \xi + M_2 \eta + M_3 \zeta); \quad \text{and since } \cos z = M_1 \xi + M_2 \eta + M_3 \zeta,$$

it follows that the potential of the forces, by which the planet's centre is reduced to rest, is  $-\mu \frac{M\rho}{r^2} \cos z$ .

The other forces acting on the particle must now be considered. The planet is spheroidal and therefore does not attract equally in all directions; but in this investigation of the forces, the ellipticity of the planet and the ellipticity of the ocean due to the planetary rotation may be neglected. Outside of its body, then, the planet contributes forces of which the potential is  $\mu \frac{E}{\rho}$ .

Next, the direct attraction of the satellite contributes forces of which the potential, being proportional to the mass of the satellite divided by the distance between the point P and the satellite, is

$$\mu \frac{M}{\sqrt{r^2 + \rho^2 - 2r\rho \cos z}}.$$

To determine the forces from this potential,  $\rho$  and  $z$  must be regarded as variables for differentiation, and a constant may be added to this potential at pleasure. As the object is to find the forces which urge P relatively to the planet, such a constant must be added, as will make the whole potential at the planet's centre zero, and thus the potential of the forces due to the attraction of the satellite must be taken as

$$\mu \frac{M}{\sqrt{r^2 + \rho^2 - 2r\rho \cos z}} - \mu \frac{M}{r}.$$

It is obvious that  $r$  is very large compared with  $\rho$ , so that the expression may be expanded in powers of  $\frac{\rho}{r}$ .

This expansion gives 
$$\mu \frac{M}{r} \left\{ \frac{\rho}{r} P_1 + \frac{\rho^2}{r^2} P_2 + \frac{\rho^3}{r^3} P_3 + \&c. \right\},$$

where  $P_1 = \cos z$ ,  $P_2 = \frac{3}{2} \cos^2 z - \frac{1}{2}$ ,  $P_3 = \frac{5}{2} \cos^3 z - \frac{3}{2} \cos z$ , &c.

Now since  $\mu \frac{M}{r} \cdot \frac{\rho}{r} P_1 = \mu \frac{M\rho}{r^2} \cos z$ , and is therefore equal and opposite to the potential by which the planet's centre was reduced to rest, the collection together of the various contributions to the potential gives as the potential of the forces acting on a particle, whose co-ordinates are  $\rho\xi, \rho\eta, \rho\zeta$ , the expression

$$\mu \frac{E}{\rho} + \mu \frac{M\rho^2}{r^3} \left( \frac{3}{2} \cos^2 z - \frac{1}{2} \right) + \mu \frac{M\rho^3}{r^4} \left( \frac{5}{2} \cos^3 z - \frac{3}{2} \cos z \right) + \&c. \quad (1)$$

The first term of (1) is the potential of gravity; consequently the terms of the series, of which two only are written, constitute the tide-generating potential,  $\mathcal{V}$ , so that

$$\mathcal{V} = \mu \frac{M\rho^2}{r^3} \left( \frac{3}{2} \cos^2 z - \frac{1}{2} \right) + \mu \frac{M\rho^3}{r^4} \left( \frac{5}{2} \cos^3 z - \frac{3}{2} \cos z \right) + \&c. \quad (2)$$

### 3.

#### *Development of the Lunar Tides.*

For the purpose of expansion, it will be more convenient to consider these two terms separately; so the tide-generating potential, due to the moon, of the second order of harmonics, at the point P is

$$\mathcal{V} = \frac{3}{2} \frac{\mu M}{r^3} \rho^2 (\cos^2 z - \frac{1}{3}) \quad (3)$$

Now, a simple tide may be defined as a spherical harmonic deformation of the waters of the ocean which executes a simple harmonic motion in time. Corresponding to this definition, the expression for each term of the tide-generating potential should consist of a solid spherical harmonic multiplied by a simple time-harmonic.

But since

$$\begin{aligned} \cos z &= \xi M_1 + \eta M_2 + \zeta M_3, \quad \xi^2 + \eta^2 + \zeta^2 = 1 \quad \text{and} \quad M_1^2 + M_2^2 + M_3^2 = 1, \\ \cos^2 z - \frac{1}{3} &= (\xi M_1 + \eta M_2 + \zeta M_3)^2 - \frac{1}{3}(M_1^2 + M_2^2 + M_3^2)(\xi^2 + \eta^2 + \zeta^2) \\ &= 2\xi\eta M_1 M_2 + 2 \frac{\xi^2 - \eta^2}{2} \cdot \frac{M_1^2 - M_2^2}{2} + 2\eta\zeta M_2 M_3 + 2\xi\zeta M_1 M_3 \\ &\quad + \frac{2}{3} \frac{\xi^2 + \eta^2 - 2\zeta^2}{3} \cdot \frac{M_1^2 + M_2^2 - 2M_3^2}{3} \end{aligned} \quad (4)$$

as will be seen by simply expanding the two expressions.

Now, let  $c$  be the moon's mean distance,  $e$  the eccentricity of the moon's orbit, and

$$\tau = \frac{3}{2} \cdot \frac{\mu M}{c^3} \quad (5)$$

Then putting

$$X = \left[ \frac{c(1-e^2)}{r} \right]^{\frac{3}{2}} M_1, \quad Y = \left[ \frac{c(1-e^2)}{r} \right]^{\frac{3}{2}} M_2, \quad Z = \left[ \frac{c(1-e^2)}{r} \right]^{\frac{3}{2}} M_3 \quad (6)$$

the expression in (3) becomes

$$\begin{aligned} \mathcal{V} \div \frac{\tau}{(1-e^2)^3} \rho^2 &= 2\xi\eta XY + 2 \frac{\xi^2 - \eta^2}{2} \cdot \frac{X^2 - Y^2}{2} \\ &+ 2\eta\zeta YZ + 2\xi\zeta XZ + \frac{2}{3} \frac{\xi^2 + \eta^2 - 2\zeta^2}{3} \cdot \frac{X^2 + Y^2 - 2Z^2}{3} \end{aligned} \quad (7)$$

In (7),  $\rho^2 \xi \eta$ ,  $\rho^2(\xi^2 - \eta^2)$ , &c., are solid spherical harmonics, and in order to complete the expression for  $\mathcal{V}$ , it is necessary to develop the five functions of  $X$ ,  $Y$ ,  $Z$  in a series of simple time-harmonics.

Let  $A$ ,  $B$ ,  $C$  (Fig. 1) be the axes of reference fixed in the earth,  $C$  being the north pole and  $AB$  being the equator.

Let  $X$ ,  $Y$ ,  $Z$ , be a second set of axes,  $XY$  being the plane of the moon's orbit.

Let  $M$  be the projection of the moon in her orbit,

- $I = ZC$ , the obliquity of the lunar orbit to the equator,
- $\chi = AX = BCY$ ,
- $l = MX$ , the moon's longitude in her orbit, measured from  $X$ .

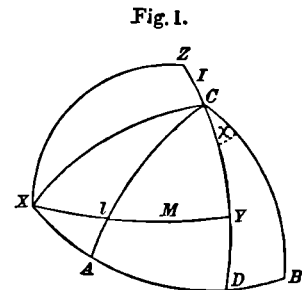


Fig. 1.

$$\begin{aligned} \text{Then } M_1 = \cos MA &= \cos l \cos \chi + \sin l \sin \chi \cos I \\ M_2 = \cos MB &= -\cos l \sin \chi + \sin l \cos \chi \cos I \\ M_3 = \cos MC &= \sin l \sin I \end{aligned} \quad (8)$$

$$\text{So that if } p = \cos \frac{1}{2} I \quad \text{and} \quad q = \sin \frac{1}{2} I \quad (9)$$

equations (8) may be written

$$\begin{aligned} M_1 &= p^2 \cos(\chi - l) + q^2 \cos(\chi + l) \\ M_2 &= -p^2 \sin(\chi - l) - q^2 \sin(\chi + l) \\ M_3 &= 2pq \sin l \end{aligned} \quad (10)$$

Whence

$$\left. \begin{aligned} M_1^2 - M_2^2 &= p^4 \cos 2(\chi - l) + 2p^2q^2 \cos 2\chi + q^4 \cos 2(\chi + l) \\ -2M_1M_2 &= \text{the same with sines instead of cosines} \\ M_2M_3 &= -p^3q \cos(\chi - 2l) + pq(p^2 - q^2) \cos \chi + pq^3 \cos(\chi + 2l) \\ M_1M_3 &= \text{the same with sines instead of cosines} \\ \frac{M_1^2 + M_2^2 - 2M_3^2}{3} &= \frac{1}{3}(p^4 - 4p^2q^2 + q^4) + 2p^2q^2 \cos 2l \end{aligned} \right\} \dots (11)$$

It will now be convenient to introduce certain auxiliary functions, namely

$$\Phi(a) = \left[ \frac{c(1-e^2)}{r} \right]^3 \cos(2l + a); \quad \Psi(a) = \left[ \frac{c(1-e^2)}{r} \right]^3 \cos a; \quad R = \left[ \frac{c(1-e^2)}{r} \right]^3 \dots (12)$$

Then from (6) and (11)

$$\left. \begin{aligned} X^2 - Y^2 &= p^4\Phi(-2\chi) + 2p^2q^2\Psi(2\chi) + q^4\Phi(2\chi) \\ 2XY &= \text{the same with } \chi + \frac{1}{4}\pi \text{ for } \chi \\ YZ &= -p^3q\Phi(-\chi) + pq(p^2 - q^2)\Psi(\chi) + pq^3\Phi(\chi) \\ XZ &= \text{the same with } \chi - \frac{1}{2}\pi \text{ for } \chi \\ \frac{1}{3}(X^2 + Y^2 - 2Z^2) &= \frac{1}{3}(p^4 - 4p^2q^2 + q^4)R + 2p^2q^2\Phi(0) \end{aligned} \right\} \dots (13)$$

Thus, when the functions  $\Phi, \Psi, R$  are expressed in a series of time-harmonics, the further development of the  $X, Y, Z$  functions consists in substitution in (13).

It will now be supposed that the moon moves in an elliptic orbit, undisturbed by the sun; the tides which arise from the lunar inequalities of the Evection and Variation will be the subject of separate treatment below.

The descending node of the equator on the lunar orbit will be called 'the Intersection.'

Let  $\sigma_1$  be the moon's mean longitude measured in her orbit from the Intersection,

$\varpi_1$  ,, longitude of the perigee measured in the same way,

and  $l$  has already been defined as the longitude of the moon in her orbit, measured from the Intersection.

The equation of the ellipse described by the moon is

$$\frac{c(1-e^2)}{r} = 1 + e \cos(l - \varpi_1) \dots (14)$$

If higher powers of  $e$  than the second be neglected,

$$\left. \begin{aligned} R &= 1 + \frac{3}{2}e^2 + 3e \cos(l - \varpi_1) + \frac{3}{2}e^2 \cos 2(l - \varpi_1) \\ \Phi(a) &= R \cos(2l + a) \\ &= (1 + \frac{3}{2}e^2) \cos(2l + a) + \frac{3}{2}e [\cos(3l + a - \varpi_1) + \cos(l + a + \varpi_1)] \\ &\quad + \frac{3}{4}e^2 [\cos(4l + a - 2\varpi_1) + \cos(a + 2\varpi_1)] \\ \Psi(a) &= R \cos a \end{aligned} \right\} \dots (15)$$

And by the theory of elliptic motion (see Godfray's Lunar Theory, third edition, page 12)

$$l = \sigma_1 + 2e \sin(\sigma_1 - \varpi_1) + \frac{5}{4}e^2 \sin 2(\sigma_1 - \varpi_1) \dots (16)$$

Consequently, in order to expand  $\Phi$ ,  $\Psi$ ,  $R$  in terms of  $\sigma_1$  (which increases uniformly with the time),  $\cos(2l + a)$  must be developed as far as  $e^2$ ;  $\cos(3l + a - \varpi_1)$ ,  $\cos(l + a + \varpi_1)$  and  $\cos(l - \varpi_1)$  as far as  $e$ ; while only the first terms of  $\cos(4l + a - 2\varpi_1)$  and  $\cos 2(l - \varpi_1)$  are necessary.

Substituting for  $l$  the value given in (16), and remembering that  $\cos \theta = 1 - \frac{\theta^2}{2}$  and  $\sin \theta = \theta$  to the order of small quantities here employed, it is easy to show that

$$\begin{aligned} \cos(2l + a) &= (1 - 4e^2) \cos(2\sigma_1 + a) - 2e \cos(\sigma_1 + a + \varpi_1) + 2e \cos(3\sigma_1 + a - \varpi_1) \\ &\quad + \frac{3}{4}e^2 \cos(a + 2\varpi_1) + \frac{1}{4}e^2 \cos(4\sigma_1 + a - 2\varpi_1), \\ \cos(3l + a - \varpi_1) &= \cos(3\sigma_1 + a - \varpi_1) - 3e \cos(2\sigma_1 + a) + 3e \cos(4\sigma_1 + a - 2\varpi_1), \\ \cos(l + a + \varpi_1) &= \cos(\sigma_1 + a + \varpi_1) + e \cos(2\sigma_1 + a) - e \cos(a + 2\varpi_1), \\ \cos(l - \varpi_1) &= -e + \cos(\sigma_1 - \varpi_1) + e \cos 2(\sigma_1 - \varpi_1), \\ \cos(4l + a - 2\varpi_1) &= \cos(4\sigma_1 + a - 2\varpi_1), \\ \cos 2(l - \varpi_1) &= \cos 2(\sigma_1 - \varpi_1). \end{aligned}$$

Substituting these values in (15) the expressions become

$$\left. \begin{aligned} \Phi(a) &= (1 - \frac{1}{2}e^2) \cos(2\sigma_1 + a) - \frac{1}{2}e \cos(\sigma_1 + a + \varpi_1) + \frac{7}{2}e \cos(3\sigma_1 + a - \varpi_1) \\ &\quad + \frac{1}{2}e^2 \cos(4\sigma_1 + a - 2\varpi_1) \\ R &= (1 - \frac{3}{2}e^2) + 3e \cos(\sigma_1 - \varpi_1) + \frac{9}{2}e^2 \cos 2(\sigma_1 - \varpi_1) \\ \Psi(a) &= (1 - \frac{3}{2}e^2) \cos a + \frac{3}{2}e [\cos(\sigma_1 + a - \varpi_1) + \cos(\sigma_1 - a - \varpi_1)] \\ &\quad + \frac{9}{4}e^2 [\cos(2\sigma_1 + a - 2\varpi_1) + \cos(2\sigma_1 - a - 2\varpi_1)] \end{aligned} \right\} \cdot \quad (17)$$

Now substituting from (17) in (13), and giving to  $a$  its appropriate value,

$$\left. \begin{aligned} X^2 - Y^2 &= (1 - \frac{1}{2}e^2) [p^4 \cos 2(\chi - \sigma_1) + q^4 \cos 2(\chi + \sigma_1)] + (1 - \frac{3}{2}e^2) 2p^2q^2 \cos 2\chi \\ &\quad + \frac{7}{2}e [p^4 \cos(2\chi - 3\sigma_1 + \varpi_1) + q^4 \cos(2\chi + 3\sigma_1 - \varpi_1)] \\ &\quad - \frac{1}{2}e [p^4 \cos(2\chi - \sigma_1 - \varpi_1) + q^4 \cos(2\chi + \sigma_1 + \varpi_1)] \\ &\quad + \frac{3}{2}e 2p^2q^2 [\cos(2\chi + \sigma_1 - \varpi_1) + \cos(2\chi - \sigma_1 + \varpi_1)] \\ &\quad + \frac{1}{2}e^2 [p^4 \cos(2\chi - 4\sigma_1 + 2\varpi_1) + q^4 \cos(2\chi + 4\sigma_1 - 2\varpi_1)] \\ &\quad + \frac{9}{4}e^2 2p^2q^2 [\cos(2\chi + 2\sigma_1 - 2\varpi_1) + \cos(2\chi - 2\sigma_1 + 2\varpi_1)] \end{aligned} \right\} \cdot \quad (18)$$

Also  $-2XY$  is the same as (18) with sines instead of cosines, and  $YZ$  is the same as  $X^2 - Y^2$  when  $\chi$  replaces  $2\chi$ ,  $-p^3q$  replaces  $p^4$ ,  $pq(p^2 - q^2)$  replaces  $2p^2q^2$ , and  $pq^3$  replaces  $q^4$ , and  $XZ$  is the same as  $YZ$  with sines instead of cosines; so that

$$\left. \begin{aligned} XZ &= - (1 - \frac{1}{2}e^2) [p^3q \sin(\chi - 2\sigma_1) - pq^3 \sin(\chi + 2\sigma_1)] + (1 - \frac{3}{2}e^2) pq(p^2 - q^2) \sin \chi \\ &\quad - \frac{7}{2}e [p^3q \sin(\chi - 3\sigma_1 + \varpi_1) - pq^3 \sin(\chi + 3\sigma_1 - \varpi_1)] \\ &\quad + \frac{1}{2}e [p^3q \sin(\chi - \sigma_1 - \varpi_1) - pq^3 \sin(\chi + \sigma_1 + \varpi_1)] \\ &\quad + \frac{3}{2}epq(p^2 - q^2) [\sin(\chi + \sigma_1 - \varpi_1) + \sin(\chi - \sigma_1 + \varpi_1)] \\ &\quad - \frac{1}{2}e^2 [p^3q \sin(\chi - 4\sigma_1 + 2\varpi_1) - pq^3 \sin(\chi + 4\sigma_1 - 2\varpi_1)] \\ &\quad + \frac{9}{4}e^2 pq(p^2 - q^2) [\sin(\chi + 2\sigma_1 - 2\varpi_1) + \sin(\chi - 2\sigma_1 + 2\varpi_1)] \end{aligned} \right\} \cdot \quad (19)$$

and

$$\left. \begin{aligned} \frac{1}{3}(X^2 + Y^2 - 2Z^2) &= \frac{1}{3}(p^4 - 4p^2q^2 + q^4) [(1 - \frac{3}{2}e^2) + 3e \cos(\sigma_1 - \varpi_1) + \frac{9}{2}e^2 \cos 2(\sigma_1 - \varpi_1)] \\ &\quad + 2p^2q^2 [(1 - \frac{1}{2}e^2) \cos 2\sigma_1 + \frac{7}{2}e \cos(3\sigma_1 - \varpi_1) - \frac{1}{2}e \cos(\sigma_1 + \varpi_1) + \frac{1}{2}e^2 \cos(4\sigma_1 - 2\varpi_1)] \end{aligned} \right\} \cdot \quad (20)$$





Hence

$$R = \left[ \frac{c(1-e^2)}{r} \right]^3 = 1 + \frac{4\frac{5}{8}me \cos(s-2h+p)}{. . . . .} \quad (24)$$

$$\Psi(\alpha) = R \cos \alpha = \cos \alpha + \frac{4\frac{5}{8}me}{. . .} [\cos(s-2h+p+\alpha) + \cos(s-2h+p-\alpha)] \quad (25)$$

$$\begin{aligned} \Phi(\alpha) = R \cos(2l+\alpha) = \cos(2\sigma_1+\alpha) + \frac{1\frac{0\frac{5}{8}me \cos(2\sigma_1+s-2h+p+\alpha)}{. . .} \\ - \frac{1\frac{0\frac{5}{8}me \cos(2\sigma_1+s-2h+p-\alpha)}{. . .}} \quad (26) \end{aligned}$$

Substituting these in (13) and neglecting terms which are nearly a reproduction of those already obtained and also those in  $q^2$  and  $q^3$ , the additional terms due to the evection become

$$\begin{aligned} X^2 - Y^2 &= \frac{1\frac{0\frac{5}{8}mep^4 \cos(2\chi - 2\sigma_1 - s + 2h - p)}{. . .} - \frac{1\frac{0\frac{5}{8}mep^4 \cos(2\chi - 2\sigma_1 + s - 2h + p)}{. . .}} \\ XZ &= -\frac{1\frac{0\frac{5}{8}mep^3q \sin(\chi - 2\sigma_1 - s + 2h - p)}{. . .} + \frac{1\frac{0\frac{5}{8}mep^3q \sin(\chi - 2\sigma_1 + s - 2h + p)}{. . .}} \\ &\quad + \frac{4\frac{5}{8}mepq(p^2 - q^2) [\sin(\chi + s - 2h + p) + \sin(\chi - s + 2h - p)]}{. . .} \\ \frac{1}{3}(X^2 + Y^2 - 2Z^2) &= \frac{1}{3}(p^4 - 4p^2q^2 + q^4) \frac{4\frac{5}{8}me \cos(s-2h+p)}{. . .} \end{aligned} \quad (27)$$

The term  $\frac{1\frac{0\frac{5}{8}me}{. . .}$  arises from the addition of the coefficient of the Evection in the longitude to three-halves of that in the reciprocal of the radius vector, the term  $\frac{1\frac{0\frac{5}{8}me}{. . .}$  from the subtraction of the same two quantities, and the term  $\frac{4\frac{5}{8}me}{. . .}$  is three times the coefficient in the reciprocal of the radius vector. When the development of the lunar theory is carried to higher orders, these coefficients differ considerably from the amounts computed from the first term, which alone occurs in the above analysis. Hence, when these coefficients are computed, the full values of coefficients in longitude and reciprocal of the radius vector must be introduced. According to Professor Adams, the full values of the coefficients are, in longitude  $\cdot 022233$ , and in  $c/r$   $\cdot 010022$ .

Now, as stated above,  $m$  is about  $\frac{1}{3}$  and is therefore a little greater than  $e$ , so that  $me$  is somewhat greater than  $e^2$ . Thus the terms to be added on account of the evection may be abridged and written

$$\begin{aligned} X^2 - Y^2 &= \frac{1\frac{0\frac{5}{8}mep^4 \cos(2\chi - 2\sigma_1 - s + 2h - p)}{. . .} - \frac{1\frac{0\frac{5}{8}mep^4 \cos(2\chi - 2\sigma_1 + s - 2h + p)}{. . .}} \\ XZ &= -\frac{1\frac{0\frac{5}{8}mep^3q \sin(\chi - 2\sigma_1 - s + 2h - p)}{. . .}} \\ \frac{1}{3}(X^2 + Y^2 - 2Z^2) &= \frac{1}{3}(p^4 - 4p^2q^2 + q^4) \frac{4\frac{5}{8}me \cos(s-2h+p)}{. . .} \end{aligned} \quad (28)$$

## 5.

### *Terms due to the Variation.*

The expressions for the inequality known as the 'Variation' in longitude and reciprocal of the radius vector are given in Godfray's Lunar Theory, third edition, arts. 79 and 93. If, as before, no distinction is made between longitudes in the orbit and in the ecliptic, these reduce to:—

$$\begin{aligned} l &= \sigma_1 + \frac{1\frac{1}{8}m^2 \sin 2(s-h)}{. . .}, \\ \frac{c(1-e^2)}{r} &= 1 + m^2 \cos 2(s-h). \end{aligned}$$

So that

$$\begin{aligned} R &= 1 + 3m^2 \cos 2(s-h), \\ \Psi(\alpha) &= \cos \alpha + \frac{3}{2}m^2 [\cos(2s-2h+\alpha) + \cos(2s-2h-\alpha)], \\ \Phi(\alpha) &= \cos(2\sigma_1+\alpha) + \frac{2\frac{3}{8}m^2 \cos(2\sigma_1+2s-2h+\alpha)}{. . .} + \frac{1}{8}m^2 \cos(2\sigma_1-2s+2h+\alpha). \end{aligned}$$



Whence to a sufficient degree of approximation,

$$\left. \begin{aligned} X^2 - Y^2 &= \frac{2}{3}m^2p^4 \cos(2\chi - 2\sigma_1 - 2s + 2h) \\ XZ &= 0 \\ \frac{1}{3}(X^2 + Y^2 - 2Z^2) &= \frac{1}{3}(p^4 - 4p^2q^2 + q^4) 3m^2 \cos(2s - 2h) \end{aligned} \right\} \dots \dots (29)$$

In this case, the value of the coefficient in  $X^2 - Y^2$  is the sum of the coefficient in longitude and three-halves of that in reciprocal radius vector; in  $\frac{1}{3}(X^2 + Y^2 - 2Z^2)$  it is three times that in reciprocal radius vector. But the actual values of the coefficients are considerably greater than those computed from the first terms and in computing, the actual values of the above coefficients must be used. According to Professor Adams these are, in longitude  $\cdot 011489$ , and in  $c/r \cdot 008249$ .

## 6.

### *Further Development of the Lunar Tides.*

The complete expressions for the  $X$ - $Y$ - $Z$  functions have now been obtained in (21), (28) and (29) in a series of simple time-harmonics; but they are not yet in a form to which the ordinary astronomical formulæ are adopted: further substitutions must be made before passing from the potential to the height of the tide generated by that potential.

The axes fixed in the earth may be taken to have their extremities in the following positions:—

The axis of  $A$  on the equator, in the meridian of the place of observation of the tides,

$B$  on the equator  $90^\circ$  East of  $A$ ,

$C$  at the north pole.

Now  $\xi$ ,  $\eta$ ,  $\zeta$  are the direction-cosines of the place of observation, so that, if  $\lambda$  be the latitude of that place,

$$\xi^2 - \eta^2 = \cos^2 \lambda, \quad \xi\eta = 0, \quad \eta\zeta = 0, \quad 2\xi\zeta = \sin 2\lambda \quad \text{and} \quad \frac{1}{3}(\xi^2 + \eta^2 - 2\zeta^2) = \frac{1}{3} - \sin^2 \lambda.$$

Then, if  $a$  is written for the radius of the earth, the expression (7) for  $V$  at the place of observation becomes

$$V = \frac{\tau a^2}{(1 - e^2)^3} \left[ \frac{1}{2} \cos^2 \lambda (X^2 - Y^2) + \sin 2\lambda XZ + \frac{3}{2} \left( \frac{1}{3} - \sin^2 \lambda \right) \frac{1}{3} (X^2 + Y^2 - 2Z^2) \right].$$

The  $X$ - $Y$ - $Z$  functions being simple time-harmonics, the principle of forced oscillations, stated on page 4, justifies the conclusion that the forces corresponding to  $V$  will generate oscillations in the ocean of the same periods and types as the terms in  $V$ , but of unknown amplitudes and phases.

If now,  $x^2 - y^2$ ,  $xz$ ,  $\frac{1}{3}(x^2 + y^2 - 2z^2)$  be three functions having forms respectively similar to those of

$$\frac{X^2 - Y^2}{(1 - e^2)^3}, \quad \frac{XZ}{(1 - e^2)^3}, \quad \frac{1}{3} \frac{(X^2 + Y^2 - 2Z^2)}{(1 - e^2)^3},$$

but differing from them in that the argument of each of the simple time-harmonics has some angle subtracted from it, and that the term is multiplied by a numerical factor: then, by means of the above principle,  $h$ , the height of the tide at the place of observation is given by

$$h = \frac{\tau a^2}{g} \left[ \frac{1}{2} \cos^2 \lambda (x^2 - y^2) + \sin 2\lambda xz + \frac{3}{2} \left( \frac{1}{3} - \sin^2 \lambda \right) \frac{1}{3} (x^2 + y^2 - 2z^2) \right] \dots \dots (30)$$

where  $g$  denotes gravity.

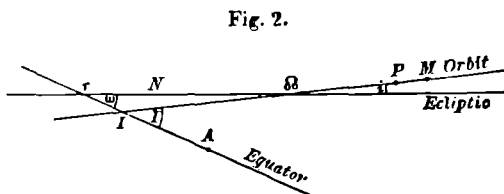


$$\frac{1}{3}(\mathbf{x}^2 + \mathbf{Y}^2 - 2\mathbf{Z}^2) = \frac{1}{3}(p^4 - 4p^2q^2 + q^4) \left[ 1 + \frac{3}{2}e^2 + 3e \cos(\sigma_1 - \varpi_1) + \frac{45}{8}me \cos(s - 2h + p) \right. \\ \left. + 3m^2 \cos(2s - 2h) \right] + 2p^2q^2 \left[ (1 - \frac{5}{2}e^2) \cos 2\sigma_1 + \frac{7}{2}e \cos(3\sigma_1 - \varpi_1) \right] \quad (33)$$

The second step is to express the angles  $\chi$ ,  $\sigma_1$ ,  $\varpi_1$ , each of which increases uniformly with the time, in terms of the sidereal hour-angle or of the local mean time, and of the mean longitudes of the moon and of the perigee.

Let  $M$  be the moon in the orbit,

- $A$  ,, extremity of the  $A$ -axis fixed in the earth,
- $g$  ,, sidereal hour-angle,
- $N$  ,, longitude of the node  $\Omega$ ,
- $\nu$  ,, right ascension of the intersection  $I$ ,
- $\xi$  ,, longitude in 'the moon's orbit' of the intersection,
- $i$  ,, inclination of the moon's orbit to the ecliptic,
- $\omega$  ,, obliquity of the ecliptic,
- $s$  ,, moon's mean longitude,
- $p$  ,, mean longitude of the perigee.\*



Then (Fig. 2)  $g = A^\nu$ ,  $\nu = \nu I$ ,  $\xi = \nu \Omega - \Omega I$ ,  $N = \nu \Omega$ .

Now  $\sigma_1$  and  $\varpi_1$  have been defined above as the moon's mean longitude and the longitude of the perigee, both measured in the orbit from the intersection  $I$ .

Therefore  $\sigma_1 - \varpi_1 = \text{moon's mean anomaly} = s - p$ .

Then if  $P$  (Fig. 2) be the perigee, supposed to describe the orbit with uniform motion,

$$\begin{aligned} p &= \nu \Omega + \Omega P, \\ \text{but} \quad \xi &= \nu \Omega - \Omega I, \\ \text{so that} \quad p - \xi &= IP. \\ \text{Therefore} \quad \left. \begin{aligned} \varpi_1 &= p - \xi \\ \text{and} \quad \sigma_1 &= s - \xi \end{aligned} \right\} \dots \dots \dots (34) \end{aligned}$$

$$\text{Again} \quad \chi = IA = A^\nu - I^\nu = g - \nu \quad \dots \dots \dots (35)$$

where  $g$  is supposed to increase uniformly from the time when the tidal observations begin.

Since, in all tidal observations, local mean solar time is used, it will be better to express  $g$  in terms of local mean solar time and the sun's mean longitude.

Let  $t$  be the local mean solar time reduced to angle, so that at noon  $t = 0^\circ$ ,

- $h$  ,, sun's mean longitude,
- $p_1$  ,, longitude of the sun's perigee.

$$\text{Then} \quad \chi = t + h - \nu \quad \dots \dots \dots (36)$$

\* To be distinguished from  $p$  representing  $\cos \frac{1}{2} I$ .

If the values in (34) and (36) be substituted in the  $x$ - $y$ - $z$  functions in (31), (32) and (33) and the functions in their new forms be introduced into (30), the final result may be expressed in the form of three schedules B, i, B, ii, B, iii (pages 46 and 47).

The schedules are arranged thus. First, there is a general coefficient  $\frac{3}{2} \frac{M}{E} \left(\frac{a}{c}\right)^3 a$ , which multiplies every term of all the schedules. Secondly, there are general coefficients, one for each schedule, *viz.*,  $\cos^2 \lambda$  for those in B, i which are evidently semi-diurnal,  $\sin 2\lambda$  for those in B, ii which are diurnal, and  $\frac{1}{2} - \frac{3}{2} \sin^2 \lambda$  for those in B, iii or the terms of long period. These three functions of the latitude of the place of observation are the values at that place of three surface spherical harmonic functions, which have the maximum value unity, at the equator for the semi-diurnal, in latitude  $45^\circ$  for the diurnal, and at the pole for the terms of long period.

Then follows a table for each schedule, the first column giving the name or initial of the tide and the second the coefficient peculiar to the tide, a function of  $I$  and  $e$ , and in two cases also of  $p$ .

The third column gives the mean value of the coefficient or the mean semi-range of the corresponding term. It will be shown below, that these mean values are found by putting  $I = \omega$  in the coefficient, and when the function of  $I$  is  $\cos^2 \frac{1}{2} I$ ,  $\sin I \cos^2 \frac{1}{2} I$ ,  $\sin I \sin^2 \frac{1}{2} I$ , or  $\sin^2 I$  (in B, iii) by multiplying further by  $\cos^2 \frac{1}{2} i$ , and where the function of  $I$  is  $\sin^2 I$  (in B, i),  $\sin I \cos I$ , or  $1 - \frac{3}{2} \sin^2 I$  by multiplying by  $1 - \frac{3}{2} \sin^2 i$ .

Next there is a column of arguments, which are all linear functions of  $t$ ,  $h$ ,  $s$ ,  $p$ ,  $\nu$  and  $\xi$ : in B, i,  $2t + 2(h - \nu)$  and in B, ii,  $t + (h - \nu)$  is common to all the arguments and is written at the top of the column; the terms in the arguments are grouped in a manner convenient for subsequent computations.

The last two columns of the table show the speed, that is, the rate of increase of the arguments in the preceding column, expressed algebraically and in degrees per mean solar hour; the letters  $\gamma$ ,  $\sigma$ ,  $\eta$ ,  $\omega$  refer respectively to the earth's angular velocity of rotation, to the mean motions of the moon, sun and lunar perigee.

To write down any term, the general coefficient, the coefficient for the schedule, the coefficient peculiar to the tide and the cosine of the argument must be multiplied together. The result is a term in the equilibrium tide with the water covering the whole earth, and the transition to the actual case by the introduction of a factor and a delay of phase, to be derived from observation, has already been explained.

## 7.

### *Solar Tides.*

The expression for the tides depending on the sun, may be written down at once by symmetry; and, as the eccentricity of the solar orbit, *viz.*, .01679, is so small, the elliptic tides may be omitted, excepting the larger elliptic semi-diurnal tide.

The lunar schedules are therefore to be transformed by writing  $s = h$ ,  $p = p_1$ ,  $\xi = \nu = 0$ ,  $\sigma = \eta$ ,  $I = \omega$ ,  $e = e_1$  and  $\omega = \omega_1$ , where  $\omega_1$  is the mean motion of the sun's perigee.

For purposes of comparison, the general coefficient  $\frac{3}{2} \frac{M}{E} \left(\frac{a}{c}\right)^3 a$  will be retained in the schedule of solar tides, and the coefficient peculiar to each tide will be made to involve the factor  $\frac{\tau_1}{\tau}$ , where  $\tau_1 = \frac{3}{2} \frac{\mu S}{c_1^3}$ ,  $S$  being the sun's mass, and  $c_1$  the mean distance of the earth and sun, so that  $\frac{\tau_1}{\tau} = \frac{S}{M} \left(\frac{c}{c_1}\right)^3$ .

Now taking  $\frac{E}{M} = 81.5$  and the following values as given in *Solar Parallax and its Related Constants*, by Prof. W. Harkness, page 140, viz.,  $\frac{S}{E+M} = 327214$ ,  $c = 238855$  miles and  $c_1 = 92796950$  miles, it follows that  $\frac{\tau_1}{\tau} = .46035 = \frac{1}{2.17226}$ .

The  $\varpi_1$  used in this section should be distinguished from that used in the preceding sections, where it represents the longitude of the lunar perigee measured from the intersection. Its use in the latter sense is discarded after page 43.

## 8.

### Schedules.

For convenience of reference, the tides are now arranged in tabular form, as explained in the preceding page.

#### Schedule of Notation.

Initial	Speed	Name of Tide	Initial	Speed	Name of Tide
$M_1$	$\gamma - \sigma - \varpi$ , and	Principal lunar series	$S_1$	$\gamma - \eta$	Principal solar series
$M_2$	$\gamma - \sigma + \varpi$		$S_2$	$2(\gamma - \eta)$	
$M_3$	$2(\gamma - \sigma)$		$S_3$	$3(\gamma - \eta)$	
&c.	$3(\gamma - \sigma)$ &c.		&c.	&c.	
$K_2$	$2\gamma$	Luni-solar semi-diurnal	T	$2\gamma - 3\eta$	Larger solar elliptic
N	$2\gamma - 3\sigma + \varpi$	Larger lunar elliptic	R	$2\gamma - \eta$	Smaller solar elliptic
L	$2\gamma - \sigma - \varpi$ and $2\gamma - \sigma + \varpi$	Smaller lunar elliptic	P	$\gamma - 2\eta$	Solar diurnal
2N	$2\gamma - 4\sigma + 2\varpi$	Lunar elliptic, second order		$\frac{dN}{dt}$	19-yearly
$\nu$	$2\gamma - 3\sigma - \varpi + 2\eta$	Larger lunar evectional	Mm	$\sigma - \varpi$	Lunar monthly
$\lambda$	$2\gamma - \sigma + \varpi - 2\eta$	Smaller lunar evectional		$\sigma - 2\eta + \varpi$	Lunar evectional monthly
O	$\gamma - 2\sigma$	Lunar diurnal	Mf	$2\sigma$	Lunar fortnightly
OO	$\gamma + 2\sigma$			$3\sigma - \varpi$	Lunar termensual
$K_1$	$\gamma$	Luni-solar diurnal	Sa	$\eta$	Solar annual
Q	$\gamma - 3\sigma + \varpi$	Larger lunar elliptic diurnal	Ssa	$2\eta$	Solar semi-annual
	$\gamma - \sigma - \varpi$ included in $M_1$	Smaller lunar elliptic diurnal	MSf	$2(\sigma - \eta)$	Luni-solar synodic fortnightly
J	$\gamma + \sigma - \varpi$		MS	$4\gamma - 2\sigma - 2\eta$	Compound tides
	$\gamma - 4\sigma + 2\varpi$	Lunar elliptic diurnal, second order	$\mu$ or 2MS	$2\gamma - 4\sigma + 2\eta$	
	$\gamma - 3\sigma - \varpi + 2\eta$	Larger lunar evectional diurnal	2SM	$2\gamma + 2\sigma - 4\eta$	
			$M_2K_1$	$3\gamma - 2\sigma$	
			$2M_2K_1$	$3\gamma - 4\sigma$	
			$M_2N$	$4\gamma - 5\sigma + \varpi$	

## Schedule of Lunar Tides.

$$\text{General Coefficient} = \frac{3}{2} \frac{M}{E} \left(\frac{a}{c}\right)^3 a.$$

[ B, i. ] *Semi-diurnal Tides; General Coefficient =  $\cos^2 \lambda$ .*

Initial	Coefficient	Mean Value of Coefficient	Argument $2t + 2(h - \nu)$	Speed	Speed in degrees per m. s. hour
M <sub>2</sub>	$\frac{1}{2} (1 - \frac{5}{2} e^2) \cos^4 \frac{1}{2} I$	·45426	$-2(s - \xi)$	$2(\gamma - \sigma)$	28·9841042
K <sub>2</sub>	$\frac{1}{2} (1 + \frac{3}{2} e^2) \frac{1}{2} \sin^2 I$	·03929	—	$2\gamma$	30·0821372
N	$\frac{1}{2} \cdot \frac{7}{2} e \cos^4 \frac{1}{2} I$	·08796	$-2(s - \xi) - (s - p)$	$2\gamma - 3\sigma + \omega$	28·4397296
L	$\frac{1}{2} \cdot \frac{1}{2} e \cos^4 \frac{1}{2} I$ $\times \sqrt{\{1 - 12 \tan^2 \frac{1}{2} I \cos 2(p - \xi)\}}$	·01257	$-2(s - \xi) + (s - p) - R + \pi$ where $\tan R = \frac{6 \sin 2(p - \xi)}{\cot^2 \frac{1}{2} I - 6 \cos 2(p - \xi)}$	$2\gamma - \sigma - \omega$	29·5284788
2N	$\frac{1}{2} \cdot \frac{17}{2} e^2 \cos^4 \frac{1}{2} I$	·01173	$-2(s - \xi) - 2(s - p)$	$2\gamma - 4\sigma + 2\omega$	27·8953548
$\nu$	$\frac{1}{2} \cdot \frac{10^5}{16} me \cos^4 \frac{1}{2} I$	·01234† ·01706	$-2(s - \xi) + (s - p) + 2h - 2s$	$2\gamma - 3\sigma - \omega + 2\eta$	28·5125830
$\lambda$	$\frac{1}{2} \cdot \frac{15}{16} me \cos^4 \frac{1}{2} I$	·00176† ·00330	$-2(s - \xi) - (s - p) - 2h + 2s + \pi$	$2\gamma - \sigma + \omega - 2\eta$	29·4556254
* $\mu$	$\frac{1}{2} \cdot \frac{2^3}{16} m^2 \cos^4 \frac{1}{2} I$	·00736† ·01094	$-2(s - \xi) + 2h - 2s$	$2\gamma - 4\sigma + 2\eta$	27·9682084

\* Indicated by 2MS as a compound tide. † The lower of the two numbers gives the value when the coefficients of the Erection and Variation have their full values as derived from the Lunar Theory.

[ B, ii. ] *Diurnal Tides; General Coefficient =  $\sin 2\lambda$ .*

Initial	Coefficient	Mean Value of Coefficient	Argument $t + (h - \nu)$	Speed	Speed in degrees per m. s. hour
O	$(1 - \frac{5}{2} e^2) \frac{1}{2} \sin I \cos^2 \frac{1}{2} I$	·18856	$-2(s - \xi) + \frac{1}{2}\pi$	$\gamma - 2\sigma$	13·9430356
OO	$(1 - \frac{5}{2} e^2) \frac{1}{2} \sin I \sin^2 \frac{1}{2} I$	·00812	$+2(s - \xi) - \frac{1}{2}\pi$	$\gamma + 2\sigma$	16·1391016
K <sub>1</sub>	$(1 + \frac{3}{2} e^2) \frac{1}{2} \sin I \cos I$	·18115	$-\frac{1}{2}\pi$	$\gamma$	15·0410686
Q	$\frac{7}{2} e \frac{1}{2} \sin I \cos^2 \frac{1}{2} I$	·03651	$-2(s - \xi) - (s - p) + \frac{1}{2}\pi$	$\gamma - 3\sigma + \omega$	13·3986609
M <sub>1</sub>	$e \frac{1}{2} \sin I \cos^2 \frac{1}{2} I$ $\times \sqrt{\{\frac{3}{2} + \frac{3}{2} \cos 2(p - \xi)\}}$	·00522* ·01649	$-(s - \xi) + Q - \frac{1}{2}\pi$ where $\tan Q = \frac{1}{2} \tan(p - \xi)$	$\gamma - \sigma$	14·4920521
J	$\frac{3}{2} e \frac{1}{2} \sin I \cos I$	·01485	$+(s - p) - \frac{1}{2}\pi$	$\gamma + \sigma - \omega$	15·5854433
	$\frac{17}{2} e^2 \frac{1}{2} \sin I \cos^2 \frac{1}{2} I$	·00487	$-2(s - \xi) - 2(s - p) + \frac{1}{2}\pi$	$\gamma - 4\sigma + 2\omega$	12·8542862
	$\frac{10^5}{16} me \frac{1}{2} \sin I \cos^2 \frac{1}{2} I$	·00512† ·00708	$-2(s - \xi) + (s - p) + 2h - 2s + \frac{1}{2}\pi$	$\gamma - 3\sigma - \omega + 2\eta$	13·4715144

\* The first of these two numbers is the mean value of the coefficient of the tide  $\gamma - \sigma - \omega$ ; the second applies to the tide M<sub>1</sub> compounded from  $\gamma - \sigma - \omega$  and  $\gamma - \sigma + \omega$ .

† The lower of these two figures gives the value when the coefficients in the Erection have the full value as derived from the Lunar Theory.

[ B, iii. ] *Long Period Tides*; General Coefficient =  $\frac{1}{2} - \frac{3}{2} \sin^2 \lambda$ .

Name or Initial	Coefficient	Mean Value of Coefficient	Argument	Speed	Speed in degrees per m. s. hour
	$(1 + \frac{3}{2}e^2) \frac{1}{2} (1 - \frac{3}{2} \sin^2 I)$	·25224†	Of variable part is <i>N</i> , the long. of node	$\frac{dN}{dt}$	19·34 per annum
Mm	$3e \frac{1}{2} (1 - \frac{3}{2} \sin^2 I)$	·04136	<i>s-p</i>	$\sigma - \omega$	0·5443747
Evection monthly	$\frac{4}{3}me \frac{1}{2} (1 - \frac{3}{2} \sin^2 I)$	·00580‡ ·00755	$-(s-p) + 2s - 2h$	$\sigma - 2\eta + \omega$	0·4715211
*	$3m^2 \frac{1}{2} (1 - \frac{3}{2} \sin^2 I)$	·00422‡ ·00621	$2(s-h)$	$2(\sigma - \eta)$	1·0158958
Mf	$(1 - \frac{5}{2}e^2) \frac{1}{2} \sin^2 I$	·07827	$2(s-\xi)$	$2\sigma$	1·0980330
Termensual	$\frac{7}{2}e \frac{1}{2} \sin^2 I$	·01516	$(s-p) + 2(s-\xi)$	$3\sigma - \omega$	1·6424077

\* Indicated by MSf as a compound tide. † The mean value of this coefficient is  $\frac{1}{2} (1 + \frac{3}{2}e^2) (1 - \frac{3}{2} \sin^2 i) (1 - \frac{3}{2} \sin^2 \omega) = \cdot 25$ , and the variable part is approximately  $-(1 + \frac{3}{2}e^2) \sin i \cos i \sin \omega \cos \omega \cos N = -\cdot 0329 \cos N$ .  
‡ The lower of these figures gives the value when the coefficients in the Evecton and Variation have their full values as derived from the Lunar Theory.

*Schedule of Solar Tides.*

$$\text{General Coefficient} = \frac{3}{2} \frac{M}{E} \left(\frac{a}{c}\right)^3 a.$$

Initial	Coefficient	Value of Coefficient	Argument	Speed	Speed in degrees per m. s. hour
[ C, i. ] <i>Semi-diurnal Tides</i> ; General Coefficient = $\cos^2 \lambda$ .					
S <sub>2</sub>	$\frac{\tau_1}{\tau} (1 - \frac{5}{2}e_1^2) \frac{1}{2} \cos^4 \frac{1}{2}\omega$	·21137	$2t$	$2(\gamma - \eta)$	30·0000000
K <sub>2</sub>	$\frac{\tau_1}{\tau} (1 + \frac{3}{2}e_1^2) \frac{1}{2} \sin^2 \omega$	·01823	$2t + 2h$	$2\gamma$	30·0821372
T	$\frac{\tau_1}{\tau} \frac{1}{2} \cdot \frac{7}{2}e_1 \cos^4 \frac{1}{2}\omega$	·01243	$2t - (h - p_1)$	$2\gamma - 3\eta$	29·9589314
R	$\frac{\tau_1}{\tau} \frac{1}{2} \cdot \frac{1}{2}e_1 \cos^4 \frac{1}{2}\omega$	·00178	$2t + h - p_1 + \pi$	$2\gamma - \eta$	30·0410686
[ C, ii. ] <i>Diurnal Tides</i> ; General Coefficient = $\sin 2\lambda$ .					
S <sub>1</sub> *	$\frac{\tau_1}{\tau} e_1 \frac{1}{2} \sin \omega \cos^2 \frac{1}{2}\omega$ $\times \sqrt{\frac{5}{2} + \frac{3}{2} \cos 2p_1}$	·00155	$t + Q_1 - \frac{1}{2}\pi$ where $\tan Q_1 = \frac{1}{2} \tan p_1$	$\gamma - \eta$	15·0000000
P	$\frac{\tau_1}{\tau} (1 - \frac{5}{2}e_1^2) \frac{1}{2} \sin \omega \cos^2 \frac{1}{2}\omega$	·08775	$t - h + \frac{1}{2}\pi$	$\gamma - 2\eta$	14·9589314
K <sub>1</sub>	$\frac{\tau_1}{\tau} (1 + \frac{3}{2}e_1^2) \frac{1}{2} \sin \omega \cos \omega$	·08407	$t + h - \frac{1}{2}\pi$	$\gamma$	15·0410686
[ C, iii. ] <i>Long Period Tides</i> ; General Coefficient = $\frac{1}{2} - \frac{3}{2} \sin^2 \lambda$ .					
Sa*	$\frac{\tau_1}{\tau} 3e_1 \frac{1}{2} (1 - \frac{3}{2} \sin^2 \omega)$	·00589	$h - p_1$	$\eta$	0·0410686
Ssa	$\frac{\tau_1}{\tau} (1 - \frac{5}{2}e_1^2) \frac{1}{2} \sin^2 \omega$	·03643	$2h$	$2\eta$	0·0821372

\* Included in the meteorological tides of rigorous speeds  $\gamma - \eta$  and  $\eta$ , see Sec. 10.

*Schedule of Speeds and of Coefficients in terms of  $M_2$ ,  $K_1$  or  $M_f$ .*

Tide	Speed in degrees per m. s. hour	Coefficient in terms of $M_2$	Tide	Speed in degrees per m. s. hour	Coefficient in terms of $K_1$	Tide	Speed in degrees per m. s. hour	Coefficient in terms of $M_f$
$M_2$	28·9841042	1·00000	$K_1$	15·0410686	1·00000	$M_f$	1·0980330	1·00000
$S_2$	30·0000000	0·46531	O	13·9430356	0·71096	$Mm$	0·5443747	0·52843
N	28·4397296	·19363	P	14·9589314	·33086	$Ssa$	0·0821372	·46544
$K_2$	30·0821372	·12662	Q	13·3986609	·13766	$3\sigma - \omega$	1·6424077	·19369
$\nu$	28·5125830	·03756	$M_1$	14·4920521	·06217	Evectional monthly	0·4715211	·09646
L	29·5284788	·02767	J	15·5854433	·05599	$2(\sigma - \eta)$	1·0158958	·07934
T	29·9589314	·02736	OO	16·1391016	·03062	Sa	0·0410686	·07525
2N	27·8953548	·02582	$\gamma - 3\sigma - \omega + 2\eta$	13·4715144	·02669			
$\mu$	27·9682084	·02108	$\gamma - 4\sigma + 2\omega$	12·8542862	·01836			
$\lambda$	29·4556254	·00726	$S_1$	15·0000000	·00584			
R	30·0410686	·00392						

A tide of greater importance than some of those retained here is that referred to where the approximation with regard to  $I$  was introduced, *viz.*, with speed  $2\gamma + \sigma - \omega$ ; the value of its coefficient is ·00323. There is also the larger variational diurnal tide which has been omitted: it would have a coefficient ·00450; also an evectional termensual tide,  $\frac{1}{16} \frac{a}{b} m e \frac{1}{2} \sin^2 I \cos(3s - 2h + p)$  with coefficient of magnitude ·00292. All other tides in a complete development as far as the second order of small quantities, without any approximation to the obliquity of the lunar orbit, would have smaller coefficients than those comprised in the above list. Such a development was made by the late Professor J. C. Adams, and the values of all the coefficients computed therefrom, in comparison with the above.

## 9.

### *Tides depending on the Fourth Power of the Moon's Parallax.*

The second term in the expression for the moon's tide-generating potential given in equation (2) *viz.* :—

$$V = \frac{\mu M}{r^4} \rho^3 \left( \frac{5}{2} \cos^3 z - \frac{3}{2} \cos z \right)$$

will give the tides depending on the fourth power of the moon's parallax.

In expanding this term, the eccentricity of the lunar orbit may be omitted; and it will appear below, when the principal terms are evaluated, that the declinational tides may be safely omitted. Thus, for this approximation,  $r = c$ ,  $M_3 = 0$ , and all terms in  $M_1$  and  $M_2$  which involve  $q^2$  may be omitted. Just as the first term in the potential was expanded in spherical harmonics of the second order, if the term under consideration is expanded in spherical harmonics of the third order it becomes

$$\begin{aligned} V \div \frac{\mu M}{c^4} \rho^3 = & \frac{5}{8}(\xi^3 - 3\xi\eta^2)(M_1^3 - 3M_1M_2^2) + \frac{5}{8}(\eta^3 - 3\xi^2\eta)(M_2^3 - 3M_1^2M_2) \\ & + \frac{3}{8}(\xi^3 + \xi\eta^2 - 4\xi^2\eta)(M_1^3 + M_1M_2^2) + \frac{3}{8}(\xi^2\eta + \eta^3 - 4\eta\xi^2)(M_1^2M_2 + M_2^3). \end{aligned}$$

Corresponding to these four terms there will be four tides of the types determined by these functions.



Now neglecting  $q^2$ ,

$$M_1 = p^2 \cos(\chi - l) \quad \text{and} \quad M_2 = -p^2 \sin(\chi - l),$$

so that

$$M_1^3 - 3M_1M_2^2 = p^6 \cos 3(\chi - l) \quad \text{and} \quad M_1^3 + M_1M_2^2 = p^6 \cos(\chi - l).$$

Also

$$\eta = 0 \quad \text{and} \quad \xi = \cos \lambda;$$

so that

$$\xi^3 - 3\xi\eta^2 = \cos^3 \lambda \quad \text{and} \quad \xi^3 + \xi\eta^2 - 4\xi\xi^2 = \cos \lambda (1 - 5 \sin^2 \lambda),$$

and following the same procedure as before, the height of the tide from the second term in the potential becomes

$$h = \frac{3}{2} \frac{M}{E} \left( \frac{a}{c} \right)^3 \frac{a^2}{c} \left[ \frac{5}{12} \cos^3 \lambda p^6 \cos 3(\chi - l) + \frac{1}{4} \cos \lambda (1 - 5 \sin^2 \lambda) p^6 \cos(\chi - l) \right] \quad . \quad (37)$$

Now,  $\cos \lambda (5 \sin^2 \lambda - 1)$  has its maximum value  $\frac{16}{3\sqrt{15}}$  when  $\cos \lambda = \frac{2}{\sqrt{15}} \sqrt{15}$ , that is when  $\lambda = 58^\circ 54'$ ; thus (37) may be written

$$h = \frac{3}{2} \frac{M}{E} \left( \frac{a}{c} \right)^3 a \left[ \cos^3 \lambda \frac{5}{12} \left( \frac{a}{c} \right) \cos^6 \frac{1}{2} I \cos [3t + 3(h - \nu) - 3(s - \xi)] \right. \\ \left. + \frac{3}{16} \sqrt{15} \cos \lambda (1 - 5 \sin^2 \lambda) \frac{4}{45} \sqrt{15} \left( \frac{a}{c} \right) \cos^6 \frac{1}{2} I \cos [t + (h - \nu) - (s - \xi)] \right] \quad . \quad (38)$$

In this expression there is the same general coefficient as before, and the spherical harmonics  $\cos^3 \lambda$ ,  $\frac{3}{16} \sqrt{15} \cos \lambda (5 \sin^2 \lambda - 1)$  have the maximum value unity, the first at the equator and the second in latitude  $58^\circ 54'$ . The speeds of the two tides are respectively  $3(\gamma - \sigma)$  or  $43^\circ \cdot 4761563$  per mean solar hour, and  $(\gamma - \sigma)$  or  $14^\circ \cdot 4920521$  per mean solar hour.

The coefficient of the tide  $3(\gamma - \sigma)$  is  $\frac{3}{12} \left( \frac{a}{c} \right) \cos^6 \frac{1}{2} I$ , and the mean value of this function multiplied by  $\cos 3(\nu - \xi)$  is  $\cdot 00599$ .

The coefficient of the tide  $(\gamma - \sigma)$  is  $\frac{4}{45} \sqrt{15} \left( \frac{a}{c} \right) \cos^6 \frac{1}{2} I$ , and the mean value of this function multiplied by  $\cos(\nu - \xi)$  is  $\cdot 00495$ .

The expression for the tides is written in a form applicable to the equatorial belt bounded by latitudes  $26^\circ 34'$  N. and S., *viz.*, where  $\sin \lambda = \frac{1}{5} \sqrt{5}$ . Outside of this belt what may be called high tide will correspond with low water, but the distribution of the land will probably seriously disturb the latitude of evanescent tide.

Comparing the mean values of these two tides with what has gone before it would appear that the terdiurnal tide  $3(\gamma - \sigma)$  or  $M_3$  is smaller than some of the tides that are neglected, but it is found with scarcely any trouble from the numerical analysis of the tidal observations, and is therefore still evaluated. The  $M_1$  tide of *rigorous* speed  $(\gamma - \sigma)$  is about the same size as the tide of speed  $\gamma - \sigma - \omega$ ; the former might be compounded with the latter and with the tide of speed  $\gamma - \sigma + \omega$  but the result, involving the latitude both in the coefficient and in the argument would be cumbersome and the composition has not hitherto been carried out.

## 10.

*Meteorological Tides.*

A rise and fall of water due to regular day and night breezes, prevalent winds, rainfall and evaporation, is called a meteorological tide.

All tides whose period is an exact multiple or sub-multiple of a mean solar day, or of a tropical year are affected by meteorological conditions. Thus all the tides of the principal solar astronomical series with speeds  $\gamma - \eta$ ,  $2(\gamma - \eta)$ ,  $3(\gamma - \eta)$ , &c., are subject to more or less meteorological perturbation, and although the diurnal elliptic tide  $S_1$  or  $\gamma - \eta$ , the semi-annual and annual tides of speeds  $2\eta$  and  $\eta$ , are all probably quite insensible as arising from astronomical causes, yet they have been found of sufficient importance to be included on the tide-predicter.

The annual and semi-annual tides are of enormous importance in some rivers, and in such cases the ter-annual tide  $3\eta$  is probably also important, but no harmonic analysis has yet been made for it.

In the reduction of these tides, the arguments of the S series are  $t$ ,  $2t$ ,  $3t$ , &c.; and of the annual, semi-annual and ter-annual tides  $h$ ,  $2h$ ,  $3h$ . As far as can be foreseen, the magnitudes of these tides will be constant from year to year.

## 11.

*Over-tides.*

When a wave runs into shallow water, its form undergoes a progressive change as it advances, the front slope generally becoming steeper and the back slope less steep. The most striking example of such a change is when the tide runs up a river in the form of a 'bore.'

A wave which in deep water presented an approximately simple harmonic contour, departs largely from that form when it has run into shallow water. Thus in rivers, the rise and fall of the water is not even approximately a simple harmonic motion. From the nature of harmonic analysis it is, however, possible to represent the motion by simple harmonic oscillations. For this purpose, it is necessary to introduce a series of over-tides whose speeds are double, treble, quadruple the speed of the fundamental astronomical tide.

The only tides, in which it has hitherto been thought necessary to represent this change of form in shallow water, belong to the principal lunar and principal solar series. Thus, besides the fundamental astronomical tides  $M_2$  and  $S_2$ , the over-tides  $M_4$ ,  $M_6$ ,  $M_8$  and  $S_4$ ,  $S_6$  have been deduced by harmonic analysis.

The height of the fundamental tide  $M_2$  varies from year to year, according to the variation in the obliquity of the lunar orbit, and this variability is represented by the coefficient  $\cos^4 \frac{1}{2}I$ . It is probable that the variability of  $M_4$ ,  $M_6$ ,  $M_8$ , will be represented by the square, cube and fourth power of that coefficient.

The law connecting the phase of an over-tide with the height of the fundamental tide is unknown, and under these circumstances it is only possible to make the argument of the over-tide a multiple of the argument of the fundamental tide, with a constant subtracted. If that constant is found to be the

same from year to year, then it will be known that the phase of an over-tide is independent of the height of the fundamental tide.

*Schedule of Over-tides.*

Tide	Coefficient	Argument	Speed	Speed in degrees per m. s. hour
$M_4$	$(\cos^4 \frac{1}{2}I)^2$	$4t + 4(h - \nu) - 4(s - \xi)$	$4\gamma - 4\sigma$	57·9682084
$M_6$	$(\cos^4 \frac{1}{2}I)^3$	$6t + 6(h - \nu) - 6(s - \xi)$	$6\gamma - 6\sigma$	86·9523126
$M_8$	$(\cos^4 \frac{1}{2}I)^4$	$8t + 8(h - \nu) - 8(s - \xi)$	$8\gamma - 8\sigma$	115·9364168
$S_4$	1	$4t$	$4\gamma - 4\eta$	60·0000000
$S_6$	1	$6t$	$6\gamma - 6\eta$	90·0000000

The column of arguments, in the above schedule, only gives that part of the argument which is derived from theory, and the constant to be subtracted from the argument is derivable from observation.

It is necessary to have recourse also to observation to determine whether the suggested law of variability in the magnitude of the M over-tides holds good.

## 12.

*Compound Tides.*

When two waves of different speeds are propagated in the same water, the vertical displacement at the surface is generally determined with sufficient accuracy by summing the displacements due to each wave separately. If, however, the height of each wave is not a small fraction of the depth of the water, the principle of superposition leads to inaccuracy, and it becomes necessary to take into account the squares and products of the displacements.

The consideration of the products of the displacements due to each tide gives what is known as compound tides, and these are found to be of considerable importance in estuaries. As each of these products contains two cosines multiplied together, which may further be exhibited as the sum of two cosines, each product will give rise to two compound tides whose arguments are respectively the sum and the difference of the arguments of the interacting waves.

Probably the best way of searching at any station for the compound tides which are likely to be important, is to take the semi-ranges of the five or six largest tides at that station, and to form index numbers of importance by multiplying the semi-ranges together two and two. Having selected as many of these combinations, in the order of importance, as may be thought expedient, the arguments of the compound tides are to be found by adding and subtracting the arguments of the components taken in pairs.

In the general case, it is only possible to take the tides which the previous schedules have shown usually to be large, and to form a list from these. The tides selected here are  $M_2$ ,  $K_1$ ,  $S_2$ , O and N, to

which are added  $M_4$  and  $S_4$ , although it is not possible to affix index numbers to combinations involving them.

*Schedule of Speeds arising out of Combinations.*

	$K_1$	$S_2$	O	N	$M_1$	$S_4$
$M_2$	$3\gamma - 2\sigma$ $\gamma - 2\sigma$ (O)	$4\gamma - 2\sigma - 2\eta$ $2\sigma - 2\eta$	$3\gamma - 4\sigma$ $\gamma$ ( $K_1$ )	$4\gamma - 5\sigma + \varpi$ $\sigma - \varpi$ (Mm)	—	$6\gamma - 2\sigma - 4\eta$ $2\gamma + 2\sigma - 4\eta$
$K_1$	—	$3\gamma - 2\eta$ $\gamma - 2\eta$ (P)	$2\gamma - 2\sigma$ ( $M_2$ ) $2\sigma$ (Mf)	$3\gamma - 3\sigma + \varpi$ $\gamma - 3\sigma + \varpi$ (Q)	$5\gamma - 4\sigma$ $3\gamma - 4\sigma$ (bis)	$5\gamma - 4\eta$ $3\gamma - 4\eta$
$S_2$	—	—	$3\gamma - 2\sigma - 2\eta$ $\gamma + 2\sigma - 2\eta$	$4\gamma - 3\sigma + \varpi - 2\eta$ $3\sigma - \varpi - 2\eta$	$6\gamma - 4\sigma - 2\eta$ $2\gamma - 4\sigma + 2\eta$	—
O	—	—	—	$3\gamma - 5\sigma + \varpi$ $\gamma - \sigma + \varpi$ ( $M_1$ )	$5\gamma - 6\sigma$ $3\gamma - 2\sigma$ (bis)	$5\gamma - 2\sigma - 4\eta$ $3\gamma + 2\sigma - 4\eta$
N	—	—	—	—	$6\gamma - 7\sigma + \varpi$ $2\gamma - \sigma - \varpi$ (L)	$6\gamma - 3\sigma + \varpi - 4\eta$ $2\gamma + 3\sigma - \varpi - 4\eta$

This schedule gives the speeds of the compound tides, and in many cases it will be observed that the compound tide itself has a speed identical with that of an astronomical or meteorological tide: these cases are indicated by the addition of the initial after the speed in question. It thus appears from the schedule that the tides O,  $K_1$ , Mm, P,  $M_2$ , Mf, Q,  $M_1$ , L are liable to perturbation in shallow water.

If either of the component tides or both be of lunar origin, the height of the compound tide will change from year to year, and will probably vary proportionally to the product of the coefficients of the component tides.

As in the case of the over-tides, the law of variability of the amplitudes of compound tides in various years is only to be tested by observation.

The following schedule contains twelve of the most important compound tides, those which are at present reduced being denoted by initials.

*Schedule of Compound Tides.*

Index of Importance	Initial	Arguments combined	Speed	Speed in degrees per m. s. hour
1205 —	$M_2K_1$	$M_2 + K_1$ $M_1 - O$	{ $3\gamma - 2\sigma$ }	44·0251728
960	MS	$M_2 + S_2$	$4\gamma - 2\sigma - 2\eta$	58·9841042
960	MSf	$S_2 - M_2$	$2\sigma - 2\eta$	1·0158958
857 —	$2M_2K_1$	$M_2 + O$ $M_1 - K_1$	{ $3\gamma - 4\sigma$ }	42·9271398
561	—	$S_2 + K_1$	$3\gamma - 2\eta$	45·0410686
400	$M_2N$	$M_2 + N$	$4\gamma - 5\sigma + \varpi$	57·4238338
399	—	$S_2 + O$	$3\gamma - 2\sigma - 2\eta$	43·9430356
399	—	$S_2 - O$	$\gamma + 2\sigma - 2\eta$	16·0569644
—	2SM	$S_4 - M_2$	$2\gamma + 2\sigma - 4\eta$	31·0158958
—	—	$M_2 + S_4$	$6\gamma - 2\sigma - 4\eta$	88·9811042
—	$\mu$ or 2MS	$M_4 - S_2$	$2\gamma - 4\sigma + 2\eta$	27·9682084
—	—	$M_4 + S_2$	$6\gamma - 4\sigma - 2\eta$	87·9682084

It will be noticed that in two cases an over-tide of one speed arises in more than one way, and accordingly different parts of it have different arguments and coefficients. In these cases, the utilisation of the results of one year for prediction in future years can only be made by dividing up the compound tide into several parts, according to its theoretical origin. In order to do this it is necessary to know the law which connects the heights of a summation and a difference compound tide. A like difficulty arises from the fact that MSf and 2SM are also variational tides.

In practice, however, the compound tide will generally be so small, that it may probably be treated as though it arose entirely in one way, and accordingly the tides  $3\gamma - 2\sigma$  or  $M_2K_1$  and  $3\gamma - 4\sigma$  or  $2M_2K_1$  are treated as though they arose entirely from  $M_2 + K_1$  and  $M_4 - K_1$  respectively, and MSf and 2SM as though they were entirely compound tides.

### 13.

#### *General Method of Reduction of Tidal Observations.*

As will be seen at the end of the next chapter, the printed tabular forms, on which the numerical harmonic analysis of the tides is carried out, are arranged so that the series of observations to be analysed is supposed to begin at noon, or 0<sup>h</sup>, of the first day, and to extend for a year from that time. It has not been found practicable to arrange that the first day shall be the same at all the ports of observation.

The tides for which the reduction by harmonic analysis has been carried out are as follows:—  
 $S_1, S_2, S_4, S_6, S_8, M_1, M_2, M_3, M_4, M_6, M_8, O, K_1, K_2, P, J, Q, L, N, \lambda, \nu, \mu, R, T, MS, 2SM, 2N, M_2N, M_2K_1, 2M_2K_1, Mm, Mf, MSf, Sa, Ssa$ : of these the tides  $S_4, S_6, S_8, M_1, M_3, M_8, \lambda, R, Mm, Mf, MSf$  are not at present used in predicting the tides.

Supposing  $n$  to be the speed of any tide in degrees per mean solar hour, and  $t$  to be mean solar time elapsing since 0<sup>h</sup> of the first day, then the immediate result of the harmonic analysis is to obtain  $A$  and  $B$ , two heights, estimated in feet and tenths, such that the height of this tide is given by

$$A \cos nt + B \sin nt.$$

The question then arises as to what further reductions it will be convenient to make, in order to present the results in the most convenient form.

Firstly, let  $R = \sqrt{A^2 + B^2}$  and  $\tan \zeta = \frac{B}{A}$ ,  
 then the tide is represented by

$$R \cos (nt - \zeta).$$

In this form,  $R$  is the semi-range of the tide in British feet, and  $\zeta$  is an angle such that  $\frac{\zeta}{n}$  is the time elapsing after 0<sup>h</sup> of the first day, until it is high-water of this particular tide. It is obvious that  $\zeta$  may have any value from 0° to 360°, and that the results of the analysis of successive years of observation will not be comparable with one another, when presented in this form.

Secondly, let the results of the analysis be presented in a number of terms of the form

$$f \Pi \cos (V + u - \kappa).$$

Here,  $V$  is a linear function of the moon's and sun's mean longitudes, the mean longitudes of the moon's and sun's perigees and the local mean solar time at the place of observation, reduced to angle at 15° per hour.  $V$  increases uniformly with the time, and its rate of increase per mean solar hour is the  $n$  of the first method, or the speed of the tide.



the resultant tide may be written

$$R \cos(t + h - \frac{1}{2} \pi - \nu' - \kappa),$$

the transition to the actual case being effected by the introduction of  $\kappa$ .

If  $h_0$  be the sun's mean longitude at 0<sup>h</sup> of the first day,  $t + h - h_0$  is equal to  $\gamma t$ , where  $t$  is now mean solar time measured from that 0<sup>h</sup> and not reduced to angle; so that if

$$\zeta = \kappa + \frac{1}{2} \pi - h_0 + \nu' \quad \dots \quad (41)$$

the expression becomes

$$R \cos(\gamma t - \zeta),$$

which is the form in which the result of harmonic analysis for the total  $K_1$  tide is expressed in the first method.

From (41)  $\kappa = \zeta + (h_0 - \frac{1}{2} \pi) - \nu' \quad \dots \quad (42)$

In this formula,  $h_0 - \frac{1}{2} \pi$  is  $\mathcal{V}_0$  for the solar  $K_1$  tide, and  $\nu'$  is a complex function of  $N$ , the longitude of the moon's node, to be computed from the second equation of (40).

It now remains to consider the coefficient  $f$ .

If  $M_0$  is the mean value of the lunar  $K_1$  tide, it will be shown in Section 18 that

$$\frac{M}{M_0} = \frac{\sin I \cos I}{\sin \omega \cos \omega (1 - \frac{3}{2} \sin^2 i)};$$

also the ratio of  $M$  to  $S$  is according to theory

$$\frac{M}{S} = \frac{\tau (1 + \frac{3}{2} e^2) \sin I \cos I}{\tau_1 (1 + \frac{3}{2} e_1^2) \sin \omega \cos \omega}.$$

Now if  $R_0$  be the mean value of  $R$ , it will be shown in Section 18 that

$$R_0 = \text{the part independent of } N \text{ in the expansion of } R \cos \nu'.$$

But  $\sec^2 \nu' = 1 + \tan^2 \nu' = \frac{1 + 2 \left(\frac{S}{M}\right) \cos \nu + \left(\frac{S}{M}\right)^2}{\left(\cos \nu + \frac{S}{M}\right)^2},$

so that  $\cos \nu' = \frac{\cos \nu + \frac{S}{M}}{\left\{1 + 2 \frac{S}{M} \cos \nu + \left(\frac{S}{M}\right)^2\right\}^{\frac{1}{2}}},$

therefore  $R \cos \nu' = M \cos \nu + S.$

Now, as will be shown in Section 18, the part independent of  $N$  in the expansion of  $M \cos \nu$  is  $M_0$ , and in  $S$  is  $S_0$ ,

so that

$$R_0 = M_0 + S_0;$$

therefore  $f = \frac{R}{R_0} = \frac{\left\{1 + \left(\frac{S}{M}\right)^2 + 2 \frac{S}{M} \cos \nu\right\}^{\frac{1}{2}} \frac{M}{M_0}}{1 + \frac{S_0}{M_0}} \left. \begin{array}{l} \\ \\ \end{array} \right\} \dots \dots \dots (43)$

where  $\frac{S_0}{M_0} = \frac{\tau_1 (1 + \frac{3}{2} e_1^2)}{\tau (1 + \frac{3}{2} e^2)} \frac{1}{(1 - \frac{3}{2} \sin^2 i)}$

and  $\frac{S}{M} = \frac{S_0}{M_0} \frac{\sin \omega \cos \omega (1 - \frac{3}{2} \sin^2 i)}{\sin I \cos I}$

Following the same process in regard to the  $K_2$  luni-solar tide, it will be found that it may be written

$$R \cos (2t + 2h - 2\nu'' - \kappa),$$

where

$$R = M \left\{ 1 + \left( \frac{S}{M} \right)^2 + 2 \frac{S}{M} \cos 2\nu \right\}^{\frac{1}{2}},$$

and

$$\tan 2\nu'' = \frac{\sin 2\nu}{\cos 2\nu + \frac{S}{M}};$$

and it follows that

$$f = \frac{\left\{ 1 + \left( \frac{S}{M} \right)^2 + 2 \frac{S}{M} \cos 2\nu \right\}^{\frac{1}{2}}}{1 + \frac{S_0}{M_0}} \frac{M}{M_0}$$

where

$$\frac{S_0}{M_0} = \frac{\tau_1 (1 + \frac{3}{2} e_1^2)}{\tau (1 + \frac{3}{2} e^2)} \frac{1}{(1 - \frac{3}{2} \sin^2 i)}$$

and

$$\frac{S}{M} = \frac{S_0}{M_0} \frac{\sin^2 \omega (1 - \frac{3}{2} \sin^2 i)}{\sin^2 I}$$

} . . . . . (44)

The numerical value of  $\frac{S_0}{M_0}$  both for  $K_1$  and  $K_2$  is 46407.

## 15.

### *Special Treatment of the Tide L.*

It does not seem to be possible to bring the rule for the reduction of the L tide into an absolutely rigorous form, and the method must be looked on as a semi-empirical one, invented to take some account of perturbation.

It appears from the schedule B, i. that this tide is proportional to

$$\cos^{\frac{1}{2}} I \sqrt{1 - 12 \tan^2 \frac{1}{2} I \cos 2(p - \xi)} \cos [2t + 2(h - \nu) - 2(s - \xi) + (s - p) - R + \pi - \kappa] \quad (45)$$

where

$$\tan R = \frac{\sin 2(p - \xi)}{\frac{1}{6} \cot^2 \frac{1}{2} I - \cos 2(p - \xi)}.$$

The tide is now only approximately harmonic and the amplitude is variable. If the part under the root were unity and  $R = 0$ , the expression would represent the pure L tide: hence, if in analysing over the period of a year, a mean value is assigned to  $R$  as a constant, and a mean value to the part under the root also as a constant, some account will have been taken of the perturbing term. Consequently,  $R$  must be considered as forming part of the function  $u$  for which the mean value is to be taken; and although this way of looking at it is not very satisfactory, seeing that  $p$  increases by nearly  $41^\circ$  per annum, yet it is practically sufficient for a small tide like L.

If then,  $P$  is taken as the longitude of the perigee at mid-year measured from the intersection, and  $R$  is computed from the formula

$$\tan R = \frac{\sin 2P}{\frac{1}{6} \cot^2 \frac{1}{2} I - \cos 2P} \quad (46)$$

the treatment will be the same as in all the other cases, if the argument  $V + u$  is taken as

$$2t + 2(h - \nu) - 2(s - \xi) + (s - p) - R + \pi.$$



The factor  $f$  will be found, by considering the part under the root as unity, to be,

$$\frac{\cos^4 \frac{1}{2} I}{\cos^4 \frac{1}{2} \omega \cos^4 \frac{1}{2} i} \sqrt{1 - 12 \tan^2 \frac{1}{2} I \cos 2P}$$

## 16.

### *Special Treatment of the Tide $M_1$ .*

The procedure in regard to this tide must also be looked on as semi-empirical; and here it is of even less importance to be correct, as the true lunar diurnal tide depending on the fourth power of the moon's parallax has been neglected.

Reference to schedule B, ii. shows that this tide is proportional to

$$\sin I \cos^2 \frac{1}{2} I \sqrt{\frac{5}{2} + \frac{3}{2} \cos 2(p - \xi)} \cos [t + (h - \nu) - (s - \xi) + Q - \frac{1}{2} \pi - \kappa] \quad (47)$$

where

$$\tan Q = \frac{1}{2} \tan (p - \xi).$$

As before,  $Q$  must be considered part of the function  $u$  for which a mean value is to be taken, the remark made about  $R$  applying equally to it.

Thus  $Q$  must be computed from the formula

$$\tan Q = \frac{1}{2} \tan P \quad (48)$$

the argument  $P + u$  being

$$t + (h - \nu) - (s - \xi) + Q - \frac{1}{2} \pi,$$

and the factor  $f$  being

$$\frac{\sin I \cos^2 \frac{1}{2} I}{\sin \omega \cos^2 \frac{1}{2} \omega \cos^4 \frac{1}{2} i} \sqrt{1 + \frac{3}{5} \cos 2P} \quad (49)$$

Through an oversight in the original computations, the quantity  $\sqrt{\frac{5}{2}}$  was left out, and the factor introduced into the computation forms as  $\frac{\sin I \cos^2 \frac{1}{2} I}{\sin \omega \cos^2 \frac{1}{2} \omega \cos^4 \frac{1}{2} i} \sqrt{\frac{5}{2} + \frac{3}{2} \cos 2P}$ . As it is a matter of indifference for the practical prediction of the tides what factor is used, this value has been allowed to stay both in the forms and in the remaining chapters of this volume.

## 17.

### *Method of computing the Arguments and Coefficients.*

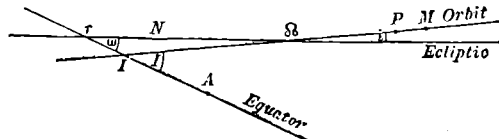
In performing the reductions of the preceding pages, a number of numerical quantities are required which are to be derived from the positions of the heavenly bodies.

In the accompanying figure,

$$I \Omega = N - \xi,$$

$$\varphi I = \nu,$$

$$\varphi \Omega = N,$$



and the angles at  $\varphi$ ,  $\Omega$  and  $I$  are now  $\omega$ ,  $i$  and  $I$  respectively.

The usual formulæ in spherical trigonometry consequently give

$$\left. \begin{aligned} \cot(N - \xi) \sin N &= \cos N \cos i + \sin i \cot \omega \\ \cot \nu \sin N &= \cos N \cos \omega + \sin \omega \cot i \\ \cos I &= \cos i \cos \omega - \sin i \sin \omega \cos N \end{aligned} \right\} \cdot \cdot \cdot \cdot (50)$$

so that

$$\text{if } \beta \text{ is an auxiliary defined by } \tan \beta = \tan i \cos N \cdot \cdot \cdot \cdot (51)$$

then

$$\left. \begin{aligned} \cos I &= \cos i \sec \beta \cos(\omega + \beta) \\ \sin \nu &= \sin i \operatorname{cosec} I \sin N \\ \sin(N - \xi) &= \sin \omega \operatorname{cosec} I \sin N \end{aligned} \right\} \cdot \cdot \cdot \cdot (52)$$

a table of values of  $\xi, \nu, I$  for every half degree of  $N$  with  $\omega = 23^\circ 27' \cdot 3$  and  $i = 5^\circ 8' \cdot 8$ , is given at the end of the next chapter.

## 18.

### *On the Mean Values of the Coefficients in Schedules [B].*

In the three schedules B, i., B, ii., B, iii. of the lunar tides, the coefficients are certain functions of  $I$ , and there are certain terms in the arguments, which are functions of  $\nu$  and  $\xi$ . All these terms may be typified by  $J \cos(T + u)$ , where  $J$  is a function of  $I$ , and  $u$  of  $\nu$  and  $\xi$ . If the values of  $J$  and  $u$  are substituted in terms of  $\omega, i$  and  $N$  and the result developed, a series of terms is obtained in which one is independent of  $N$ . Now, it is shown in what follows that the part independent of  $N$  in  $J \sin u$  is zero, and in  $J \cos u$  is  $J_1$ , say; therefore the part independent of  $N$  in the expression  $J \cos(T + u)$  is  $J_1 \cos T$ , so that  $J_1$  is the mean value of the semi-range of the tide in question.

A reference to the schedules shows that the following values of  $J \cos u$  are required:—

$$\begin{aligned} \cos^4 \frac{1}{2} I \cos 2(\nu - \xi); \quad \sin^2 I \cos 2\nu; \quad \sin I \cos^2 \frac{1}{2} I \cos(2\xi - \nu); \quad \sin I \sin^2 \frac{1}{2} I \cos(2\xi + \nu); \\ \sin I \cos I \cos \nu; \quad \sin^2 I \cos 2\xi; \quad 1 - \frac{3}{2} \sin^2 I, \end{aligned}$$

with corresponding values for  $J \sin u$ .

Now let

$$P = \cos \frac{1}{2} \omega, \quad p = \cos \frac{1}{2} i, \quad Q = \sin \frac{1}{2} \omega \quad \text{and} \quad q = \sin \frac{1}{2} i,$$

and let

$$\pi = Pp - Qqe^{N\sqrt{-1}}, \quad \kappa = Qp + Pqe^{N\sqrt{-1}},$$

$$\pi_1 = Pp - Qqe^{-N\sqrt{-1}}, \quad \kappa_1 = Qp + Pqe^{-N\sqrt{-1}}.$$

Then

$$\begin{aligned} \sin I \cos(N - \xi) &= \sin i \cos \omega + \cos i \sin \omega \cos N \\ &= 2[(P^2 - Q^2)pq + PQ(p^2 - q^2) \cos N], \end{aligned}$$

and

$$\sin I \sin(N - \xi) = 2PQ \sin N.$$

Therefore

$$\begin{aligned} \sin I e^{(N - \xi)\sqrt{-1}} &= \sin I \{ \cos(N - \xi) + \sqrt{-1} \sin(N - \xi) \} \\ &= 2[(P^2 - Q^2)pq + PQ(p^2 - q^2) \cos N + PQ(p^2 + q^2)\sqrt{-1} \sin N] \\ &= 2[(P^2 - Q^2)pq + PQp^2 e^{N\sqrt{-1}} - PQq^2 e^{-N\sqrt{-1}}] \\ &= 2[Pq(Pp - Qqe^{-N\sqrt{-1}}) + Qp(Ppe^{N\sqrt{-1}} - Qq)] \\ &= 2\pi_1 [Pq + Qpe^{N\sqrt{-1}}] \\ &= 2\pi_1 \kappa_1 e^{N\sqrt{-1}} \end{aligned}$$

so that

$$\sin I e^{-\xi\sqrt{-1}} = 2\pi_1 \kappa_1;$$

again  $\sin I \cos \nu = \sin \omega \cos i + \cos \omega \sin i \cos N$   
 $= 2[PQ(p^2 - q^2) + pq(P^2 - Q^2) \cos N],$

and  $\sin I \sin \nu = 2pq \sin N;$

so that similarly  $\sin I e^{\nu\sqrt{-1}} = 2\pi_1 \kappa.$

Also  $\cos I = \cos \omega \cos i - \sin \omega \sin i \cos N$   
 $= (P^2 - Q^2)(p^2 - q^2) - 4PQpq \cos N$   
 $= P^2p^2 - P^2q^2 - Q^2p^2 + Q^2q^2 - 2PQpq(e^{N\sqrt{-1}} + e^{-N\sqrt{-1}})$   
 $= \pi \pi_1 - \kappa \kappa_1;$

and  $\pi \pi_1 + \kappa \kappa_1 = P^2p^2 + Q^2q^2 + Q^2p^2 + P^2q^2$   
 $= (P^2 + Q^2)(p^2 + q^2)$   
 $= 1;$

therefore  $2\cos^2 \frac{1}{2} I = 1 + \cos I = 2\pi \pi_1$

or  $\cos^2 \frac{1}{2} I = \pi \pi_1$  and  $\sin^2 \frac{1}{2} I = \kappa \kappa_1.$

Now  $\sin^2 I e^{(\nu-\xi)\sqrt{-1}} = 4\pi_1^2 \kappa \kappa_1,$

so that  $e^{(\nu-\xi)\sqrt{-1}} = \frac{\pi_1}{\pi};$

therefore  $\cos 2(\nu - \xi) = \frac{e^{2(\nu-\xi)\sqrt{-1}} + e^{-2(\nu-\xi)\sqrt{-1}}}{2} = \frac{\pi^4 + \pi_1^4}{2\pi^2 \pi_1^2},$

or  $\cos^4 \frac{1}{2} I \cos 2(\nu - \xi) = \frac{1}{2}(\pi^4 + \pi_1^4) \dots \dots \dots (i)$

Again  $e^{\nu\sqrt{-1}} = \frac{2\pi_1 \kappa}{\sin I} = \sqrt{\frac{\pi_1 \kappa}{\pi \kappa_1}};$

therefore  $\cos 2\nu = \frac{\pi_1^3 \kappa^2 + \pi^2 \kappa_1^2}{2\pi \pi_1 \kappa \kappa_1},$

or  $\sin^2 I \cos 2\nu = 2(\pi^2 \kappa_1^2 + \pi_1^2 \kappa^2) \dots \dots \dots (ii)$

Similarly  $\sin I \cos^2 \frac{1}{2} I \cos(2\xi - \nu) = \pi^3 \kappa + \pi_1^3 \kappa_1 \dots \dots \dots (iii)$

$\sin I \sin^2 \frac{1}{2} I \cos(2\xi + \nu) = \pi \kappa^3 + \pi_1 \kappa_1^3 \dots \dots \dots (iv)$

$\sin I \cos I \cos \nu = (\pi \kappa_1 + \pi_1 \kappa)(\pi \pi_1 - \kappa \kappa_1) \dots \dots \dots (v)$

$\sin^2 I \cos 2\xi = 2(\pi^2 \kappa^2 + \pi_1^2 \kappa_1^2) \dots \dots \dots (vi)$

and  $1 - \frac{3}{2} \sin^2 I = \pi^2 \pi_1^2 - 4\pi \pi_1 \kappa \kappa_1 + \kappa^2 \kappa_1^2 \dots \dots \dots (vii)$

Now  $\pi^4 = P^4 p^4 - 4P^3 p^3 Q q e^{N\sqrt{-1}} + 6P^2 p^2 Q^2 q^2 e^{2N\sqrt{-1}} - 4P p Q^3 q^3 e^{3N\sqrt{-1}} + Q^4 q^4 e^{4N\sqrt{-1}},$

and  $\pi_1^4 =$  same with  $e^{-N\sqrt{-1}}$  written for  $e^{N\sqrt{-1}},$

therefore  $\frac{1}{2}(\pi^4 + \pi_1^4) = P^4 p^4 - 4P^3 p^3 Q q \cos N + 6P^2 p^2 Q^2 q^2 \cos 2N - 4P p Q^3 q^3 \cos 3N + Q^4 q^4 \cos 4N,$

so that the part independent of  $N$  in (i) is  $P^4 p^4$  or  $\cos^4 \frac{1}{2} \omega \cos^4 \frac{1}{2} i.$

Again  $\pi_1 \kappa = PQp^3 - PQq^3 + P^2pqe^{N\sqrt{-1}} - Q^2pqe^{-N\sqrt{-1}},$

and  $\pi_1^2 \kappa^2 = P^2Q^2(p^3 - q^3)^2 - 2P^2Q^2p^2q^2 + 2PQ(p^3 - q^3) [P^2pqe^{N\sqrt{-1}} - Q^2pqe^{-N\sqrt{-1}}]$   
 $+ P^4p^2q^2e^{2N\sqrt{-1}} + Q^4p^2q^2e^{-2N\sqrt{-1}},$

and  $\pi^2 \kappa_1^2 = \text{same with } e^{-N\sqrt{-1}} \text{ written for } e^{N\sqrt{-1}},$

so that the part independent of  $N$  in (ii) is

$$4P^2Q^2 \{(p^2 - q^2)^2 - 2p^2q^2\},$$

or  $4P^2Q^2 \{(p^2 + q^2)^2 - 6p^2q^2\},$

or  $\sin^2 \omega \{1 - \frac{3}{2} \sin^2 i\}.$

Similarly, the part independent of  $N$  in (iii) is

$$2P^3p^3Qp \text{ or } \sin \omega \cos^2 \frac{1}{2} \omega \cos^4 \frac{1}{2} i;$$

$$\text{and in (iv) is } 2Q^3p^3Pp \text{ or } \sin \omega \sin^2 \frac{1}{2} \omega \cos^4 \frac{1}{2} i.$$

Again  $\pi \kappa_1 + \pi_1 \kappa = 2PQ(p^2 - q^2) + (P^2 - Q^2)pqe^{N\sqrt{-1}} + (P^2 - Q^2)pqe^{-N\sqrt{-1}},$

and  $\pi \pi_1 - \kappa \kappa_1 = (P^2 - Q^2)(p^2 - q^2) - 2PQpqe^{N\sqrt{-1}} - 2PQpqe^{-N\sqrt{-1}};$

therefore the part independent of  $N$  in (v) is

$$2PQ(P^2 - Q^2)(p^4 - q^4) - 4PQ(P^2 - Q^2)p^2q^2,$$

or  $2PQ(P^2 - Q^2)(1 - 6p^2q^2),$

or  $\sin \omega \cos \omega (1 - \frac{3}{2} \sin^2 i).$

Again  $\pi \kappa = PQp^3 + (P^2 - Q^2)pqe^{N\sqrt{-1}} - PQq^3e^{2N\sqrt{-1}},$

$$\pi_1 \kappa_1 = \text{same with } e^{-N\sqrt{-1}} \text{ for } e^{N\sqrt{-1}},$$

therefore the part independent of  $N$  in (vi) is

$$4P^2Q^2p^4 \text{ or } \sin^2 \omega \cos^4 \frac{1}{2} i.$$

Again  $\pi^2 \pi_1^2 - 4\pi \pi_1 \kappa \kappa_1 + \kappa^2 \kappa_1^2 = 1 - 6\pi \pi_1 \kappa \kappa_1$

But  $\pi \kappa = PQp^3 + (P^2 - Q^2)pqe^{N\sqrt{-1}} - PQq^3e^{2N\sqrt{-1}},$

and  $\pi_1 \kappa_1 = \text{same with } e^{-N\sqrt{-1}} \text{ instead of } e^{N\sqrt{-1}},$

therefore the part independent of  $N$  in (vii) is

$$1 - 6 \{P^3Q^2p^4 + (P^2 - Q^2)^2p^2q^2 + P^2Q^2q^4\},$$

which reduces to

$$(1 - \frac{3}{2} \sin^2 \omega) (1 - \frac{3}{2} \sin^2 i).$$

Proceeding in a similar manner, it will easily be seen that the parts independent of  $N$  in the expressions  $\cos^4 \frac{1}{2} I \sin 2(\nu - \xi)$ ;  $\sin^2 I \sin 2\nu$ ;  $\sin I \cos^2 \frac{1}{2} I \sin(2\xi - \nu)$ ;  $\sin I \sin^2 \frac{1}{2} I \sin(2\xi + \nu)$ ;  $\sin I \cos I \sin \nu$  and  $\sin^2 I \sin 2\xi$  are all zero, so that the mean values of the semi-ranges are as given above.

As then  $f$  is the ratio of the mean value of a coefficient to the coefficient itself, and the mean value of the coefficients have just been found, it follows that the various values of  $\frac{1}{f}$  which are required are:—

$$(i). \frac{\cos^4 \frac{1}{2} \omega \cos^4 \frac{1}{2} i}{\cos^4 \frac{1}{2} I}; \quad (ii). \frac{\sin^2 \omega (1 - \frac{3}{2} \sin^2 i)}{\sin^2 I}; \quad (iii). \frac{\sin \omega \cos^2 \frac{1}{2} \omega \cos^4 \frac{1}{2} i}{\sin I \cos^2 \frac{1}{2} I};$$

$$(iv). \frac{\sin \omega \sin^2 \frac{1}{2} \omega \cos^4 \frac{1}{2} i}{\sin I \sin^2 \frac{1}{2} I}; \quad (v). \frac{\sin \omega \cos \omega (1 - \frac{3}{2} \sin^2 i)}{\sin I \cos I}; \quad (vi). \frac{\sin^2 \omega \cos^4 \frac{1}{2} i}{\sin^2 I};$$

$$(vii). \frac{(1 - \frac{3}{2} \sin^2 \omega) (1 - \frac{3}{2} \sin^2 i)}{1 - \frac{3}{2} \sin^2 I}; \quad (viii). \frac{1 \cdot 46407 k_2}{\sqrt{\{1 + (0 \cdot 46407 \times k_2)^2 + 0 \cdot 92814 k_2 \cos 2\nu\}}}, \text{ where}$$

$k_2$  is the value of  $\frac{1}{f}$  in (ii);  $(ix). \frac{1 \cdot 46407 k_1}{\sqrt{\{1 + (0 \cdot 46407 \times k_1)^2 + 0 \cdot 92814 k_1 \cos \nu\}}}$ , where  $k_1$  is the value of  $\frac{1}{f}$  in (v), the two latter being for the  $K_2$  and  $K_1$  tides respectively.

The angle  $I$  ranges from  $18^\circ 18' \cdot 5$ , when it is  $\omega - i$ , to  $28^\circ 36' \cdot 1$ , when it is  $\omega + i$ , and tables have been constructed giving  $\frac{1}{f}$  and  $f$  for every  $0^\circ \cdot 1$  between these limits.

The coefficients for the over-tides and compound tides may be found from tables of squares and cubes, and by multiplication.

## 19.

### *Evaluation of the Quantities $s, p, h, p_1,$ and $N.$*

The quantities  $s, p, h, p_1,$  and  $N$  required in the calculations of the arguments and coefficients may be computed from the formulæ given in the preface to Hansen's *Tables de la Lune*, page 15. These are for  $0^h$ , January 0, 1800:—

$$g = 110^\circ 19' 33'' \cdot 64 + (13 \times 360^\circ + 331158'' \cdot 3715) (t - 1800) + 49'' \cdot 435 \left(\frac{t - 1800}{100}\right)^2 + 0'' \cdot 050073 \left(\frac{t - 1800}{100}\right)^3,$$

$$g' = 0^\circ 24' 28'' \cdot 22 + (360^\circ - 33'' \cdot 9218) (t - 1800) - 0'' \cdot 5612 \left(\frac{t - 1800}{100}\right)^2,$$

$$\omega = 192^\circ 7' 21'' \cdot 91 + 216115'' \cdot 2207 (t - 1800) - 44'' \cdot 323 \left(\frac{t - 1800}{100}\right)^2 - 0'' \cdot 043759 \left(\frac{t - 1800}{100}\right)^3,$$

$$\omega' = 246^\circ 13' 50'' \cdot 28 + 69690'' \cdot 9809 (t - 1800) - 6'' \cdot 518 \left(\frac{t - 1800}{100}\right)^2 - 0'' \cdot 007159 \left(\frac{t - 1800}{100}\right)^3,$$

$$\Theta = 326^\circ 43' 28'' \cdot 85 + 69629'' \cdot 3961 (t - 1800) - 8'' \cdot 189 \left(\frac{t - 1800}{100}\right)^2 - 0'' \cdot 007159 \left(\frac{t - 1800}{100}\right)^3,$$

where  $g$  and  $g'$  are the mean anomalies of the moon and sun respectively,  $\omega$  and  $\omega'$  the distances from the moon's and sun's perigees to the ascending node,  $\Theta$  the supplement of the longitude of the ascending node, and  $t$  the time in Julian years of  $365\frac{1}{4}$  days;

so that

$$N = 360^\circ - \Theta,$$

$$p = \omega - \Theta,$$

$$p_1 = \omega' - \Theta,$$

$$s = g + p,$$

$$h = g' + p_1.$$

These formulæ when reduced to a more convenient epoch and to forms appropriate to the present investigation become

$$\begin{aligned} s &= 150^{\circ}0419 + [13 \times 360^{\circ} + 132^{\circ}67900] T + 13^{\circ}1764 D + 0^{\circ}5490165 H, \\ p &= 240^{\circ}6322 + 40^{\circ}69035 T + 0^{\circ}1114 D + 0^{\circ}0046418 H, \\ h &= 280^{\circ}5287 + 360^{\circ}00769 T + 0^{\circ}9856 D + 0^{\circ}0410686 H, \\ p_1 &= 280^{\circ}8748 + 0^{\circ}01711 T + 0^{\circ}000047 D, \\ N &= 285^{\circ}9569 - 19^{\circ}34146 T - 0^{\circ}0529540 D, \end{aligned}$$

where  $T$  is the number of Julian years of  $365\frac{1}{4}$  mean solar days,

$D$  the number of mean solar days,

$H$  the number of mean solar hours,

after 0<sup>h</sup> Greenwich mean time, January 1, 1880.

From these coefficients it appears that

$$\sigma = 0^{\circ}5490165,$$

$$\varpi = 0^{\circ}0046418,$$

$$\eta = 0^{\circ}0410686,$$

whence

$$\gamma = 15^{\circ}0410686.$$

For the purpose of using the forms for the harmonic analysis of the tidal observations, these formulæ may be reduced to yet more convenient and simple forms.

The mean values of  $N$  and  $p_1$  are required and, for the treatment of the  $L$  and  $M_1$  tides, the mean value of  $p - \xi$  denoted by  $P$ .

Half the coefficients of  $T$  may therefore be added once for all, and these three quantities written,

$$\begin{aligned} N &= 276^{\circ}2861 - 0^{\circ}05295 D - 19^{\circ}34146 T, \\ p_1 &= 280^{\circ}8833 + 0^{\circ}00005 D + 0^{\circ}01711 T, \\ P + \xi &= 261^{\circ}0 + 0^{\circ}111 D + 40^{\circ}69 T, \end{aligned}$$

where  $T$  is simply the number of years, whether there be leap-years or not among them, since 1880 and  $D$  the number of days from January 1, numbered as zero, up to the first day of the year to be analysed.

Now suppose,  $d$  to denote the number of quarter days, either one, two, or three in excess of the Julian years, which have elapsed since 0<sup>h</sup> January 1, 1880 up to 0<sup>h</sup> January 1 of the year in question; let  $D$  denote the same as before, and let  $L$  be the east longitude of the place of observation in hours and decimals of hours, then the formulæ give for  $s_0$ ,  $p_0$ ,  $h_0$ , the values of  $s$ ,  $p$  and  $h$  at 0<sup>h</sup> of the first day,

$$\begin{aligned} s_0 &= 150^{\circ}0419 + 132^{\circ}67900 T + 3^{\circ}29410 d + 13^{\circ}1764 D - 0^{\circ}54902 L, \\ p_0 &= 240^{\circ}6322 + 40^{\circ}69035 T + 0^{\circ}02785 d + 0^{\circ}1114 D - 0^{\circ}00464 L, \\ h_0 &= 280^{\circ}5287 + 0^{\circ}00769 T + 0^{\circ}24641 d + 0^{\circ}9856 D - 0^{\circ}04107 L. \end{aligned}$$

In these formulæ  $T$  is an integer, being the excess of the year in question above 1880, and  $d$  is to be determined thus:—If the excess of the year above 1880 divided by 4 leaves remainder 3,  $d$  is 1; if

remainder 2, it is 2; if remainder 1, it is 3; and if remainder zero, it is zero. For example for 1895,  $T = 15$ ,  $d = 1$ ; because from 0<sup>h</sup> January 1, 1880 to 0<sup>h</sup> January 1, 1895 is 15 Julian years and a quarter day. For all dates after February 28, 1900, one day's motion must be subtracted from  $s_0$ ,  $p_0$ ,  $h_0$ ,  $p$ , and  $P + \xi$ , and one day's motion added to  $N$ .

The terms in  $L$  may be described as corrections for longitude: the multiple of  $360^\circ$  which occurred in  $s$  and  $h$  are omitted as  $T$  is essentially an integer. If it be preferred, the values of  $s_0$  and  $N$  may be extracted from the *Nautical Almanac*, and  $h_0$  is (neglecting nutation) the sidereal time reduced to angle. Also  $p_0$  can be taken from the tables in Chapter VII which are reprinted from those given at pages 299 and 300 of Hansen's *Tables de la Lune*.

The results of the various kinds of tides are scattered throughout the preceding pages, and it will therefore be convenient to collect them together. In order to present the results in a form convenient for computation, each argument is given by reference to any previous argument which contains the same element. In the following schedule Arg.  $M_2$  and Fac.  $M_2$  (for example) mean the argument and factor computed for the tide  $M_2$ .

*Schedule of Arguments at 0<sup>h</sup> of the First Day, and Factors for the Ensuing Year.*

Tide	Initial Argument. $r_0 + u$	Factor for Reduction. $\frac{1}{f}$
$S_1$ $S_2$ $S_3$ $S_4$	zero	unity
P	$-h_0 + \frac{1}{2}\pi$	unity
T	$-(h_0 - p_1)$	unity
$M_1$	$(h_0 - \nu) - (s_0 - \xi) + Q - \frac{1}{2}\pi$ , where $\tan Q = \frac{1}{2} \tan P$	Fac. O $\div \sqrt{\frac{5}{2} + \frac{3}{2} \cos 2P}$
$M_2$	$2(h_0 - \nu) - 2(s_0 - \xi)$	$\left(\frac{\cos \frac{1}{2}\omega \cos \frac{1}{2}i}{\cos \frac{1}{2}I}\right)^4$
$M_3$	$\frac{3}{2}$ Arg. $M_2$	(Fac. $M_2$ ) $^{\frac{3}{2}}$
$M_4$	2 Arg. $M_2$	(Fac. $M_2$ ) $^2$
$M_6$	3 Arg. $M_2$	(Fac. $M_2$ ) $^3$
$M_8$	4 Arg. $M_2$	(Fac. $M_2$ ) $^4$
$K_2$	$2h_0 - 2\nu''$ , where $\tan 2\nu'' = \frac{\sin 2\nu}{\cos 2\nu + .464 \times k}$	$\frac{1 \cdot 46407 k}{\sqrt{\{1 + (.464 \times k)^2 + .928 k \cos 2\nu\}}}$ where $k = \frac{\sin^2 \omega (1 - \frac{3}{2} \sin^2 i)}{\sin^2 I}$
$K_1$	$h_0 - \nu' - \frac{1}{2}\pi$ , where $\tan \nu' = \frac{\sin \nu}{\cos \nu + .464 \times k}$	$\frac{1 \cdot 46407 k}{\sqrt{\{1 + (.464 \times k)^2 + .928 k \cos \nu\}}}$ where $k = \frac{\sin 2\omega (1 - \frac{3}{2} \sin^2 i)}{\sin 2I}$
N	Arg. $M_2 - (s_0 - p_0)$	Fac. $M_2$
2N	Arg. N $- (s_0 - p_0)$	Fac. $M_2$

## Schedule of Arguments.—(Continued).

Tide	Initial Argument. $r_0 + u$	Factor for Reduction. $\frac{1}{f}$
L	Arg. $M_3 + (s_0 - p_0) - R + \pi$ where $\tan R = \frac{\sin 2P}{\frac{1}{2} \cot^2 \frac{1}{2} I - \cos 2P}$	Fac. $M_3 \div \sqrt{1 - 12 \tan^2 \frac{1}{2} I \cos 2P}$
$\nu$	Arg. $M_2 + (s_0 - p_0) 2h_0 - 2s_0$	Fac. $M_2$
O	$(h_0 - \nu) - 2(s_0 - \xi) + \frac{1}{2}\pi$	$\frac{\sin \omega \cos^2 \frac{1}{2} \omega \cos^4 \frac{1}{2} i}{\sin I \cos^2 \frac{1}{2} I}$
OO	$(h_0 - \nu) + 2(s_0 - \xi) - \frac{1}{2}\pi$	$\frac{\sin \omega \sin^2 \frac{1}{2} \omega \cos^4 \frac{1}{2} i}{\sin I \sin^2 \frac{1}{2} I}$
Q	Arg. O - $(s_0 - p_0)$	Fac. O
J	$(h_0 - \nu) + (s_0 - p_0) - \frac{1}{2}\pi$	$\frac{\sin 2\omega (1 - \frac{3}{2} \sin^2 i)}{\sin 2I}$
MS	Arg. $M_3$	Fac. $M_2$
$\mu$ or 2MS	Arg. $M_4$	Fac. $M_4$
2SM	$2\pi - \text{Arg. } M_2$	Fac. $M_2$
$M_2K_1$	Arg. $M_3 + \text{Arg. } K_1$	Fac. $M_2 \times \text{Fac. } K_1$
$2M_2K_1$	Arg. $M_4 - \text{Arg. } K_1$	Fac. $M_4 \times \text{Fac. } K_1$
$M_2N$	Arg. $M_3 + \text{Arg. } N$	Fac. $M_2 \times \text{Fac. } N$
MSf	$2\pi - \text{Arg. } M_2$	Fac. $M_2$
Mm	$s_0 - p_0$	$\frac{(1 - \frac{3}{2} \sin^2 \omega) (1 - \frac{3}{2} \sin^2 i)}{1 - \frac{3}{2} \sin^2 I}$
Mf	$2(s_0 - \xi)$	$\frac{\sin^2 \omega \cos^4 \frac{1}{2} i}{\sin^2 I}$
Sa	$h_0$	unity
Ssa	$2h_0$	unity



## CHAPTER VII.

### DESCRIPTION OF THE NUMERICAL HARMONIC ANALYSIS OF THE TIDES.

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#### 1.

##### *Measurement of the Heights of the Water.*

The tide-gauge gives a graphical record of the height of the water above some known datum for every instant of time. The first operation performed on the tidal record is the measurement, in feet and decimals, at every mean solar hour of the height of the water above the true zero of the gauge, the height of which relatively to the datum is known. The period chosen for analysis is about one year, and the first measurement corresponds to noon, but it has been found inconvenient hitherto to have the same initial noon at the several ports.

It would seem, at first sight, preferable to take the measurements at each lunar hour; but the whole of the actual process in use is based on measurements taken at the mean solar hours, and a change to lunar time would involve a great deal of fresh labour and expense.

The process used in reducing the short-period tides differs entirely from that employed for the long-period tides.

#### 2.

##### *Short-period Tides:—Manipulation of the Measurements.*

If  $T$  be the period of any one of the diurnal tides, or the double period of any one of the semi-diurnal tides, it approximates more or less nearly to 24 mean solar hours, and if it be divided into 24 equal parts, each part may be spoken of as a  $T$ -hour, while for brevity mean solar time will be referred to as  $S$ -time.

Let it be supposed, now, that there are two clocks, each marked with  $360^\circ$  or 24 hours, and that the hand of the first or  $S$ -clock goes round once in 24  $S$ -hours, and that of the second or  $T$ -clock once in 24  $T$ -hours; and that the two clocks are started at  $0^\circ$  or  $0^h$  at noon of the initial day. For the sake of distinctness, let a  $T$ -hour be longer than an  $S$ -hour, so that the  $T$ -clock goes slower than the  $S$ -clock.

The measurements of the tide-curve give the heights of the water at each *S*-hour, and it is required from these data to determine the height of the water at each *T*-hour. For this end, it is necessary to count *T*-time, but it must be done with reference to *S*-time, and moreover the time must be specified as an integral number of hours.

Beginning, then, with 0<sup>h</sup> of the first day, it is necessary to count 0, 1, 2, &c., as the *T*-hand comes up to its hour marks. But as the *S*-hand gains on the *T*-hand, there will come a time when, the *T*-hand being exactly at the *p* hour mark, the *S*-hand is nearly as far as  $p + \frac{1}{2}$ . When, however, the *T*-hand has advanced to the  $p + 1$  hour mark, the *S*-hand will be a little beyond  $p + 1 + \frac{1}{2}$ , that is to say, a little less than half-an-hour before  $p + 2$ . Counting, then, the *T*-hours in *S*-time, it is necessary to jump from *p* to  $p + 2$ . The counting will go on continuously for a number of hours nearly equal to  $2p$ , and then another number will be dropped, and so on throughout the whole year.

If the *T*-hand went faster than the *S*-hand, it is obvious that one number would be repeated at two successive hours instead of being dropped. Each such process may be described as a 'change.'

Now, if there is a sheet marked for entries of heights of water according to *T*-hours from results measured in *S*-hours, the *S*-measurements must be entered continuously up to *p*; then comes a 'change' and the dropping of one of the *S*-series, after which the entry goes on continuously until another 'change' when another is dropped, and so on.

Since a 'change' occurs when a *T*-hour falls almost exactly between two *S*-hours, it will be more accurate to insert the two *S*-entries which fall on each side of the truth. If this be done, the whole of the *S*-series of measurements will be entered on the *T*-sheet. Similarly, if it is the *T*-hand which goes faster than the *S*-hand, a gap may be left in the *T*-series instead of duplicating an entry.

For the analysis of the *T*-tide there is, therefore, prepared a sheet arranged in rows and columns: each row corresponds to one *T*-day and the columns are marked 0<sup>h</sup>, 1<sup>h</sup> and . . . 23<sup>h</sup>, the 0<sup>h</sup> of which may be called a *T*-noon. A dot is put in each space for the entry, and where there is a 'change' two dots are put if there is to be a double entry, or a bar if there is to be no entry, while black vertical lines mark the end of each *S*-day. The black vertical lines will of course fall into slightly irregular diagonal lines across the page, being steeper and steeper the more nearly *T*-time approaches to *S*-time. They slope downwards from right to left if the *T*-hour is longer than the *S*-hour, and the other way in the opposite case. The 'changes' also run diagonally with a slope in the opposite direction to that of the black lines when the *T*-hour is longer than the *S*-hour, and in the same direction in the opposite case.

These 'changes' and black lines will be found exhibited in the specimen of the reductions given at the end of this chapter.

Since the first day is numbered 1, and the first hour 0<sup>h</sup>, it follows that to find the period which has elapsed from 0<sup>h</sup> of the first day, it is necessary to subtract 1 from the number of the day and to add 1 to the number of the hour.

For each class of tide there are five pages in the computation forms, each page occupying two in the specimen of the reductions at the end of this chapter, giving in all about 370 values for the height of the water at each of the 24 special hours: the number of values for each hour varies slightly according as more or less changes fall into each column.

The numbers entered in each column are summed on each of the five pages: the five sets of results are now summed and the results divided each by the proper divisor for its column, thus giving a mean result for that column. In this way 24 numbers are found which give the mean height of the water at each of the 24 special hours.

It is obvious that if this process were continued over a very long time, in the end, the tide under analysis would be extracted from among all the others, and the heights thus found would accurately represent the heights of the water due to this tide; but as the process only extends over about a year, the elimination of the others is not quite complete.

### 3.

*Short-period Tides:—Selection of Periods for Analysis.*

The elimination of the effects of the other tides may be improved by choosing the period for analysis not exactly equal to one year. For, suppose that the expression for the height of the water is

$$A_1 \cos n_1 t + B_1 \sin n_1 t + A_2 \cos n_2 t + B_2 \sin n_2 t$$

where  $n_2$  is nearly equal to  $n_1$ , and that it is required to eliminate the  $n_2$ -tide so as to be left only with the  $n_1$ -tide.

The expression for the height of the water is equal to

$$\{A_1 + A_2 \cos (n_1 - n_2)t - B_2 \sin (n_1 - n_2)t\} \cos n_1 t \\ + \{B_1 + A_2 \sin (n_1 - n_2)t + B_2 \cos (n_1 - n_2)t\} \sin n_1 t,$$

so that the tide may be regarded as oscillating with a speed  $n_1$  but with slowly varying range.

Now, in the column appertaining to any hour in the form,  $n_1 t$  is a multiple of  $15^\circ$  if  $n_1$  be a diurnal, and of  $30^\circ$ , if  $n_1$  be a semi-diurnal tide. Consider the column headed ' $p$ -hours', then  $n_1 t = 15^\circ p$  for diurnals, and  $30^\circ p$  for semi-diurnals.

Hence the sum of all entries, supposing there are  $q$  of them in the column numbered  $p$ -hours, is for diurnal tides

$$\cos 15^\circ p \left\{ A_1 q + A_2 \left[ \cos (n_1 - n_2) \frac{15p}{n_1} + \cos (n_1 - n_2) \left( \frac{2\pi}{n_1} + \frac{15p}{n_1} \right) + \cos (n_1 - n_2) \left( \frac{2\pi}{n_1} + \frac{15p}{n_1} \right) \right. \right. \\ \left. \left. + \&c. \right] + B_2 [\&c.] \right\} + \sin 15^\circ p \left\{ \&c. \right\}$$

and for semi-diurnal tides, the arguments of all the circular functions in the expression are to be doubled.

Now such a number of terms is to be chosen that the series by which  $A_2$  and  $B_2$  are multiplied may vanish. This is exactly the case if the series is exactly re-entrant and is nearly the case if nearly re-entrant.

The condition is exactly satisfied where  $r$  is either a positive or negative integer for diurnal tides, if  $(n_1 - n_2) q \frac{2\pi}{n_1} = 2\pi r$ ; and for semi-diurnal tides if  $(n_1 - n_2) q \frac{4\pi}{n_1} = 2\pi r$ : that is to say, if

$$(n_1 - n_2) q = n_1 r \quad \text{for diurnal tides;}$$

or

$$(n_1 - n_2) q = \frac{1}{2} n_1 r \quad \text{for semi-diurnal tides.}$$

It is not worth while attempting to eliminate the effects of the semi-diurnal tides on the diurnal tides, and *vice versa*, because any period will satisfy the above equations within the fraction of a day, and owing to the incommensurability of the speeds, it is impossible to avoid being wrong to that amount.

It is of course impossible to choose for each tide  $n_1$ , a period which shall minimise the effects of more than one of the short-period tides  $n_2$  in vitiating the values of the mean semi-ranges of the tide  $n_1$ ; accordingly the periods have been chosen so as to minimise the effect of the principal solar semi-diurnal  $S_2$  upon the principal lunar semi-diurnal  $M_2$ , and of  $M_2$  on the other semi-diurnal tides: in the case of the diurnal tides the periods are chosen to minimise the effect of either O or  $K_1$ .

In analysing for the  $S_2$  tide, it is required to find the period which will minimise the effect of the  $M_2$  tide.

$$\begin{aligned} \text{Here} \quad n_1 &= 2(\gamma - \eta) = 2 \times 15^\circ \text{ per hour,} \\ n_2 &= 2(\gamma - \sigma), \\ n_1 - n_2 &= 2(\sigma - \eta) = 1^\circ \cdot 0158958 \text{ per hour;} \end{aligned}$$

the equation therefore is

$$1 \cdot 0158958 q = 15 r;$$

and if  $r = 25$ ,  $q = 369 \cdot 13$ . Thus 25 periods of  $2(\sigma - \eta)$  is  $369 \cdot 13$  mean solar days, so that in order to get as great accuracy as possible, the series must be summed over  $369 \cdot 13$  days. Now, this is true of all the columns, and as each must have the same number of entries, the period which should be chosen is 369 days.

In analysing for the  $M_2$  tide, it is required to find the period which will minimise the effect of the  $S_2$  tide.

$$\begin{aligned} \text{Here} \quad n_1 &= 2(\gamma - \sigma) = 2 \times 14^\circ \cdot 4920521 \text{ per hour,} \\ n_2 &= 2(\gamma - \eta), \\ n_1 - n_2 &= 2(\eta - \sigma) = -1^\circ \cdot 0158958 \text{ per hour;} \end{aligned}$$

hence, taking  $r$  negative,

$$1 \cdot 0158958 q = 14 \cdot 4920521 r;$$

and if  $r = 25$ ,  $q = 356 \cdot 63$ , so that the period should be 357 days, corresponding to a period of  $369^d 12^h$  mean solar time.

In analysing for the  $K_2$  tide, it is required to find the period which will minimise the effect of the  $M_2$  tide.

$$\begin{aligned} \text{Here} \quad n_1 &= 2\gamma = 2 \times 15^\circ \cdot 0410686 \text{ per hour,} \\ n_2 &= 2(\gamma - \sigma), \\ n_1 - n_2 &= 2\sigma = 1^\circ \cdot 0980330 \text{ per hour;} \end{aligned}$$

hence

$$1 \cdot 0980330 q = 15 \cdot 0410686 r;$$

and if  $r = 27$ ,  $q = 369 \cdot 85$ .

In analysing for the  $K_1$  tide, it is required to find the period which will minimise the effect of the O tide.

$$\begin{aligned} \text{Here} \quad n_1 &= \gamma = 15^\circ \cdot 0410686 \text{ per hour,} \\ n_2 &= \gamma - 2\sigma, \\ n_1 - n_2 &= 2\sigma = 1^\circ \cdot 0980330 \text{ per hour,} \end{aligned}$$

which again gives  $q = 369 \cdot 85$ , so that for both the K tides the period should be 370 days, corresponding to a period of  $369^d 0^h$  mean solar time.

In analysing for the N tide, it is required to find the period which will minimise the effect of the  $M_2$  tide.

$$\begin{aligned} \text{Here} \quad n_1 &= 2\gamma - 3\sigma + \varpi = 2 \times 14^\circ \cdot 2198648 \text{ per hour,} \\ n_2 &= 2\gamma - 2\sigma, \\ n_1 - n_2 &= -(\sigma - \varpi) = -0^\circ \cdot 5443747 \text{ per hour;} \end{aligned}$$

hence

$$0 \cdot 5443747 q = 14 \cdot 2198648 r;$$

and if  $r = 13$ ,  $q = 339 \cdot 58$ , so that the period should be 340 days, corresponding to a period of  $358^d 16^h$  mean solar time.

In analysing for the L tide, it is required to find the period which will minimise the effect of the  $M_2$  tide.

$$\begin{aligned} \text{Here} \quad n_1 &= 2\gamma - \sigma - \varpi = 2 \times 14^\circ \cdot 7642394 \text{ per hour,} \\ n_2 &= 2\gamma - 2\sigma, \\ n_1 - n_2 &= \sigma - \varpi = 0^\circ \cdot 5443747 \text{ per hour;} \end{aligned}$$

hence

$$0 \cdot 5443747 q = 14 \cdot 7642394 r;$$

and if  $r = 13$ ,  $q = 352 \cdot 58$ , so that the period should be 353 days, corresponding to a period of  $358^d 15^h$  mean solar time.

In analysing for the  $\nu$  tide, it is required to find the period which will minimise the effect of the  $M_2$  tide.

$$\begin{aligned} \text{Here} \quad n_1 &= 2\gamma - 3\sigma - \varpi + 2\eta = 2 \times 14^\circ \cdot 2562915 \text{ per hour,} \\ n_2 &= 2\gamma - 2\sigma, \\ n_1 - n_2 &= -\sigma - \varpi + 2\eta = -0^\circ \cdot 4715211 \text{ per hour;} \end{aligned}$$

hence

$$0 \cdot 4715211 q = 14 \cdot 2562915 r;$$

and if  $r = 11$ ,  $q = 332 \cdot 58$ , so that the period should be 333 days, corresponding to a period of  $350^d 9^h$  mean solar time.

In analysing for the  $\lambda$  tide, it is required to find the period which will minimise the effect of the  $M_2$  tide.

$$\begin{aligned} \text{Here} \quad n_1 &= 2\gamma - \sigma + \varpi - 2\eta = 2 \times 14^\circ \cdot 7278127 \text{ per hour,} \\ n_2 &= 2\gamma - 2\sigma, \\ n_1 - n_2 &= \sigma + \varpi - 2\eta = 0^\circ \cdot 4715211 \text{ per hour;} \end{aligned}$$

hence

$$0 \cdot 4715211 q = 14 \cdot 7278127 r;$$

and if  $r = 11$ ,  $q = 343 \cdot 58$ , so that the period should be 344 days, corresponding to a period of  $350^d 9^h$  mean solar time.

In analysing for the 2N tide, it is required to find the period which will minimise the effect of the  $M_2$  tide.

$$\text{Here} \quad n_1 = 2\gamma - 4\sigma + 2\omega = 2 \times 13^\circ.9476774 \text{ per hour,}$$

$$n_2 = 2\gamma - 2\sigma,$$

$$n_1 - n_2 = -2(\sigma - \omega) = -1^\circ.0887494 \text{ per hour;}$$

hence

$$1.0887494 q = 13.9476774 r;$$

and if  $r = 26$ ,  $q = 333.08$ , so that the period should be 333 days, corresponding to a period of  $358^d 3^h$  mean solar time.

In analysing for the T tide, it is required to find the period which will minimise the effect of the  $M_2$  tide.

$$\text{Here} \quad n_1 = 2\gamma - 3\eta = 2 \times 14^\circ.9794657 \text{ per hour,}$$

$$n_2 = 2\gamma - 2\sigma,$$

$$n_1 - n_2 = 2\sigma - 3\eta = 0^\circ.9748272 \text{ per hour;}$$

hence

$$0.9748272 q = 14.9794657 r;$$

and if  $r = 24$ ,  $q = 368.79$ , so that the period should be 369 days, corresponding to a period of  $369^d 12^h$  mean solar time.

In analysing for the R tide, it is required to find the period which will minimise the effect of the  $M_2$  tide.

$$\text{Here} \quad n_1 = 2\gamma - \eta = 2 \times 15^\circ.0205343 \text{ per hour,}$$

$$n_2 = 2\gamma - 2\sigma,$$

$$n_1 - n_2 = 2\sigma - \eta = 1^\circ.0569644 \text{ per hour;}$$

hence

$$1.0569644 q = 15.0205343 r;$$

and if  $r = 25$ ,  $q = 355.28$ ; or if  $r = 26$ ,  $q = 369.49$ , so that the period should be either 355 days or 369 days, corresponding to a period of  $354^d 12^h$ , or  $368^d 12^h$  mean solar time respectively.

In analysing for the  $\mu$  tide, it is required to find the period which will minimise the effect of the  $M_2$  tide.

$$\text{Here} \quad n_1 = 2\gamma - 4\sigma + 2\eta = 2 \times 13^\circ.9841042 \text{ per hour,}$$

$$n_2 = 2\gamma - 2\sigma,$$

$$n_1 - n_2 = -2(\sigma - \eta) = -1^\circ.0158958 \text{ per hour;}$$

hence

$$1.0158958 q = 13.9841042 r;$$

and if  $r = 24$ ,  $q = 330.37$ ; or if  $r = 25$ ,  $q = 344.13$ , so that the period should be either 330 days or 344 days, corresponding to a period of  $353^d 23^h$ , or  $369^d 0^h$  mean solar time respectively.

In analysing for the 2SM tide, it is required to find the period which will minimise the effect of the  $M_2$  tide.

$$\text{Here} \quad n_1 = 2\gamma + 2\sigma - 4\eta = 2 \times 15^\circ.5079479 \text{ per hour,}$$

$$n_2 = 2\gamma - 2\sigma,$$

$$n_1 - n_2 = 4(\sigma - \eta) = 2^\circ.0317916 \text{ per hour;}$$

hence

$$2.0317916 q = 15.5079479 r;$$

and if  $r = 48$ ,  $q = 366.37$ ; or if  $r = 49$ ,  $q = 374.00$ ; or if  $r = 50$ ,  $q = 381.63$ , so that the period should be 366 days, or 374 days, or 382 days, corresponding to a period of  $354^d 0^h$ ,  $361^d 18^h$ , or  $369^d 12^h$  mean solar time respectively.

In analysing for the O tide, it is required to find the period which will minimise the effect of the  $K_1$  tide.

$$\text{Here} \quad n_1 = \gamma - 2\sigma = 13^\circ.9430356 \text{ per hour,}$$

$$n_2 = \gamma,$$

$$n_1 - n_2 = -2\sigma = -1^\circ.0980330 \text{ per hour;}$$

$$\text{hence} \quad 1.0980330 q = 13.9430356 r;$$

and if  $r = 27$ ,  $q = 342.85$ , so that the period should be 343 days, corresponding to a period of  $369^d 0^h$  mean solar time.

In analysing for the P tide, it is open to question whether it is better to minimise the effect of the  $K_1$  tide or of the O tide.

In the case of the  $K_1$  tide,

$$n_1 = \gamma - 2\eta = 14^\circ.9589314 \text{ per hour,}$$

$$n_2 = \gamma,$$

$$n_1 - n_2 = -2\eta = -0^\circ.0821372 \text{ per hour;}$$

$$\text{hence} \quad 0.0821372 q = 14.9589314 r;$$

and if  $r = 2$ ,  $q = 364.24$ .

In the case of the O tide,

$$n_2 = \gamma - 2\sigma,$$

$$n_1 - n_2 = 2(\sigma - \eta) = 1^\circ.0158958 \text{ per hour;}$$

$$\text{hence} \quad 1.0158958 q = 14.9589314 r;$$

and if  $r = 25$ ,  $q = 368.12$ . It is better to abide by the last number, because in the former case  $n_1 - n_2$  varies slowly and by this means the adequate elimination of both O and  $K_1$  will be effected. The period should therefore be 368 days, corresponding to a period of  $369^d 0^h$  mean solar time.

In analysing for the J tide, the same remark applies in regard to the  $K_1$  tide or the O tide.

In the case of the  $K_1$  tide,  $\blacklozenge$

$$n_1 = \gamma + \sigma - \varpi = 15^\circ.5854433 \text{ per hour,}$$

$$n_2 = \gamma,$$

$$n_1 - n_2 = \sigma - \varpi = 0^\circ.5443747 \text{ per hour;}$$

$$\text{hence} \quad 0.5443747 q = 15.5854433 r;$$

and if  $r = 12$ ,  $q = 343.56$ ; or if  $r = 13$ ,  $q = 372.19$ .

In the case of the O tide,

$$n_2 = \gamma - 2\sigma,$$

$$n_1 - n_2 = 3\sigma - \varpi = 1^\circ.6424077 \text{ per hour;}$$

$$\text{hence} \quad 1.6424077 q = 15.5854433 r;$$

and if  $r = 36$ ,  $q = 341.62$ ; or if  $r = 39$ ,  $q = 370.09$ .

Since in the latter case, when the effect of the O tide is minimized,  $n_1 - n_2$  varies three times as fast as in the former when the  $K_1$  tide is employed, it will be better to take the period either 342 days or 370 days, corresponding to a period of  $329^d 4^h$ , or  $356^d 2^h$  mean solar time respectively.

In analysing for the Q tide the same remark applies in regard to the  $K_1$  tide or the O tide.

In the case of the  $K_1$  tide,

$$n_1 = \gamma - 3\sigma + \varpi = 13^\circ \cdot 3986609 \text{ per hour,}$$

$$n_2 = \gamma,$$

$$n_1 - n_2 = - (3\sigma - \varpi) = - 1^\circ \cdot 6424077 \text{ per hour;}$$

hence

$$1 \cdot 6424077 q = 13 \cdot 3986609 r;$$

and if  $r = 39$ ,  $q = 318 \cdot 16$ .

In the case of the O tide,

$$n_2 = \gamma - 2\sigma,$$

$$n_1 - n_2 = - (\sigma - \varpi) = - 0^\circ \cdot 5443747 \text{ per hour;}$$

hence

$$0 \cdot 5443747 q = 13 \cdot 3986609 r;$$

and if  $r = 13$ ,  $q = 319 \cdot 97$ . As before, it will be better to take the period 318 days, corresponding to a period of  $356^d 0^h$  mean solar time.

With regard to the quaterdiurnal and terdiurnal tides  $MS$ ,  $M_2N$ ,  $M_2K_1$  and  $2M_2K_1$  it does not matter what period is taken, but it seems reasonable to stop with the exact year of 365 mean solar days.

## 4.

### *Short-period Tides:—Augmenting Factors.*

Returning now to the general notation and considering the 24 mean values pertaining to the 24  $T$ -hours, it may be supposed that all the tides except the  $T$ -tide are adequately eliminated, and in fact, that this is the case will be found on reference to the *Report of the British Association for the Advancement of Science*, 1872, page 366, where the necessary corrections for the absence of complete elimination are given.

Now it is obvious that any one of the 24 values does not give the true height of the  $T$ -tide at that  $T$ -hour, but that it gives the average height of the water as due to the  $T$ -tide, estimated over half a  $T$ -hour before and after a  $T$ -hour. A correction must therefore be determined on this account.

The required expression for the height of the tide at any  $T$ -hour is

$$h = A_1 \cos \theta + B_1 \sin \theta + \&c. + A_r \cos r \theta + B_r \sin r \theta + \&c.$$

But the results of analysis gives instead of this, the mean of all the  $h$ 's between the limits  $\theta + \frac{\alpha}{2}$  and  $\theta - \frac{\alpha}{2}$  where  $\alpha = 15^\circ$ .

If then  $\Sigma$  represents the summation between these limits, it follows that,

$$\begin{aligned} h \alpha &= \Sigma h \\ &= \&c. + \Sigma A_r \cos r \theta + \Sigma B_r \sin r \theta + \&c. \\ &= \&c. + A_r \frac{2}{r} \sin \frac{r \alpha}{2} \cos r \theta + B_r \frac{2}{r} \sin \frac{r \alpha}{2} \sin r \theta + \&c., \end{aligned}$$



whence 
$$h = \&c. + \frac{\sin \frac{ra}{2}}{\frac{ra}{2}} A_r \cos r\theta + \frac{\sin \frac{ra}{2}}{\frac{ra}{2}} B_r \sin r\theta + \&c.,$$

consequently, the coefficients expressing that oscillation which goes through its period  $r$  times in 24  $T$ -hours must be augmented by the factor  $\frac{\frac{ra}{2}}{\sin \frac{ra}{2}}$  to give the true  $A_r$  and  $B_r$ .

Remembering that  $a$  is  $15^\circ$ , and putting 1, 2, 3, &c., in succession for  $r$ , the augmenting factors for the diurnal, semi-diurnal, terdiurnal oscillations &c., become

$$\frac{7.5 \pi}{180 \sin 7^\circ 30'}; \quad \frac{15 \pi}{180 \sin 15^\circ}; \quad \frac{22.5 \pi}{180 \sin 22^\circ 30'}; \quad \&c.$$

The augmenting factors are therefore as follows:—

for $A_1, B_1$	. . . . .	1.00286,
$A_2, B_2$	. . . . .	1.01152,
$A_3, B_3$	. . . . .	1.02617,
$A_4, B_4$	. . . . .	1.04720,
$A_6, B_6$	. . . . .	1.11072,
$A_8, B_8$	. . . . .	1.20920.

In the case of the S-series of tides, since the numbers treated are the actual heights of the water exactly at the  $S$ -hours, no augmenting factors are required.

## 5.

### *Short-period Tides:—Determination of the Constants.*

If now  $t$  denotes  $T$ -time expressed in hours and  $n$  is  $15^\circ$ , the height  $h$ , as expressed by the averaging process explained above, is given by the formula

$$h = A_0 + A_1 \cos nt + B_1 \sin nt + A_2 \cos 2nt + B_2 \sin 2nt + \&c.,$$

where  $t$  is 0, 1, 2 . . . 23.

Now  $\Sigma \cos rnt$ , from  $t = 0$  to  $t = 23$ , is equal to zero, since there are corresponding positive and negative values of the cosine: similarly  $\Sigma \sin rnt = 0$ .

Also  $\Sigma \frac{\cos^2}{\sin^2} rnt = \Sigma (\frac{1}{2} \pm \frac{1}{2} \cos 2rnt) = 12$ ,  $\Sigma \frac{\cos}{\sin} rnt \frac{\cos}{\sin} snt = \frac{1}{2} \Sigma \{ \cos(r-s)nt \pm \cos(r+s)nt \} = 0$ , and  $\Sigma \cos rnt \sin snt = \frac{1}{2} \Sigma \{ \sin(r+s)nt - (r-s)nt \} = 0$ , where  $r$  and  $s$  are any positive integers.

Therefore it follows that

$$A_0 = \frac{1}{24} \Sigma h; \quad A_1 = \frac{1}{12} \Sigma h \cos nt; \quad B_1 = \frac{1}{12} \Sigma h \sin nt; \quad A_2 = \frac{1}{12} \Sigma h \cos 2nt; \quad B_2 = \frac{1}{12} \Sigma h \sin 2nt;$$

and so on.

Also, since  $n = 15^\circ$ , and  $l$  is an integer, all the cosines and sines involved will be found among the following:  $-0; \pm \sin 15^\circ; \pm \sin 30^\circ; \pm \sin 45^\circ; \pm \sin 60^\circ; \pm \sin 75^\circ; \pm 1$ . These are denoted in the computation forms by  $0; \pm S_1; \pm S_2; \pm S_3; \pm S_4; \pm S_5; \pm 1$ . This enables the forms to be arranged neatly as given in the specimen of the reductions at the end of this chapter, where the 24 hourly values to be submitted to analysis are entered continuously in columns I and II. The subsequent operations are sufficiently indicated by the headings to the columns, and it will be found on examination that the results are in reality the sums of the several series given above.

The A's and B's are thus deduced, and then  $R = \sqrt{A^2 + B^2}$ : it must be multiplied by the augmenting factor, already evaluated, to obtain the augmented R which when multiplied by  $\frac{1}{F}$  gives H. Next the angle whose tangent is  $\frac{B}{A}$  gives  $\zeta$ , which must be added to the appropriate  $V_0 + u$  to find  $\kappa$ . The form used will be found in the specimen of the reductions: it also serves for the final treatment of the long-period tides, except that there is no augmenting factor, and that the increase of  $n$  for  $11\frac{1}{2}$  hours has to be added to  $\zeta$ .

## 6.

### *Long-period Tides:—Formation and Clearance of Daily Means.*

For the purpose of determining the tides of long-period, it is necessary to eliminate the oscillations of water level arising from the tides of short-period. As the quickest of the long-period tides has a period of many days, the height of the water at one instant for each day gives sufficient data. Thus there will, in a year's observations, be 365 heights to be submitted to harmonic analysis. In leap-year the last day's observation must be dropped, because the treatment is adapted for analysing 365 values.

In finding the value of the height of the water for each day, the algebraical mean of 24 consecutive hourly values, beginning with the height at noon, is taken: the result applies to the middle instant of the period  $0^h$  to  $23^h$ , that is to say, to  $11^h 30^m$  at night.

The formation of a daily mean does not obliterate the oscillations of the short-period tides, because none of the latter, excepting those of the principal solar series, have commensurable periods in mean solar hours.

A correction or 'clearance of the daily mean' has therefore to be applied for all important tides of short-period excepting for the solar series.

Let  $R \cos(nt - \zeta)$  be the expression for one of the tides of short-period, as evaluated by the harmonic analysis, and let  $\alpha$  be the value of  $nt - \zeta$  at any noon. Then the 24 consecutive hourly heights of the water due to this tide, beginning with that noon, are:—

$$R \cos \alpha, \quad R \cos(n + \alpha), \quad R \cos(2n + \alpha) \quad . \quad . \quad . \quad . \quad . \quad R \cos(23n + \alpha).$$

Now the sum of these 24 quantities is  $R \frac{\sin 12n}{\sin \frac{1}{2}n} \cos(\alpha + 11\frac{1}{2}n)$ , so that the 'clearance' is  $-\frac{1}{24} R \frac{\sin 12n}{\sin \frac{1}{2}n} \cos(\alpha + 11\frac{1}{2}n)$ , and is additive.

It has been found, practically, that only three tides of short period, *viz.*, M, N and O exercise any appreciable effect, so that clearances for them have to be applied. It was formerly the custom to compute the clearances for these three tides for every day of the year, as above, and to correct the daily

means accordingly: but in the present procedure, a single correction, for each of the three short-period tides, is applied to each of the final equations instead of to each daily mean. The process will be explained more fully below.

The late Professor J. C. Adams suggested an alternative plan in which the tide-predicting machine may be used for the evaluation of the sum of the clearances. It is evident that  $R \cos(a + 11\frac{1}{2}n)$  is the height of the tide  $n$  at 11<sup>h</sup> 30<sup>m</sup>, and the same is true for each such tide. Hence if the tide predictor is used to run off a year of fictitious tides with the semi-range of each tide equal to  $\frac{1}{24} \frac{\sin 12n}{\sin \frac{1}{2}n}$  of its true semi-range, and with all the solar series and the annual and semi-annual tides put at zero, the height given at each 11<sup>h</sup> 30<sup>m</sup> in the year is the sum for each day of all the clearances to be subtracted.

## 7.

### *Long-period Tides:—Final Equations.*

The 365 daily means are then taken and their mean value found. This is the mean height of the water for the year, and even if the daily means are uncorrected, the result cannot be sensibly vitiated.

The mean height is next subtracted from each of the daily means, leaving 365 quantities  $\delta h$ , the daily height of the water above the mean height. These quantities are to be the subject of harmonic analysis: and the tides chosen for evaluation are those which have been denoted above as Mm, Mf, MSf, Sa, Ssa.

$$\begin{aligned} \text{Let} \quad \delta h = & A \cos(\sigma - \varpi)t & + B \sin(\sigma - \varpi)t \\ & + C \cos 2\sigma t & + D \sin 2\sigma t \\ & + C' \cos 2(\sigma - \eta)t & + D' \sin 2(\sigma - \eta)t \\ & + E \cos \eta t & + F \sin \eta t \\ & + G \cos 2\eta t & + H \sin 2\eta t, \end{aligned}$$

where  $t$  is measured from the first 11<sup>h</sup> 30<sup>m</sup>.

Now if  $l_1, l_2$  are the increments in 24 mean solar hours of any two of the five arguments  $(\sigma - \varpi)t, 2\sigma t, 2(\sigma - \eta)t, \eta t, 2\eta t$ , and if  $A_1, B_1; A_2, B_2$ , are the corresponding coefficients of the cosine and sine in the expression for  $\delta h$ , and if  $\delta h_i$  be the value of  $\delta h$  at the  $(i + 1)^{\text{th}}$  11<sup>h</sup> 30<sup>m</sup> in the year, then

$$\delta h_i = A_1 \cos l_1 i + B_1 \sin l_1 i + A_2 \cos l_2 i + B_2 \sin l_2 i + \&c.$$

and therefore, if the terms in  $A_2$  and  $B_2$  alone be written,

$$\delta h_i \cos l_1 i = \frac{1}{2} A_2 \{ \cos(l_1 + l_2) i + \cos(l_1 - l_2) i \} + \frac{1}{2} B_2 \{ \sin(l_1 + l_2) i - \sin(l_1 - l_2) i \} + \&c.$$

$$\delta h_i \sin l_1 i = \frac{1}{2} A_2 \{ \sin(l_1 + l_2) i + \sin(l_1 - l_2) i \} + \frac{1}{2} B_2 \{ -\cos(l_1 + l_2) i + \cos(l_1 - l_2) i \} + \&c.$$

Now let 
$$\phi(x) = \frac{1}{2} \frac{\sin \frac{365}{2} x}{\sin \frac{1}{2} x},$$

so that 
$$\phi(l_1 \pm l_2) = \frac{1}{2} \frac{\sin \frac{365}{2} (l_1 \pm l_2)}{\sin \frac{1}{2} (l_1 \pm l_2)};$$

then, it is clear that  $\phi(x) = \phi(-x)$  and  $\phi(0) = 182.5$ .

If, therefore,  $\Sigma$  denote the summation for the 365 values from  $i = 0$  to  $i = 364$ , it follows that

$$\begin{aligned} \Sigma \delta h \cos l_1 i &= [\phi(l_1 + l_2) \cos 182(l_1 + l_2) + \phi(l_1 - l_2) \cos 182(l_1 - l_2)] A_2 \\ &+ [\phi(l_1 + l_2) \sin 182(l_1 + l_2) - \phi(l_1 - l_2) \sin 182(l_1 - l_2)] B_2 + \&c. \end{aligned}$$

$$\begin{aligned} \Sigma \delta h \sin l_1 i &= [\phi(l_1 + l_2) \sin 182(l_1 + l_2) + \phi(l_1 - l_2) \sin 182(l_1 - l_2)] A_2 \\ &+ [-\phi(l_1 + l_2) \cos 182(l_1 + l_2) + \phi(l_1 - l_2) \cos 182(l_1 - l_2)] B_2 + \&c. \end{aligned}$$

In these equations there is always one pair of terms in which  $l_2$  is identical with  $l_1$ , and since  $\phi(l_1 - l_1) = 182.5$  and as  $\cos 182(l_1 - l_1) = 1$ , it follows that there is one term in each equation, in which there is a coefficient nearly equal to 182.5. In the cosine series, it will be the coefficient of an A and in the sine series, of a B.

The following are the equations with the coefficients inserted, as computed from these formulæ, or their equivalents:—

*Final Equations for Tides of Long-period\*.*

	Co-efficient of A	Co-efficient of B	Co-efficient of C	Co-efficient of D	Co-efficient of C'	Co-efficient of D'	Co-efficient of E	Co-efficient of F	Co-efficient of G	Co-efficient of H
$\Sigma \delta h \times \cos(\sigma - \varpi)t =$	+183.05	+ 2.14	+ 0.72	+ 4.29	+ 0.76	+ 5.04	+ 4.88	- 0.34	+ 4.96	- 0.70
„ $\times \sin(\sigma - \varpi)t =$	+ 2.14	+181.95	- 4.15	+ 1.01	- 4.90	+ 1.06	+ 3.80	+ 0.34	+ 3.88	+ 0.68
„ $\times \cos 2\sigma t =$	+ 0.72	- 4.15	+183.17	+ 0.88	+ 0.56	+ 0.92	- 1.50	- 0.09	- 1.51	- 0.18
„ $\times \sin 2\sigma t =$	+ 4.29	+ 1.01	+ 0.88	+181.83	+ 0.92	- 0.80	+ 3.05	- 0.08	+ 3.06	- 0.17
„ $\times \cos 2(\sigma - \eta)t =$	+ 0.76	- 4.90	+ 0.56	+ 0.92	+183.19	+ 0.97	- 1.68	- 0.11	- 1.70	- 0.21
„ $\times \sin 2(\sigma - \eta)t =$	+ 5.04	+ 1.06	+ 0.92	- 0.80	+ 0.97	+181.81	+ 3.24	- 0.10	+ 3.25	- 0.20
„ $\times \cos \eta t =$	+ 4.88	+ 3.80	- 1.50	+ 3.05	- 1.68	+ 3.24	+182.38	+ 0.00	- 0.24	+ 0.01
„ $\times \sin \eta t =$	- 0.34	+ 0.34	- 0.09	- 0.08	- 0.11	- 0.10	+ 0.00	+182.62	+ 0.00	+ 0.00
„ $\times \cos 2\eta t =$	+ 4.96	+ 3.88	- 1.51	+ 3.06	- 1.70	+ 3.25	- 0.24	+ 0.00	+182.38	+ 0.00
„ $\times \sin 2\eta t =$	- 0.70	+ 0.68	- 0.18	- 0.17	- 0.21	- 0.20	+ 0.01	+ 0.00	+ 0.00	+182.62

If the daily means have been cleared by the use of the tide-predictor as above described, these ten equations are ready for solution, but if not, then before solution of the final equations, corrections for clearance must be applied to the left-hand sides.

## 8.

*Long-period Tides:—Evaluation of Clearances.*

Let  $n$  be the speed of short-period tide in degrees per mean solar hour, and let  $\psi(n) = \frac{1}{24} \frac{\sin 12n}{\sin \frac{1}{2}n}$ .

Then it has been already shown that the clearance to  $\delta h_i$ , the mean height of water at 11<sup>h</sup> 30<sup>m</sup> of the  $(i + 1)^{\text{th}}$  day, will be

$$- \psi(n) R \cos [n \{ 24i + 11\frac{1}{2} \} - \zeta].$$

\* The figures here given differ slightly from those given in the computation forms but the difference is immaterial.

If  $m$  is put equal to  $24n$  (so that  $m$  is the daily increase of the argument of the short-period tide) and  $\beta = n \times 11\frac{1}{2} - \zeta$ , this becomes

$$-\psi(n) R \cos(mi + \beta).$$

Hence the clearance for  $\delta h_i \cos li$  is

$$-\frac{1}{2}\psi(n) R \{ \cos[(m+l)i + \beta] + \cos[(m-l)i + \beta] \},$$

and for  $\delta h_i \sin li$  is

$$-\frac{1}{2}\psi(n) R \{ \sin[(m+l)i + \beta] - \sin[(m-l)i + \beta] \}.$$

Summing the series of 365 terms, the additive clearance for  $\Sigma \delta h_i \cos li$  becomes

$$-R\psi(n) \{ \phi(m+l) \cos[182(m+l) + \beta] + \phi(m-l) \cos[182(m-l) + \beta] \},$$

where as before

$$\phi(x) = \frac{1}{2} \frac{\sin \frac{365}{2} x}{\sin \frac{1}{2} x}.$$

If  $\Delta n$  denote the increment of the argument  $nt$  in  $182^d 11^h 30^m$ , this may now be written

$$-R\psi(n) \{ \phi(m+l) \cos[\Delta n + 182l - \zeta] + \phi(m-l) \cos[\Delta n - 182l - \zeta] \}.$$

If therefore  $R \cos \zeta = A$  and  $R \sin \zeta = B$ , so that  $A$  and  $B$  are the component semi-ranges of the tide  $n$  as immediately deduced from the harmonic analysis for the tides of short-period, the clearance to  $\Sigma \delta h_i \cos li$  becomes

$$\begin{aligned} & -[\psi(n) \phi(m+l) \cos(\Delta n + 182l) + \psi(n) \phi(m-l) \cos(\Delta n - 182l)] A \\ & -[\psi(n) \phi(m+l) \sin(\Delta n + 182l) + \psi(n) \phi(m-l) \sin(\Delta n - 182l)] B. \end{aligned}$$

In precisely the same manner the clearance for  $\Sigma \delta h_i \sin li$  is found to be

$$\begin{aligned} & -[\psi(n) \phi(m+l) \sin(\Delta n + 182l) - \psi(n) \phi(m-l) \sin(\Delta n - 182l)] A \\ & +[\psi(n) \phi(m+l) \cos(\Delta n + 182l) - \psi(n) \phi(m-l) \cos(\Delta n - 182l)] B. \end{aligned}$$

If then

$$K(n, l) = \phi(m+l) + \phi(m-l),$$

and

$$Z(n, l) = \phi(m+l) - \phi(m-l);$$

and if

$$C(n) = \psi(n) \cos \Delta n = \frac{1}{24} \frac{\sin 12n}{\sin \frac{1}{2} n} \cos \Delta n,$$

and

$$S(n) = \psi(n) \sin \Delta n;$$

and if the additive clearances for  $\Sigma \delta h_i \cos li$ , and  $\Sigma \delta h_i \sin li$ , be denoted respectively by

$$[A, n, l, \cos] A + [B, n, l, \cos] B,$$

and

$$[A, n, l, \sin] A + [B, n, l, \sin] B;$$

then

$$[A, n, l, \cos] = -C(n) K(n, l) \cos 182l + S(n) Z(n, l) \sin 182l,$$

$$[B, n, l, \cos] = -S(n) K(n, l) \cos 182l - C(n) Z(n, l) \sin 182l,$$

$$[A, n, l, \sin] = -S(n) Z(n, l) \cos 182l - C(n) K(n, l) \sin 182l,$$

$$[B, n, l, \sin] = +C(n) Z(n, l) \cos 182l - S(n) K(n, l) \sin 182l.$$

In the case when  $l$  refers to the tide MSf of speed  $2(\sigma - \eta)$ , and  $m$  to the tide  $M_2$  of speed  $2(\gamma - \sigma)$ ,  $\frac{1}{2}(m+l) = 360^\circ$ , and  $\phi(m+l) = 182.5$ .

The following schedule gives the value of these coefficients for the various tides :—

*Schedule of Coefficients for Clearance of Daily Means in the Final Equations\*.*

	Coefficient	$l = \sigma - \varpi$	$l = 2\sigma$	$l = 2(\sigma - \eta)$	$l = \eta$	$l = 2\eta$
$M_2$ $n = 2(\gamma - \sigma)$	[A, $n, l$ , cos]	- 0.05557	+ 0.00302	+ 5.7393	- 0.10410	- 0.10465
	[B, $n, l$ , cos]	- 0.17036	- 0.03773	- 2.9228	- 0.07525	- 0.07546
	[A, $n, l$ , sin]	- 0.17075	+ 0.04170	- 2.8400	- 0.00176	- 0.00353
	[B, $n, l$ , sin]	+ 0.04410	+ 0.01052	- 5.7271	+ 0.00476	+ 0.00958
$N$ $n = 2\gamma - 3\sigma + \varpi$	[A, $n, l$ , cos]	- 0.05884	+ 0.03680	+ 0.02938	- 0.01760	- 0.01760
	[B, $n, l$ , cos]	- 0.07758	- 0.22357	- 0.19384	+ 0.00254	+ 0.00254
	[A, $n, l$ , sin]	- 0.02059	- 0.15257	- 0.12210	+ 0.00020	+ 0.00041
	[B, $n, l$ , sin]	+ 0.11381	- 0.08544	- 0.08081	+ 0.00007	+ 0.00015
$O$ $n = \gamma - 2\sigma$	[A, $n, l$ , cos]	- 0.06485	+ 0.01662	+ 0.01571	- 0.19240	- 0.19340
	[B, $n, l$ , cos]	- 0.34765	- 0.07775	- 0.08158	- 0.18260	- 0.18311
	[A, $n, l$ , sin]	- 0.34523	+ 0.08411	+ 0.08754	- 0.00460	- 0.00926
	[B, $n, l$ , sin]	+ 0.04052	+ 0.03384	+ 0.03306	+ 0.00897	+ 0.01802

## 9.

### *Long-period Tides:—Solution of Equations.*

As the determination of each of the ten quantities  $\Sigma \delta h \cos(\sigma - \varpi)t$ ,  $\Sigma \delta h \sin(\sigma - \varpi)t$ , &c., by multiplying each of the 365  $\delta h$ 's by its proper cosine or sine and adding the results together, would be extremely laborious, the method of equivalent multipliers was devised by the late Professor Adams. The values of the respective cosines and sines are divided into eleven groups according as they fall nearest to 1.0, .9, .8 . . . . .2, .1, 0. Then as each of the values of  $\delta h$  is to be multiplied by some value of the cosine or sine, and as this value must fall into one of the groups, all the values of  $\delta h$  which belong to one of these groups are collected together, summed, and the sum multiplied by the corresponding value of the cosine or sine. Also since there are as many positive as negative values of the cosine or sine, the signs of half the  $\delta h$ 's must be changed. This is effected mechanically as follows:— in the spaces in the forms for the entry of  $\delta h$ 's those  $\delta h$ 's in which the signs are to be unchanged are entered on the left hand side of the space, if positive, and on the right, if negative. Thus in the column corresponding to each multiplier there are two sub-columns: these are separately summed, and the difference of these sums gives the total of the column for the  $\delta h$ 's whose signs are to be unchanged. This process is carried out in the upper half of the form and the result is called  $a$ . Exactly the same process is carried out in the lower half of the form with the  $\delta h$ 's in which the signs are to be changed,

\* The figures here differ slightly from those used in the computation forms but the difference is immaterial.

and the result is denoted by  $b$ . The complete sum of the  $\delta h$ 's is thus  $a - b$ , and the value of  $a - b$  in each column is multiplied by the multiplier corresponding to that column, the sum of the products giving the result required. A pair of forms, one for the cosine and the other for the sine series, is required for each long-period tide.

The ten equations are to be solved by successive approximation, the results being the component semi-amplitudes  $A$ ,  $B$ , &c., of the five long-period tides. But the initial instant of time is the first 11<sup>h</sup> 30<sup>m</sup> in the year, instead of the first noon: hence, if, as before,  $R^2 = A^2 + B^2$  and  $\tan \zeta_1 = \frac{B}{A}$ , then, in order to reduce the results to the normal form in which the noon of the first day is the initial instant of time, the increment of the corresponding argument for 11<sup>h</sup> 30<sup>m</sup> must be added to  $\zeta_1$ .

## 10.

### *Long-period Tides:—Breaks in the Record.*

It may happen from time to time, that the tide-gauge breaks down for a few days, from the stoppage of the clock, the choking of the tube, or some other accident, and that other readings are not taken during the interruption. In this case there will be a hiatus in the values of  $\delta h$ . Now the whole process employed depends on the existence of 365 continuous values of  $\delta h$ . Unless, therefore, the year's observations are to be sacrificed, this hiatus must be filled. If not more than three or four days' observations are wanting, it is best to plot out the values of  $\delta h$  graphically on each side of the hiatus and, filling in the gap with a curve drawn by hand, to use the values of  $\delta h$  given by the conjectural curve. The tide-table predictions are invariably utilised in this process when available.

If the gap is somewhat longer, several plans might be adopted, for example, if there is another station in the neighbourhood, the values of  $\delta h$  for that station might be inserted; or, the values of  $\delta h$  for another part of the year, in which the moon's and sun's declinations are as nearly as possible the same as they were during the gap, might be used, and, as a matter of fact, these methods have been employed.

When the hiatus is of considerable length, the preceding methods are inapplicable, and the method employed is as follows:—The actual  $\delta h$ 's are entered in their proper places and in the ten final equations all the terms with small coefficients are neglected, and in the terms whose coefficients are approximately 182·5, a coefficient equal to 182·5 diminished by half the number of days of the hiatus, is substituted: the computations are then carried out as if there was no gap, until the values of  $R$  and  $\zeta$  are obtained for each long-period tide. From these approximate values of  $R$  and  $\zeta$ , the height of each tide for each day of the gap is computed by the formula  $R \cos (nt - \zeta)$ , where  $t$  is the number of days since the commencement of the year of observation and  $n$  is the speed of the particular long-period tide in degrees per mean solar day. Thus five heights, above or below mean water level, are obtained for each day of the gap. These five heights are added together and the sum is the missing  $\delta h$  for the particular day. The gap having been thus filled in with computed  $\delta h$ 's, the whole computation is repeated with the completed series of  $\delta h$ 's.

When a break extends over two or three months in the first half of the working year, the observations antecedent to the break in that half-year are rejected, and the date of the working year put forward to the date following the end of the break: but if the break occurs in the second half of the working year, that year is considered to end at the commencement of the break and to begin 365 days before it; and the year following the break will begin at the end of the break.

FORMS FOR SHORT-PERIOD TIDES.  
BOMBAY—Commencing 0 hours, Astronomical Time, 1st January, 1885.

Motion per mean Solar hour = 15°.

SERIES S.

Argument (γ - η).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Daily Sum	Daily Mean
1	15.52	13.06	9.13	5.76	3.03	1.68	2.28	4.80	7.90	11.70	15.50	18.00	18.95	18.08	15.14	11.54	8.50	6.21	5.53	6.08	8.20	11.31	14.16	16.06	247.92	10.330
2	16.66	15.40	12.16	8.40	4.86	2.56	1.71	2.90	5.56	8.82	12.94	16.44	18.58	18.97	17.67	14.24	10.56	7.53	5.57	5.16	6.10	8.63	11.84	14.68	247.94	10.331
3	16.63	16.06	15.24	11.92	8.00	4.87	2.80	2.57	4.24	6.84	10.20	14.07	17.26	18.86	18.84	17.06	13.20	9.77	6.90	5.23	4.96	6.16	8.86	12.14	253.58	10.566
4	14.87	16.40	16.40	14.38	11.00	7.63	4.88	3.55	5.86	5.55	8.01	11.36	14.83	17.16	18.38	17.93	15.80	12.16	8.68	6.10	5.05	5.25	6.68	9.24	255.05	10.627
5	12.28	14.51	15.96	15.58	13.48	10.47	7.54	5.76	5.07	5.67	7.22	9.17	12.11	15.02	17.02	17.55	16.63	14.11	10.96	8.16	6.22	5.47	5.84	7.18	258.98	10.791
6	9.67	12.12	14.04	15.00	14.45	12.62	10.24	8.07	7.04	6.84	7.54	8.67	10.60	12.84	15.06	16.36	16.35	15.24	12.76	10.11	6.22	6.64	6.17	6.55	262.98	10.958
7	7.86	9.76	11.80	13.27	14.00	13.64	12.22	10.47	9.05	8.44	8.46	9.03	9.97	11.20	13.05	14.64	15.46	15.18	13.87	11.68	9.76	8.10	7.16	7.03	265.10	11.046
8	7.40	8.29	9.82	11.16	12.55	13.24	13.07	12.20	11.16	10.27	9.64	9.60	9.90	10.60	11.70	12.96	14.02	14.44	13.75	12.27	10.82	9.20	7.93	7.24	263.23	10.968
9	7.06	7.34	8.07	9.14	10.55	11.74	12.48	12.66	12.27	11.60	10.93	10.34	9.98	9.86	10.17	11.07	12.14	13.06	13.56	12.72	11.71	10.43	9.14	7.97	255.79	10.658
10	7.14	6.75	6.94	7.74	8.96	10.26	11.64	12.67	13.14	12.97	12.20	11.24	10.48	10.12	10.05	10.23	10.84	11.64	12.27	12.68	12.37	11.53	10.42	8.97	253.25	10.552
11	7.80	6.96	6.38	6.44	7.28	8.73	10.47	12.14	13.23	13.84	13.63	12.58	11.38	10.27	9.77	9.62	9.89	10.44	11.24	11.97	12.52	12.50	11.87	10.54	251.49	10.479
12	8.76	7.34	6.16	5.74	6.34	7.62	9.54	11.46	13.22	14.24	14.58	13.94	12.72	11.24	10.02	9.32	9.14	9.46	10.37	11.48	12.46	13.04	12.84	11.88	252.91	10.538
13	10.23	8.20	6.52	5.62	5.56	6.50	8.14	10.17	12.34	14.10	15.20	15.17	13.97	12.27	10.58	9.35	8.75	8.76	9.26	10.34	11.68	12.96	13.64	13.36	252.67	10.528
14	11.80	9.66	7.32	5.82	5.14	5.44	6.74	8.86	11.26	13.66	15.38	15.87	15.24	13.66	11.54	9.82	8.71	8.16	8.36	9.30	10.74	12.46	13.64	13.98	252.56	10.523
15	13.00	10.84	8.24	6.20	4.76	4.46	5.40	7.36	9.78	12.37	14.82	16.13	15.97	14.56	12.25	10.95	8.46	7.82	7.74	8.41	9.71	11.76	13.30	14.26	247.85	10.327
16	14.09	12.44	9.76	7.00	5.12	4.20	4.63	6.12	8.44	11.24	14.04	15.74	16.36	15.71	13.82	11.22	8.94	7.54	6.94	7.15	8.40	10.27	12.44	14.06	245.67	10.236
17	14.68	13.74	11.50	8.60	5.94	4.37	4.02	5.06	7.26	9.66	12.72	15.20	16.55	16.63	15.27	12.77	9.97	7.86	6.84	6.68	7.56	9.32	11.40	13.55	247.25	10.302
18	14.80	14.78	13.22	10.43	7.48	5.34	4.30	4.66	6.25	8.54	11.38	14.15	16.15	16.88	16.08	14.04	11.02	8.54	6.76	6.12	6.34	7.60	9.84	12.14	246.84	10.285
19	14.06	14.84	14.14	12.06	9.06	6.46	4.67	4.24	5.16	7.15	9.68	12.56	14.97	16.44	16.45	15.00	12.42	9.50	7.22	5.80	5.43	6.26	8.16	10.65	242.28	10.095
20	12.88	14.28	14.56	13.33	10.92	8.30	6.04	4.87	5.06	6.54	8.66	11.04	13.64	15.62	16.36	15.76	13.82	11.00	8.37	6.37	5.54	5.64	6.83	8.93	244.36	10.182
21	11.40	13.32	14.42	14.25	12.47	10.10	7.91	6.34	5.70	6.30	7.70	9.76	12.17	14.36	15.74	15.96	14.86	12.76	10.13	7.78	6.17	5.70	6.11	7.62	249.03	10.376
22	9.70	11.76	13.36	14.14	13.72	12.06	9.94	8.32	7.22	7.01	7.74	8.97	10.80	12.97	14.62	15.50	15.17	13.80	11.46	9.14	7.34	6.17	6.00	6.68	253.59	10.566
23	8.02	9.76	11.65	13.04	13.76	13.34	12.14	10.65	9.07	8.15	8.14	8.68	9.86	11.56	13.36	14.56	15.02	14.37	12.76	10.76	8.71	6.96	6.23	6.09	256.64	10.693
24	6.68	7.86	9.46	11.24	12.66	13.36	13.34	12.38	11.08	9.94	9.11	8.88	9.28	10.22	11.70	13.06	14.14	14.41	13.66	12.06	10.26	8.46	7.10	6.25	256.53	10.689
25	6.08	6.56	7.64	9.14	10.84	12.34	13.44	13.81	13.33	12.18	10.75	9.76	9.24	9.34	10.07	11.16	12.40	13.38	13.66	13.03	11.87	10.24	8.47	7.00	255.73	10.655
26	5.83	5.38	5.68	6.78	8.55	10.33	12.22	13.56	14.30	14.16	13.05	11.56	10.06	9.11	8.87	9.40	10.46	11.87	12.94	13.44	13.33	12.40	10.74	8.86	252.88	10.537
27	6.83	5.22	4.41	4.77	6.10	8.10	10.50	12.63	14.53	15.56	15.33	13.76	11.64	9.52	8.28	7.92	8.25	9.53	11.24	12.70	13.80	14.14	13.30	11.34	249.40	10.392
28	8.72	6.20	4.24	3.38	3.76	5.30	7.76	10.55	13.50	15.72	16.74	16.12	14.56	11.40	8.83	7.24	6.86	7.53	9.20	11.11	12.97	14.55	15.08	14.17	245.29	10.220
29	11.84	8.82	5.70	3.60	2.56	3.06	5.04	7.88	11.48	14.56	17.04	17.86	17.00	14.36	10.96	8.07	6.27	5.77	6.57	8.62	11.25	13.92	15.74	16.28	244.25	10.177
30	14.06	12.18	8.44	5.42	3.22	2.16	3.07	5.52	8.75	12.46	16.01	18.10	18.47	17.26	13.80	10.14	7.09	5.27	5.02	6.02	8.40	11.85	14.65	16.52	244.78	10.199
31	16.84	15.28	11.68	7.88	4.80	2.74	2.38	4.00	6.66	10.10	13.98	17.01	18.64	18.38	16.30	12.42	8.97	6.01	4.46	4.57	6.12	9.14	12.56	15.46	246.38	10.266
32	17.00	16.86	14.76	11.06	7.36	4.34	2.72	2.99	4.86	7.74	11.40	14.94	17.54	18.47	17.66	14.67	11.08	7.54	5.01	3.93	4.32	6.55	9.62	13.04	245.46	10.228
33	15.80	16.84	16.08	13.73	10.16	6.82	4.54	3.58	4.44	6.30	9.36	12.84	15.86	17.74	17.94	16.48	13.27	9.84	6.84	4.96	4.33	5.26	7.44	10.66	251.17	10.465
34	13.70	15.74	16.43	15.42	12.82	9.66	6.90	5.44	5.14	6.20	8.06	10.66	13.66	16.02	17.12	16.74	14.88	11.68	8.76	6.34	4.74	5.86	8.26	255.13	10.630	
35	11.07	13.60	15.16	15.34	14.06	11.68	9.04	7.34	6.56	6.94	8.04	9.56	11.76	14.24	15.60	16.04	15.34	13.02	10.16	7.86	6.27	5.54	5.86	7.18	257.26	10.719



36	9.07	11.36	13.26	14.34	14.26	12.88	11.00	9.39	8.26	7.92	8.30	9.05	10.36	12.08	13.76	14.66	14.44	13.11	11.12	9.39	7.54	6.26	6.13	6.68	254.53	10.605
37	7.86	9.28	10.86	12.27	13.10	12.94	11.93	10.66	9.72	9.12	9.06	9.26	9.66	10.60	11.82	12.86	13.34	12.82	11.45	10.03	8.74	7.48	6.86	6.78	248.50	10.354
38	7.17	7.94	9.05	10.30	11.34	11.97	11.92	11.42	10.84	10.34	10.07	9.97	9.77	9.94	10.44	11.32	12.06	12.26	11.78	10.88	9.87	8.84	7.86	7.24	244.59	10.191
39	6.94	7.18	8.03	9.07	10.14	11.00	11.56	11.85	11.77	11.46	11.12	10.57	10.07	9.70	9.70	10.13	10.80	11.27	11.45	11.25	10.76	9.97	9.00	8.00	242.79	10.116
40	7.11	6.58	6.74	7.44	8.51	9.84	10.90	11.76	12.34	12.55	12.30	11.60	10.57	9.76	9.34	9.17	9.56	10.24	10.94	11.36	11.44	10.97	10.10	9.07	240.19	10.008
41	7.87	6.85	6.30	6.50	7.26	8.50	10.16	11.44	12.65	13.26	13.32	12.56	11.36	10.08	9.16	8.67	8.64	9.01	9.76	10.58	11.25	11.66	11.34	10.36	238.54	9.939
42	8.82	7.36	6.12	5.54	5.82	6.94	8.54	10.36	12.06	13.46	13.97	13.64	12.30	10.76	9.26	8.14	7.84	8.12	8.96	10.24	11.52	12.40	12.66	12.07	236.90	9.871
43	10.47	8.56	6.64	5.46	5.70	5.93	7.55	9.56	11.72	13.53	14.67	14.84	13.98	12.14	10.00	8.54	7.66	7.53	8.16	9.56	11.03	12.66	13.62	13.60	234.61	10.109
44	13.30	10.24	7.77	5.88	4.84	4.96	6.33	8.27	10.66	13.07	14.85	15.64	15.33	13.68	12.26	9.64	7.54	6.79	7.00	8.13	9.87	11.85	13.00	14.38	242.99	10.125
45	13.88	11.93	9.10	6.54	4.66	4.00	4.90	6.86	9.20	11.97	14.34	15.82	15.96	14.78	12.26	9.64	7.46	6.24	5.96	6.74	8.48	10.85	13.07	14.56	239.20	9.967
46	14.85	13.63	10.90	7.86	5.57	4.07	4.04	5.46	7.84	10.63	13.64	15.83	16.64	16.01	13.87	10.90	8.00	6.17	5.46	5.63	7.26	9.70	12.25	14.42	240.74	10.931
47	15.50	15.15	13.08	9.90	6.94	4.75	3.92	4.66	6.62	6.62	7.84	10.68	15.00	11.93	9.02	7.54	6.66	6.24	5.96	6.74	8.48	10.85	13.07	14.56	239.20	9.967
48	15.12	15.66	14.46	11.76	8.44	5.86	4.26	4.25	5.52	7.84	10.68	13.68	15.84	16.68	15.86	13.15	10.22	7.36	6.65	5.06	5.54	7.84	10.54	13.30	241.46	10.061
49	14.06	15.54	15.51	13.57	10.53	7.47	5.38	4.52	5.04	6.70	9.14	12.16	14.74	16.26	16.26	14.64	11.74	8.68	6.28	4.46	4.54	5.07	7.06	9.74	238.79	9.950
50	12.44	14.55	15.46	14.76	12.57	9.68	7.24	5.84	5.60	6.54	8.40	10.77	13.32	15.42	16.26	15.47	13.18	10.24	7.54	5.62	4.54	4.69	5.80	7.87	243.80	10.158
51	10.40	12.80	14.50	15.06	14.03	11.86	9.36	7.58	6.64	6.76	7.86	9.66	11.66	13.73	15.08	15.32	14.12	11.86	9.24	6.90	5.18	4.58	5.06	6.46	245.64	10.335
52	8.24	10.33	12.41	13.86	14.34	13.44	11.46	9.53	8.05	7.40	7.66	8.58	9.92	11.68	13.36	14.16	14.12	12.82	10.83	8.73	6.87	5.45	4.92	5.44	243.60	10.150
53	6.63	8.23	10.14	11.77	12.96	13.40	12.76	11.56	10.24	9.04	8.45	8.28	8.67	9.76	11.20	12.50	13.18	13.06	11.88	10.25	8.57	6.98	5.77	5.38	240.66	10.028
54	5.64	6.37	7.82	9.54	11.17	12.38	13.02	12.96	12.16	11.07	10.02	8.94	8.44	8.48	9.27	10.44	11.57	12.34	12.34	11.70	10.50	8.90	7.32	5.96	238.35	9.931
55	5.24	5.12	5.86	7.17	8.90	10.63	12.10	13.16	13.56	13.13	11.86	10.27	8.88	8.08	7.87	8.42	9.56	10.87	11.93	12.44	12.26	11.27	9.76	7.96	236.30	9.846
56	6.27	5.06	4.55	5.02	6.47	8.52	10.67	12.72	14.14	14.86	14.44	12.70	10.66	8.86	7.60	7.21	7.64	9.18	11.00	12.40	13.36	13.52	12.60	10.86	240.25	10.010
57	8.63	6.40	4.63	4.06	4.70	6.46	8.84	11.30	13.80	15.56	16.25	15.33	12.96	10.26	7.95	6.54	6.18	7.03	8.83	11.00	12.96	14.40	14.74	13.76	242.57	10.107
58	11.70	8.84	6.08	4.95	3.42	4.14	6.18	8.80	12.06	14.93	16.76	17.15	15.84	12.87	9.66	7.00	5.18	5.12	6.26	8.52	11.16	13.67	15.38	15.86	240.63	10.026
59	14.57	11.93	8.26	5.48	3.42	2.92	4.14	6.52	9.58	13.16	16.04	17.62	17.34	15.27	11.66	8.27	5.56	4.16	4.32	5.84	8.66	11.92	14.74	16.46	237.84	9.910
60	16.54	14.66	11.26	7.66	4.94	3.20	3.27	4.70	7.52	10.86	14.63	17.06	17.98	16.96	13.90	10.20	6.96	4.47	3.56	4.02	6.04	9.40	12.86	15.55	238.20	9.925
61	16.86	16.36	13.86	10.44	6.92	4.54	3.37	3.90	5.80	8.56	12.33	15.44	17.27	17.45	15.46	12.03	8.50	5.70	3.74	3.27	4.33	7.10	10.34	13.76	247.28	9.887
62	15.97	16.76	15.76	12.96	9.44	6.74	4.67	4.23	5.26	7.43	10.37	13.82	16.13	17.08	16.40	13.86	10.50	7.26	4.84	3.56	3.86	5.60	8.27	11.55	242.32	10.097
63	14.34	16.02	16.28	14.66	11.66	8.60	6.46	5.26	5.46	6.56	8.86	11.44	14.36	15.97	16.18	14.88	12.00	8.86	6.28	4.57	4.06	4.86	6.67	9.40	243.69	10.154
64	12.24	14.39	15.64	15.33	13.25	10.46	8.22	6.76	6.34	7.00	8.36	10.22	12.44	14.42	15.27	14.71	12.72	10.14	7.72	5.93	4.86	5.00	6.10	8.03	245.55	10.231
65	10.30	12.47	13.97	14.58	13.92	12.03	10.14	8.54	7.56	7.56	8.42	9.82	11.34	12.96	14.04	14.24	13.22	11.36	9.36	7.56	6.27	5.84	6.34	7.46	249.30	10.388
66	9.00	10.76	12.44	13.56	13.74	12.74	11.40	10.07	9.16	8.96	9.27	9.77	10.46	11.36	12.44	13.07	13.03	12.12	10.46	8.86	7.68	7.02	7.66	8.66	252.05	10.502
67	8.54	9.66	10.96	12.24	12.88	12.88	12.24	11.43	10.66	10.24	10.16	10.24	10.47	10.86	11.44	12.02	12.40	12.24	11.36	10.18	8.87	7.97	7.67	7.94	255.55	10.648
68	8.50	9.00	9.78	10.74	11.76	12.46	12.67	12.27	11.74	11.26	10.87	10.56	10.36	10.22	10.36	10.76	11.26	11.56	11.38	10.86	9.96	9.14	8.40	7.98	253.85	10.577
69	7.80	7.86	8.34	9.30	10.46	11.44	12.08	12.36	12.27	12.03	11.50	10.78	10.20	9.73	9.58	9.87	10.35	10.80	11.10	11.10	10.78	10.32	9.72	8.86	248.72	10.363
70	7.97	7.28	7.26	7.87	8.97	10.32	11.56	12.46	13.04	13.10	12.54	11.68	10.56	9.64	9.08	8.82	9.16	9.88	10.74	11.40	11.75	11.70	11.14	10.07	247.99	10.333
71	8.84	7.56	6.74	6.70	7.63	8.94	10.62	12.06	13.26	13.78	13.68	12.86	11.34	9.88	8.86	8.16	8.03	8.46	9.64	10.86	12.06	12.78	12.56	11.57	246.87	10.286
72	9.92	8.17	6.67	5.98	6.16	7.20	8.87	10.76	12.70	14.08	14.61	14.06	12.53	10.68	8.96	7.55	6.88	7.05	8.07	9.84	11.76	12.97	13.54	13.03	242.04	10.085
73	11.46	9.42	7.27	5.74	5.30	5.90	7.44	9.66	11.92	14.02	15.17	15.16	13.87	11.66	9.44	7.56	6.34	6.07	6.86	8.68	10.80	12.96	14.26	14.55	241.51	10.083
74	13.37	11.16	8.45	6.26	5.16	5.12	6.24	8.10	10.63	13.22	15.15	15.86	15.17	13.22	10.40	7.86	6.06	5.25	5.54	6.90	9.14	11.72	13.95	15.20	239.23	9.968
Sum	814.09	807.47	768.68	713.90	656.10	612.63	601.16	628.55	691.30	776.04	866.90	936.49	975.00	976.40	939.65	873.58	794.64	719.55	662.98	634.76	641.91	681.53	734.50	786.21	18294.03	

FORMS FOR SHORT-PERIOD TIDES.  
 SERIES S.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Daily Sum	Daily Mean	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
75	15.12	13.30	10.64	7.57	5.44	4.44	4.96	6.46	8.94	11.85	14.34	16.00	16.06	14.53	11.64	8.54	5.76	4.22	3.97	5.24	7.30	10.10	13.02	15.04	234.57	9.774	
76	16.00	15.30	12.86	9.54	6.67	4.92	4.38	5.52	7.55	10.33	13.50	15.75	16.73	13.66	10.42	7.22	4.92	4.92	3.64	4.00	5.66	8.33	11.52	14.30	238.69	9.945	
77	16.06	16.52	15.06	12.13	8.73	6.13	4.66	4.99	6.52	8.92	11.86	14.66	16.40	16.56	15.07	11.90	8.47	5.62	3.74	3.22	4.26	6.60	9.60	12.85	240.53	10.022	
78	15.31	16.56	16.25	14.26	10.83	8.00	5.75	5.11	5.88	7.84	10.46	13.38	15.68	16.60	15.80	13.36	10.12	7.06	4.83	3.54	3.76	5.34	7.86	11.00	244.50	10.188	
79	13.93	15.92	16.74	15.74	13.36	10.24	7.64	6.12	6.08	7.14	9.00	11.56	13.90	15.66	15.98	14.76	13.06	8.90	6.13	4.34	3.62	4.36	6.06	8.47	247.71	10.321	
80	11.31	13.87	15.62	16.12	14.97	12.74	10.02	8.05	6.96	7.06	7.93	9.67	12.07	14.08	15.23	15.08	13.57	11.16	8.26	6.08	4.76	4.47	5.46	7.26	251.80	10.492	
81	9.48	11.88	13.90	15.36	15.50	14.66	12.67	10.54	8.74	7.94	8.14	9.06	10.62	12.40	13.77	14.54	14.20	12.80	10.64	8.47	6.76	5.86	5.82	6.49	260.22	10.843	
82	7.75	9.52	11.71	13.54	14.73	14.90	14.06	12.63	11.05	9.70	8.86	8.72	9.12	10.24	11.76	13.06	13.60	13.34	12.06	10.56	8.92	7.40	6.43	6.30	259.96	10.832	
83	6.68	7.68	9.46	11.24	13.02	14.08	14.52	14.22	13.04	11.70	10.34	9.24	8.84	9.04	9.84	10.96	12.05	12.86	12.96	12.44	11.22	9.67	8.30	7.06	260.46	10.853	
84	6.48	6.64	7.48	8.86	10.64	12.34	13.74	14.48	14.44	13.62	12.12	10.36	8.96	8.11	7.96	8.44	9.76	11.26	12.36	12.92	12.78	11.94	10.50	8.78	254.97	10.624	
85	7.20	6.06	5.92	6.72	8.34	10.26	12.20	13.86	15.00	15.14	14.16	12.20	9.88	8.00	6.90	6.56	7.46	9.22	11.16	12.56	13.57	14.06	13.37	11.72	251.52	10.480	
86	9.38	7.17	5.72	5.38	6.17	7.82	10.00	12.50	14.54	15.84	15.94	14.64	12.14	9.36	6.97	5.74	5.63	6.67	8.88	11.24	13.46	14.86	15.36	14.34	249.75	10.406	
87	12.05	9.44	6.93	5.38	5.00	5.82	7.83	10.50	13.30	15.60	16.72	16.28	14.37	11.37	8.36	6.00	4.67	4.80	6.40	9.20	12.06	14.62	16.12	16.16	248.98	10.374	
88	14.90	12.22	9.12	6.60	5.05	4.86	5.87	8.10	11.14	14.15	16.35	17.15	16.24	13.58	10.14	7.06	4.83	3.96	4.70	6.72	9.92	13.20	15.64	17.04	248.54	10.356	
89	16.75	14.92	11.81	8.56	6.27	5.14	5.64	6.94	9.43	12.61	15.44	17.03	17.08	15.36	11.92	8.64	6.18	4.48	4.25	5.24	7.57	11.00	14.10	16.43	251.79	10.533	
90	17.34	16.56	14.28	10.82	7.84	5.95	5.42	6.12	7.87	10.62	13.66	16.10	17.14	16.46	13.96	10.44	7.12	4.80	3.83	4.41	6.45	8.78	12.04	14.74	252.73	10.530	
91	16.66	17.13	15.64	12.86	9.53	7.16	5.81	5.93	7.22	9.26	12.02	14.66	16.44	16.67	15.06	12.02	8.56	5.84	4.04	3.84	4.93	7.24	10.09	13.23	251.83	10.493	
92	15.56	16.90	16.56	14.74	11.68	8.84	7.02	6.48	7.04	8.26	10.50	13.00	14.94	15.83	15.12	12.94	9.87	7.14	5.16	4.22	4.76	6.40	8.73	11.37	253.06	10.544	
93	14.00	15.82	16.34	15.34	13.10	10.40	8.36	7.32	7.28	8.03	9.50	11.53	13.48	14.74	14.92	13.67	11.34	8.76	6.67	5.40	5.22	6.16	7.85	9.97	255.20	10.633	
94	12.30	14.30	15.48	15.46	14.27	12.24	10.20	8.78	8.26	8.47	9.24	10.52	12.04	13.48	14.16	13.84	12.27	10.16	8.14	6.47	5.74	6.22	7.44	9.20	258.68	10.778	
95	10.85	12.64	14.05	14.67	14.27	12.97	11.44	10.04	9.16	8.84	9.16	9.84	10.95	11.96	12.80	12.96	12.28	10.94	9.24	7.80	6.78	6.70	7.30	8.37	256.01	10.667	
96	9.54	10.90	12.34	13.52	13.80	13.26	12.13	10.96	10.04	9.60	9.33	9.54	9.90	10.56	11.44	11.92	12.05	11.54	10.36	9.16	8.12	7.47	7.44	7.87	252.79	10.533	
97	8.52	9.46	10.73	11.93	12.74	12.98	12.60	11.86	11.07	10.34	9.94	9.77	9.87	10.02	10.36	10.81	11.14	11.27	10.92	10.30	9.34	8.36	7.74	7.58	249.65	10.402	
98	7.98	8.76	9.87	11.04	11.96	12.50	12.66	12.42	11.96	11.34	10.55	9.91	9.47	9.34	9.52	9.94	10.53	10.94	11.12	11.02	10.62	10.00	9.22	8.40	251.07	10.461	
99	8.01	8.13	8.63	9.76	10.66	11.77	12.66	13.06	12.40	11.47	10.50	9.62	8.94	8.94	8.54	8.74	9.48	10.45	11.36	11.88	11.80	11.44	11.00	9.40	252.17	10.507	
100	8.46	7.84	7.76	8.47	9.46	10.86	12.30	13.36	13.82	13.66	12.66	11.42	10.02	8.72	7.96	7.82	8.36	9.47	10.86	11.90	12.70	12.87	12.44	11.06	254.21	10.592	
101	9.52	8.12	7.40	7.47	8.26	9.54	11.08	12.70	14.06	14.56	14.22	12.80	10.96	8.88	7.46	6.81	6.84	7.92	9.62	11.52	13.00	13.97	14.12	13.00	253.83	10.576	
102	11.02	9.95	7.48	6.74	6.92	7.97	9.72	11.72	13.58	14.86	15.12	14.21	12.35	9.67	7.47	5.98	5.58	6.14	7.76	9.84	12.16	14.02	15.18	15.06	249.60	10.400	
103	13.40	10.95	8.28	6.66	6.02	6.46	7.88	10.06	12.53	14.55	15.72	15.49	13.80	11.08	8.22	5.93	4.52	4.32	5.47	7.72	10.54	13.27	15.36	16.20	244.43	10.185	
104	15.32	13.00	9.88	7.34	5.76	5.40	6.24	8.22	10.70	13.40	15.52	16.25	15.36	12.80	9.46	6.56	4.47	3.42	3.91	5.74	8.31	11.40	14.40	16.28	239.14	9.964	
105	16.72	15.47	12.68	9.44	6.81	5.47	5.38	6.52	8.91	11.80	14.40	15.97	16.08	14.35	11.30	7.80	4.97	2.93	2.46	3.76	6.21	9.51	12.97	15.58	237.49	9.895	
106	17.14	17.04	14.94	11.68	8.36	6.14	5.06	5.57	7.24	10.07	13.10	15.40	16.44	15.82	13.44	9.74	6.67	4.03	2.50	2.77	4.44	7.50	10.96	14.33	240.38	10.016	
107	16.70	17.72	16.91	14.37	10.87	8.10	6.15	5.71	6.50	8.36	11.33	14.12	13.97	16.50	15.10	12.22	8.67	5.24	3.17	2.56	3.47	5.74	8.64	12.02	246.14	10.256	
108	15.12	16.94	17.54	16.24	13.40	7.62	6.17	6.07	6.07	7.04	9.13	12.00	14.47	15.69	15.54	13.66	10.74	7.44	4.88	3.28	3.04	4.36	6.67	9.40	246.76	10.282	
109	13.47	15.06	16.74	16.94	15.60	13.03	10.01	7.87	6.76	6.80	7.71	9.70	12.14	14.15	15.02	14.50	12.53	9.92	7.24	5.36	4.17	4.16	5.20	7.26	250.28	10.428	

110	9.89	12.40	14.57	15.77	15.74	14.47	12.12	9.90	8.07	7.14	7.11	7.83	9.54	11.58	13.16	13.74	13.28	11.76	9.56	7.60	5.96	4.93	5.02	5.86	247.00	10.292
111	7.52	9.74	12.00	13.87	14.87	14.77	13.76	12.06	10.26	8.74	7.82	7.54	8.00	9.34	11.00	12.36	12.96	12.72	11.58	10.14	8.48	6.94	6.06	5.96	248.49	10.354
112	6.60	7.87	9.72	11.62	13.34	14.34	14.44	13.66	12.26	10.62	9.10	8.03	7.66	7.76	8.68	10.20	11.63	12.43	12.66	12.10	10.96	9.47	8.14	7.03	250.32	10.430
113	6.54	6.88	7.94	9.57	11.42	13.00	14.07	14.44	13.93	12.76	11.00	9.18	7.74	6.96	6.96	7.85	9.40	10.96	12.36	13.06	13.12	12.22	10.65	8.87	250.88	10.453
114	7.52	6.74	6.84	7.66	9.26	11.04	12.88	14.12	14.66	14.30	12.64	10.64	8.60	6.78	5.94	5.93	7.08	9.00	11.04	12.64	13.72	13.87	12.97	11.36	247.23	10.301
115	9.32	7.66	6.62	6.47	7.28	8.88	10.96	12.96	14.54	15.17	14.54	12.77	10.22	7.74	5.76	4.88	5.14	6.58	8.88	11.33	13.36	14.66	14.94	13.86	244.52	10.188
116	11.70	9.34	7.26	6.22	6.20	7.24	9.00	11.22	13.36	14.86	15.37	14.44	12.10	9.16	6.48	4.70	4.20	4.74	6.70	9.17	11.77	14.02	15.57	15.54	240.36	10.015
117	14.03	11.54	8.80	6.96	6.07	6.34	7.48	9.44	11.96	14.10	15.48	15.44	13.84	10.92	7.66	5.31	3.77	3.70	5.12	7.30	10.10	12.94	15.14	16.26	239.70	9.988
118	15.76	13.86	11.00	8.24	6.47	5.97	6.54	7.98	10.16	12.70	14.64	15.66	14.96	12.70	9.46	6.57	4.32	3.42	4.04	5.80	8.48	11.42	14.32	16.17	240.64	10.027
119	16.57	15.46	12.94	10.06	7.64	6.36	6.16	6.82	8.40	10.90	13.45	15.07	15.35	15.81	11.00	7.70	5.15	3.44	3.36	4.67	6.96	9.52	12.56	14.92	238.27	9.928
120	16.36	16.28	14.70	11.93	9.06	7.20	6.40	6.70	7.74	9.37	11.47	13.86	15.04	15.06	12.96	9.73	7.17	4.24	3.42	4.04	5.68	8.27	10.68	13.46	240.82	10.034
121	15.48	16.25	15.62	13.50	10.52	8.22	6.72	6.40	7.02	8.34	10.44	12.60	14.08	14.45	13.26	10.82	7.87	5.57	3.94	3.86	4.88	6.80	9.18	11.76	237.58	9.899
122	14.24	15.56	15.54	14.30	11.86	9.46	7.76	6.94	7.06	7.86	9.36	11.24	13.06	13.96	13.66	11.90	9.20	6.72	5.07	4.36	4.90	6.32	8.22	10.36	238.91	9.953
123	12.80	14.56	15.43	14.76	13.04	10.84	8.96	7.76	7.44	7.76	8.80	10.26	11.94	13.06	13.30	12.28	10.40	8.28	6.46	5.35	5.20	6.00	7.54	9.26	241.48	10.062
124	11.42	13.34	14.60	14.86	13.86	12.06	10.14	8.84	8.15	8.06	8.40	9.36	10.62	11.94	12.68	12.46	11.36	9.58	7.94	6.74	6.04	6.20	7.12	8.46	244.23	10.176
125	10.24	12.10	13.38	14.08	13.92	12.90	11.41	10.00	8.90	8.46	8.56	9.00	9.74	10.55	11.36	11.86	11.68	10.72	9.26	7.86	6.96	6.92	7.44	8.22	245.52	10.230
126	9.26	10.47	12.10	13.34	13.78	13.40	12.16	10.87	9.94	9.24	8.96	8.94	9.17	9.58	10.34	10.96	11.44	11.34	10.58	9.56	8.46	7.76	7.66	7.97	247.28	10.303
127	8.66	9.74	10.97	12.22	13.24	13.54	13.24	12.12	10.96	9.98	9.27	8.94	8.74	8.80	9.24	10.03	10.80	11.26	11.29	10.79	10.06	9.26	8.46	8.06	249.67	10.403
128	8.04	8.56	9.72	10.94	12.20	12.96	13.22	12.94	12.14	11.17	9.96	8.96	8.20	7.92	8.00	8.62	9.56	10.46	11.34	11.77	11.44	10.76	9.74	8.78	247.40	10.308
129	8.17	8.10	8.66	9.60	10.93	12.30	13.21	13.50	13.18	12.36	11.16	9.68	8.30	7.26	6.90	7.45	8.52	10.00	11.40	12.36	12.92	12.66	11.62	10.20	250.44	10.435
130	8.85	8.06	7.83	8.24	9.37	10.96	12.50	13.57	14.02	13.54	12.37	10.74	8.97	7.34	6.24	5.98	6.71	8.26	10.20	12.12	13.50	14.22	13.67	12.20	249.46	10.394
131	10.16	8.55	7.53	7.27	7.93	9.36	11.30	13.16	14.26	14.66	13.94	12.24	9.97	7.60	5.85	4.92	5.06	6.42	8.60	10.95	13.28	14.84	15.34	14.46	247.65	10.319
132	12.38	10.01	8.14	6.95	6.90	8.01	9.74	11.84	13.66	14.84	15.16	14.10	11.76	8.83	6.14	4.18	3.66	4.53	6.46	9.08	11.92	14.30	15.96	16.28	244.83	10.201
133	14.95	12.41	9.36	7.14	6.17	6.50	7.92	10.02	12.44	14.46	15.64	15.47	13.76	10.66	7.20	4.46	2.86	2.74	4.17	6.63	9.77	13.00	15.72	17.16	240.61	10.025
134	16.96	15.18	11.90	8.78	6.57	5.95	6.52	7.94	10.30	12.84	15.02	15.97	15.24	12.56	8.86	5.70	3.17	1.97	2.43	4.23	7.22	10.62	13.96	16.50	236.39	9.850
135	17.69	17.06	14.58	10.90	8.02	5.94	5.46	6.30	8.25	10.90	13.74	15.64	16.06	14.62	11.54	7.86	4.52	2.14	1.42	2.56	5.03	8.20	11.45	14.68	234.56	9.773
136	16.97	17.83	16.77	14.06	10.36	7.60	5.84	5.52	6.20	8.20	11.20	14.02	15.72	15.74	13.76	10.48	6.92	4.07	2.24	1.86	3.24	5.60	8.58	12.24	235.02	9.793
137	15.14	17.16	17.74	16.33	13.21	10.00	7.30	5.76	5.60	6.58	8.80	11.97	14.34	15.47	15.07	12.82	9.66	6.36	4.08	2.67	2.88	4.46	6.78	9.71	240.09	10.004
138	12.92	15.50	17.10	17.16	15.40	12.67	9.57	7.36	6.16	6.11	7.20	9.40	12.06	14.14	14.98	14.36	12.18	9.28	6.58	4.76	3.86	4.30	5.66	7.78	246.49	10.270
139	10.44	13.15	15.36	16.54	16.23	14.86	11.94	9.56	7.54	6.48	6.38	7.36	9.30	11.76	13.38	13.98	13.42	11.66	9.36	7.30	5.74	4.98	5.26	6.33	248.31	10.346
140	8.08	10.42	12.87	14.66	15.72	15.46	14.00	11.78	9.46	7.72	6.96	6.82	7.44	8.91	10.74	12.30	13.13	12.92	11.76	10.08	8.18	6.84	6.28	6.46	248.99	10.375
141	7.26	8.54	10.38	12.48	14.22	14.94	14.74	13.52	11.62	9.46	7.84	6.86	6.52	6.83	8.02	9.54	11.12	12.28	12.53	12.07	10.86	9.35	7.86	6.87	245.71	10.238
142	6.74	7.36	8.54	10.16	11.86	13.27	14.14	13.98	12.92	11.14	9.14	7.48	6.36	5.86	5.93	7.12	8.94	10.74	12.22	12.86	12.65	11.60	10.06	8.56	239.63	9.985
143	7.47	7.24	7.70	8.44	10.00	11.62	13.06	13.93	13.82	12.68	10.82	9.01	7.20	5.72	5.17	5.56	6.97	8.92	10.90	12.46	13.44	13.42	12.46	10.72	238.73	9.947
144	9.12	8.02	7.47	7.63	8.26	9.76	11.56	13.14	14.05	13.96	12.62	10.76	8.52	6.66	5.32	4.84	5.46	7.38	9.67	11.66	13.40	14.34	14.36	13.24	241.20	10.050
145	11.36	9.64	8.16	7.52	7.50	8.44	10.16	11.93	13.46	14.20	13.97	12.62	10.50	7.84	5.72	4.46	4.54	5.90	7.82	10.17	12.67	14.36	15.22	14.76	242.92	10.122
146	13.34	11.12	9.16	7.84	7.36	7.72	8.72	10.32	12.06	13.66	14.36	13.76	11.92	9.27	6.82	4.82	3.97	4.57	6.16	8.40	11.03	13.46	15.10	15.52	240.46	10.019
147	14.67	12.94	10.67	8.77	7.60	7.38	7.93	9.10	10.86	12.73	14.28	14.53	13.00	10.66	7.86	5.58	4.22	4.13	5.24	7.24	9.70	12.30	14.40	15.74	241.53	10.064
148	15.70	14.12	12.14	9.74	8.36	7.64	7.54	8.20	9.70	11.80	13.62	14.54	14.16	12.22	9.68	6.84	4.84	3.94	4.50	6.00	8.33	10.94	13.60	15.42	243.57	10.149
Sum	885.27	889.48	864.56	818.97	767.77	731.08	714.25	726.49	762.13	811.55	860.03	891.16	889.23	848.64	777.93	694.49	619.85	569.27	555.03	578.32	633.64	709.45	788.20	850.54	18237.33	

FORMS FOR SHORT-PERIOD TIDES.  
 SERIES S.—(Continued).

Day	0 <sup>a</sup>	1 <sup>b</sup>	2 <sup>b</sup>	3 <sup>b</sup>	4 <sup>b</sup>	5 <sup>b</sup>	6 <sup>b</sup>	7 <sup>b</sup>	8 <sup>b</sup>	9 <sup>b</sup>	10 <sup>b</sup>	11 <sup>b</sup>	12 <sup>b</sup>	13 <sup>b</sup>	14 <sup>b</sup>	15 <sup>b</sup>	16 <sup>b</sup>	17 <sup>b</sup>	18 <sup>b</sup>	19 <sup>b</sup>	20 <sup>b</sup>	21 <sup>b</sup>	22 <sup>b</sup>	23 <sup>b</sup>	Daily Sum	Daily Mean	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
140	16.13	15.62	13.90	11.47	9.28	7.84	7.40	7.74	8.92	10.62	12.60	14.02	14.27	13.22	10.78	8.10	5.76	4.27	4.17	5.26	7.20	9.70	12.28	14.66	245.21	10.217	
150	15.94	16.04	14.86	12.64	10.27	8.44	7.54	7.34	8.10	9.52	11.55	13.36	14.27	13.92	12.06	9.48	6.90	5.12	4.32	4.97	6.54	8.70	11.00	13.46	246.34	10.264	
151	15.32	16.07	15.67	14.17	11.77	9.56	8.16	7.68	7.83	8.74	10.50	12.26	13.66	14.02	12.96	10.86	8.34	6.24	5.04	4.82	5.84	7.60	9.46	11.87	248.44	10.332	
152	14.10	15.30	15.60	14.66	12.78	10.74	9.03	7.96	7.73	8.24	9.44	11.07	12.62	13.44	13.16	11.96	9.94	7.67	6.16	5.18	5.56	6.86	8.64	10.66	248.50	10.354	
153	12.74	14.30	15.12	15.06	13.65	11.84	10.00	8.46	7.75	7.78	8.46	9.92	11.36	12.37	12.84	12.22	10.98	9.18	7.32	6.03	5.94	6.87	8.17	9.67	248.03	10.335	
154	11.58	13.28	14.64	14.97	14.22	12.62	11.08	9.47	8.38	8.08	8.30	9.20	10.24	11.40	12.12	12.46	11.72	10.38	8.77	7.37	6.70	6.93	7.78	8.83	250.52	10.438	
155	10.30	11.90	13.54	14.68	14.80	13.77	12.16	10.50	9.20	8.47	8.28	8.60	9.36	10.36	11.26	11.83	12.05	11.56	10.60	9.20	8.14	7.72	7.83	8.62	254.73	10.614	
156	9.82	11.10	13.64	13.94	14.46	14.16	13.26	11.74	10.42	9.26	8.54	8.34	8.46	9.23	10.10	10.93	11.70	11.97	11.72	11.06	9.98	8.86	8.32	8.36	258.37	10.765	
157	9.00	10.04	11.54	12.92	13.86	14.25	13.85	12.88	11.48	10.08	8.98	8.20	8.20	8.37	9.12	10.03	11.29	12.14	12.58	12.36	11.84	11.02	10.06	9.23	263.32	10.972	
158	8.78	9.20	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	10.03	8.74	7.92	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	269.32	11.222	
159	9.66	9.64	10.17	11.38	12.77	13.98	14.67	15.14	14.88	13.86	12.46	10.48	8.82	7.82	7.50	8.19	9.46	11.28	13.22	14.76	15.82	15.76	14.97	13.34	290.03	12.085	
160	11.70	10.67	10.27	10.56	11.52	12.90	14.12	15.30	15.65	15.48	14.17	12.02	9.86	8.00	7.09	6.85	7.72	9.34	11.40	13.77	15.84	16.86	16.85	15.70	293.64	12.235	
161	13.66	11.52	9.95	9.55	9.80	10.84	12.57	14.21	15.47	16.06	15.22	13.50	10.84	8.22	6.16	4.95	5.15	6.50	8.61	11.37	14.18	16.48	17.54	17.17	279.46	11.644	
162	15.66	12.50	10.97	8.34	8.17	8.96	10.27	12.23	14.24	15.74	16.29	15.33	12.77	9.46	6.32	4.44	3.62	4.30	6.30	8.54	11.95	15.02	17.28	17.95	265.69	11.070	
163	17.20	15.02	11.76	9.04	7.44	7.22	7.81	9.55	12.08	14.54	16.07	16.21	14.76	11.87	8.16	5.07	3.07	2.74	3.80	5.94	9.24	12.80	15.92	18.07	255.38	10.641	
164	18.53	17.65	14.65	10.90	8.00	6.62	6.55	7.50	9.65	12.45	14.89	16.40	16.14	14.28	10.90	7.10	4.31	2.62	2.37	3.68	6.30	9.76	13.48	16.44	251.17	10.465	
165	18.12	18.40	17.00	13.80	10.17	7.55	6.20	6.18	7.30	9.60	12.79	15.16	16.42	15.96	13.80	10.33	6.77	4.00	2.33	2.54	4.18	7.11	10.40	13.95	250.06	10.419	
166	16.74	17.85	17.95	16.07	12.81	9.60	7.05	5.72	5.77	7.00	9.56	12.80	15.12	16.05	15.26	12.76	9.20	6.14	3.95	2.88	3.47	5.52	7.93	11.04	248.24	10.343	
167	14.21	16.44	17.72	17.40	15.44	12.07	9.02	6.70	5.67	5.93	7.41	10.97	13.02	14.92	15.57	14.68	12.28	9.20	6.52	4.77	4.20	4.94	6.52	8.80	253.50	10.563	
168	11.67	14.34	16.42	17.20	16.60	14.54	11.30	8.66	6.74	6.05	6.16	7.65	10.05	12.50	14.32	14.85	14.05	11.96	9.47	7.26	6.66	5.80	6.39	7.66	257.70	10.738	
169	9.64	11.92	14.25	15.90	16.46	15.74	13.76	10.84	8.61	6.86	6.32	6.58	7.80	9.82	12.04	13.55	14.17	13.54	12.03	10.34	8.60	7.57	7.26	7.62	261.22	10.884	
170	8.41	9.92	12.12	14.20	15.46	15.54	14.58	12.66	10.40	8.31	7.04	6.60	6.77	7.78	9.32	11.22	12.80	13.58	13.46	12.40	10.90	9.62	8.66	8.31	260.09	10.837	
171	8.49	9.03	10.30	12.04	13.70	14.74	14.75	13.73	12.02	10.10	8.46	7.12	6.53	6.70	7.50	9.03	10.90	12.32	13.20	13.38	12.91	11.94	10.67	9.60	259.17	10.799	
172	8.94	8.82	9.24	10.33	11.90	13.24	14.06	14.10	13.34	11.84	10.05	8.26	6.94	6.44	6.67	7.49	9.06	10.86	12.50	13.66	14.10	13.63	12.46	11.06	258.99	10.791	
173	10.06	9.30	9.95	9.33	10.22	11.60	12.90	13.82	13.85	13.08	11.64	9.76	8.00	6.70	6.08	6.22	7.28	9.00	10.54	12.77	14.05	14.63	14.17	12.86	257.31	10.721	
174	11.33	10.04	9.14	8.86	9.20	10.08	11.26	12.44	13.30	13.52	12.80	11.00	8.85	7.06	5.67	5.05	5.60	7.15	9.26	11.30	13.28	14.45	14.84	13.95	249.43	10.393	
175	12.40	10.90	9.46	8.62	8.24	8.56	9.64	11.12	12.55	13.40	13.37	12.07	10.07	8.20	6.17	4.94	4.74	5.62	7.74	9.76	12.14	14.01	15.00	14.86	243.58	10.149	
176	13.77	12.06	10.27	8.84	8.10	7.94	8.52	9.68	11.18	12.64	13.37	13.05	11.52	9.17	6.76	5.11	4.16	4.64	6.10	8.00	10.50	12.90	14.56	15.33	238.17	9.924	
177	14.70	13.32	11.14	9.44	8.17	7.54	7.57	8.34	9.81	11.65	13.20	13.60	12.56	10.40	7.97	5.83	4.38	4.04	4.96	6.82	9.02	11.57	13.86	15.24	235.13	9.797	
178	15.44	14.56	12.56	10.36	8.63	7.62	7.30	7.74	8.86	10.67	12.47	13.67	13.60	12.02	9.66	6.93	4.96	3.94	4.22	5.70	7.84	10.40	12.82	14.74	236.71	9.863	
179	15.56	15.33	13.80	11.44	9.35	7.79	7.04	7.03	7.90	9.44	11.66	13.22	13.92	13.00	10.74	8.00	5.64	4.04	3.83	4.76	6.70	9.02	11.37	13.67	234.25	9.760	
180	15.12	15.46	14.48	12.44	9.96	8.16	6.86	6.42	6.94	8.42	10.44	12.57	13.67	13.68	12.22	9.64	6.86	4.96	3.98	4.36	5.65	7.72	10.02	12.26	232.29	9.679	
181	14.31	15.28	15.12	13.77	11.30	9.01	7.37	6.64	6.56	7.46	9.06	11.01	12.70	13.51	13.01	11.07	8.44	6.12	4.72	4.42	5.32	6.94	8.07	11.17	233.28	9.750	
182	13.22	14.74	15.17	14.22	12.16	9.74	7.86	6.74	6.51	7.07	8.16	9.92	11.66	12.82	13.10	11.86	9.72	7.36	5.70	5.01	5.24	6.42	8.07	10.12	232.60	9.692	
183	11.98	13.73	14.86	14.72	13.40	11.17	9.22	7.55	6.51	6.57	7.34	8.72	10.61	12.04	12.77	12.64	11.27	9.34	7.48	6.30	5.87	6.54	7.66	9.24	227.53	9.697	

184	10'97	12'94	14'38	14'88	14'20	12'50	10'34	8'44	7'22	6'77	6'97	7'87	9'34	10'94	12'19	12'66	12'22	10'84	9'25	7'90	6'96	6'92	7'56	8'50	242'76	10'115	
185	10'00	11'48	13'23	14'36	14'44	13'38	11'42	9'60	8'02	6'94	6'56	6'92	7'79	9'26	10'80	11'92	12'43	12'16	11'12	9'70	8'48	7'63	7'56	8'14	243'34	10'139	
186	9'04	10'41	11'98	13'30	13'98	13'72	12'51	10'84	8'96	7'47	6'70	6'48	6'84	7'86	9'16	10'52	11'71	12'36	12'28	11'46	10'38	9'16	8'34	8'14	243'60	10'150	
187	8'38	9'04	10'37	11'82	13'16	13'66	13'27	11'87	10'24	8'57	7'05	6'14	5'87	6'26	7'22	8'72	10'36	11'70	12'56	12'86	12'14	11'14	9'86	8'86	241'12	10'047	
188	8'32	8'34	9'02	10'46	11'88	13'12	13'48	12'96	11'86	10'30	8'58	7'00	5'74	5'32	5'74	6'86	8'67	10'62	12'30	13'47	13'96	13'31	12'10	10'48	243'89	10'162	
189	9'04	8'28	8'37	8'98	10'28	11'72	13'02	13'62	13'24	12'02	10'14	8'20	6'16	4'76	4'31	4'90	6'40	8'62	10'94	13'04	14'57	15'22	14'64	12'87	243'34	10'139	
190	10'58	8'66	7'68	7'62	8'40	10'00	11'70	13'12	13'97	13'69	12'32	10'27	7'76	5'44	3'88	3'19	3'88	5'80	8'60	11'46	13'90	15'54	16'06	15'08	238'60	9'942	
191	12'92	10'40	8'23	7'07	6'90	7'82	9'54	11'60	13'35	14'38	14'34	12'76	10'16	7'15	4'46	2'56	2'27	3'49	5'92	8'80	12'36	15'04	16'76	17'06	235'34	9'806	
192	15'90	13'27	10'08	7'42	6'03	6'04	7'17	9'30	11'84	13'92	15'05	14'90	13'08	9'91	6'43	3'53	1'84	1'84	3'58	6'20	9'54	13'00	15'92	17'60	233'39	9'725	
193	17'55	15'88	12'54	9'04	6'46	5'24	5'54	6'76	9'24	12'48	14'76	16'12	15'46	13'17	9'32	5'65	2'96	1'56	1'90	3'97	6'70	10'13	13'94	16'80	233'17	9'715	
194	18'22	17'87	15'72	12'00	8'47	5'86	4'66	4'98	6'66	9'72	13'12	15'46	16'44	15'54	12'76	8'60	5'17	2'76	1'62	2'37	4'50	7'60	11'14	14'80	236'04	9'835	
195	17'30	18'38	17'46	14'77	11'14	7'30	5'12	4'24	4'66	6'66	9'96	13'24	15'56	16'37	15'10	12'10	8'47	5'36	3'22	2'47	3'46	5'71	8'66	12'13	238'84	9'952	
196	15'36	17'38	17'97	16'76	13'80	10'58	7'04	4'79	4'26	5'04	7'14	10'42	13'85	15'77	16'14	14'53	11'60	8'45	5'84	4'20	3'82	5'12	6'97	9'80	246'63	10'276	
197	13'00	15'56	17'04	17'17	15'44	12'60	9'26	6'86	5'22	4'84	5'76	8'06	10'85	13'97	15'36	15'40	13'86	11'04	8'20	6'43	5'40	5'54	6'64	7'95	251'45	10'477	
198	10'24	12'80	15'30	16'34	15'86	14'11	11'28	8'50	6'30	5'34	5'40	6'24	8'00	10'50	12'97	14'30	14'44	12'94	10'92	9'08	7'74	7'24	7'56	8'14	251'54	10'481	
199	9'16	11'11	13'10	14'71	15'40	14'72	12'96	10'60	8'38	6'86	5'92	6'05	6'82	8'26	10'28	12'30	13'38	13'40	12'62	11'34	10'16	9'24	8'58	8'59	253'94	10'581	
200	8'86	9'62	10'96	12'55	13'78	14'07	13'40	11'92	10'10	8'37	6'87	6'38	6'51	7'24	8'41	9'82	11'28	12'52	12'90	12'68	11'87	10'93	10'01	9'34	250'39	10'433	
201	9'14	9'27	9'97	10'90	12'12	13'14	13'41	12'71	11'34	9'77	8'47	7'34	6'76	6'86	6'76	6'86	7'36	8'56	11'46	12'50	13'02	12'96	12'57	11'86	10'96	252'51	10'521
202	10'04	9'53	9'52	9'76	10'73	11'74	12'78	13'04	12'50	11'42	10'20	8'76	7'52	6'90	6'26	6'26	7'25	8'50	10'20	11'86	13'24	13'87	13'87	13'28	12'22	255'49	10'645
203	11'04	10'07	9'54	9'50	9'87	10'64	11'70	12'60	12'94	12'66	11'70	10'10	8'56	7'16	6'24	6'28	7'14	8'62	10'44	12'07	13'40	14'20	14'14	13'28	253'89	10'579	
204	12'08	10'74	9'52	8'94	8'94	9'48	10'50	11'72	12'63	13'06	12'60	11'28	9'36	7'66	6'38	5'86	6'06	7'07	8'94	10'96	13'07	14'58	15'07	14'54	251'04	10'460	
205	13'34	11'84	10'26	9'14	8'46	8'46	9'16	10'36	11'74	13'14	13'52	12'81	11'24	9'13	7'31	5'74	5'33	6'10	7'65	9'76	12'02	14'00	15'20	15'33	251'04	10'460	
206	14'58	12'97	11'01	9'35	8'37	8'18	8'73	9'62	10'95	12'64	13'76	13'92	12'56	10'36	8'02	6'14	5'26	5'24	6'52	8'36	10'60	12'96	14'83	16'05	250'98	10'458	
207	15'68	14'35	12'14	9'94	8'56	8'04	8'20	8'78	9'99	11'82	13'73	14'66	14'04	11'84	8'90	6'50	5'04	4'74	5'78	7'22	9'33	11'77	14'22	15'86	251'13	10'464	
208	16'07	15'15	13'18	10'77	8'67	7'57	7'18	7'78	8'96	10'77	12'83	14'27	14'50	13'28	10'70	7'76	5'53	4'56	4'86	6'26	8'20	10'44	13'14	15'37	247'80	10'325	
209	16'51	16'11	14'47	11'94	9'36	7'58	6'88	7'16	8'00	9'72	11'80	13'84	14'90	14'32	12'37	9'57	6'78	5'10	4'56	5'42	7'13	9'26	11'96	14'36	249'10	10'379	
210	15'96	16'14	15'17	12'96	10'25	8'01	6'67	6'34	6'89	8'16	10'14	12'46	14'24	14'84	13'50	10'90	8'02	5'86	4'76	5'04	6'52	8'34	10'66	13'15	244'98	10'208	
211	15'27	16'14	15'82	14'14	11'47	8'96	7'02	6'16	6'33	7'34	9'23	11'44	13'54	14'58	14'24	12'42	9'84	7'44	5'64	5'14	5'97	7'54	9'60	11'76	247'03	10'293	
212	13'95	15'50	15'83	14'93	12'72	10'10	7'72	6'16	5'77	6'54	7'96	9'86	12'04	13'74	14'37	13'56	11'51	8'97	7'02	5'96	5'96	7'12	8'61	10'53	246'43	10'268	
213	12'64	14'44	15'55	15'26	13'84	11'46	8'86	6'95	5'97	6'05	7'05	8'56	10'54	12'48	13'67	13'96	12'84	10'98	9'00	7'60	6'88	7'24	8'26	9'66	249'74	10'406	
214	11'57	13'15	14'57	15'10	14'32	12'72	10'34	8'27	6'67	6'12	6'40	7'34	8'74	10'52	12'26	13'26	13'32	12'36	10'84	9'38	8'24	7'77	8'12	8'86	250'04	10'418	
215	10'16	11'76	13'33	14'29	14'38	13'46	11'64	9'64	7'76	6'48	6'10	6'50	7'54	9'00	10'63	12'05	12'96	13'18	12'64	11'47	10'24	9'16	8'76	9'04	252'17	10'507	
216	9'66	10'72	12'02	13'24	14'10	14'04	13'02	11'29	9'63	7'96	6'84	6'50	6'73	7'66	9'04	10'52	12'10	13'14	13'55	13'28	12'50	11'34	10'26	9'52	258'66	10'778	
217	9'35	9'67	10'59	11'83	12'88	13'62	13'44	12'54	11'15	9'50	7'86	6'50	5'94	6'16	7'10	8'50	10'20	11'94	13'44	14'14	14'16	13'42	12'16	10'76	256'85	10'702	
218	9'56	9'05	9'15	9'96	11'33	12'62	13'38	13'55	12'96	11'68	9'90	7'96	6'26	5'30	5'46	6'46	8'25	10'24	12'44	14'18	15'26	15'50	14'64	12'94	258'03	10'751	
219	10'78	9'16	8'56	8'76	9'78	11'16	12'57	13'70	14'26	14'02	12'80	10'52	8'01	5'84	4'76	4'81	5'98	7'77	10'32	13'02	15'24	16'66	16'76	15'58	260'82	10'868	
220	13'24	10'54	8'38	7'60	7'78	8'76	10'54	12'56	14'24	15'18	14'86	13'21	10'40	7'41	4'97	3'62	3'84	5'16	7'44	10'44	13'54	16'14	17'54	17'44	254'83	10'618	
221	15'84	12'90	9'72	7'44	6'60	6'85	8'10	10'22	12'92	15'15	16'26	15'72	13'66	10'33	6'96	4'40	3'04	3'33	5'32	7'86	11'08	14'56	17'30	18'37	253'83	10'576	
222	18'04	16'16	12'38	8'82	6'46	5'54	5'95	7'72	10'60	13'60	16'07	17'04	16'38	13'96	10'25	6'47	3'74	2'56	3'20	5'12	8'18	11'74	15'30	17'66	252'94	10'539	
Sum	943'28	948'07	928'91	889'06	838'11	788'76	748'57	726'62	726'18	746'27	773'80	793'58	793'05	769'34	722'70	666'49	620'53	596'14	604'10	640'99	705'26	783'60	857'11	913'59	18524'11		

FORMS FOR SHORT-PERIOD TIDES.  
 SERIES S.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Daily Mean	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
223	18.50	17.76	14.76	10.60	7.27	5.06	4.48	5.07	7.18	10.36	13.94	16.34	17.16	16.04	13.12	9.20	5.80	3.36	2.56	3.60	5.73	9.03	12.78	15.94	18.78	21.35
224	17.78	18.04	16.74	13.32	9.36	6.05	4.18	3.80	4.90	7.56	11.10	14.46	16.66	16.88	15.39	12.15	8.23	5.44	3.52	3.32	4.58	7.04	10.14	13.35	16.33	19.10
225	16.16	17.52	17.26	15.28	11.80	8.22	5.32	3.80	4.02	5.58	8.40	11.50	14.51	16.18	16.06	14.38	11.26	7.98	5.62	4.54	4.80	6.25	8.27	11.00	14.57	18.23
226	13.96	16.12	17.26	16.43	14.32	10.85	7.62	5.16	4.10	4.64	6.45	8.92	12.00	14.70	15.80	15.18	13.36	10.62	7.94	6.32	5.74	6.44	7.77	9.72	12.51	15.48
227	13.07	14.12	15.66	15.72	14.46	12.06	9.36	6.96	5.40	5.07	5.84	7.33	9.54	11.87	13.60	14.46	13.96	12.48	10.40	8.65	7.45	7.28	8.00	9.26	11.00	14.58
228	10.72	13.27	13.74	14.47	14.18	12.78	10.82	8.78	6.78	5.83	5.86	6.74	8.34	10.14	12.02	13.26	13.57	12.85	11.76	10.70	9.74	9.12	8.90	9.34	11.21	14.53
229	10.06	10.94	12.10	13.88	13.72	13.38	11.88	10.06	8.17	7.02	6.68	7.00	7.70	8.77	10.10	11.44	12.33	12.66	12.46	12.00	11.36	10.62	10.07	9.67	11.00	14.53
230	9.77	10.12	10.82	11.54	12.43	12.67	12.12	11.23	11.38	10.53	9.44	8.35	7.66	7.57	8.30	9.04	10.10	11.17	12.34	12.90	12.34	11.72	11.15	10.62	12.00	14.53
231	10.30	10.00	10.14	10.50	11.34	11.96	12.26	12.32	12.18	11.42	10.36	9.44	8.35	7.66	7.57	8.30	9.04	10.10	11.17	12.34	12.90	12.34	11.72	11.15	10.62	12.00
232	10.72	10.26	9.92	9.63	10.00	10.71	11.62	12.32	12.18	11.42	10.36	9.44	8.35	7.66	7.57	8.30	9.04	10.10	11.17	12.34	12.90	12.34	11.72	11.15	10.62	12.00
233	11.22	10.18	9.34	8.97	9.08	9.88	10.76	11.64	12.26	12.35	11.85	10.40	8.78	7.36	6.44	6.28	7.14	8.37	10.20	11.94	13.38	14.40	14.54	13.58	12.00	14.31
234	12.17	10.70	9.34	8.82	8.84	9.26	10.00	11.16	12.50	13.30	13.42	12.06	10.16	8.40	6.86	6.06	6.14	7.20	8.95	10.80	12.76	13.96	14.91	14.84	13.58	12.00
235	13.64	11.84	9.97	8.77	8.36	8.48	8.96	10.06	11.56	13.12	13.97	13.64	12.06	9.70	7.27	5.96	5.56	6.35	7.80	9.76	11.70	13.66	15.10	15.46	13.58	12.00
236	14.62	12.86	10.57	8.64	7.46	7.31	7.76	8.84	10.72	12.64	14.21	14.62	13.44	11.00	8.24	6.24	5.17	5.36	6.54	8.54	10.66	13.00	15.02	15.96	13.58	12.00
237	15.50	14.08	11.60	8.97	7.34	6.70	6.84	7.80	9.62	11.70	13.76	14.95	14.67	12.76	10.00	7.37	5.56	4.97	5.74	7.38	9.36	11.94	14.36	16.04	14.58	12.00
238	16.27	15.32	13.08	10.11	7.72	6.36	6.10	6.94	8.63	10.83	13.20	15.21	15.71	14.43	11.89	8.54	6.26	4.97	5.06	6.36	8.22	10.64	13.40	15.80	13.58	12.00
239	16.62	16.16	14.21	11.38	8.34	6.35	5.46	5.74	7.13	9.22	11.84	14.36	15.71	15.48	13.64	10.66	7.60	5.70	4.96	5.70	7.24	9.54	12.02	14.56	14.58	12.00
240	16.24	16.56	15.34	12.80	9.60	7.06	5.50	5.18	5.94	7.72	10.28	13.04	15.14	15.90	14.88	12.52	9.63	7.07	5.74	5.64	6.67	8.36	10.62	13.17	14.58	12.00
241	15.30	16.38	15.97	14.06	11.04	8.16	6.11	5.05	5.41	6.72	8.83	11.26	13.77	15.36	15.38	14.00	11.50	8.72	6.86	5.97	6.34	7.52	9.30	11.47	14.58	12.00
242	13.80	15.46	15.84	14.77	12.44	9.37	7.06	5.37	4.85	5.64	7.12	9.24	11.64	13.96	15.06	14.75	13.17	10.76	8.64	7.30	6.86	7.44	8.64	10.38	14.58	12.00
243	13.36	14.06	15.24	15.10	13.64	11.26	8.61	6.50	5.32	5.38	6.34	7.85	9.86	11.96	13.64	14.58	14.07	13.68	10.68	8.97	8.02	7.81	8.36	9.26	11.55	10.48
244	10.60	12.24	13.73	14.44	13.86	12.25	10.02	8.06	6.46	5.62	5.78	6.47	7.80	9.63	11.38	12.97	13.74	13.44	12.44	11.04	9.83	8.84	8.57	8.87	10.08	10.337
245	9.67	10.67	11.96	13.06	13.46	13.08	11.68	9.86	8.26	6.87	6.17	6.26	7.02	8.17	9.66	11.26	12.55	13.37	13.57	12.94	11.92	10.73	9.67	9.16	10.02	10.459
246	9.18	9.63	10.54	11.48	12.46	12.92	12.84	13.98	12.32	11.66	11.74	10.46	6.21	6.66	7.76	9.20	10.76	12.36	13.54	14.05	13.67	12.68	11.26	10.02	10.02	10.498
247	9.22	8.90	9.14	9.86	10.86	12.02	12.84	13.98	12.32	11.66	11.74	10.46	6.21	6.66	7.76	9.20	10.76	12.36	13.54	14.05	13.67	12.68	11.26	10.02	10.02	10.498
248	10.04	8.66	8.02	8.14	9.04	10.38	12.00	13.14	13.74	13.40	12.04	10.04	7.64	5.76	4.78	5.02	6.24	8.16	10.78	14.28	14.96	14.74	13.66	11.85	10.53	10.553
249	11.96	9.30	7.37	6.55	6.70	8.06	9.98	13.06	13.93	14.86	14.44	12.80	10.18	7.37	5.17	3.90	4.03	5.50	7.96	10.88	13.80	16.04	17.04	16.46	14.34	10.264
250	14.44	11.04	8.24	6.27	5.15	5.63	7.24	9.64	12.52	14.74	15.98	15.46	13.29	9.94	6.63	4.34	3.17	2.53	5.38	8.20	11.40	14.56	16.82	17.44	14.05	10.002
251	16.36	13.83	9.98	6.70	4.46	3.84	4.58	6.80	10.06	13.28	15.76	16.64	15.75	12.94	9.26	6.06	3.66	2.67	3.72	5.66	8.70	12.20	15.53	17.33	14.05	9.824
252	17.53	15.87	12.42	8.56	5.32	3.44	3.17	4.55	7.26	10.87	14.22	16.50	17.05	15.47	12.37	8.44	5.52	3.48	3.10	4.46	6.74	9.94	13.47	16.32	13.97	9.824
253	17.47	17.02	14.77	10.84	7.23	4.52	3.00	3.30	5.07	8.06	11.72	14.94	16.86	16.90	14.94	11.54	8.00	5.38	3.90	4.20	5.52	7.95	11.06	14.30	13.849	9.937
254	16.51	17.04	15.88	12.99	9.17	5.97	3.70	2.94	3.94	6.16	9.14	12.43	15.42	16.68	16.10	13.81	10.56	7.46	5.47	4.87	5.60	7.04	9.54	12.35	14.069	10.029
255	14.81	16.16	16.06	14.44	11.07	7.87	5.34	3.84	3.92	5.16	7.43	10.36	13.44	15.47	16.04	14.92	12.66	9.98	7.74	6.47	6.36	7.02	8.54	10.58	14.568	10.237
256	12.80	14.58	15.36	14.73	12.52	9.86	7.17	5.31	4.44	5.02	6.44	8.50	11.04	13.56	14.79	14.77	13.46	11.46	9.44	8.00	7.36	7.56	8.36	9.51	14.604	10.252
257	11.10	12.60	13.73	13.94	12.90	11.02	8.73	6.90	5.70	5.63	6.34	7.60	9.36	11.36	13.14	13.88	13.60	12.43	10.94	9.64	8.76	8.44	8.70	9.18	14.562	10.234

258	9.95	10.88	12.06	12.76	12.71	11.64	9.87	8.26	7.04	6.44	6.67	7.34	8.36	9.74	11.16	12.22	12.70	12.20	11.38	10.60	9.88	9.34	9.16	9.13	241.49	10.062
259	9.34	9.87	10.66	11.30	11.62	11.37	10.56	9.48	8.44	7.52	7.14	7.33	7.86	8.66	9.84	10.90	11.62	11.97	11.87	11.54	11.08	10.42	9.92	9.60	239.91	9.996
260	9.42	9.54	9.86	10.24	10.70	10.91	10.80	10.34	9.74	9.06	8.35	7.72	7.46	7.67	8.44	9.64	10.73	11.52	11.88	12.06	11.88	11.53	10.97	10.23	240.69	10.029
261	9.48	9.04	9.01	9.38	10.01	10.64	11.05	11.18	10.94	10.46	9.52	8.56	7.74	7.42	7.64	8.34	9.42	10.67	11.65	12.46	12.82	12.62	12.04	10.96	243.05	10.127
262	9.85	8.96	8.54	8.42	8.86	9.64	10.44	11.23	11.67	11.60	10.92	9.74	8.36	7.26	6.68	6.86	7.74	9.24	10.86	12.34	13.24	13.55	13.17	12.08	241.25	10.052
263	10.64	9.21	8.06	7.54	7.74	8.74	9.92	11.30	12.38	12.82	12.42	11.17	9.62	7.86	6.55	6.10	6.54	7.88	9.68	11.56	13.16	14.03	14.06	13.18	242.16	10.090
264	11.60	9.86	8.07	6.97	6.64	7.14	8.38	10.20	11.92	13.16	13.44	12.50	10.70	8.70	6.90	5.75	5.50	6.36	8.04	10.20	12.32	13.87	14.64	14.36	237.22	9.884
265	12.87	10.73	8.45	6.71	5.90	6.17	7.29	9.02	11.07	13.02	14.14	14.04	12.68	10.30	7.96	6.07	5.14	5.48	6.87	9.06	11.46	13.68	15.18	15.37	238.66	9.944
266	14.28	12.24	9.67	7.34	5.74	5.30	6.12	7.84	9.97	12.54	14.50	15.33	14.46	12.23	9.34	6.94	5.36	4.94	5.94	8.06	10.08	12.62	14.76	15.76	241.36	10.057
267	15.26	13.46	10.67	7.88	5.74	4.48	4.66	6.00	8.44	11.24	13.97	15.67	15.66	14.20	11.46	8.47	6.20	4.97	5.22	6.65	8.86	11.54	14.06	15.76	240.52	10.022
268	16.07	14.86	12.14	9.06	6.37	4.56	3.93	4.93	6.93	9.67	12.77	15.34	16.35	15.80	13.61	10.52	7.73	5.58	4.88	5.77	7.56	10.04	12.74	14.90	242.11	10.088
269	15.94	15.62	13.71	10.64	7.47	5.10	3.54	3.83	5.50	7.97	11.14	14.16	16.01	16.37	15.04	12.33	9.34	6.97	5.54	5.42	6.51	8.50	11.14	13.77	241.56	10.065
270	15.60	15.98	14.86	12.14	8.87	6.16	4.30	3.67	4.60	6.44	9.03	12.27	14.84	16.21	15.07	14.09	11.42	8.56	6.75	5.86	6.17	7.42	9.65	12.22	243.01	10.125
271	14.26	15.46	15.24	13.48	10.57	7.65	5.42	3.96	4.06	5.34	7.30	9.97	12.69	14.83	15.87	15.16	13.24	10.76	8.47	7.04	6.08	7.20	8.44	10.38	243.47	10.145
272	12.56	14.16	14.83	14.05	12.07	9.24	7.02	5.32	4.44	4.61	5.87	7.97	10.37	13.07	14.81	15.06	14.13	12.37	10.44	8.86	7.87	7.56	7.92	8.94	243.54	10.148
273	10.67	12.44	13.74	13.97	12.81	10.83	8.83	7.10	5.78	5.25	5.76	6.66	8.34	10.76	12.86	14.16	14.44	13.68	12.40	10.86	9.52	8.53	8.21	8.56	246.16	10.257
274	9.40	10.68	12.08	13.04	13.08	11.93	10.54	9.95	7.64	6.61	6.06	6.30	7.97	8.81	10.63	12.30	13.68	14.16	13.66	12.66	11.46	10.12	9.18	8.77	248.91	10.371
275	8.56	9.10	10.17	11.30	12.30	12.61	12.14	11.16	9.92	8.44	7.14	6.37	6.38	7.34	8.76	10.57	12.10	13.44	13.92	13.88	13.56	12.37	11.18	9.72	252.43	10.518
276	8.32	7.60	7.94	9.26	10.84	12.04	12.52	12.48	11.98	11.16	9.77	7.94	6.58	6.06	6.50	7.97	9.84	11.56	13.26	14.17	14.66	14.52	13.27	11.34	251.58	10.483
277	9.06	7.37	6.82	7.46	8.74	10.60	12.11	13.20	14.04	13.84	12.76	10.92	8.58	6.74	5.94	6.30	7.68	9.72	11.97	13.90	15.26	15.99	15.54	13.97	258.51	10.771
278	11.26	8.63	6.70	5.98	6.37	7.97	10.25	12.66	14.44	15.38	15.04	13.48	11.97	8.36	6.38	5.47	5.87	7.36	9.62	12.14	14.54	16.28	16.98	16.37	258.60	10.775
279	13.80	10.49	7.50	5.61	5.14	5.74	7.77	10.54	13.45	15.71	16.85	16.30	14.16	10.84	7.77	5.85	5.07	5.66	7.50	9.87	12.74	15.25	16.92	17.15	257.68	10.737
280	15.62	12.54	8.66	5.94	4.14	3.96	5.28	7.85	11.15	14.38	16.70	17.32	16.33	13.48	9.84	7.20	5.47	4.98	5.96	7.74	10.38	13.66	16.26	17.40	252.44	10.518
281	16.86	14.56	10.89	7.40	4.72	3.37	3.98	5.86	8.86	12.43	15.47	17.34	17.64	16.26	12.76	9.26	6.56	5.24	5.38	6.54	8.77	11.76	14.62	16.82	253.35	10.556
282	17.12	15.72	12.71	9.14	6.06	3.77	3.17	4.42	6.67	9.72	13.44	16.25	17.55	17.22	15.06	11.70	8.40	6.26	5.44	6.06	7.47	10.01	12.74	15.12	251.22	10.468
283	16.37	16.06	14.21	11.04	7.42	4.80	3.12	3.62	5.50	8.04	11.13	14.40	16.50	17.22	16.16	13.58	10.36	7.77	6.24	6.04	6.91	8.53	10.52	13.06	248.60	10.358
284	15.02	15.64	14.36	11.93	8.64	6.01	4.31	3.47	4.52	6.20	8.94	11.94	14.56	16.24	16.32	14.74	12.13	9.47	7.47	6.58	6.90	7.84	9.30	11.26	243.79	10.158
285	13.26	14.41	14.26	12.74	10.35	7.88	5.80	4.44	4.58	5.92	7.85	10.30	12.70	14.67	15.54	15.01	13.36	11.14	9.11	7.80	7.42	7.74	8.64	10.04	244.96	10.207
286	11.80	13.04	13.64	13.06	11.36	9.07	7.14	5.84	5.47	6.20	7.44	9.04	10.97	13.06	14.36	14.36	13.40	11.82	10.44	9.16	8.44	8.24	8.54	9.46	245.15	10.215
287	10.30	11.46	12.12	12.22	11.46	10.00	8.37	7.08	6.36	6.44	7.32	8.34	9.60	11.24	12.72	13.46	13.28	12.32	11.06	10.10	9.27	8.97	8.94	9.08	241.51	10.063
288	9.61	10.14	11.01	11.52	11.46	10.73	9.52	8.47	7.66	7.41	7.56	8.04	8.76	9.91	11.17	12.30	12.88	12.06	11.92	11.04	10.37	9.76	9.36	9.12	242.38	10.099
289	9.08	9.27	9.86	10.44	10.68	10.66	10.30	9.78	9.22	8.56	8.06	7.74	8.02	8.86	10.06	11.16	12.02	12.40	12.34	12.06	11.48	10.82	9.97	9.34	243.08	10.087
290	8.77	8.68	8.96	9.55	10.22	10.70	10.88	10.82	10.57	10.03	9.26	8.44	7.90	8.07	8.80	9.84	10.90	11.78	12.36	12.58	12.54	12.07	11.12	9.97	244.81	10.200
291	8.90	8.23	8.12	8.56	9.27	10.10	10.90	11.50	11.78	11.53	10.67	9.30	8.14	7.56	7.77	8.55	9.74	11.07	12.15	12.94	13.28	13.04	12.24	10.77	246.11	10.255
292	9.14	7.88	7.18	7.36	8.12	9.26	10.62	11.94	12.78	12.88	12.06	10.48	8.86	7.70	7.28	7.65	8.65	10.02	11.54	12.81	13.77	14.04	13.50	12.16	247.68	10.320
293	10.00	8.34	6.96	6.50	6.88	7.96	9.76	11.52	13.07	13.96	13.77	12.48	10.52	8.76	7.36	6.77	7.26	8.52	10.36	12.17	13.66	14.56	14.48	13.40	249.02	10.376
294	11.12	8.84	6.87	5.64	5.46	6.30	8.06	10.30	12.80	14.34	15.00	14.16	12.26	9.96	7.92	6.50	6.22	7.10	8.82	10.86	13.12	14.54	15.07	14.56	245.82	10.243
295	12.60	9.98	7.47	5.46	4.96	6.60	9.03	11.80	14.15	15.84	15.96	14.52	12.00	9.24	7.24	6.16	6.40	7.67	9.66	11.93	14.14	15.62	15.76	14.87	248.75	10.365
296	14.36	11.76	8.61	6.02	4.24	3.86	5.14	7.32	10.15	13.10	15.67	16.78	16.26	14.16	11.00	8.32	6.36	5.84	6.47	8.16	10.16	12.84	15.02	16.10	247.70	10.321
Sum	937.59	911.22	832.77	773.80	692.27	628.64	595.34	600.56	643.42	708.54	779.87	831.26	853.14	845.43	805.24	749.88	695.89	659.99	659.79	621.62	747.19	815.87	881.94	940.26	37	18288.63

FORMS FOR SHORT-PERIOD TIDES.  
 SERIES S.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Daily Sum	Daily Mean	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
297	15.46	13.28	9.87	6.84	4.45	3.04	3.57	5.44	8.15	11.37	14.60	16.81	17.35	16.28	13.64	10.44	7.71	6.07	5.84	6.88	8.87	11.47	14.12	15.94	247.49	10.312	
298	16.32	14.81	11.87	8.55	5.46	3.46	2.87	4.17	6.35	9.32	13.00	15.95	17.47	17.44	15.72	12.68	9.66	7.28	5.94	6.04	7.36	9.64	12.45	14.84	248.55	10.356	
299	16.04	15.60	13.70	10.52	7.15	4.66	2.92	3.10	4.72	7.47	10.55	13.92	16.35	17.36	16.74	14.57	11.67	8.85	6.76	5.94	6.28	7.70	9.92	12.68	245.17	10.215	
300	14.78	15.58	14.78	12.36	9.26	6.36	4.20	3.07	3.72	5.55	8.04	11.05	14.10	16.17	16.96	16.12	14.06	11.35	8.82	7.14	6.57	7.02	8.46	11.56	246.08	10.253	
301	13.14	14.64	15.04	13.76	11.47	8.74	6.42	4.70	4.22	5.00	6.80	9.02	11.88	14.60	16.14	16.22	15.16	13.26	10.86	8.86	7.58	7.14	7.44	8.84	250.93	10.455	
302	10.92	12.84	13.84	13.86	12.57	10.68	8.54	6.84	5.56	5.27	5.98	7.33	9.36	11.72	14.00	15.22	15.38	14.58	12.88	11.01	9.42	8.12	7.64	7.92	251.48	10.478	
303	8.94	10.40	11.85	12.91	13.12	12.26	10.75	9.22	7.66	6.68	6.30	6.72	7.86	9.44	11.59	13.34	14.46	14.06	13.96	12.74	11.30	9.76	8.54	7.93	252.30	10.513	
304	7.84	8.40	9.60	10.88	12.06	12.64	12.40	11.47	10.10	8.76	7.68	7.01	7.06	7.90	9.22	10.97	12.56	13.72	14.38	14.04	13.04	11.45	9.76	8.15	251.09	10.462	
305	7.22	7.02	7.48	8.84	10.32	11.48	12.55	12.87	12.46	11.36	9.70	8.28	7.14	6.80	7.40	8.84	10.74	12.56	13.87	14.54	14.38	13.40	11.67	9.60	250.52	10.438	
306	7.53	6.30	5.88	6.50	8.20	10.07	11.93	13.36	14.04	13.66	12.30	10.26	8.61	7.37	6.86	7.24	8.35	10.36	12.50	14.13	15.08	14.96	13.80	11.64	250.93	10.455	
307	9.03	6.96	5.44	5.04	5.86	7.79	10.12	12.66	14.54	15.37	14.86	13.04	10.66	8.56	7.12	6.44	6.77	8.02	10.14	12.62	14.56	15.55	15.25	13.56	249.96	10.415	
308	10.92	8.12	5.82	4.22	4.10	5.32	7.70	10.85	13.60	15.51	16.05	15.06	12.86	10.40	8.16	6.53	5.96	6.51	8.24	10.85	13.27	15.16	15.84	15.93	246.08	10.253	
309	12.98	9.78	7.04	4.71	3.46	3.86	5.60	8.44	11.74	14.64	16.50	16.72	15.38	12.86	9.98	7.70	6.25	5.93	6.71	8.67	11.25	13.84	15.52	15.84	245.40	10.225	
310	14.55	11.68	8.46	5.64	3.63	3.01	4.08	6.50	9.62	13.08	15.81	17.12	16.72	14.87	12.03	9.20	7.26	6.32	6.37	7.46	9.60	12.20	14.35	15.67	245.23	10.218	
311	15.28	13.15	10.15	7.00	4.47	3.03	3.22	5.03	7.60	10.76	14.05	16.38	17.05	16.14	13.92	11.10	8.66	6.87	6.16	6.46	8.00	10.44	13.10	14.76	242.78	10.116	
312	15.16	13.92	11.40	8.36	5.66	3.69	2.94	3.94	6.18	9.01	12.24	14.92	16.53	16.56	15.16	12.66	10.06	7.96	6.74	6.60	7.35	9.00	11.24	13.43	240.71	10.030	
313	14.50	14.36	12.66	9.94	7.20	4.97	3.56	3.77	5.34	7.72	10.56	13.46	15.64	16.34	15.71	13.92	11.46	9.28	7.66	6.86	6.98	7.98	9.96	12.00	241.83	10.076	
314	13.52	14.02	13.37	11.18	8.81	6.52	4.86	4.33	5.20	6.90	9.14	11.80	14.20	15.72	15.81	14.66	12.72	10.71	8.96	7.82	7.56	7.92	9.16	10.68	245.57	10.232	
315	12.24	13.26	12.58	12.23	11.04	9.16	7.62	6.54	7.18	7.20	7.86	8.80	9.98	11.46	12.91	14.18	14.40	13.64	12.37	9.58	8.78	8.46	8.68	9.30	247.03	10.293	
316	10.96	12.18	11.57	11.80	11.36	10.28	8.94	7.84	7.18	7.20	7.86	8.80	9.98	11.46	12.86	13.86	13.83	12.96	11.72	10.53	9.66	9.14	8.92	8.80	249.42	10.319	
317	10.00	10.94	11.57	11.80	11.36	10.28	8.94	7.84	7.18	7.20	7.86	8.80	9.98	11.46	12.86	13.86	13.83	12.96	11.72	10.53	9.66	9.14	8.92	8.80	249.42	10.319	
318	9.17	9.66	10.40	11.10	11.37	11.01	10.20	9.26	8.46	8.10	8.14	8.66	9.44	10.56	11.74	12.76	13.34	13.26	12.61	11.72	10.86	9.76	9.04	8.80	247.65	10.319	
319	8.85	9.16	9.64	10.14	10.74	11.18	11.32	11.06	10.38	9.58	8.94	8.71	8.90	9.50	10.42	11.46	12.48	13.10	13.15	12.64	11.84	10.76	9.71	8.88	252.54	10.523	
320	8.35	8.19	8.42	9.04	9.96	10.86	11.50	11.80	11.55	10.96	9.98	9.08	8.64	8.75	9.38	10.38	11.46	12.41	13.07	13.16	12.84	11.84	10.56	9.24	251.42	10.476	
321	8.13	7.50	7.43	7.86	8.83	10.03	11.16	12.23	12.80	12.64	11.66	10.25	9.04	8.36	8.34	8.96	10.02	11.20	12.46	13.23	13.47	13.00	11.72	10.14	250.46	10.436	
322	8.38	7.93	6.27	6.31	7.08	8.52	10.23	11.92	13.17	13.63	13.10	11.86	10.18	8.76	7.98	7.96	8.75	10.13	11.64	13.14	13.94	13.94	13.04	11.34	248.30	10.346	
323	9.30	7.45	5.86	5.13	5.46	6.76	8.80	11.15	13.20	14.66	14.98	13.87	11.76	9.58	8.70	7.27	7.36	8.22	9.82	11.76	13.33	14.28	14.14	13.87	245.11	10.213	
324	10.56	7.98	5.77	4.12	3.74	4.67	6.71	9.27	12.02	14.40	15.66	15.44	13.71	11.16	8.14	7.02	6.40	6.78	8.22	10.37	13.25	13.88	14.74	14.20	237.83	9.910	
325	12.26	9.36	6.51	4.12	2.75	2.94	4.56	7.03	10.05	13.27	15.65	16.62	15.90	13.76	10.86	8.17	6.45	5.84	6.36	8.12	10.44	12.84	14.46	15.08	233.40	9.745	
326	13.97	11.41	8.07	4.96	2.57	1.63	2.58	4.74	7.64	11.12	14.22	16.47	17.07	15.75	12.96	9.86	7.26	5.65	4.46	6.44	8.40	11.20	13.57	15.11	228.11	9.595	
327	15.17	13.27	9.96	6.40	3.62	1.76	1.54	3.26	6.02	9.35	12.97	15.66	17.40	17.25	15.37	12.23	9.00	6.75	5.63	5.63	6.88	9.32	12.22	14.41	231.00	9.645	
328	15.50	14.80	12.31	8.84	5.46	3.00	1.66	2.20	4.15	6.95	10.46	13.81	16.44	17.54	16.82	14.56	11.38	8.50	6.32	5.44	5.74	7.26	10.06	12.76	231.96	9.665	
329	14.67	15.26	14.06	11.32	8.05	5.16	2.94	2.16	3.11	5.16	7.96	11.23	14.30	16.57	17.22	16.23	13.81	10.68	8.07	6.16	5.50	5.88	7.64	10.25	233.39	9.725	
330	12.77	14.29	14.72	13.33	10.74	7.81	5.32	3.66	3.26	4.42	6.34	8.86	11.67	14.58	16.33	16.57	15.28	12.84	9.93	7.47	6.23	5.72	6.26	7.94	226.34	9.848	
331	10.30	12.38	13.76	13.96	12.68	10.50	8.18	6.48	4.97	4.83	5.73	7.34	9.38	12.05	14.37	15.76	15.80	14.56	12.28	9.94	8.13	6.64	6.14	6.54	222.56	10.107	





FORMS FOR SHORT-PERIOD TIDES.

BOMBAY—Commencing 0 hours, Astronomical Time, 1st January, 1885.

SERIES M.

Motion per mean Solar hour = 14°.4920521.

Argument ( $\gamma - \sigma$ ).

Day	0 <sup>a</sup>	1 <sup>a</sup>	2 <sup>a</sup>	3 <sup>a</sup>	4 <sup>a</sup>	5 <sup>a</sup>	6 <sup>a</sup>	7 <sup>a</sup>	8 <sup>a</sup>	9 <sup>a</sup>	10 <sup>a</sup>	11 <sup>a</sup>	12 <sup>a</sup>	13 <sup>a</sup>	14 <sup>a</sup>	15 <sup>a</sup>	16 <sup>a</sup>	17 <sup>a</sup>	18 <sup>a</sup>	19 <sup>a</sup>	20 <sup>a</sup>	21 <sup>a</sup>	22 <sup>a</sup>	23 <sup>a</sup>	Solar Hour		
1	15.53	12.96	9.13	5.76	3.03	1.68	2.28	4.80	7.90	11.70	15.50	18.00	18.85	18.08	15.14	8.50	6.21	5.53	6.08	8.20	11.31	14.16	16.06	16.66	2	0	
2	15.40	13.16	8.40	4.86	2.56	1.71	2.90	5.56	8.82	12.94	16.44	18.58	18.97	17.67	14.24	10.56	7.53	5.57	5.16	8.63	11.84	14.68	16.63	16.96	3	1	
3	15.24	11.93	8.00	4.87	2.80	2.37	4.24	6.84	10.20	14.07	17.26	18.86	18.84	17.06	13.20	9.77	6.90	5.23	4.96	6.16	8.86	12.14	14.97	16.40	4	2	
4	14.28	11.00	7.63	4.88	3.55	3.86	5.55	8.01	11.36	14.83	17.16	18.38	17.93	15.80	12.16	8.68	6.10	5.05	5.23	6.68	9.24	12.28	14.51	15.96	5	2	
5	15.58	13.48	10.47	7.54	5.07	5.67	7.22	9.17	12.11	15.02	17.02	17.55	16.63	14.11	10.96	8.16	6.22	5.47	5.84	7.18	9.67	12.12	14.04	15.00	6	3	
6	14.45	12.63	10.24	8.07	7.04	6.84	7.54	8.67	12.84	15.06	16.36	16.35	15.24	12.76	10.11	8.00	6.64	6.17	6.55	7.86	9.76	11.80	13.27	14.00	7	4	
7	13.64	12.22	10.47	9.95	8.44	8.46	9.03	9.97	11.20	13.05	14.64	15.46	13.87	11.68	9.76	8.10	7.16	7.03	7.40	8.29	9.82	11.16	12.55	13.24	8	5	
8	13.07	12.20	11.16	10.37	9.64	9.60	9.90	10.60	11.70	12.96	14.02	14.44	13.75	12.27	10.82	9.20	7.93	7.06	7.34	8.07	9.14	10.35	11.74	12.48	9	6	
9	12.66	12.27	11.60	10.93	10.34	9.98	9.86	10.17	11.07	12.14	13.06	13.36	12.72	11.71	10.43	9.14	7.97	7.14	7.14	8.07	9.14	10.35	11.74	12.48	10	7	
10	13.14	12.97	12.20	11.24	10.48	10.12	10.05	10.23	10.84	11.64	12.27	12.68	12.37	11.53	10.42	8.97	7.80	6.96	6.38	6.44	7.28	8.73	10.47	12.14	11	7	
11	13.23	13.84	13.63	11.38	10.27	9.77	9.62	9.89	10.44	11.24	11.97	12.52	12.80	11.87	10.54	8.76	7.34	6.16	5.74	6.34	7.62	9.54	11.46	13.22	12	8	
12	14.24	14.58	13.94	12.72	11.24	10.02	9.32	9.14	10.37	11.48	12.46	13.04	12.84	11.88	10.23	8.20	6.52	5.62	5.56	6.50	8.14	10.17	12.34	14.10	13	9	
13	15.20	15.17	13.97	12.27	10.58	9.35	8.75	8.76	9.26	10.34	11.68	12.96	13.64	13.36	11.80	9.66	7.32	5.82	5.14	5.44	6.74	8.86	11.26	13.66	15.38	14	10
14	15.87	15.24	13.66	11.54	9.82	8.71	8.16	8.36	9.30	10.74	12.46	13.64	13.98	13.00	10.84	8.24	4.76	4.46	4.63	5.40	7.36	9.78	12.57	14.82	16.13	15	11
15	15.97	14.56	12.25	10.95	8.46	7.82	7.74	8.41	9.71	11.76	13.30	14.26	14.06	13.84	11.50	8.60	5.94	4.37	4.02	5.06	7.26	9.66	12.72	15.20	16.55	17	12
16	15.71	13.83	11.22	8.94	7.54	6.94	7.15	8.40	10.37	12.44	14.06	14.68	13.82	11.50	9.60	5.94	4.37	4.02	5.06	7.26	9.66	12.72	15.20	16.55	17	12	
17	16.63	15.37	9.97	7.86	6.84	6.68	7.56	9.32	11.40	13.55	14.80	14.78	13.82	12.44	10.43	7.48	5.34	4.30	4.66	6.35	8.54	11.38	14.15	16.15	16.88	18	13
18	16.08	14.04	11.02	8.54	6.76	6.34	6.26	8.16	10.65	12.88	14.28	14.56	14.25	12.47	10.10	6.34	5.70	6.30	7.70	9.76	12.17	14.36	15.62	16.44	16.45	19	14
19	15.00	12.42	9.50	7.22	5.80	5.43	6.26	8.16	10.65	12.88	14.28	14.56	14.25	12.47	10.10	6.34	5.70	6.30	7.70	9.76	12.17	14.36	15.62	16.44	16.45	20	15
20	13.82	11.00	8.37	6.37	5.54	5.64	6.83	8.93	11.40	13.32	14.42	14.25	12.47	10.10	6.34	5.70	6.30	7.70	9.76	12.17	14.36	15.62	16.44	16.45	21	16	
21	12.76	10.13	7.78	6.17	5.70	6.11	7.62	9.70	11.76	13.36	14.14	13.72	12.06	9.94	8.32	7.22	7.01	7.74	8.97	12.97	14.62	15.50	15.17	13.80	22	17	
22	11.46	9.14	7.34	6.17	6.00	6.68	8.02	9.76	11.65	13.04	13.76	13.34	12.14	10.65	9.07	8.15	8.14	8.68	9.86	11.56	13.36	14.56	15.02	12.76	23	18	
23	10.76	8.71	6.96	6.23	6.09	6.68	7.86	9.46	11.24	12.66	13.36	13.34	12.38	11.08	9.94	9.11	8.88	9.28	10.22	11.70	13.06	14.14	14.41	13.60	24	18	
24	12.06	10.26	8.46	7.10	6.08	6.56	7.64	9.14	10.84	12.34	13.44	13.81	13.33	12.18	10.75	9.76	9.24	9.34	10.07	11.16	12.40	13.38	13.66	13.03	25	19	
25	11.87	10.24	8.47	7.00	5.83	5.38	5.68	6.78	8.55	12.22	13.56	14.30	14.16	13.05	11.56	10.06	9.11	8.87	9.40	10.46	11.87	12.94	13.44	13.33	26	20	
26	12.40	10.74	8.86	6.83	5.22	4.41	4.77	6.10	8.10	10.50	12.63	14.53	15.56	15.33	11.64	9.52	8.28	7.92	8.35	9.53	11.24	12.70	13.60	14.14	27	21	
27	13.30	11.34	8.72	6.20	4.24	3.38	3.76	5.30	7.76	10.55	13.50	15.72	16.74	16.12	14.36	11.40	8.83	7.24	7.53	9.20	11.11	12.97	14.55	15.08	28	22	
28	14.17	11.84	8.82	5.70	3.60	2.56	3.06	5.04	7.88	11.48	14.56	17.04	17.86	17.00	14.36	10.96	8.97	6.27	5.77	6.57	8.62	11.25	15.74	16.28	29	23	
29	14.96	12.18	8.44	5.42	3.22	2.16	3.07	5.52	8.75	12.46	16.01	18.10	18.47	17.26	13.80	10.14	7.09	5.27	5.02	6.02	8.40	11.85	14.65	16.52	30	23	
30	16.84	15.28	7.88	4.80	2.74	2.38	4.00	6.66	10.10	13.98	17.01	18.64	18.38	16.30	12.42	8.97	6.01	4.46	4.57	6.12	9.14	12.56	15.46	17.00	32	0	
31	16.86	14.76	11.06	7.36	4.34	2.72	2.99	4.86	11.40	14.94	17.54	18.47	17.66	14.67	11.08	7.54	5.01	3.93	4.32	6.55	9.62	13.04	15.80	16.84	33	1	
32	16.08	13.73	10.16	6.82	4.54	3.58	4.44	6.36	9.36	12.84	15.86	17.74	16.48	13.27	9.84	6.84	4.96	4.33	5.26	7.44	10.66	13.70	15.74	16.43	34	2	
33	15.42	12.82	9.66	6.90	5.42	5.14	6.20	8.06	10.66	13.66	16.02	17.12	16.74	14.88	11.68	8.76	6.34	4.74	5.86	8.26	11.07	13.60	15.16	15.34	35	3	
34	14.06	11.68	9.04	7.34	6.36	6.94	8.04	9.56	11.76	14.24	15.60	16.04	15.34	13.02	10.16	7.86	6.27	5.54	5.86	7.18	9.07	11.56	14.34	14.26	36	4	
35	12.88	11.00	9.39	8.26	7.94	8.30	9.03	10.36	12.08	13.76	14.66	14.44	13.11	11.12	9.30	7.54	6.26	6.13	6.68	7.86	9.28	10.86	12.27	13.10	37	4	

36	12.94	11.03	9.72	9.12	9.06	9.26	9.66	10.60	11.82	12.86	13.34	12.82	11.45	10.03	8.74	7.48	6.86	6.78	7.17	7.94	9.05	10.30	11.34	11.97	38	5	
37	11.92	11.42	10.84	10.34	10.07	9.97	9.77	10.44	11.32	12.06	12.26	11.78	10.88	9.87	8.84	7.86	7.24	6.94	7.18	8.03	9.07	10.14	11.00	11.56	39	6	
38	11.85	11.77	11.46	11.12	10.57	10.07	9.70	9.70	10.13	10.80	11.27	11.25	10.76	9.97	9.00	8.00	7.11	6.58	6.74	7.44	8.51	9.84	10.90	11.76	40	7	
39	12.34	12.55	12.30	11.60	10.57	9.76	9.34	9.17	9.56	10.24	10.94	11.36	11.44	10.97	10.10	9.07	8.25	7.65	6.50	7.26	8.50	10.16	11.44	12.65	41	8	
40	13.26	13.32	12.56	11.36	10.08	9.16	8.67	8.64	9.01	9.76	10.58	11.25	11.66	11.34	10.36	9.22	8.22	7.36	6.12	5.54	6.94	10.36	12.06	13.46	42	9	
41	13.97	13.64	12.30	10.76	9.26	8.14	7.84	8.12	8.96	10.24	11.52	12.40	12.66	12.07	10.47	8.56	6.64	5.46	5.20	5.93	7.55	9.56	11.72	13.33	43	9	
42	14.67	13.98	12.14	10.00	8.54	7.66	7.53	8.16	9.36	11.03	12.66	13.62	13.60	12.30	10.24	7.77	5.88	4.84	4.96	6.33	8.27	10.66	13.97	14.85	44	10	
43	15.64	15.23	13.64	11.13	9.02	6.79	7.00	8.13	9.87	11.85	13.60	14.38	13.88	11.93	9.10	6.54	4.66	4.00	4.90	6.86	9.20	11.97	14.34	15.82	45	11	
44	15.96	14.78	12.26	9.64	7.46	6.24	5.96	6.74	8.48	10.85	14.56	14.85	13.63	10.90	7.86	5.57	4.07	4.04	5.46	7.84	10.63	13.64	15.83	16.64	46	12	
45	16.01	13.87	10.90	8.00	6.17	5.46	5.74	7.26	9.70	12.25	14.42	15.50	15.15	13.08	6.94	4.75	3.92	4.66	6.62	9.46	12.60	15.08	16.60	16.64	47	13	
46	15.00	11.93	8.96	6.76	5.63	5.06	5.54	7.84	10.54	13.30	15.12	15.66	14.46	11.76	8.44	5.86	4.26	4.25	5.52	10.68	13.68	15.84	16.68	15.86	48	14	
47	13.15	10.22	7.36	5.65	4.23	4.46	6.07	8.56	11.57	14.06	15.54	15.51	13.57	10.53	7.47	5.38	4.52	5.04	6.70	9.14	12.18	14.74	16.26	14.64	49	15	
48	11.74	8.68	6.28	4.54	4.14	5.07	7.06	9.74	12.44	14.55	15.46	14.76	12.57	9.68	7.24	5.84	5.60	6.54	8.40	10.77	13.32	15.42	16.26	15.47	50	15	
49	13.18	10.24	7.54	5.62	4.69	5.80	7.87	10.40	12.80	14.50	15.06	14.03	11.86	9.36	7.58	6.64	6.76	7.86	9.60	11.66	13.73	15.08	15.32	14.12	51	16	
50	11.86	9.24	6.90	5.18	4.58	5.06	6.46	8.24	10.33	13.86	14.34	13.44	11.46	9.53	8.05	7.40	7.66	8.58	9.92	11.68	13.36	14.16	14.12	12.82	52	17	
51	10.83	8.73	6.87	5.45	4.92	5.44	6.63	8.23	10.14	11.77	12.96	13.40	12.76	10.24	9.04	8.45	8.28	8.67	9.76	11.20	12.50	13.18	13.06	11.88	53	18	
52	10.25	8.57	6.98	5.77	5.38	5.64	6.37	7.82	9.54	11.17	12.38	13.02	12.96	11.16	11.07	10.02	8.94	8.48	9.27	10.44	11.57	12.34	12.34	11.70	54	19	
53	10.50	8.90	7.32	5.96	5.12	5.86	7.17	8.90	10.63	12.10	13.16	13.16	13.56	13.13	11.86	11.86	10.27	8.88	8.08	8.42	9.56	11.93	12.44	12.26	55	20	
54	11.27	9.76	7.96	6.27	5.06	4.55	5.02	6.47	8.52	10.67	12.72	14.14	14.86	14.44	12.70	10.66	8.80	7.60	7.21	7.64	9.18	11.00	12.40	13.36	56	20	
55	13.52	12.60	10.86	6.40	4.63	4.06	4.70	6.46	8.84	11.30	13.80	15.56	16.25	15.33	12.96	10.26	7.95	6.54	6.18	7.03	8.83	11.00	12.96	14.40	57	21	
56	14.74	13.76	11.70	8.84	6.08	4.05	4.14	5.42	6.18	8.80	12.06	14.93	16.76	17.15	15.84	12.87	7.00	5.18	5.12	6.26	8.52	11.16	13.67	15.38	58	22	
57	15.86	14.57	11.93	8.26	5.48	3.42	2.92	4.14	6.52	9.58	13.16	17.62	17.34	15.27	11.66	8.27	5.56	4.16	4.32	5.84	8.66	11.92	14.74	16.46	59	23	
58	16.54	14.66	11.24	7.66	4.94	3.27	4.70	7.52	10.86	14.63	17.06	17.06	17.98	16.96	13.90	10.20	4.47	3.56	4.02	6.04	9.40	12.86	15.55	16.86	61	0	
59	16.36	13.80	10.44	6.92	4.54	3.37	3.90	5.80	8.56	12.33	15.44	17.27	17.40	15.46	12.93	8.50	5.70	3.74	3.27	4.33	10.34	13.76	15.97	16.76	62	1	
60	15.76	12.96	9.44	6.74	4.67	4.23	5.26	7.43	10.37	13.82	16.13	17.08	16.40	13.86	10.50	7.26	4.84	3.56	3.86	5.60	8.27	11.55	14.34	16.02	63	1	
61	16.28	11.66	8.60	6.46	5.26	5.46	6.56	8.86	11.44	14.36	15.97	16.18	14.88	12.00	8.86	6.28	4.57	4.06	4.86	6.67	9.40	12.24	14.39	15.64	64	2	
62	15.33	13.25	10.46	8.22	6.76	7.00	8.36	10.22	12.44	14.42	15.27	14.71	12.72	10.14	7.72	5.93	5.00	6.10	8.03	10.30	12.47	13.97	14.58	65	3		
63	13.92	12.03	10.14	8.54	7.56	7.56	8.42	9.82	11.34	12.96	14.24	13.22	11.36	9.36	7.56	6.27	5.84	6.34	7.46	9.00	10.76	12.44	13.56	13.74	66	4	
64	12.74	11.40	10.07	9.16	8.96	9.27	9.77	10.46	11.36	12.44	13.07	13.03	12.12	10.46	7.68	7.02	7.02	7.66	8.54	9.66	10.96	12.24	12.88	12.88	67	5	
65	12.24	11.43	10.66	10.24	10.16	10.24	10.47	10.86	11.44	12.02	12.40	12.24	11.36	10.18	8.97	7.97	7.67	7.94	8.50	9.78	10.74	11.76	12.46	12.67	68	6	
66	12.27	11.74	11.26	10.87	10.56	10.36	10.22	10.36	10.76	11.26	11.56	11.38	10.86	9.96	9.14	8.40	7.98	7.80	8.00	8.34	9.30	10.46	11.44	12.08	69	7	
67	12.27	12.03	11.50	10.78	10.20	9.73	9.58	9.87	10.35	10.89	11.10	11.10	10.78	10.32	9.72	8.86	7.97	7.28	7.26	7.87	8.97	10.32	11.56	12.46	70	7	
68	13.04	13.10	12.54	10.56	9.64	9.08	8.82	9.16	9.88	10.74	11.40	11.75	11.70	11.14	10.07	8.84	7.56	6.74	6.70	7.63	8.94	10.62	12.06	13.26	71	8	
69	13.78	13.68	12.86	11.34	9.88	8.86	8.16	8.03	8.46	10.86	12.06	12.78	12.56	11.57	9.92	8.17	6.67	5.98	6.16	7.20	8.87	10.76	12.70	14.08	72	9	
70	14.61	14.06	12.53	10.68	8.96	7.55	6.88	7.05	8.07	9.84	11.76	12.97	13.54	13.02	9.42	7.27	5.74	5.30	5.90	7.44	9.66	11.92	14.02	15.17	73	10	
71	15.16	13.87	11.66	9.44	7.56	6.34	6.07	6.86	8.68	10.80	12.96	14.26	14.55	13.37	11.16	8.45	6.26	5.16	5.12	6.24	8.10	10.63	13.22	15.15	15.86	74	11
Sum	1020.87	990.44	752.96	600.02	497.60	465.12	502.71	600.78	765.87	901.35	1016.37	1068.59	1045.66	921.58	748.92	586.33	476.86	459.09	492.81	595.88	744.51	912.16	1021.90	1075.13	No. of Days.	73 <sup>a</sup> 12 <sup>b</sup> .	
No.	73	73	74	74	73	73	73	73	75	73	78	73	74	74	74	73	73	75	74	73	73	74	73	74	74	74	18173.51

FORMS FOR SHORT-PERIOD TIDES.

SERIES M.—(Continued).

Day	0 <sup>a</sup>	1 <sup>b</sup>	2 <sup>b</sup>	3 <sup>b</sup>	4 <sup>b</sup>	5 <sup>b</sup>	6 <sup>b</sup>	7 <sup>b</sup>	8 <sup>b</sup>	9 <sup>b</sup>	10 <sup>b</sup>	11 <sup>b</sup>	12 <sup>b</sup>	13 <sup>b</sup>	14 <sup>b</sup>	15 <sup>b</sup>	16 <sup>b</sup>	17 <sup>b</sup>	18 <sup>b</sup>	19 <sup>b</sup>	20 <sup>b</sup>	21 <sup>b</sup>	22 <sup>b</sup>	23 <sup>b</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
72	15'17	13'22	10'40	7'86	6'06	5'25	5'34	6'90	9'24	11'72	13'95	15'20	15'12	13'39	10'64	7'57	5'44	4'44	4'96	6'46	8'94	11'85	14'34	16'00	16'06	75 12
73	14'53	11'64	8'54	5'76	4'22	3'97	5'24	7'30	10'10	13'02	15'04	16'00	15'20	12'86	9'54	6'67	4'92	4'38	5'52	7'55	10'33	13'50	15'75	16'73	16'73	76 12
74	16'07	13'66	10'42	7'22	4'92	3'64	4'00	5'66	8'33	11'52	14'30	16'06	16'52	15'06	12'13	8'73	6'13	4'66	4'99	6'52	8'92	11'86	14'66	16'40	16'56	77 13
75	15'07	11'90	8'47	5'62	3'74	3'22	4'26	6'60	9'60	12'85	15'23	16'56	16'25	14'26	10'83	8'00	5'75	5'11	5'88	7'84	10'46	13'38	15'68	16'60	15'80	78 14
76	13'36	10'12	7'06	4'83	3'54	3'76	5'34	7'86	11'00	13'93	15'92	16'74	15'74	13'36	10'24	7'64	6'12	6'08	7'14	9'00	11'56	13'90	15'66	15'98	14'76	79 15
77	12'06	8'90	6'13	4'34	3'62	4'36	6'06	8'47	11'31	13'87	15'62	16'12	14'97	12'74	10'02	8'05	7'06	7'93	9'67	12'07	14'08	15'23	15'08	13'57	80 16	
78	11'16	8'26	6'08	4'76	4'47	5'46	7'26	9'48	11'88	13'90	15'36	15'50	14'66	12'67	10'54	8'74	7'94	8'14	9'06	10'62	12'40	13'77	14'52	14'20	12'80	81 17
79	10'64	8'47	6'76	5'86	5'82	6'49	7'75	9'52	11'71	13'54	14'73	14'90	14'06	12'63	11'05	9'70	8'86	8'72	9'12	10'24	11'76	13'06	13'60	13'34	13'34	82 17
80	12'06	10'56	8'92	7'40	6'43	6'30	6'68	7'68	9'46	11'24	13'02	14'08	14'52	14'22	13'04	11'70	10'34	9'24	8'84	9'04	9'84	10'96	12'05	12'86	12'96	83 18
81	12'44	11'22	9'67	8'30	7'06	6'48	6'64	7'48	8'86	10'64	12'34	13'74	14'48	14'44	13'62	12'12	10'36	8'96	8'11	7'96	8'44	9'76	11'26	12'36	12'92	84 19
82	12'78	11'94	10'30	8'78	7'20	6'06	5'92	6'72	8'34	10'26	12'20	13'86	15'00	15'14	14'16	12'20	9'88	8'00	6'90	6'56	7'46	9'22	11'16	12'56	13'57	85 20
83	14'06	13'37	11'72	9'38	7'17	5'72	5'38	6'17	7'82	10'00	12'50	14'54	15'84	15'94	14'64	12'14	9'36	6'97	5'74	5'63	6'67	8'88	11'24	13'46	14'86	86 21
84	15'36	14'34	12'05	5'44	6'93	5'38	5'00	5'82	7'83	10'50	13'30	15'60	16'72	16'28	14'37	11'37	8'36	6'00	4'67	4'80	6'40	9'20	12'06	14'62	16'12	87 22
85	16'16	14'90	12'22	9'12	6'60	5'05	4'86	5'87	8'10	11'14	14'15	16'35	17'15	16'24	13'58	10'14	7'06	4'83	3'96	4'70	6'72	9'92	13'20	15'64	17'04	88 23
86	16'75	14'92	11'81	8'56	6'37	5'14	5'64	6'94	9'43	12'61	15'44	17'03	17'08	15'36	11'92	8'64	6'18	4'48	4'25	5'24	7'57	11'00	14'10	16'43	17'04	89 23
87	17'34	16'56	14'28	10'82	7'84	5'42	6'12	7'87	10'62	13'66	16'10	17'14	16'46	13'96	10'44	7'12	4'80	3'83	4'41	6'43	8'78	12'04	14'74	16'66	17'04	91 0
88	17'13	15'64	12'86	9'53	7'16	5'81	5'93	7'22	9'26	12'02	14'66	16'44	16'67	15'06	12'02	8'56	5'84	4'04	3'84	4'93	7'24	10'09	13'22	15'56	16'90	92 1
89	16'56	14'74	11'68	8'84	7'02	6'48	7'04	8'26	10'50	13'00	14'94	15'83	15'12	12'94	9'87	7'14	5'16	4'22	4'76	6'40	8'73	11'37	14'00	15'82	16'34	93 2
90	15'34	13'10	10'40	8'36	7'32	7'28	8'03	9'50	11'53	13'48	14'74	14'92	13'67	11'34	8'76	6'67	5'40	5'22	6'16	9'97	12'30	14'30	15'48	15'46	14'67	94 3
91	14'27	12'24	10'20	8'78	8'26	8'47	9'24	10'52	12'04	13'48	14'16	13'84	12'27	10'16	8'14	6'47	5'74	6'22	7'44	9'20	10'85	12'64	14'05	14'67	14'27	95 4
92	12'97	11'44	10'04	9'16	8'84	9'16	9'84	10'95	11'96	12'80	12'96	12'28	10'94	9'24	7'80	6'78	6'70	7'30	8'37	9'54	10'90	12'34	13'52	13'80	13'80	96 4
93	13'26	12'13	10'96	10'04	9'33	9'54	9'90	10'56	11'44	11'92	12'05	11'54	10'36	9'16	8'12	7'47	7'44	7'87	8'52	9'46	10'73	11'93	12'74	12'98	12'98	97 5
94	12'60	11'86	11'07	10'34	9'94	9'77	9'87	10'02	10'81	11'14	11'27	10'92	10'30	9'34	8'36	7'74	7'58	7'98	8'76	9'87	11'04	11'96	12'50	12'66	12'66	98 6
95	12'42	11'96	11'34	10'55	9'91	9'47	9'34	9'52	9'94	10'53	10'94	11'12	11'02	10'00	9'22	8'40	8'01	8'13	8'63	9'70	10'66	11'77	12'66	13'06	13'06	99 7
96	12'94	12'40	11'47	10'50	9'62	8'94	8'34	8'74	9'48	10'45	11'36	11'88	11'89	11'44	10'50	9'40	8'46	7'76	8'43	9'46	10'86	12'30	13'36	13'82	13'82	100 8
97	13'66	12'66	11'42	10'02	8'72	7'96	7'82	8'36	9'47	10'86	11'90	12'70	12'87	12'44	11'06	9'52	8'12	7'40	7'47	8'26	9'54	11'08	12'70	14'06	14'56	101 9
98	14'22	12'80	10'96	8'88	7'46	6'81	6'84	7'92	9'62	11'52	13'00	13'97	14'12	13'00	11'02	9'05	7'48	6'74	6'92	7'97	9'72	11'72	13'58	14'86	14'86	102 9
99	15'12	14'21	13'35	9'67	7'47	5'98	5'58	6'14	7'76	9'84	12'16	14'02	15'18	15'06	13'40	10'95	8'28	6'66	6'02	6'46	7'88	10'06	12'53	14'55	15'72	103 10
100	15'49	13'80	11'08	8'22	5'93	4'52	4'32	5'47	7'72	10'54	13'27	15'36	16'20	15'32	13'00	9'88	7'34	5'76	5'40	6'24	8'22	10'70	13'40	15'52	16'25	104 11
101	15'36	12'80	9'46	6'56	4'47	3'42	3'91	5'74	8'31	11'40	14'40	16'72	15'47	12'68	9'44	6'81	5'47	5'38	6'52	8'91	11'80	14'40	15'97	16'08	16'08	105 12
102	14'35	11'30	7'80	4'97	2'93	2'46	3'76	6'21	9'51	12'97	15'58	17'14	17'04	14'94	11'68	8'36	6'14	5'06	5'57	7'24	10'07	13'10	15'40	16'44	15'82	106 13
103	13'44	9'74	6'67	4'03	2'50	2'77	4'44	7'50	10'96	14'33	16'70	17'72	16'91	14'37	10'87	8'10	6'15	5'71	6'50	8'36	11'33	14'12	15'97	16'50	15'10	107 14
104	12'22	8'67	5'24	3'17	2'56	3'47	5'74	8'64	12'02	15'12	16'94	17'54	16'24	13'40	10'32	7'62	6'17	6'07	7'04	9'13	12'00	14'47	15'69	15'54	14'54	108 14
105	13'66	10'74	7'44	4'88	3'28	3'04	4'36	6'67	9'40	12'47	15'00	16'74	16'94	15'60	13'03	10'01	7'87	6'76	7'71	9'70	12'14	14'15	15'02	14'50	14'50	109 15
106	12'53	9'92	7'24	5'36	4'16	5'20	7'26	9'89	12'40	14'57	15'77	15'74	14'47	12'12	9'90	8'07	7'14	7'11	7'83	9'54	11'58	13'16	13'74	13'28	13'28	110 16

TIDAL OBSERVATIONS.

[Cont. VII.]



FORMS FOR SHORT-PERIOD TIDES.

SERIES M.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
144	16'13	15'62	13'90	11'47	9'28	7'84	7'40	7'74	8'92	10'62	12'60	14'02	14'27	13'22	10'78	8'10	5'76	4'27	4'17	5'26	7'20	9'70	12'28	14'66	15'94	150 0
145	16'04	14'86	12'64	10'27	8'44	7'54	7'34	8'10	9'52	11'55	13'36	14'27	13'92	12'06	9'48	6'90	5'12	4'32	4'97	6'54	8'70	11'00	13'46	15'32	16'07	151 1
146	15'67	14'17	11'77	9'56	8'16	7'68	7'83	8'74	10'50	12'26	13'66	14'02	12'96	10'86	8'34	6'24	5'04	4'82	5'84	7'60	9'46	11'87	14'10	15'30	15'60	152 2
147	14'66	12'78	10'74	9'03	7'96	7'73	8'24	9'44	11'07	12'62	13'44	13'16	11'96	9'94	7'67	6'16	5'18	5'56	6'86	8'64	10'66	12'74	14'30	15'12	15'06	153 3
148	13'65	11'84	10'00	8'46	7'75	7'78	8'46	9'92	11'36	12'37	12'84	12'22	10'98	9'18	7'32	6'03	5'94	6'87	8'17	9'67	11'58	13'28	14'64	14'97	154 3	
149	14'22	11'08	9'47	8'38	8'08	8'30	9'20	10'24	11'40	12'12	12'46	11'72	10'38	8'77	7'37	6'70	6'93	7'78	8'83	10'30	11'90	13'54	14'68	14'80	155 4	
150	13'77	12'16	10'50	9'20	8'47	8'28	8'60	9'36	10'36	11'26	11'83	12'05	11'56	10'60	9'20	8'14	7'72	7'83	8'62	9'82	11'10	12'64	13'94	14'46	14'16	156 5
151	13'26	11'74	10'42	9'26	8'54	8'34	8'46	9'23	10'10	10'93	11'70	11'97	11'72	11'06	9'98	8'86	8'32	8'36	9'00	10'04	11'54	12'92	13'86	14'25	13'85	157 6
152	12'88	11'48	10'08	8'98	8'20	8'20	8'37	9'12	10'03	11'29	12'14	12'58	12'36	11'84	11'02	10'06	9'23	8'78	9'20	10'37	11'98	13'44	14'22	14'34	13'94	158 7
153	12'86	11'59	10'03	8'74	7'92	7'54	7'76	8'67	9'66	11'54	12'84	13'87	13'86	13'28	12'03	10'56	9'66	9'64	10'17	11'38	12'77	13'98	14'67	15'14	14'88	159 8
154	13'86	12'46	10'48	8'82	7'82	7'50	8'19	9'46	11'28	13'22	14'76	15'82	15'76	14'97	13'34	11'70	10'67	10'27	10'56	11'52	12'90	14'12	15'30	15'65	15'48	160 9
155	14'17	12'02	9'86	8'00	7'09	6'85	7'72	9'34	11'40	13'77	15'84	16'86	16'85	15'70	13'60	11'52	9'95	9'55	9'80	10'84	12'57	14'21	15'47	16'06	16'29	161 9
156	15'22	13'50	10'84	8'22	6'16	4'95	5'15	6'50	8'61	11'37	14'18	16'48	17'54	17'17	15'60	12'50	10'07	8'34	8'17	8'96	10'27	12'23	14'24	15'74	16'29	162 10
157	15'33	12'77	9'46	6'32	4'44	3'62	4'30	6'30	8'54	11'95	15'02	17'28	17'95	17'20	15'02	11'76	9'04	7'44	7'22	7'81	9'55	12'08	14'54	16'07	16'21	163 11
158	14'76	11'87	8'16	5'07	3'07	2'74	3'80	5'94	9'24	12'80	15'92	18'07	18'53	17'65	14'65	10'90	8'00	6'62	6'55	7'50	9'65	12'45	14'89	16'40	16'14	164 12
159	14'28	10'90	7'10	4'31	2'62	2'37	3'68	6'30	9'76	13'48	16'44	18'12	18'40	17'00	13'80	10'17	7'55	6'20	6'18	7'30	9'60	12'79	15'16	16'42	15'96	165 13
160	13'80	10'33	6'77	4'00	2'33	2'54	4'18	7'11	10'40	13'95	16'74	17'85	17'95	16'07	12'81	9'60	7'05	5'72	5'77	7'00	9'56	12'80	15'12	16'05	15'26	166 14
161	12'76	9'20	6'14	3'95	2'88	3'47	5'52	7'93	11'04	14'21	16'44	17'72	17'40	15'44	12'07	9'02	6'70	5'67	5'93	7'41	10'07	13'02	14'92	15'57	16'14	167 14
162	14'68	12'28	6'52	4'77	4'20	4'94	6'52	8'80	11'67	14'34	16'42	17'20	16'60	14'54	11'30	8'66	6'74	6'05	6'16	7'65	10'05	12'50	14'32	14'85	168 15	
163	14'05	11'96	9'47	7'26	6'06	5'80	6'39	7'66	9'64	11'92	14'25	15'90	16'46	15'74	13'76	10'84	8'61	6'86	6'32	6'58	7'80	9'82	12'04	13'55	14'17	169 16
164	13'54	12'03	10'34	8'60	7'57	7'26	7'62	8'44	9'92	12'12	14'20	15'46	15'54	14'58	12'66	10'40	8'31	7'04	6'60	6'77	7'78	9'32	11'22	12'80	13'58	170 17
165	13'46	12'40	10'90	9'62	8'66	8'31	8'49	9'03	10'30	12'04	13'70	14'74	14'75	13'73	12'02	10'10	8'46	7'12	6'53	6'70	7'50	9'03	10'90	12'32	13'20	171 18
166	13'38	12'92	11'94	10'67	9'60	8'94	8'82	9'24	10'33	11'90	13'24	14'06	14'10	13'34	11'84	10'05	8'26	6'94	6'44	6'67	7'49	9'06	10'86	12'50	13'66	172 19
167	14'10	13'63	12'46	11'06	10'06	9'30	9'05	9'33	10'22	11'60	12'90	13'82	13'85	13'08	11'64	9'76	8'00	6'70	6'08	6'22	7'28	9'00	10'94	12'77	173 19	
168	14'05	14'17	12'86	11'33	10'04	9'14	8'86	9'20	10'08	11'26	12'44	13'30	13'52	12'80	11'00	8'85	7'06	5'67	5'05	5'60	7'15	9'26	11'30	13'28	174 20	
169	14'45	14'84	13'95	12'40	10'90	9'46	8'62	8'24	8'56	9'64	11'12	12'55	13'40	13'37	12'07	10'07	8'20	6'17	4'94	4'74	5'62	7'74	9'76	12'14	14'01	175 21
170	15'00	14'86	13'77	12'06	10'27	8'84	8'10	7'94	8'52	9'68	11'18	12'64	13'37	13'05	11'52	9'17	6'76	5'11	4'16	4'64	6'10	8'00	10'50	12'90	14'56	176 22
171	15'33	14'70	13'32	11'14	9'44	8'17	7'54	7'57	8'34	9'81	11'65	13'20	13'60	12'56	10'40	5'83	4'38	4'04	4'96	6'82	9'02	11'57	13'86	15'24	177 23	
172	15'44	14'56	12'56	10'36	8'63	7'62	7'30	7'74	8'86	10'67	12'47	13'67	13'60	12'02	9'66	6'93	4'96	3'94	4'22	5'70	7'84	10'40	12'82	14'74	15'56	179 0
173	15'33	13'80	11'44	9'35	7'79	7'04	7'03	7'90	9'44	11'66	13'22	13'92	13'00	10'74	8'00	5'64	4'04	3'83	4'76	6'70	9'02	11'37	13'67	15'12	15'46	180 1
174	14'48	12'44	9'96	8'16	6'86	6'42	6'94	8'42	10'44	12'57	13'67	13'68	12'22	9'64	6'86	4'96	3'98	4'36	5'65	7'72	10'02	12'26	14'31	15'28	181 1	
175	15'12	13'77	11'30	9'01	7'37	6'64	6'56	7'46	9'06	11'01	12'70	13'51	13'01	11'07	8'44	6'12	4'72	4'42	5'32	6'94	8'97	11'17	13'22	14'74	15'17	182 2
176	14'22	12'16	9'74	7'86	6'74	6'51	7'07	8'16	9'92	11'66	12'82	13'10	11'86	9'72	7'36	5'70	5'02	5'24	6'42	8'07	10'12	11'98	13'73	14'86	14'72	183 3
177	13'40	11'17	9'22	7'55	6'51	6'57	7'34	8'72	10'61	12'04	12'77	12'64	11'27	7'48	6'30	5'87	6'54	7'66	9'24	10'97	12'94	14'38	14'88	14'20	184 4	
178	12'50	10'34	8'44	7'22	6'77	6'97	7'87	9'34	10'94	12'19	12'66	12'22	10'84	9'25	7'90	6'96	6'92	7'56	10'00	11'48	13'23	14'36	14'44	13'38	185 5	

179	11.42	9.60	8.02	6.94	6.56	6.92	7.79	9.26	10.80	11.92	12.43	12.16	11.12	9.70	8.48	7.63	7.56	8.14	9.04	10.41	11.98	13.30 13.98	13.72	12.51	186	6
180	10.84	8.96	7.47	6.70	6.48	6.84	7.86	9.16	10.52	11.71	12.36	12.28	11.46	10.38	9.16	8.34	8.14	8.38	9.04	10.37	11.82	13.16	13.66	13.27	187	6
181	11.87	10.24	8.57 7.05	6.14	5.87	6.26	7.22	8.72	10.36	11.70	12.56	12.86	12.14	11.14	9.86	8.86	8.32	8.34	9.02	10.46	11.88	13.12	13.48	12.96	188	7
182	11.86	10.30	8.58	7.00	5.74	5.32	5.74 6.86	8.67	10.62	12.30	13.47	13.96	13.31	12.10	10.48	9.04	8.28	8.37	8.98	10.28	11.72	13.02	13.62	13.24	189	8
183	12.02	10.14	8.20	6.16	4.76	4.31	4.90	6.40	8.62	10.94	13.04	14.57 15.22	14.64	12.87	10.58	8.66	7.68	7.62	8.40	10.00	11.70	13.12	13.97	13.69	190	9
184	12.32	10.27	7.76	5.44	3.88	3.19	3.88	5.80	8.60	11.46	13.90	15.54	16.06	15.08	12.92	10.40 8.23	7.07	6.90	7.82	9.54	11.60	13.35	14.38	14.34	191	10
185	12.76	10.16	7.15	4.46	2.56	2.27	3.49	5.92	8.80	12.36	15.04	16.76	17.06	15.90	13.27	10.08	7.42	6.03	6.04	7.17	9.30 11.84	13.92	15.05	14.90	192	11
186	13.08	9.91	6.43	3.53	1.84	1.84	3.58	6.20	9.54	13.00	15.92	17.60	17.55	15.88	12.54	9.04	6.46	5.24	5.54	6.76	9.24	12.48	14.76	16.12	193	11
187	13.46	13.17 9.32	5.65	2.96	1.56	1.90	3.97	6.70	10.13	13.94	16.80	18.22	17.87	15.72	12.00	8.47	5.86	4.66	4.98	6.66	9.72	13.12	15.46	16.44	194	12
188	15.54	12.76	8.60	5.17	2.76	1.62 2.37	4.50	7.60	11.14	14.80	17.30	18.38	17.46	14.77	11.14	7.30	5.12	4.24	4.66	6.66	9.96	13.24	15.56	16.37	195	13
189	15.10	12.10	8.47	5.36	3.22	2.47	3.46	5.71	8.66	12.13	15.36 17.38	17.97	16.76	13.80	10.58	7.04	4.79	4.26	5.04	7.14	10.42	13.85	15.77	16.14	196	14
190	14.53	11.60	8.45	5.84	4.20	3.82	5.12	6.97	9.80	13.00	15.56	17.04	17.17	15.44	12.60 9.26	6.86	5.22	4.84	5.76	8.06	10.85	13.97	15.36	15.40	197	15
191	13.86	11.04	8.20	6.43	5.40	5.54	6.64	7.95	10.24	12.80	15.30	16.34	15.86	14.11	11.28	8.50	6.30	5.34	5.40	6.24 8.00	10.50	12.97	14.30	14.44	198	16
192	12.94	10.92	9.08	7.74	7.24	7.56	8.14	9.16	11.11	13.10	14.71	15.40	14.72	12.96	10.60	8.38	6.86	5.92	6.05	6.82	8.26	10.28	12.30	13.38 13.40	199	17
193	12.62	11.34	10.16	9.24	8.58	8.59	8.86	9.62	10.96	12.55	13.78	14.07	13.40	11.92	10.10	8.37	6.87	6.38	6.51	7.24	8.41	9.82	11.28	12.52	200	17
194	12.90	12.68	11.87	10.93	10.01 9.34	9.14	9.27	9.97	10.90	12.12	13.14	13.41	12.71	11.34	9.77	8.47	7.34	6.76	6.86	7.36	8.56	10.06	11.46	12.50	201	18
195	13.02	12.96	12.57	11.86	10.95	10.04	9.53	9.52	9.76 10.73	11.74	12.78	13.04	12.50	11.42	10.20	8.76	7.52	6.90	6.76	7.25	8.50	10.20	11.86	13.24	202	19
196	13.87	13.87	13.28	12.22	11.04	10.07	9.54	9.50	9.87	10.64	11.70	12.60	12.94	11.70	10.10	8.56	7.16	6.24	6.28	7.14	8.62	10.44	12.07	13.40	203	20
197	14.20	14.14	13.28	12.08	10.74	9.52	8.94	8.94	9.48	10.50	11.72	12.63	13.06	12.60	11.28	9.36	7.66	6.38 5.86	6.06	7.07	8.94	10.96	13.07	14.38	204	21
198	15.07	14.54	13.34	11.84	10.26	9.14	8.46	8.46	9.16	10.36	11.74	13.14	13.52	12.81	11.24	9.13	7.31	5.74	5.33	6.10	7.65	9.76	14.00	15.20	205	22
199	15.33	14.58	12.97	11.01	9.35	8.37	8.18	8.73	9.62	10.95	12.64	13.76	13.92	12.56	10.36	8.02	6.14	5.26	5.24	6.52	8.36	10.60	12.96	14.83	206	22
200	16.05	15.68	14.35 12.14	9.94	8.56	8.04	8.20	8.78	9.99	11.82	13.73	14.66	14.04	11.84	8.90	6.50	5.04	4.74	5.78	7.22	9.33	11.77	14.22	15.86	207	23
201	16.07	15.15	13.18	10.77	8.67	7.57	7.18	7.78 8.96	10.77	12.83	14.27	14.50	13.28	10.70	7.76	5.55	4.56	4.86	6.26	8.20	10.44	13.14	15.37	16.51	209	0
202	16.11	14.47	11.94	9.36	7.58	6.88	7.16	8.00	9.72	11.80	13.84	14.90 14.32	12.37	9.57	6.78	5.10	4.56	5.42	7.13	9.26	11.96	14.36	15.96	16.14	210	1
203	15.17	22.96	10.25	8.01	6.67	6.34	6.89	8.16	10.14	12.46	14.24	14.84	13.50	10.90	8.02	5.86	4.76 5.04	6.52	8.34	10.66	13.13	15.27	16.14	15.82	211	2
204	14.14	11.47	8.96	7.02	6.16	6.33	7.34	9.23	11.44	13.54	14.58	14.24	12.42	9.84	7.44	5.64	5.14	5.97	7.54	9.60	11.76 13.95	15.50	15.83	14.93	212	3
205	12.72	10.10	7.72	6.16	5.77	6.54	7.96	9.86	12.04	13.74	14.37	13.56	11.51	8.97	7.02	5.96	5.96	7.12	8.61	10.53	12.64	14.44	15.55	15.26	213	3
206	13.84	11.46 8.86	6.95	5.97	6.05	7.05	8.56	10.54	12.48	13.67	13.96	12.84	10.98	9.00	7.60	6.88	7.24	8.26	9.66	11.37	13.15	14.57	15.10	14.32	214	4
207	12.72	10.34	8.27	6.67	6.12	6.40	7.34 8.74	10.52	12.26	13.26	13.32	12.36	10.84	9.38	8.24	7.77	8.12	8.86	10.16	11.76	13.33	14.29	14.38	13.46	215	5
208	11.64	9.64	7.76	6.48	6.10	6.50	7.54	9.00	10.63	12.05	12.96 13.18	12.64	11.47	10.24	9.16	8.76	9.04	9.66	10.72	12.02	13.24	14.10	14.04	13.02	216	6
209	11.29	9.63	7.96	6.84	6.50	6.73	7.66	9.04	10.52	12.10	13.14	13.55	13.28	12.50	11.34	10.26 9.52	9.35	9.67	10.59	11.83	12.88	13.62	13.44	12.54	217	7
210	11.15	9.50	7.86	6.50	5.94	6.16	7.10	8.50	10.20	11.94	13.44	14.14	14.16	13.42	12.16	10.76	9.56	9.05	9.15	9.96 11.33	12.62	13.38	13.55	12.96	218	8
211	11.68	9.90	7.96	6.26	5.30	5.46	6.46	8.25	10.24	12.44	14.18	15.26	15.50	14.64	12.94	10.78	9.16	8.56	8.76	9.78	11.16	12.57	13.70	14.26	219	8
212	14.02 12.80	10.52	8.01	5.84	4.76	4.81	5.98	7.77	10.32	13.02	15.24	16.66	16.76	15.58	13.24	10.54	8.38	7.60	7.78	8.76	10.54	12.56	14.24	15.18	220	9
213	14.86	13.21	10.40	7.41	4.97 3.62	3.84	5.16	7.44	10.44	13.54	16.14	17.54	17.44	15.84	12.90	9.72	7.44	6.60	6.85	8.10	10.22	12.92	15.15	16.26	221	10
214	15.72	13.66	10.33	6.96	4.40	3.04	3.33	5.32	7.86	11.08 14.56	17.20	18.37	18.04	16.16	12.38	8.82	6.46	5.54	5.95	7.72	10.60	13.60	16.07	17.04	222	11
Sum	1027.69	892.75	725.74	583.23	502.54	476.45	523.48	615.47	754.55	913.26	1051.87	1066.39	1021.39	899.21	742.68	599.35	494.34	482.75	533.46	650.77	799.94	940.31	1041.05	1070.88	No. of Days.	
No.	74	74	73	73	74	74	74	73	73	74	75	73	73	73	74	74	73	73	74	74	73	73	73	73	18409.55	79 <sup>d</sup> 12 <sup>h</sup> .

FORMS FOR SHORT-PERIOD TIDES.

SERIES M.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
215	16.38	13.96	10.25	6.47	3.74	2.56	3.20	5.12	8.18	11.74	15.30	17.66	18.50	17.76 14.76	10.60	7.27	5.06	4.48	5.07	7.18	10.36	13.94	16.34	17.16	223	12
216	16.04	13.12	9.20	5.80	3.36	2.56	3.60	5.73	9.03	12.78	15.94	17.78	18.04	16.74	13.32	9.36	6.05	4.18	3.80 4.90	7.56	11.10	14.46	16.66	16.88	224	13
217	15.39	12.15	8.23	5.44	3.52	3.32	4.58	7.04	10.14	13.35	16.16	17.52	17.26	15.28	11.80	8.22	5.32	3.80	4.02	5.58	8.40	11.50	14.52 16.18	16.06	225	14
218	14.38	11.26	7.98	5.62	4.54	4.80	6.25	8.27	11.00	13.96	16.32	17.26	16.42	14.32	10.85	7.62	5.16	4.10	4.64	6.45	8.92	12.05	14.70	15.80	226	14
219	15.18	13.36	10.62	7.04 6.32	5.74	6.44	7.77	9.72	12.07	14.12	15.66	15.72	14.46	12.06	9.36	6.96	5.40	5.07	5.84	7.33	9.54	11.87	13.60	14.46	227	15
220	13.96	12.48	10.40	8.65	7.45	7.28	8.00	9.26 10.72	12.27	13.74	14.47	14.18	12.78	10.82	8.78	6.78	5.83	5.86	6.74	8.34	10.14	12.02	13.26	13.57	228	16
221	12.85	11.76	10.70	9.74	9.12	8.90	9.34	10.06	10.94	12.10	12.88	13.72	13.38 11.88	10.06	8.17	7.02	6.68	7.00	7.70	8.77	10.10	11.44	12.33	12.66	229	17
222	12.46	12.00	11.36	10.62	10.07	9.67	9.77	10.12	10.82	11.54	12.43	12.67	12.12	11.23	9.96	8.64	7.77 7.46	7.69	8.30	9.04	10.10	11.17	12.34	12.90	230	18
223	12.90	12.34	11.72	11.15	10.62	10.30	10.00	10.14	10.50	11.34	11.96	12.26	11.97	11.38	10.53	9.44	8.35	7.66	7.57	8.12	9.06	10.48 11.57	12.72	13.42	231	19
224	13.56	13.18	12.30	11.45	10.72	10.26	9.92	9.63	10.00	10.71	11.62	12.32	12.18	11.42	10.36	9.08	8.15	7.53	7.24	7.70	8.54	9.82	11.43	12.72	232	19
225	13.64	13.66	13.26 12.36	11.22	10.18	9.34	8.97	9.08	9.88	10.76	11.64	12.26	12.35	11.85	10.40	8.78	7.36	6.44	6.28	7.14	8.37	10.20	11.94	13.38	233	20
226	14.40	14.54	13.58	12.17	10.70	9.34	8.82 8.84	9.26	10.00	11.16	12.50	13.30	13.42	12.06	10.16	8.40	6.86	6.06	6.14	7.20	8.95	10.80	12.76	13.96	234	21
227	14.91	14.84	13.64	11.84	9.97	8.77	8.36	8.48	8.96	10.06	11.56	13.12 13.97	13.64	12.06	9.70	7.27	5.96	5.56	6.35	7.80	9.76	11.70	13.66	15.10	235	22
228	15.46	14.62	12.86	10.57	8.64	7.46	7.31	7.76	8.84	10.72	12.64	14.21	14.62	13.44	11.00	8.24 6.24	5.17	5.36	6.54	8.54	10.66	13.00	15.02	15.96	236	23
229	15.50	14.08	11.60	8.97	7.34	6.70	6.84	7.80	9.62	11.70	13.76	14.95	14.67	12.76	10.00	7.37	5.56	4.97	5.74	7.38	9.36 11.94	14.36	16.04	16.27	238	0
230	15.32	13.08	10.11	7.72	6.36	6.10	6.94	8.63	10.83	13.20	15.21	15.71	14.43	11.89	8.54	6.26	4.97	5.06	6.36	8.22	10.64	13.40	15.80	16.62	239	0
231	16.16 14.21	11.38	8.34	6.35	5.46	5.74	7.13	9.22	11.84	14.36	15.71	15.48	13.64	10.66	7.60	5.70	4.96	5.70	7.24	9.54	12.02	14.56	16.24	16.56	240	1
232	15.34	12.80	9.60	7.06	5.50	5.18 5.94	7.72	10.28	13.04	15.14	15.90	14.88	12.52	9.63	7.07	5.74	5.64	6.67	8.36	10.62	13.17	15.30	16.38	15.97	241	2
233	14.06	11.04	8.16	6.11	5.05	5.41	6.72	8.83	11.26	13.77 15.30	15.38	14.00	11.50	8.72	6.86	5.97	6.34	7.52	9.30	11.47	13.80	15.46	15.84	14.77	242	3
234	12.44	9.37	7.06	5.37	4.83	5.64	7.12	9.24	11.64	13.96	15.06	14.75	13.17	10.76	8.64 7.30	6.86	7.44	8.64	10.38	12.36	14.06	15.24	15.10	13.64	243	4
235	11.26	8.61	6.50	5.32	5.38	6.34	7.85	9.86	11.96	13.64	14.58	14.07	12.68	10.68	8.97	8.02	7.81	8.36	9.26 10.60	12.24	13.73	14.44	13.86	12.25	244	5
236	10.02	8.06	6.46	5.62	5.78	6.47	7.80	9.63	11.38	12.97	13.74	13.44	12.44	11.04	9.83	8.84	8.57	8.87	9.67	10.67	11.96	13.06	13.46	13.08 11.68	245	6
237	9.86	8.26	6.87	6.17	6.26	7.02	8.17	9.66	11.26	12.55	13.37	13.57	12.94	11.92	10.73	9.67	9.16	9.18	9.63	10.54	11.48	12.46	12.92	12.66	246	6
238	11.74	10.42	8.87	7.44 6.44	6.21	6.66	7.76	9.20	10.76	12.36	13.54	14.05	13.67	12.68	11.26	10.02	9.22	8.90	9.14	9.86	10.86	12.02	12.84	12.98	247	7
239	12.36	11.16	9.57	7.60	6.24	5.63	5.97	7.17	8.80 10.66	12.80	14.28	14.96	14.74	13.66	11.85	10.04	8.66	8.02	8.14	9.04	10.38	12.00	13.14	13.74	248	8
240	13.40	12.04	10.04	7.64	5.76	4.78	5.02	6.24	8.16	10.78	13.20	15.04	15.98 15.74	14.33	11.96	9.30	7.37	6.55	6.70	8.06	9.98	12.06	13.93	14.86	249	9
241	14.44	12.80	10.18	7.37	5.17	3.90	4.03	5.50	7.96	10.88	13.80	16.04	17.04	16.46	14.44	11.04	8.24	6.27 5.15	5.63	7.24	9.64	12.52	14.74	15.98	250	10
242	15.46	13.29	9.94	6.63	4.34	3.17	2.53	5.38	8.20	11.40	14.56	16.82	17.44	16.36	13.83	9.98	6.70	4.46	3.84	4.58	6.80	10.06 13.28	15.76	16.64	251	11
243	15.75	12.94	9.26	6.06	3.66	2.67	3.72	5.66	8.70	12.20	15.53	17.33	17.53	15.87	12.42	8.56	5.32	3.44	3.17	4.55	7.26	10.87	14.22	16.50	252	11
244	17.05	15.47	12.37 8.44	5.52	3.48	3.10	4.46	6.74	9.94	13.47	16.22	17.47	17.02	14.77	10.84	7.23	4.52	3.00	3.30	5.07	8.06	11.72	14.94	16.86	253	12
245	16.90	14.94	11.54	8.00	5.38	3.90	4.20	5.52 7.95	11.06	14.30	16.51	17.04	15.88	12.99	9.17	5.97	3.70	2.94	3.94	6.16	9.14	12.45	15.42	16.68	254	13
246	16.10	13.81	10.56	7.46	5.47	4.87	5.60	7.04	9.54	12.25	14.81	16.16 16.06	14.44	11.07	7.87	5.34	3.84	3.02	5.16	7.43	10.36	13.44	15.47	16.04	255	14
247	14.92	12.66	9.98	7.74	6.47	6.36	7.02	8.54	10.58	12.80	14.58	15.36	14.73	12.52	9.86	7.17	5.31 4.44	5.02	6.44	8.50	11.04	13.56	14.79	14.77	256	15
248	13.46	11.46	9.44	8.00	7.36	7.56	8.36	9.51	11.10	12.60	13.73	13.94	12.90	11.02	8.73	6.90	5.70	5.63	6.34	7.60	9.36 11.36	13.14	13.88	13.60	257	16
249	12.43	10.94	9.64	8.76	8.44	8.70	9.18	9.95	10.88	12.06	12.76	12.71	11.64	9.87	8.26	7.04	6.44	6.67	7.34	8.36	9.74	11.16	12.22	12.70	258	16



250	12.20	11.38 10.60	9.88	9.34	9.16	9.13	9.34	9.87	10.66	11.30	11.62	11.37	10.56	9.48	8.44	7.52	7.14	7.33	7.86	8.66	9.84	10.90	11.62	11.97	259 17
251	11.87	11.54	11.08	10.42	9.92	9.60 9.42	9.54	9.86	10.24	10.70	10.91	10.80	10.34	9.74	9.06	8.35	7.72	7.46	7.67	8.44	9.64	10.73	11.52	11.88	260 18
252	12.06	11.88	11.53	10.97	10.23	9.48	9.04	9.01	9.38	10.01	10.64 11.05	11.18	10.94	10.46	9.52	8.56	7.74	7.42	7.64	8.43	9.42	10.67	11.65	12.46	261 19
253	12.82	12.62	12.04	10.96	9.85	8.96	8.54	8.42	8.86	9.64	10.44	11.23	11.67	11.60 10.92	9.74	8.36	7.26	6.68	6.86	7.74	9.24	10.86	12.34	13.24	262 20
254	13.55	13.17	12.08	10.64	9.21	8.06	7.54	7.74	8.74	9.92	11.30	12.38	12.82	12.42	11.17	9.62	7.86	6.55	6.10	6.54 7.88	9.68	11.56	13.16	14.03	263 21
255	14.06	13.18	11.60	9.86	8.07	6.97	6.64	7.14	8.38	10.20	11.92	13.16	13.44	12.50	10.70	8.70	6.90	5.75	5.50	6.36	8.04	10.20	12.32	13.87 14.64	264 22
256	14.36	12.87	10.73	8.45	6.71	5.90	6.17	7.29	9.02	11.07	13.02	14.14	14.04	12.68	10.30	7.96	6.07	5.14	5.48	6.87	9.06	11.46	13.68	15.18	265 22
257	15.37	14.28	12.24	9.67	7.34 5.74	5.30	6.12	7.84	9.97	12.54	14.50	15.33	14.46	12.23	9.34	6.94	5.36	4.94	5.94	8.06	10.08	12.62	14.76	15.76	266 23
258	15.26	13.46	10.67	7.88	5.74	4.48	4.66	6.00	8.44 11.24	13.97	15.67	15.66	14.20	11.46	8.47	6.20	4.97	5.22	6.65	8.86	11.54	14.06	15.76	16.07	268 0
259	14.86	12.14	9.06	6.37	4.56	3.93	4.93	6.93	9.67	12.77	15.34	16.35	15.80 13.61 10.52	7.73	5.58	4.88	5.77	7.56	10.04	12.74	14.90	15.94	15.62	269 1	
260	13.71	10.64	7.47	5.10	3.54	3.83	5.50	7.97	11.14	14.16	16.01	16.37	15.04	12.33	9.34	6.97	5.54	5.42 6.51	8.50	11.14	13.77	15.60	15.98	14.86	270 2
261	12.14	8.87	6.16	4.30	3.67	4.60	6.44	9.03	12.27	14.84	16.21	15.96	14.09	11.42	8.56	6.75	5.80	6.17	7.42	9.65	12.22	14.26	15.46 15.24	13.48	271 3
262	10.57	7.65	5.42	3.96	4.06	5.34	7.30	9.97	12.69	14.83	15.87	15.16	13.24	10.76	8.47	7.04	6.68	7.20	8.44	10.38	12.56	14.16	14.83	14.05	272 3
263	12.07	9.24	7.02 5.32	4.44	4.61	5.87	7.97	10.37	13.07	14.81	15.06	14.13	12.37	10.44	8.86	7.87	7.56	7.92	8.94	10.67	12.44	13.74	13.97	12.81	273 4
264	10.83	8.83	7.10	5.78	5.25	5.76	6.66	8.34 10.76	12.86	14.16	14.44	13.68	12.40	10.86	9.52	8.53	8.21	8.56	9.40	10.68	12.08	13.04	13.08	11.93	274 5
265	10.54	9.05	7.64	6.61	6.06	6.30	7.07	8.81	10.63	12.30	13.68	14.16	13.66 12.66	11.46	10.12	9.18	8.77	8.56	9.10	10.17	11.30	12.30	12.61	12.14	275 6
266	11.16	9.92	8.44	7.14	6.37	6.38	7.34	8.76	10.57	12.10	13.44	13.92	13.88	13.56	12.37	11.18	9.72 8.32	7.60	7.94	9.26	10.84	12.04	12.52	12.48	276 7
267	11.98	11.16	9.77	7.94	6.58	6.06	6.50	7.97	9.84	11.56	13.26	14.17	14.66	14.52	13.27	11.34	9.06	7.37	6.82	7.46	8.74	12.11	13.20	14.04	277 8
268	13.84	12.76	10.92	8.58	6.74	5.94	6.30	7.68	9.72	11.97	13.90	15.26	15.99	15.54	13.97	11.26	8.63	6.70	5.98	6.37	7.97	10.25	12.66	14.44	278 8
269	15.38	15.04 13.48	11.07	8.36	6.38	5.47	5.87	7.36	9.62	12.14	14.54	16.28	16.98	16.37	13.80	10.49	7.50	5.61	5.14	5.74	7.77	10.54	13.45	15.71	279 9
270	16.85	16.30	14.16	10.84	7.77	5.85 5.66	5.97 5.66	7.50	9.87	12.74	15.25	16.92	17.15	15.62	12.54	8.66	5.94	4.14	3.96	5.28	7.85	11.15	14.38	16.70	280 10
271	17.32	16.33	13.48	9.84	7.20	5.47	4.98	5.96	7.74	10.58	13.66 16.26	17.40	16.86	14.56	10.89	7.40	4.72	3.37	3.98	5.86	8.86	12.43	15.47	17.34	281 11
272	17.64	16.26	12.76	9.26	6.56	5.24	5.38	6.54	8.77	11.76	14.62	16.82	17.12	15.72	12.71	9.14 6.06	3.77	3.17	4.42	6.67	9.72	13.44	16.25	17.55	282 12
273	17.22	15.06	11.70	8.40	6.26	5.44	6.06	7.47	10.01	12.74	15.12	16.37	16.06	14.21	11.04	7.42	4.80	3.12	3.62	5.30 8.04	11.13	14.40	16.50	17.22	283 13
274	16.16	13.58	10.36	7.77	6.24	6.04	6.91	8.53	10.52	13.06	15.02	15.64	14.36	11.93	8.64	6.01	4.31	3.47	4.52	6.20	8.94	11.94	14.56	16.24	284 13
275	16.32 14.74	12.13	9.47	7.47	6.58 7.80 9.14	6.90	7.84	9.30	11.26	13.26	14.41	14.26	12.74	10.35	7.88	5.80	4.44	4.58	5.92	7.85	10.30	12.70	14.67	15.54	285 14
276	15.01	13.36	11.14	9.11	7.80 7.42	7.74	8.64	10.04	11.80	13.04	13.64	13.06	11.36	9.07	7.14	5.84	5.47	6.20	7.44	9.04	10.97	13.06	14.36	14.36	286 15
277	13.40	11.82	10.44	9.16	8.44	8.24	8.54	9.26	10.30	11.46	12.22	11.46	10.00	8.37	7.08	6.36	6.44	7.32	8.34	9.60	11.24	12.72	13.46	13.28	287 16
278	12.32	11.06	10.10	9.27	8.97	8.94	9.08	9.61	10.14	11.01	11.52	11.46	10.73	9.52 8.47	7.66	7.41	7.56	8.04	8.76	9.91	11.17	12.30	12.88	12.66	288 17
279	11.92	11.04	10.37	9.76	9.36	9.12	9.08	9.27	9.86	10.44	10.68	10.66	10.30	9.78	9.22	8.56	8.06	7.74	8.02 8.86	10.06	11.16	12.02	12.40	13.34	289 18
280	12.06	11.48	10.82	9.97	9.24	8.77	8.68	8.96	9.55	10.22	10.70	10.88	10.82	10.57	10.03	9.26	8.44	7.90	8.07	8.80	9.84	10.90	11.78 12.36	12.58	290 19
281	12.54	12.07	11.12	9.97	8.90	8.23	8.12	8.56	9.27	10.10	10.90	11.50	11.78	11.53	10.67	9.30	8.14	7.56	7.77	8.55	9.74	11.07	12.15	12.94	291 19
282	13.28	13.04	12.24	10.77 9.14	7.88	7.18	7.36	8.12	9.26	10.62	11.94	12.78	12.88	12.06	10.48	8.86	7.70	7.28	7.65	8.65	10.02	11.54	12.81	13.77	292 20
283	14.04	13.50	12.16	10.00	8.34	6.96	6.50	6.88	7.96 9.76	11.52	13.07	13.96	13.77	12.48	10.52	8.76	7.36	6.77	7.26	8.52	10.36	12.17	13.66	14.56	293 21
284	14.48	13.40	11.12	8.84	6.87	5.64	5.46	6.30	8.06	10.30	12.80	14.34	15.00 14.16	12.26	9.96	7.92	6.50	6.22	7.10	8.82	10.86	13.12	14.54	15.07	294 22
285	14.56	12.60	9.98	7.47	5.46	4.56	4.96	6.60	9.03	11.80	14.15	15.84	15.96	14.52	12.00	9.24	7.24	6.16 6.40	7.67	9.66	11.93	14.14	15.62	15.76	295 28
286	14.36	11.76	8.61	6.02	4.24	3.86	5.14	7.32	10.15	13.10	15.67	16.78	16.26	14.16	11.00	8.32	6.36	5.84	6.47	8.16	10.16	12.84 15.02	16.10	15.46	297 0
Sum	1032.54	910.43	760.26	608.18	501.65	473.80	511.80	621.28	762.12	907.49	1021.76	1072.60	1060.31	924.04	744.15	591.06	495.43	460.89	511.58	610.72	763.36	946.14	1054.15	1072.91	No. of Days. 74 13 1/2
No.	74	74	75	75	74	74	74	75	75	74	74	74	76	75	74	74	75	75	75	74	74	76	75	74	18418.65

FORMS FOR SHORT-PERIOD TIDES.

SERIES M.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Hour		
287	13.88	9.87	6.84	4.45	3.04	3.57	5.44	8.15	11.37	14.60	16.81	17.35	16.28	13.64	10.44	7.71	6.07	5.84	6.88	8.87	11.47	14.12	15.94	16.22	288	0	
288	14.81	11.87	8.55	5.46	2.87	4.17	6.35	9.32	13.00	15.95	17.47	17.44	15.72	12.68	9.66	7.28	5.94	6.04	7.36	9.64	12.45	14.84	16.04	15.66	289	1	
289	13.70	10.52	7.15	4.66	2.91	3.10	7.47	10.55	13.92	16.35	17.36	16.74	14.57	11.67	8.85	6.76	5.94	6.28	7.70	9.92	12.68	14.78	15.58	14.78	800	2	
290	12.36	9.26	6.36	4.20	3.07	3.72	7.47	8.04	11.05	14.10	16.17	16.12	14.06	11.35	8.82	7.14	6.57	7.02	8.46	10.56	13.14	14.64	15.04	13.76	801	3	
291	11.47	8.74	6.42	4.70	4.22	5.00	6.80	9.02	11.88	14.60	16.14	16.22	15.16	13.26	10.86	8.86	7.58	7.14	7.44	8.84	10.92	12.84	13.84	13.86	12.57	802	4
292	10.68	8.54	6.84	5.56	5.27	5.98	7.33	9.36	11.72	14.00	15.22	15.38	14.58	12.88	11.01	9.42	8.12	7.64	7.92	8.94	11.85	13.84	13.12	13.26	803	5	
293	10.75	9.22	7.66	6.68	6.30	6.72	7.86	9.44	11.50	13.34	14.46	14.66	13.96	12.74	11.30	9.76	8.54	7.93	7.84	8.40	9.60	10.88	12.06	12.64	804	5	
294	12.40	10.10	8.76	7.68	7.01	7.06	7.90	9.22	10.74	12.56	13.72	14.38	14.04	13.04	11.45	9.76	8.15	7.22	7.02	7.48	8.84	10.32	11.48	12.55	805	6	
295	12.87	12.46	11.36	9.70	8.28	6.80	7.14	7.40	8.84	10.74	12.56	13.87	14.54	13.40	11.67	9.66	7.53	6.30	5.88	6.50	8.20	10.07	11.93	13.36	806	7	
296	14.04	13.66	12.30	10.26	8.61	7.37	6.86	7.24	8.35	10.36	12.62	14.13	14.96	13.80	11.64	9.03	6.96	5.44	5.04	5.86	7.79	10.12	12.66	14.54	807	8	
297	15.37	14.86	13.04	10.66	8.56	7.12	6.44	6.77	8.02	10.14	12.62	14.56	15.55	15.25	13.56	8.12	5.82	4.22	4.10	5.32	7.70	10.85	13.60	15.51	808	9	
298	16.05	15.06	12.86	10.40	8.16	6.53	5.96	6.51	8.24	10.85	13.27	15.16	15.84	15.03	12.98	9.78	7.04	4.71	3.86	5.46	8.44	11.74	14.64	16.50	809	10	
299	16.72	15.38	12.86	9.98	7.70	6.25	5.93	6.71	8.67	11.25	13.84	15.32	15.84	15.03	12.98	9.78	7.04	3.63	3.01	4.08	6.50	9.62	13.08	15.81	810	11	
300	16.72	14.87	12.03	9.20	7.26	6.32	6.37	7.46	9.60	12.20	14.35	15.67	15.28	13.15	10.15	7.00	4.47	3.03	3.22	5.03	7.60	10.76	14.05	16.38	811	11	
301	17.05	16.14	13.92	8.66	6.87	6.16	6.46	8.00	10.44	13.10	14.76	15.16	13.92	11.40	8.36	5.66	3.69	2.94	3.94	6.18	9.01	12.24	14.92	16.53	812	12	
302	16.56	15.16	12.66	10.06	7.96	6.74	6.60	7.35	9.00	13.43	14.50	14.36	12.66	9.94	7.20	4.97	3.56	3.77	5.34	7.72	10.56	13.46	15.64	16.34	813	13	
303	15.71	13.92	11.46	9.28	7.66	6.86	6.98	7.98	9.96	12.00	13.52	14.02	13.37	11.18	6.52	4.86	4.33	5.20	6.90	9.14	11.80	14.20	15.72	15.81	814	14	
304	14.66	12.72	10.71	8.96	7.82	7.56	7.92	9.16	10.68	13.24	13.26	13.26	12.06	10.17	8.00	6.25	5.31	5.50	8.34	10.52	12.80	14.44	15.18	14.68	815	15	
305	13.32	11.56	10.02	8.76	8.10	8.00	8.60	9.65	10.96	12.18	12.58	12.23	11.04	9.16	7.62	6.54	6.20	6.84	7.96	9.38	11.14	12.91	14.40	13.64	816	16	
306	12.97	10.90	9.58	8.78	8.46	8.68	9.38	10.00	10.94	11.57	11.80	11.36	10.28	8.94	7.84	7.18	7.20	7.86	8.80	9.98	11.46	12.86	13.86	13.83	817	16	
307	12.96	11.72	10.53	9.14	8.92	8.96	9.17	9.66	10.40	11.10	11.37	11.01	10.20	9.26	8.46	8.10	8.14	8.66	9.44	10.56	11.74	12.76	13.34	13.26	818	17	
308	12.61	11.72	10.86	9.76	9.04	8.80	8.85	9.64	10.14	10.74	11.18	11.32	11.06	10.38	9.58	8.94	8.71	8.90	9.50	10.42	11.46	12.48	13.10	13.15	819	18	
309	12.64	11.84	10.76	9.71	8.88	8.35	8.19	8.42	9.04	9.96	10.86	11.50	11.55	10.96	9.98	9.08	8.64	8.75	9.38	10.38	11.46	12.41	13.07	13.16	820	19	
310	12.84	11.84	10.56	9.24	8.13	7.50	7.43	7.86	8.83	10.03	11.16	12.23	12.80	12.64	11.66	10.25	8.36	8.34	8.96	10.02	11.20	12.46	13.23	13.47	821	20	
311	13.00	11.72	10.14	8.38	7.03	6.27	6.31	7.08	8.52	10.23	11.92	13.17	13.63	13.10	11.86	10.18	8.76	7.98	7.96	8.75	10.13	13.14	13.94	13.94	822	21	
312	13.04	11.34	9.30	7.45	5.86	5.13	5.46	6.76	8.80	11.15	13.20	14.66	14.98	13.87	11.76	9.58	8.10	7.27	7.36	8.22	9.82	11.76	13.33	14.28	823	21	
313	14.14	12.87	7.98	5.77	4.14	3.74	4.67	6.71	9.27	12.02	14.40	15.66	15.44	13.71	11.16	8.74	7.02	6.40	6.78	8.22	10.37	12.25	13.88	14.74	824	22	
314	14.20	12.26	9.36	6.51	4.12	2.75	4.56	7.03	10.05	13.27	15.65	16.62	15.90	13.76	10.86	8.17	6.45	5.84	6.36	8.12	10.44	12.84	14.46	15.08	825	23	
315	13.97	11.41	8.07	4.96	2.57	1.63	2.58	4.74	7.64	11.12	14.22	17.07	15.75	12.96	9.86	7.26	5.65	5.46	6.24	8.40	11.20	13.57	15.11	15.17	827	0	
316	13.27	9.96	6.40	3.62	1.66	2.20	3.26	6.02	9.25	12.97	15.66	17.40	17.25	13.37	11.30	8.50	6.32	5.63	6.88	9.32	12.22	14.44	15.50	14.80	828	1	
317	12.31	8.84	5.46	3.00	1.66	2.20	4.15	6.95	10.46	13.81	16.44	17.54	16.82	14.56	11.38	8.50	6.32	5.44	5.74	7.26	12.76	14.67	15.26	14.06	829	2	
318	11.32	8.05	5.16	2.94	2.16	3.11	5.16	7.96	11.23	14.30	16.57	17.22	16.23	13.81	10.68	8.07	6.16	5.50	5.88	7.64	10.55	12.77	14.29	14.72	830	3	
319	10.74	7.81	5.32	3.06	3.26	4.42	6.34	8.86	11.67	14.58	16.33	16.57	15.28	12.84	9.93	7.47	6.23	5.72	6.26	7.94	10.30	12.38	13.76	13.96	831	3	
320	12.68	10.56	8.18	6.28	4.83	5.73	7.34	9.38	12.05	14.37	15.76	15.80	14.56	12.28	9.94	8.13	6.64	6.14	6.54	8.04	10.04	11.78	12.86	13.16	832	4	
321	12.74	10.73	8.96	7.20	6.24	5.96	6.50	7.80	9.84	13.88	14.87	14.84	13.77	11.77	10.06	8.23	6.86	6.34	6.56	7.70	9.30	10.84	12.16	12.76	833	5	



FORMS FOR SHORT-PERIOD TIDES.  
BOMBAY—Commencing 0 hours, Astronomical Time, 1st January, 1885.

SERIES O.

Motion per mean Solar hour = 13° 9' 43.856".

Argument ( $\gamma - 2\sigma$ ).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour		
1	15.52	12.96	9.13	5.66	3.03	1.68	2.28	7.90	11.70	15.50	18.00	18.85	18.08	15.14	11.54	8.50	6.21	5.53	6.08	8.20	14.16	16.06	16.66	15.40	2	1	
2	12.16	8.40	4.86	2.56	1.71	2.90	5.56	8.82	12.94	18.58	18.97	17.06	14.24	10.56	7.53	5.57	5.16	6.10	8.63	11.84	14.68	16.63	16.96	11.92	3	3	
3	8.00	4.87	2.80	2.57	4.24	6.84	10.20	14.07	17.26	18.86	18.84	13.20	9.77	6.90	5.23	4.96	6.16	8.86	12.14	14.87	16.40	16.40	14.28	11.00	4	4	
4	7.61	3.55	3.86	5.55	8.01	11.36	14.83	17.16	18.38	17.93	15.80	12.16	8.68	6.10	5.23	6.68	9.24	12.28	14.51	15.96	15.58	13.48	10.47	7.54	5	6	
5	5.76	5.97	7.23	9.17	12.11	15.02	17.02	17.55	16.63	14.11	10.96	8.16	6.22	5.47	5.84	7.18	9.67	14.04	15.00	14.45	12.62	10.24	8.07	7.04	6	8	
6	6.84	7.54	8.67	10.60	12.84	16.36	18.36	15.24	12.76	10.11	8.00	6.64	6.17	6.55	7.86	9.76	11.80	13.27	13.64	12.22	10.47	9.05	8.44	8.46	7	10	
7	9.03	9.97	11.20	13.05	14.64	15.46	15.18	13.87	9.76	8.10	7.16	7.03	7.40	8.29	9.82	11.16	12.48	12.66	12.27	11.60	10.93	10.34	9.98	10.17	8	12	
8	10.60	11.70	12.96	14.02	14.44	13.75	12.27	10.82	9.20	7.93	7.24	7.34	8.07	9.14	10.55	11.74	12.48	12.66	12.27	11.24	10.48	10.12	10.05	10.23	9	14	
9	11.07	12.14	13.06	13.36	12.72	11.71	10.43	9.14	7.97	7.14	6.75	6.94	7.74	10.26	11.64	12.67	13.14	12.97	12.20	11.24	10.27	9.77	9.62	10.44	10	15	
10	10.84	11.64	12.68	12.37	11.53	10.42	8.97	7.80	6.96	6.38	6.44	7.28	8.13	10.47	12.14	13.84	13.63	12.58	11.38	10.27	9.32	9.14	9.46	10.37	11	17	
11	11.24	11.97	12.52	12.50	10.54	11.87	8.76	7.34	6.16	5.74	6.34	7.62	8.54	11.46	13.22	14.24	14.58	13.94	12.72	11.24	10.02	9.46	10.37	11.44	12	19	
12	12.46	13.04	12.84	11.88	10.23	9.20	5.62	5.56	6.50	8.14	10.17	12.34	14.10	15.20	15.17	13.97	12.27	10.58	9.35	8.75	9.26	10.34	11.68	12.96	13	21	
13	13.64	13.36	11.80	9.66	7.32	5.82	5.14	5.44	8.86	11.26	13.66	15.38	15.87	15.24	13.66	11.54	9.82	8.71	8.16	8.36	9.30	10.74	12.46	13.98	14	23	
14	13.00	10.84	8.24	6.20	4.76	4.46	5.40	7.36	9.78	12.57	14.82	16.13	14.56	12.25	10.05	8.46	7.82	7.74	8.41	9.71	11.76	13.30	14.26	14.09	15	0	
15	12.44	7.00	5.12	4.20	4.63	6.12	8.44	11.24	14.04	15.74	16.36	15.71	13.82	11.22	7.54	6.94	7.15	8.40	10.27	12.44	14.06	14.68	13.84	11.50	16	2	
16	8.60	5.94	4.02	4.37	5.06	7.26	9.66	12.72	15.20	16.55	15.27	12.77	9.97	7.86	6.84	7.56	8.32	11.40	13.55	14.80	14.78	13.22	10.43	7.48	17	4	
17	5.34	4.30	4.66	6.35	8.54	14.15	16.45	16.88	16.08	14.04	11.02	8.54	6.76	6.12	6.34	7.60	9.84	12.14	14.06	14.14	12.06	9.06	6.46	4.67	18	6	
18	4.24	5.16	7.15	9.68	12.56	14.87	16.44	15.00	12.42	9.50	7.22	5.80	5.43	6.26	8.16	10.65	12.88	14.28	14.56	13.33	10.92	6.04	4.87	5.06	19	8	
19	6.54	8.66	11.04	13.64	15.62	16.36	15.76	13.82	11.00	8.37	5.54	5.64	6.83	8.93	11.40	13.32	14.42	14.25	12.47	10.10	7.91	6.34	5.70	6.30	20	10	
20	9.76	12.17	14.36	15.74	15.96	14.86	12.76	10.13	7.78	6.17	5.70	6.11	7.62	11.76	13.35	14.14	13.72	12.06	9.94	8.32	7.22	7.01	7.74	8.97	21	11	
21	10.80	12.97	15.50	15.17	13.80	11.46	9.14	7.34	6.17	6.00	6.68	8.02	9.76	11.65	13.02	13.34	12.14	10.65	9.07	8.15	8.14	8.68	9.86	11.56	22	13	
22	13.36	14.56	15.02	14.37	10.76	8.71	6.96	6.23	6.09	6.68	7.86	9.46	11.24	12.66	13.36	13.34	12.38	9.94	9.11	8.88	9.28	10.22	11.70	13.06	23	15	
23	14.14	14.41	13.60	12.06	10.26	8.46	7.00	6.08	6.36	7.64	9.14	10.84	12.34	13.44	13.81	13.33	12.18	10.75	9.76	9.24	10.07	11.16	12.40	13.38	24	17	
24	13.66	13.03	11.87	10.24	8.47	7.00	5.83	5.58	6.78	8.55	10.33	12.22	13.56	14.30	14.16	13.05	11.56	10.06	9.11	8.87	9.40	10.46	12.94	13.44	25	19	
25	13.33	12.40	10.74	8.86	6.83	5.22	4.41	4.77	6.10	8.10	10.50	14.53	15.56	15.33	13.76	11.64	9.52	8.28	7.92	8.25	9.53	11.24	12.70	13.80	26	20	
26	14.14	11.34	8.72	6.20	4.24	3.38	3.76	5.30	7.76	10.55	13.50	15.72	16.74	16.12	11.40	8.83	7.24	6.86	7.53	9.20	11.11	12.97	14.55	15.08	27	22	
27	14.17	11.84	8.82	5.70	3.60	2.56	3.06	5.04	7.88	11.48	17.04	17.86	17.00	14.36	10.96	6.27	5.77	6.57	8.62	11.25	13.92	15.74	16.28	14.96	28	0	
28	12.18	8.44	5.42	3.22	2.16	3.97	5.52	8.75	12.46	16.01	18.47	17.26	13.80	10.14	7.09	5.27	5.02	6.02	8.40	11.85	14.65	16.52	16.84	15.28	11.68	31	2
29	7.88	4.80	2.74	2.38	4.00	6.66	10.10	13.98	18.64	18.38	16.30	12.42	8.97	6.01	4.46	4.57	6.12	9.14	12.56	15.46	16.86	14.76	11.06	7.36	32	4	
30	4.34	2.72	2.99	4.86	7.74	11.40	14.94	17.54	18.47	17.66	11.08	7.54	5.01	3.93	4.32	6.55	9.62	13.04	15.80	16.84	16.08	13.73	6.82	6.90	33	6	
31	3.58	4.44	6.36	9.36	12.84	15.86	17.74	17.94	16.48	13.27	9.84	6.84	4.33	5.26	7.44	10.66	13.70	15.74	16.43	15.42	12.82	9.66	6.56	6.94	34	7	
32	5.14	8.06	10.66	13.66	16.02	17.12	16.74	14.88	11.68	8.76	6.34	4.92	4.74	5.86	11.07	13.00	15.16	15.34	14.06	11.68	9.04	7.34	6.56	6.94	35	9	
33	8.04	9.56	11.76	14.24	16.04	15.34	13.02	10.16	7.86	6.27	5.54	5.86	7.18	9.07	11.36	13.26	14.34	12.88	11.00	9.39	8.26	7.92	8.30	9.05	36	11	
34	10.36	12.08	13.76	14.66	14.44	13.11	11.12	7.54	6.26	6.13	6.68	7.86	9.28	10.86	12.27	13.10	12.94	11.94	10.66	9.72	9.06	9.26	9.66	10.60	37	13	
35	11.82	12.86	13.34	12.82	11.45	10.03	8.74	7.48	6.78	7.17	7.94	9.95	10.30	11.34	11.97	11.92	11.42	10.84	10.34	10.07	9.97	9.24	10.44	11.37	38	15	

36	12.06	12.26	12.46	12.66	12.86	13.06	13.26	13.46	13.66	13.86	14.06	14.26	14.46	14.66	14.86	15.06	15.26	15.46	15.66	15.86	16.06	16.26	16.46	16.66	16.86	17.06	17.26	17.46	17.66	17.86	18.06	39	16			
37	11.27	11.47	11.67	11.87	12.07	12.27	12.47	12.67	12.87	13.07	13.27	13.47	13.67	13.87	14.07	14.27	14.47	14.67	14.87	15.07	15.27	15.47	15.67	15.87	16.07	16.27	16.47	16.67	16.87	17.07	17.27	17.47	17.67	17.87	40	18
38	11.36	11.56	11.76	11.96	12.16	12.36	12.56	12.76	12.96	13.16	13.36	13.56	13.76	13.96	14.16	14.36	14.56	14.76	14.96	15.16	15.36	15.56	15.76	15.96	16.16	16.36	16.56	16.76	16.96	17.16	17.36	17.56	17.76	17.96	41	20
39	11.66	11.86	12.06	12.26	12.46	12.66	12.86	13.06	13.26	13.46	13.66	13.86	14.06	14.26	14.46	14.66	14.86	15.06	15.26	15.46	15.66	15.86	16.06	16.26	16.46	16.66	16.86	17.06	17.26	17.46	17.66	17.86	18.06	42	22	
40	12.07	12.27	12.47	12.67	12.87	13.07	13.27	13.47	13.67	13.87	14.07	14.27	14.47	14.67	14.87	15.07	15.27	15.47	15.67	15.87	16.07	16.27	16.47	16.67	16.87	17.07	17.27	17.47	17.67	17.87	18.07	43	0			
41	10.24	10.44	10.64	10.84	11.04	11.24	11.44	11.64	11.84	12.04	12.24	12.44	12.64	12.84	13.04	13.24	13.44	13.64	13.84	14.04	14.24	14.44	14.64	14.84	15.04	15.24	15.44	15.64	15.84	16.04	16.24	16.44	16.64	16.84	44	2
42	6.54	6.74	6.94	7.14	7.34	7.54	7.74	7.94	8.14	8.34	8.54	8.74	8.94	9.14	9.34	9.54	9.74	9.94	10.14	10.34	10.54	10.74	10.94	11.14	11.34	11.54	11.74	11.94	12.14	12.34	12.54	12.74	12.94	13.14	45	3
43	5.57	5.77	5.97	6.17	6.37	6.57	6.77	6.97	7.17	7.37	7.57	7.77	7.97	8.17	8.37	8.57	8.77	8.97	9.17	9.37	9.57	9.77	9.97	10.17	10.37	10.57	10.77	10.97	11.17	11.37	11.57	11.77	11.97	12.17	46	5
44	3.92	4.12	4.32	4.52	4.72	4.92	5.12	5.32	5.52	5.72	5.92	6.12	6.32	6.52	6.72	6.92	7.12	7.32	7.52	7.72	7.92	8.12	8.32	8.52	8.72	8.92	9.12	9.32	9.52	9.72	9.92	10.12	10.32	10.52	47	7
45	5.52	5.72	5.92	6.12	6.32	6.52	6.72	6.92	7.12	7.32	7.52	7.72	7.92	8.12	8.32	8.52	8.72	8.92	9.12	9.32	9.52	9.72	9.92	10.12	10.32	10.52	10.72	10.92	11.12	11.32	11.52	11.72	11.92	12.12	48	9
46	9.14	9.34	9.54	9.74	9.94	10.14	10.34	10.54	10.74	10.94	11.14	11.34	11.54	11.74	11.94	12.14	12.34	12.54	12.74	12.94	13.14	13.34	13.54	13.74	13.94	14.14	14.34	14.54	14.74	14.94	15.14	15.34	15.54	15.74	49	11
47	13.32	13.52	13.72	13.92	14.12	14.32	14.52	14.72	14.92	15.12	15.32	15.52	15.72	15.92	16.12	16.32	16.52	16.72	16.92	17.12	17.32	17.52	17.72	17.92	18.12	18.32	18.52	18.72	18.92	19.12	19.32	19.52	19.72	19.92	50	13
48	15.08	15.28	15.48	15.68	15.88	16.08	16.28	16.48	16.68	16.88	17.08	17.28	17.48	17.68	17.88	18.08	18.28	18.48	18.68	18.88	19.08	19.28	19.48	19.68	19.88	20.08	20.28	20.48	20.68	20.88	21.08	21.28	21.48	21.68	51	15
49	14.16	14.36	14.56	14.76	14.96	15.16	15.36	15.56	15.76	15.96	16.16	16.36	16.56	16.76	16.96	17.16	17.36	17.56	17.76	17.96	18.16	18.36	18.56	18.76	18.96	19.16	19.36	19.56	19.76	19.96	20.16	20.36	20.56	20.76	52	16
50	13.06	13.26	13.46	13.66	13.86	14.06	14.26	14.46	14.66	14.86	15.06	15.26	15.46	15.66	15.86	16.06	16.26	16.46	16.66	16.86	17.06	17.26	17.46	17.66	17.86	18.06	18.26	18.46	18.66	18.86	19.06	19.26	19.46	19.66	53	18
51	11.70	11.90	12.10	12.30	12.50	12.70	12.90	13.10	13.30	13.50	13.70	13.90	14.10	14.30	14.50	14.70	14.90	15.10	15.30	15.50	15.70	15.90	16.10	16.30	16.50	16.70	16.90	17.10	17.30	17.50	17.70	17.90	18.10	18.30	54	20
52	11.27	11.47	11.67	11.87	12.07	12.27	12.47	12.67	12.87	13.07	13.27	13.47	13.67	13.87	14.07	14.27	14.47	14.67	14.87	15.07	15.27	15.47	15.67	15.87	16.07	16.27	16.47	16.67	16.87	17.07	17.27	17.47	17.67	17.87	55	22
53	10.86	11.06	11.26	11.46	11.66	11.86	12.06	12.26	12.46	12.66	12.86	13.06	13.26	13.46	13.66	13.86	14.06	14.26	14.46	14.66	14.86	15.06	15.26	15.46	15.66	15.86	16.06	16.26	16.46	16.66	16.86	17.06	17.26	17.46	56	24
54	8.84	9.04	9.24	9.44	9.64	9.84	10.04	10.24	10.44	10.64	10.84	11.04	11.24	11.44	11.64	11.84	12.04	12.24	12.44	12.64	12.84	13.04	13.24	13.44	13.64	13.84	14.04	14.24	14.44	14.64	14.84	15.04	15.24	15.44	57	26
55	8.26	8.46	8.66	8.86	9.06	9.26	9.46	9.66	9.86	10.06	10.26	10.46	10.66	10.86	11.06	11.26	11.46	11.66	11.86	12.06	12.26	12.46	12.66	12.86	13.06	13.26	13.46	13.66	13.86	14.06	14.26	14.46	14.66	14.86	58	28
56	4.94	5.14	5.34	5.54	5.74	5.94	6.14	6.34	6.54	6.74	6.94	7.14	7.34	7.54	7.74	7.94	8.14	8.34	8.54	8.74	8.94	9.14	9.34	9.54	9.74	9.94	10.14	10.34	10.54	10.74	10.94	11.14	11.34	11.54	59	30
57	3.37	3.57	3.77	3.97	4.17	4.37	4.57	4.77	4.97	5.17	5.37	5.57	5.77	5.97	6.17	6.37	6.57	6.77	6.97	7.17	7.37	7.57	7.77	7.97	8.17	8.37	8.57	8.77	8.97	9.17	9.37	9.57	9.77	60	32	
58	5.26	5.46	5.66	5.86	6.06	6.26	6.46	6.66	6.86	7.06	7.26	7.46	7.66	7.86	8.06	8.26	8.46	8.66	8.86	9.06	9.26	9.46	9.66	9.86	10.06	10.26	10.46	10.66	10.86	11.06	11.26	11.46	11.66	11.86	61	34
59	8.86	9.06	9.26	9.46	9.66	9.86	10.06	10.26	10.46	10.66	10.86	11.06	11.26	11.46	11.66	11.86	12.06	12.26	12.46	12.66	12.86	13.06	13.26	13.46	13.66	13.86	14.06	14.26	14.46	14.66	14.86	15.06	15.26	15.46	62	36
60	10.22	10.42	10.62	10.82	11.02	11.22	11.42	11.62	11.82	12.02	12.22	12.42	12.62	12.82	13.02	13.22	13.42	13.62	13.82	14.02	14.22	14.42	14.62	14.82	15.02	15.22	15.42	15.62	15.82	16.02	16.22	16.42	16.62	16.82	63	38
61	12.96	13.16	13.36	13.56	13.76	13.96	14.16	14.36	14.56	14.76	14.96	15.16	15.36	15.56	15.76	15.96	16.16	16.36	16.56	16.76	16.96	17.16	17.36	17.56	17.76	17.96	18.16	18.36	18.56	18.76	18.96	19.16	19.36	19.56	64	40
62	13.07	13.27	13.47	13.67	13.87	14.07	14.27	14.47	14.67	14.87	15.07	15.27	15.47	15.67	15.87	16.07	16.27	16.47	16.67	16.87	17.07	17.27	17.47	17.67	17.87	18.07	18.27	18.47	18.67	18.87	19.07	19.27	19.47	19.67	65	42
63	12.24	12.44	12.64	12.84	13.04	13.24	13.44	13.64	13.84	14.04	14.24	14.44	14.64	14.84	15.04	15.24	15.44	15.64	15.84	16.04	16.24	16.44	16.64	16.84	17.04	17.24	17.44	17.64	17.84	18.04	18.24	18.44	18.64	18.84	66	44
64	10.86	11.06	11.26	11.46	11.66	11.86	12.06	12.26	12.46	12.66	12.86	13.06	13.26	13.46	13.66	13.86	14.06	14.26	14.46	14.66	14.86	15.06	15.26	15.46	15.66	15.86	16.06	16.26	16.46	16.66	16.86	17.06	17.26	17.46	67	46
65	10.78	10.98	11.18	11.38	11.58	11.78	11.98	12.18	12.38	12.58	12.78	12.98	13.18	13.38	13.58	13.78	13.98	14.18	14.38	14.58	14.78	14.98	15.18	15.38	15.58	15.78	15.98	16.18	16.38	16.58	16.78	16.98	17.18	17.38	68	48
66	11.14	11.34	11.54	11.74	11.94	12.14	12.34	12.54	12.74	12.94	13.14	13.34	13.54	13.74	13.94	14.14	14.34	14.54	14.74	14.94	15.14	15.34	15.54	15.74	15.94	16.14	16.34	16.54	16.74	16.94	17.14	17.34	17.54	17.74	69	50
67	9.92	10.12	10.32	10.52	10.72	10.92	11.12	11.32	11.52	11.72	11.92	12.12	12.32	12.52	12.72	12.92	13.12	13.32	13.52	13.72	13.92	14.12	14.32	14.52	14.72	14.92	15.12	15.32	15.52	15.72	15.92	16.12	16.32	16.52	70	52
68	7.27	7.47	7.67	7.87	8.07	8.27	8.47	8.67	8.87	9.07	9.27	9.47	9.67	9.87	10.07	10.27	10.47	10.67	10.87	11.07	11.27	11.47	11.67	11.87	12.07	12.27	12.47	12.67	12.87	13.07	13.27	13.47	13.67	71	54	
69	5.16	5.36	5.56	5.76	5.96	6.16	6.36	6.56	6.76	6.96	7.16	7.36	7.56	7.76	7.96	8.16	8.36	8.56	8.76	8.96	9.16	9.36	9.56	9.76	9.96	10.16	10.36	10.56	10.76	10.96	11.16	11.36	11.56	11.76	72	56
Sum	745.01	691.67	695.23	687.13	680.95	730.71	722.78	789.33	788.74	80																										

FORMS FOR SHORT-PERIOD TIDES.

SERIES O.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
70	4'96	6'46	8'94	11'85	14'34	16'00	16'06	14'53	11'64	8'54	5'76	4'22	3'97 5'24	7'30	10'10	13'02	15'04	16'00	15'20	12'86	9'54	6'67	4'92	4'38	76 6	
71	5'52	7'55	10'33	13'50	15'75	16'73	16'07	13'66	10'42	7'22	4'92	3'64	4'00	5'66	8'33	11'52	14'30 16'06	16'52	15'06	12'13	8'73	6'13	4'66	4'99	6'52	77 8
72	8'92	11'86	14'66	16'40	16'56	15'07	11'90	8'47	5'62	3'74	3'22	4'26	6'60	9'60	12'85	15'23	16'56	16'25	14'26 10'83	8'00	5'75	5'11	5'88	7'84	10'46	78 10
73	13'38	15'68	16'60	15'80	13'36	10'12	7'06	4'83	3'54	3'76	5'34	7'86	11'00	13'93	15'92	16'74	15'74	13'36	10'24	7'64	6'12 6'08	7'14	9'00	11'56	13'90	79 12
74	15'66	15'98	14'76	12'06	8'90	6'13	4'34	3'62	4'36	6'06	8'47	11'31	13'87	15'62	16'12	14'97	12'74	10'02	8'05	6'96	7'06	7'93	9'67	12'07 14'08	15'23	80 14
75	15'08	13'57	11'16	8'26	6'08	4'76	4'47	5'46	7'26	9'48	11'88	13'90 15'36	15'50	14'66	12'67	10'54	8'74	7'94	8'14	9'06	10'62	12'40	13'77	14'52	81 15	
76	14'20 12'80	10'64	8'47	6'76	5'86	5'82	6'49	7'75	9'52	11'71	13'54	14'73	14'90	14'06 12'63	11'05	9'70	8'86	8'72	9'12	10'24	11'76	13'06	13'60	13'34	82 17	
77	12'06	10'56	8'92	7'40	6'30	6'68	7'68	9'46	11'24	13'02	14'08	14'52	14'22	13'04	11'70	10'34	9'24 8'84	9'04	9'84	10'96	12'05	12'86	12'96	12'44	83 19	
78	11'22	9'67	8'30	7'06	6'48	6'64 7'48	8'86	10'64	12'34	13'74	14'48	14'44	13'62	12'12	10'36	8'96	8'11	7'96	8'44 9'76	11'26	12'36	12'92	12'78	11'94	84 21	
79	10'50	8'78	7'20	6'06	5'92	6'72	8'34	10'26 12'20	13'86	15'00	15'14	14'16	12'20	9'88	8'00	6'90	6'56	7'46	9'22	11'16	12'56 13'57	14'06	13'37	11'72	85 23	
80	9'38	7'17	5'72	5'38	6'17	7'82	10'00	12'50	14'54	15'84	15'94 14'64	12'14	9'36	6'97	5'74	5'63	6'67	8'88	11'24	13'46	14'86	15'36	14'34	12'05 9'44	87 1	
81	6'93	5'38	5'00	5'82	7'83	10'50	13'30	15'60	16'72	16'28	14'37	11'37	8'36 6'00	4'67	4'80	6'40	9'20	12'06	14'62	16'12	16'16	14'90	12'22	9'12	88 2	
82	6'60	5'05 4'86	5'87	8'10	11'14	14'15	16'35	17'15	16'24	13'58	10'14	7'06	4'83	3'96	4'70 6'72	9'92	13'20	15'64	17'04	16'75	14'92	11'81	8'56	6'27	89 4	
83	5'14	5'64	6'94	9'43	12'61 15'44	17'03	17'08	15'36	11'92	8'64	6'18	4'48	4'25	5'24	7'57	11'00	14'10	16'43 17'34	16'56	14'28	10'82	7'84	5'95	5'42	90 6	
84	6'12	7'87	10'62	13'66	16'10	17'14	16'46 13'96	10'44	7'12	4'80	3'83	4'41	6'43	8'78	12'04	14'74	16'66	17'13	15'64	12'86 9'53	7'16	5'81	5'93	7'22	91 8	
85	9'26	12'02	14'66	16'44	16'67	15'06	12'02	8'56	5'84 4'04	3'84	4'93	7'24	10'09	13'22	15'56	16'90	16'56	14'74	11'68	8'84	7'02	6'48	7'04 8'26	10'50	92 10	
86	13'00	14'94	15'83	15'12	12'94	9'87	7'14	5'16	4'22	4'76	6'40	8'73 11'37	14'00	15'82	16'34	15'34	13'10	10'40	8'36	7'32	7'28	8'03	9'50	11'53	93 11	
87	13'48 14'74	14'92	13'67	11'34	8'76	6'67	5'40	5'22	6'16	7'85	9'97	12'30	14'30	15'48 15'46	14'27	12'24	10'20	8'78	8'26	8'47	9'24	10'52	12'04	13'48	94 13	
88	14'16	13'84	12'27 10'16	8'14	6'47	5'74	6'22	7'44	9'20	10'85	12'64	14'50	14'67	14'27	12'97	11'44	10'04 9'16	8'84	9'16	9'84	10'95	11'06	12'80	12'96	95 15	
89	12'28	10'94	9'24	7'80	6'78	6'70 7'30	8'37	9'54	10'90	12'34	13'52	13'80	13'26	12'13	10'96	10'04	9'60	9'33	9'54 9'90	10'56	11'44	11'92	12'05	11'54	96 17	
90	10'36	9'16	8'12	7'47	7'44	7'87	8'52	9'46 10'73	11'93	12'74	12'98	12'60	11'86	11'07	10'34	9'94	9'77	9'87	10'02	10'36	10'81 11'14	11'27	10'92	10'30	97 19	
91	9'34	8'36	7'74	7'58	7'98	8'76	9'87	11'04	11'96	12'50	12'66 12'42	11'96	11'34	10'55	9'91	9'47	9'34	9'52	9'94	10'53	10'94	11'12	11'02	10'62 10'00	98 21	
92	9'22	8'40	8'01	8'13	8'63	9'70	10'66	11'77	12'66	13'06	12'94	12'40	11'47 10'50	9'62	8'94	8'54	8'74	9'48	10'45	11'36	11'88	11'89	11'44	10'50	99 22	
93	9'40	8'46 7'84	7'76	8'43	9'46	10'86	12'30	13'36	13'82	13'66	12'66	11'42	10'02	8'72	7'96 7'82	8'36	9'47	10'86	11'90	12'70	12'87	12'44	11'06	9'52	101 0	
94	8'12	7'40	7'47	9'54	11'08	12'70	14'06	14'56	14'22	12'80	10'96	8'88	7'46	6'81	6'84	7'92	9'62	11'52 13'00	13'97	14'12	13'00	11'02	9'05	7'48	102 2	
95	6'74	6'92	7'97	9'72	11'72	13'58	14'86 15'12	14'21	12'35	9'67	7'47	5'98	5'58	6'14	7'76	9'84	12'16	14'02	15'18	15'06 13'40	10'95	8'28	6'66	6'02	103 4	
96	6'46	7'88	10'06	12'53	14'55	15'72	15'49	13'80	11'08 8'22	5'93	4'52	4'32	5'47	7'72	10'54	13'27	15'36	16'20	15'32	13'00	9'88	7'34 5'76	5'40	6'24	104 6	
97	8'22	10'70	13'40	15'52	16'25	15'36	12'80	9'46	6'56	4'47	3'42	3'91 5'74	8'31	11'40	14'40	16'28	16'72	15'47	12'68	9'44	6'81	5'47	5'38	6'52	105 7	
98	8'91 11'80	14'40	15'97	16'08	14'35	11'30	7'80	4'97	2'93	2'46	3'76	6'21	9'51	12'97 15'58	17'14	17'04	14'94	11'68	8'36	6'14	5'06	5'57	7'24	10'07	106 9	
99	13'10	15'40	16'44 15'82	13'44	9'74	6'67	4'03	2'50	2'77	4'44	7'50	10'96	14'33	16'70	17'72	16'91 14'37	10'87	8'10	6'15	5'71	6'50	8'36	11'33	14'12	107 11	
100	15'97	16'50	15'10	12'22	8'67	5'24 3'17	2'56	3'47	5'74	8'64	12'02	15'12	16'94	17'54	16'24	13'40	10'32	7'62	6'17 6'07	7'04	9'13	12'00	14'47	15'69	108 13	
101	15'54	13'66	10'74	7'44	4'88	3'28	3'04	4'36 6'67	9'40	12'47	15'00	16'74	16'94	15'60	13'03	10'01	7'87	6'76	6'80	7'71	9'70 12'14	14'15	15'02	14'50	109 15	
102	12'53	9'92	7'24	5'36	4'17	4'16	5'20	7'26	9'89	12'40 14'37	15'77	15'74	14'47	12'12	9'90	8'07	7'14	7'11	7'83	9'54	11'58	13'16	13'74	11'76	110 17	
103	9'56	7'60	5'96	4'93	5'02	5'86	7'52	9'74	12'00	13'87	14'87	14'77	13'76 12'06	10'26	8'74	7'82	7'54	8'00	9'34	11'00	12'36	12'96	12'72	11'58	111 18	
104	10'14	8'48 6'94	6'06	5'96	6'60	7'87	9'72	11'62	13'34	14'34	14'44	13'66	12'26	10'62	8'03	7'66	7'76	8'68	10'20	11'63	12'43	12'66	12'50	10'96	112 20	

105	9'47	8'14	7'03	6'54 6'88	7'94	9'57	11'42	13'00	14'07	14'44	13'93	12'76	11'00	9'18	7'74	6'96	6'96 7'85	9'40	10'96	12'36	13'06	13'17	12'22	10'65	113 22	
106	8'87	7'52	6'74	6'84	7'66	9'26	11'04 12'88	14'12	14'66	14'30	12'64	10'64	8'60	6'78	5'94	5'93	7'08	9'00	11'04	12'64 13'72	13'87	12'97	11'36	9'32	115 0	
107	7'66	6'62	6'47	7'28	8'88	10'96	12'96	14'54	15'17 14'54	12'77	10'22	7'74	5'76	4'88	5'14	6'58	8'88	11'33	13'36	14'66	14'94	13'86 11'70	9'34	7'26	116 2	
108	6'22	6'20	7'24	9'00	11'22	13'36	14'86	15'37	14'44	12'10	9'16 6'48	4'70	4'20	4'74	6'70	9'17	11'77	14'02	15'57	15'54	14'03	11'54	8'80	6'96	117 3	
109	6'07 6'34	7'48	9'44	11'96	14'10	15'48	15'44	13'84	10'92	7'66	5'31	3'77	3'70	5'12 7'30	10'10	12'94	15'14	16'26	15'76	13'86	11'00	8'24	6'47	5'97	118 5	
110	6'54	7'98	10'26 13'70	14'64	15'66	14'96	12'70	9'46	6'57	4'32	3'42	4'04	5'80	8'48	11'42	14'32 16'17	16'57	15'46	12'94	10'06	7'64	6'36	6'16	6'82	119 7	
111	8'40	10'90	13'45	15'07	15'35 13'81	11'00	7'70	5'15	3'44	3'36	4'67	6'96	9'52	12'56	14'92	16'36	16'28	14'70	11'93 9'06	7'20	6'40	6'70	7'74	9'37	120 9	
112	11'47	13'86	15'04	15'06	12'96	9'73	7'17	4'24 3'42	4'04	5'68	8'27	10'68	13'46	15'48	16'25	15'62	13'50	10'52	8'22	6'72	7'02	8'34	10'44	12'60	121 11	
113	14'08	14'45	13'26	10'82	7'87	5'57	3'94	3'86	4'88	6'80 9'18	11'76	14'24	15'56	15'54	14'30	11'86	9'46	7'76	6'94	7'06	7'86	9'36	11'24 13'06	13'96	122 13	
114	13'66	11'90	9'20	6'72	5'07	4'36	4'90	6'32	8'22	10'36	12'80	14'56	15'43 14'76	13'04	10'84	8'96	7'76	7'44	7'76	8'80	10'26	11'94	13'06	13'30	123 14	
115	12'28	10'40 8'28	6'46	5'35	5'20	6'00	7'54	9'26	11'42	13'34	14'60	14'86	13'86	12'06	10'14 8'84	8'15	8'06	8'40	9'36	10'62	11'94	12'68	12'46	11'36	124 16	
116	9'58	7'94	6'74	6'04 6'20	7'12	8'46	10'24	12'10	13'38	14'08	13'92	12'90	11'41	10'00	8'90	8'46	8'56 9'00	9'74	10'55	11'36	11'86	11'68	10'72	9'26	125 18	
117	7'86	6'96	6'92	7'44	8'22	9'26	10'47 12'10	13'34	13'78	13'40	12'16	10'87	9'94	9'24	8'96	8'94	9'17	9'58	10'34	10'96 11'44	11'34	10'58	9'56	8'46	126 20	
118	7'76	7'66	7'97	8'66	9'74	10'97	12'22	13'24	13'54 13'24	12'12	10'96	9'98	9'27	8'94	8'74	8'80	9'24	10'03	10'80	11'26	11'29	10'79 10'06	9'26	8'46	127 22	
119	8'06	8'04	8'56	9'72	10'94	12'20	12'96	13'22	12'94	12'14	11'17 9'96	8'96	8'20	7'92	8'00	8'62	9'56	10'46	11'34	11'77	11'44	10'76	9'74	8'78 8'17	129 0	
120	8'10	8'66	9'60	10'93	12'30	13'21	13'50	13'18	12'36	11'16	9'68	8'30	7'26	6'90 7'45	8'52	10'00	11'40	12'36	12'92	12'66	11'62	10'20	8'85	8'06	130 1	
121	7'83	8'24	9'37 10'96	12'50	13'57	14'02	13'54	12'37	10'74	8'97	7'34	6'24	5'98	6'71	8'26	10'20 12'12	13'50	14'22	13'67	12'20	10'16	8'55	7'53	7'27	131 3	
122	7'93	9'36	11'30	13'16	14'26 14'66	13'94	12'24	9'97	7'60	5'85	4'92	5'06	6'42	8'60	10'95	13'28	14'84	15'34 14'46	12'38	10'01	8'14	6'95	6'90	8'01	132 5	
123	9'74	11'84	13'66	14'84	15'16	14'10	11'76	8'83 6'14	4'18	3'66	4'53	6'46	9'08	11'92	14'30	15'96	16'28	14'95	12'41	9'36	7'14 6'17	6'50	7'92	10'02	133 7	
124	12'44	14'46	15'64	15'47	13'76	10'66	7'20	4'46	2'86	2'74 4'17	6'63	9'77	13'00	15'72	17'16	16'96	15'18	11'90	8'78	6'57	5'95	6'52	12'84	134 9		
125	15'02	15'97	15'24	12'56	8'86	5'70	3'17	1'97	2'43	4'23	7'22	10'62 13'96	16'50	17'69	17'06	14'58	10'90	8'02	5'94	5'46	6'30	8'25	10'90	13'74	135 10	
126	15'64	14'62	11'54	7'86	4'52	2'14	1'42	2'56	5'03	8'20	11'45	14'68	16'97	17'83	16'77 14'06	10'36	7'60	5'84	5'52	6'20	8'20	11'20	14'02	15'72	136 12	
127	15'74	13'76	10'48	6'92	4'07	2'24	1'86	3'24	5'60	8'58	12'24	15'14	17'16	17'74	16'33	13'21	10'00	5'76	5'60	6'58	8'80	11'97	14'34	15'47	137 14	
128	12'82	9'66	6'56	4'08	2'67	2'88	4'46	6'78	9'71	12'92	15'50	17'10	17'16	15'40	12'67	9'57	7'36	6'16	6'11	7'20	9'40 12'06	14'14	14'98	14'36	12'18	138 16
129	9'28	6'58	4'76	3'86	4'30	5'66	7'78	10'44	13'15 15'36	16'54	16'23	14'86	11'94	9'56	7'54	6'48	6'38	7'36	9'30	11'76	13'38	13'42	11'66	9'36	139 18	
130	7'30	5'74	4'98	5'26	6'33	8'08	10'42	12'87	14'66	15'72	14'00	11'78	9'46	7'72	6'96	6'82	7'44	8'91	10'74	12'30	13'13	12'92	11'76	10'08 8'18	140 20	
131	6'84	6'28	6'46	7'26	8'54	10'38	12'48	14'22	14'94	14'74	13'52	11'62	9'46	7'84 6'86	6'52	6'83	8'02	9'54	11'12	12'28	12'53	12'07	10'86	9'35	141 21	
132	7'86	6'87	6'74 7'36	8'54	10'16	11'86	13'27	14'14	13'98	12'92	11'14	9'14	7'48	6'36	5'86	5'93 7'12	8'94	10'74	12'22	12'86	12'65	11'60	10'06	8'56	142 23	
133	7'47	7'24	7'70	8'44	10'00 11'62	13'06	13'93	13'82	12'68	10'82	9'01	7'20	5'72	5'17	5'56	6'97	8'92	10'90 12'46	13'44	13'42	12'46	10'72	9'12	8'02	143 1	
134	7'47	7'63	8'26	9'76	11'56	13'14	14'05 13'96	12'62	10'76	8'52	6'66	5'32	4'84	5'46	7'38	9'67	11'66	13'40	14'34	14'36	13'24 11'36	9'64	8'16	7'52	145 3	
135	7'50	8'44	10'16	11'93	13'46	14'20	13'97	12'62	10'50	7'84 5'72	4'46	4'54	5'90	7'82	10'17	12'67	14'36	15'22	14'76	13'34	11'12	9'16	7'84 7'36	7'72	146 5	
136	8'72	10'32	12'06	13'66	14'36	13'76	11'92	9'27	6'82	4'82	3'97	4'57 6'16	8'40	11'03	13'46	15'10	15'52	14'67	12'94	10'67	8'77	7'60	7'38	7'93	147 6	
137	9'10 10'86	12'73	14'28	14'53	13'00	10'66	7'86	5'58	4'22	4'13	5'24	7'24	9'70	12'30	14'40 15'74	15'70	14'12	12'14	9'74	8'36	7'64	7'54	8'20	9'70	148 8	
138	11'80	13'62	14'54	14'16 12'22	9'68	6'84	4'84	3'94	4'50	6'00	8'33	10'94	13'60	15'42	16'13	15'62	13'90 11'47	9'28	7'84	7'40	7'74	8'92	10'62	12'60	149 10	
Sum	744'58	744'14	745'38	733'90	753'80	700'15	747'98	708'24	728'23	716'84	751'36	754'60	777'61	804'95	814'93	824'98	812'14	820'54	774'60	795'55	779'96	755'00	757'02	755'77	No. of Days	
No.	74	75	74	75	74	73	75	74	74	74	74	74	74	75	75	74	75	74	73	75	75	74	74	74	18302'25	







FORMS FOR SHORT-PERIOD TIDES.

SERIES O.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
207	6.47	3.74	2.56	3.20	5.12	8.18	11.74	15.30	17.66	18.50	14.76	10.60	7.27	5.06	4.48	5.07	7.18	10.36	13.94	16.34	17.16	16.04	13.12	9.20	5.80	223 16
208	3.36	3.52	4.58	5.73	9.03	12.78	15.94	17.78	18.04	16.74	13.32	9.36	4.18	3.80	4.00	7.56	11.10	14.46	16.66	16.88	15.39	12.15	8.33	5.44	224 17	
209	4.80	6.25	8.27	11.00	13.35	16.16	17.52	17.26	15.28	11.80	8.22	5.32	3.80	4.02	5.38	11.50	14.52	16.18	16.06	14.38	11.26	7.98	5.62	4.54	225 19	
210	7.77	9.72	12.07	13.96	16.32	17.72	12.06	9.36	6.96	5.40	5.07	4.10	4.04	6.45	8.92	12.05	14.70	15.18	12.48	8.65	7.45	6.32	5.74	6.44	226 21	
211	10.72	13.27	13.74	14.47	14.18	12.78	10.82	8.78	5.83	5.83	7.70	8.34	7.33	9.54	11.87	13.60	14.46	13.96	10.40	7.45	9.12	8.90	8.00	9.26	227 23	
212	12.10	12.88	13.72	13.38	11.88	10.06	8.17	7.02	6.68	7.00	8.77	10.10	11.41	12.02	13.26	13.57	12.85	11.76	10.70	9.74	9.67	9.77	10.12	11.54	10.82	230 3
213	12.43	12.67	12.12	11.23	9.96	8.64	7.77	7.46	7.69	8.30	9.04	10.10	11.17	12.90	12.90	12.34	11.72	11.15	10.62	10.30	10.00	10.14	10.50	11.34	11.34	231 4
214	11.96	12.26	11.97	10.53	9.44	8.35	7.66	7.57	8.12	9.06	10.48	11.57	12.72	13.42	13.36	13.18	11.45	10.72	10.26	9.92	9.63	10.00	10.71	11.62	11.62	232 6
215	12.33	12.18	11.42	10.36	9.08	7.53	7.24	7.70	8.54	9.82	11.43	12.72	13.64	13.66	13.26	12.36	11.22	10.18	9.97	9.08	8.88	10.76	11.64	12.26	12.26	233 8
216	12.55	11.85	10.40	8.78	7.36	6.44	7.14	8.37	10.20	11.94	13.38	14.40	14.54	13.58	12.17	10.70	9.34	8.82	8.84	9.26	11.16	12.50	13.30	13.42	13.42	234 10
217	12.06	10.16	8.40	6.86	6.06	6.14	7.20	8.95	10.80	12.76	14.91	14.84	13.64	11.84	9.97	8.77	8.36	8.48	8.96	10.06	11.56	13.12	13.97	12.06	12.06	235 12
218	9.70	7.27	5.96	5.56	6.35	7.80	9.76	11.70	13.66	15.10	15.46	12.86	10.57	8.64	7.46	7.31	7.76	8.84	10.72	12.64	14.21	14.62	13.44	11.00	11.00	236 13
219	8.24	5.17	5.36	6.54	8.54	10.66	13.00	15.02	15.96	15.50	14.08	11.60	8.97	7.34	6.70	7.80	9.62	11.70	13.76	14.95	14.67	12.76	10.40	7.37	7.37	237 15
220	5.56	4.97	5.74	7.38	11.94	14.36	16.04	16.27	15.32	13.08	10.11	7.72	6.36	6.10	6.94	8.63	10.83	15.21	15.71	14.43	11.89	8.54	6.26	4.97	4.97	238 17
221	5.06	6.36	8.22	10.64	13.40	15.80	16.16	14.21	11.38	8.34	6.35	5.46	5.74	7.13	9.22	11.84	14.36	15.71	15.48	10.66	7.60	5.70	4.96	5.70	5.70	239 19
222	7.24	9.54	12.02	14.56	16.24	16.56	15.34	12.80	7.06	5.50	5.18	5.94	7.72	10.28	13.04	15.14	15.90	14.88	12.52	9.63	7.07	5.74	6.67	8.36	8.36	240 21
223	10.62	13.17	15.30	16.38	15.97	14.06	11.04	8.16	6.11	5.05	6.72	8.83	11.26	13.77	15.36	15.38	14.00	11.50	8.72	6.86	5.97	6.34	7.52	9.30	9.30	241 23
224	13.80	15.46	15.84	14.77	12.44	9.37	7.06	5.37	4.85	5.64	7.12	9.24	11.64	15.06	14.75	13.17	10.76	8.64	7.30	6.86	7.44	8.64	10.38	11.47	11.47	242 23
225	14.06	15.10	13.64	11.26	8.61	6.50	5.32	5.38	6.34	7.85	9.86	11.96	13.74	13.44	12.44	11.04	9.83	8.97	8.02	7.81	8.36	9.26	10.60	12.24	12.24	244 2
226	14.44	13.86	12.25	10.02	8.06	6.46	6.17	7.02	8.17	9.66	11.26	12.55	13.57	12.94	11.92	10.73	9.67	9.16	9.18	9.63	10.67	11.96	13.06	13.06	13.06	245 4
227	13.08	11.68	9.86	8.26	6.87	6.17	7.02	8.17	9.66	11.26	12.55	13.57	12.94	11.92	10.73	9.67	9.16	9.18	9.18	9.63	10.67	11.96	13.06	13.06	13.06	246 6
228	11.74	10.42	8.97	7.44	6.44	6.21	7.02	8.17	9.66	11.26	12.55	13.57	12.94	11.92	10.73	9.67	9.16	9.18	9.18	9.63	10.67	11.96	13.06	13.06	13.06	247 8
229	11.16	9.57	7.60	6.24	5.63	5.97	7.17	8.80	10.66	12.80	14.28	14.96	13.66	11.85	10.04	8.66	8.02	8.14	9.04	10.38	12.00	13.14	13.74	13.40	13.40	248 9
230	12.04	7.64	5.76	4.78	5.02	6.24	8.16	10.78	13.20	15.04	15.98	15.74	14.33	11.96	7.37	6.55	6.70	8.06	9.98	12.06	13.93	14.86	14.44	12.86	12.86	249 11
231	10.18	7.37	5.17	4.03	5.90	7.96	10.88	13.80	16.04	17.04	16.46	14.44	11.04	8.24	6.27	5.15	5.63	9.64	12.52	14.74	15.98	15.46	13.59	9.94	9.94	250 13
232	6.63	4.34	3.17	2.53	5.38	8.20	14.56	16.82	17.44	16.36	13.83	9.98	6.70	4.46	3.84	4.58	6.80	10.06	13.28	16.64	15.75	12.94	9.26	6.06	6.06	251 15
233	3.66	2.67	3.72	5.66	8.70	12.20	15.53	17.33	15.87	12.42	8.56	5.32	3.44	3.17	4.55	7.26	10.87	14.22	16.50	17.05	15.47	12.37	5.52	3.48	3.48	252 17
234	3.10	4.46	6.74	9.94	13.47	16.22	17.47	17.02	14.77	10.84	4.52	3.00	3.30	5.07	8.06	11.72	14.94	16.86	16.90	14.94	11.54	8.00	5.38	4.20	4.20	253 19
235	5.52	7.95	11.06	14.30	16.51	17.04	15.88	12.99	9.17	5.97	3.70	2.94	3.94	9.14	12.45	15.42	16.68	16.10	13.81	10.56	7.46	5.47	4.87	5.60	5.60	254 20
236	7.04	9.54	14.81	16.16	16.06	14.44	11.07	7.87	5.34	3.84	3.92	5.16	7.43	10.36	13.44	16.04	14.92	12.66	9.98	7.74	6.47	6.36	7.02	8.34	8.34	255 22
237	10.58	12.80	14.58	15.36	12.52	9.86	7.17	5.31	4.44	5.02	6.44	8.50	11.04	13.56	14.79	14.77	13.46	11.46	8.00	7.36	7.56	8.36	9.51	11.10	11.10	257 0
238	12.60	13.73	15.94	12.90	11.02	8.73	5.70	5.63	6.34	7.60	9.36	11.36	13.14	13.88	13.60	12.43	10.94	9.64	8.76	8.44	9.18	9.95	10.88	11.66	11.66	258 2
239	12.76	12.71	11.64	9.87	8.26	7.04	6.44	6.67	8.36	9.74	11.16	12.22	12.70	12.20	11.38	10.60	9.88	9.34	9.34	9.87	9.86	10.34	10.91	10.91	10.91	260 5
240	10.37	10.56	9.48	8.44	7.52	7.14	7.33	7.86	8.66	9.84	10.90	11.97	11.87	11.54	11.08	10.42	9.92	9.66	9.46	9.54	9.86	10.34	10.70	10.70	10.70	260 5







**FORMS FOR SHORT-PERIOD TIDES.**  
**BOMBAY—Commencing 0 hours, Astronomical Time, 1st January, 1885.**  
**SERIES K. Motion per mean Solar hour = 15°04'10686.**

Argument ( $\gamma$ ).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	
1	15.52	13.96	9.13	5.76	3.03	1.68	2.28	4.80	7.90	11.70	15.50	18.00	18.85	18.08	15.14	11.54	8.50	6.21	5.53	6.08	8.20	11.31	14.16	16.06	1	23
2	16.66	15.40	12.16	8.40	4.86	2.56	1.71	2.90	5.56	8.82	12.94	16.44	18.58	18.97	17.67	14.24	10.56	7.53	5.57	5.16	6.10	8.63	11.84	14.68	2	23
3	16.63	16.96	15.24	11.92	8.00	4.87	2.80	2.57	4.24	6.84	10.20	14.07	17.26	18.86	18.84	17.06	13.20	9.77	6.90	5.23	4.96	6.16	8.86	12.14	3	23
4	14.87	16.40	16.40	15.58	11.00	7.63	4.88	3.55	3.86	5.55	8.01	11.36	14.83	17.16	18.38	17.93	15.20	12.16	8.68	6.10	5.05	5.25	6.68	9.24	4	23
5	13.28	14.51	15.96	15.58	13.48	10.47	7.54	5.76	5.07	7.22	9.17	12.11	15.02	17.02	17.55	16.63	14.11	10.96	8.16	6.22	5.47	5.84	7.18	8.24	5	23
6	9.67	13.12	14.04	15.00	14.45	12.62	10.24	8.07	7.04	8.84	7.54	8.67	10.60	12.84	15.06	16.36	16.35	15.24	12.76	10.11	8.00	6.64	6.17	6.55	6	23
7	7.86	9.76	11.80	13.27	14.00	13.64	12.22	10.47	9.05	8.44	8.40	9.03	9.97	11.20	13.05	14.64	15.46	15.18	13.87	11.68	9.76	8.10	7.16	7.93	7	23
8	7.40	8.29	9.81	11.16	12.55	13.24	13.07	12.20	11.16	10.27	9.64	9.60	9.90	10.60	11.70	12.96	14.02	14.44	13.75	12.27	10.82	9.20	7.93	8.22	8	23
9	7.24	7.06	7.34	8.07	9.14	10.55	11.74	12.48	12.66	12.27	11.60	10.93	10.34	9.98	9.86	10.17	11.07	12.14	13.06	13.36	12.72	11.71	10.43	9.14	9	23
10	7.97	7.14	6.75	6.94	7.74	8.96	10.26	11.64	12.67	13.14	12.97	12.20	11.24	10.48	10.12	10.95	10.23	10.84	11.64	12.27	12.68	12.37	11.53	10.42	10	23
11	8.97	7.80	6.96	6.38	6.44	7.28	8.73	10.47	12.14	13.23	13.84	13.63	12.58	11.38	10.27	9.77	9.62	9.89	10.44	11.24	11.97	12.52	12.50	11.87	11	23
12	10.54	8.76	7.34	6.16	5.74	6.34	7.62	9.54	11.46	13.22	14.24	14.58	13.94	12.72	11.24	10.02	9.32	9.14	9.46	10.37	11.48	12.46	13.04	12.84	12	23
13	11.88	10.23	8.20	6.52	5.62	5.56	6.50	8.14	10.17	12.34	14.10	15.20	15.17	13.97	12.27	10.58	9.35	8.75	8.76	9.26	10.34	11.68	12.96	13.64	13	23
14	13.36	11.80	10.84	8.24	6.20	4.76	5.44	6.74	8.86	11.26	13.66	15.38	15.87	15.24	13.66	11.84	9.82	8.71	8.16	8.36	9.30	10.74	12.46	13.64	14	23
15	13.98	13.00	10.84	8.24	6.20	4.76	5.40	6.74	7.36	9.78	12.57	14.82	16.13	15.97	14.56	12.35	10.05	8.46	7.82	7.74	8.41	9.71	11.76	13.30	15	23
16	14.26	14.09	12.44	9.76	7.00	5.12	4.20	4.63	6.12	8.44	11.24	14.04	15.74	16.36	15.71	13.82	11.22	8.94	7.54	6.94	7.15	8.40	10.27	12.44	16	23
17	14.06	14.68	13.84	11.50	8.60	5.94	4.37	4.02	5.06	7.26	9.66	12.72	15.20	16.55	16.63	13.27	12.77	9.97	7.86	6.84	6.68	7.56	9.32	11.40	17	23
18	13.55	14.80	14.78	13.22	10.43	7.48	5.34	4.30	4.66	6.35	8.54	11.38	14.15	16.15	16.88	16.08	14.04	11.02	8.54	6.76	6.12	6.34	7.60	9.84	18	23
19	13.14	14.06	14.84	14.14	12.06	9.06	6.46	4.67	4.24	5.16	7.15	9.68	12.56	14.87	16.44	16.45	15.00	12.42	9.50	7.22	5.80	5.43	6.26	8.16	19	23
20	10.65	12.88	14.28	14.56	13.33	10.92	8.30	6.04	4.87	5.06	6.54	8.66	11.04	13.64	15.62	16.36	15.76	13.82	11.00	8.37	6.37	5.54	5.64	6.83	20	23
21	8.93	11.40	13.32	14.42	14.25	12.47	10.10	7.91	6.34	5.70	6.30	7.70	9.76	12.17	14.36	15.74	15.96	14.86	12.76	10.13	7.78	6.17	5.70	6.11	21	23
22	7.62	9.70	11.76	13.36	14.14	13.72	12.06	9.94	8.32	7.22	7.01	7.74	8.97	10.80	12.97	14.62	15.50	15.17	13.80	11.46	9.14	7.34	6.17	6.00	22	23
23	6.68	8.02	9.76	11.65	13.04	13.76	13.34	12.14	10.65	9.07	8.15	8.14	8.68	9.86	11.56	13.36	14.56	15.02	14.37	12.76	10.76	8.71	6.00	6.96	23	21
24	6.23	6.09	6.68	7.86	9.46	11.24	12.66	13.36	13.34	12.38	11.08	9.94	9.11	8.88	9.28	10.22	11.70	13.06	14.14	14.41	13.60	12.06	10.26	8.46	24	21
25	7.10	6.25	6.08	6.56	7.64	9.14	10.84	12.34	13.44	13.81	13.33	12.18	10.75	9.76	9.24	9.34	10.07	11.16	12.40	13.38	13.66	13.03	11.87	10.24	25	21
26	8.47	7.00	5.85	5.38	5.68	6.78	8.55	10.33	12.22	13.56	14.30	14.16	13.05	11.56	10.06	9.11	8.87	9.40	10.46	11.87	12.94	13.44	13.33	12.40	26	21
27	10.74	8.86	6.83	5.22	4.41	4.77	6.10	8.10	10.50	12.63	14.53	15.56	15.72	16.74	16.12	14.36	11.40	8.83	7.24	6.86	7.53	9.20	11.11	12.97	27	21
28	13.30	11.34	8.72	6.20	4.24	3.38	3.76	5.30	7.76	10.55	13.50	15.72	16.74	17.04	17.86	17.00	14.36	10.96	8.07	6.27	5.77	6.57	8.62	14.55	28	21
29	15.08	14.17	11.84	8.82	5.70	3.60	2.56	3.06	5.04	7.88	11.48	14.56	17.04	18.10	18.47	17.26	13.80	10.14	7.09	5.27	5.02	6.02	8.40	11.85	30	21
30	15.74	16.28	14.96	12.18	8.44	5.42	3.22	2.16	3.07	5.52	8.75	12.46	16.01	18.10	18.47	17.26	13.80	10.14	7.09	5.27	5.02	6.02	8.40	11.85	30	21
31	14.65	16.32	16.84	15.28	11.68	7.88	4.80	2.74	2.38	4.00	6.66	10.10	13.98	17.01	18.64	18.38	16.30	12.42	8.97	6.01	4.46	4.57	6.12	9.14	31	21
32	12.56	15.46	17.00	16.86	14.76	11.06	7.36	4.34	2.72	2.99	4.86	7.74	11.40	14.94	17.54	18.47	17.66	14.67	11.08	7.54	5.01	3.93	4.32	6.55	32	21
33	9.63	13.04	15.80	16.84	16.08	13.73	10.16	6.82	4.54	3.58	4.44	6.36	9.36	12.84	15.86	17.74	17.94	16.48	13.27	9.84	6.84	4.96	4.33	5.26	33	21
34	7.44	10.66	13.70	15.74	16.43	15.42	12.82	9.66	6.90	5.42	5.14	6.20	8.06	10.66	13.66	16.02	17.12	16.74	14.88	11.68	8.76	6.34	4.92	4.74	34	21
35	5.86	8.26	11.07	13.60	15.16	15.34	14.66	11.68	9.04	7.34	6.56	6.94	8.04	9.56	11.76	14.24	15.60	16.04	15.34	13.02	10.16	7.86	6.27	5.54	35	21

36	5.86	7.18	9.07	11.36	13.26	14.94	14.26	12.88	11.00	9.39	8.46	7.92	8.30	9.05	10.36	12.08	13.76	14.66	14.44	13.11	11.12	9.30	7.54	6.26	36	21
37	6.13	6.68	7.86	9.28	10.86	12.27	13.10	12.94	11.93	10.66	9.72	9.12	9.06	9.26	9.66	10.60	11.82	12.86	13.34	12.82	11.45	10.03	8.74	7.48	37	21
38	6.86	6.78	7.17	7.94	9.05	10.30	11.34	11.97	11.92	11.42	10.84	10.34	10.07	9.97	9.77	9.94	10.44	11.32	12.06	12.26	11.78	10.88	9.87	8.84	38	21
39	7.86	7.24	6.94	7.18	8.03	9.07	10.14	11.00	11.56	11.42	11.85	11.77	11.46	11.12	10.57	10.07	9.70	9.70	10.13	10.80	11.27	11.45	11.25	10.76	39	20
40	9.97	9.00	8.00	7.11	6.58	6.74	7.44	8.51	9.84	10.90	11.76	12.34	12.55	12.30	11.60	10.57	9.76	9.34	9.17	9.56	10.24	10.94	11.36	11.44	40	20
41	10.97	10.10	9.07	7.87	6.85	6.30	6.50	7.26	8.50	10.16	11.44	12.65	13.26	13.32	12.56	11.36	10.08	9.16	8.67	8.64	9.01	9.76	10.58	11.25	41	20
42	11.66	11.34	10.36	8.82	7.36	6.12	5.54	5.82	6.94	8.54	10.36	12.06	13.46	13.97	13.64	12.30	10.76	9.26	8.14	7.84	8.12	8.96	10.24	11.52	42	20
43	12.40	12.66	12.07	10.47	8.56	6.64	5.46	5.20	5.93	7.55	9.56	11.72	13.53	14.67	14.84	13.98	12.14	10.00	8.54	7.66	7.53	8.16	9.56	11.03	43	20
44	12.66	13.62	13.60	12.30	10.24	7.77	5.88	4.84	4.96	6.33	8.27	10.66	13.07	14.85	15.64	15.23	13.64	11.13	9.02	7.54	6.79	7.00	8.13	9.87	44	20
45	11.85	13.60	14.38	13.88	11.93	9.10	6.54	4.66	4.00	4.90	6.86	9.20	11.97	14.34	15.82	15.96	14.78	12.26	9.64	7.46	6.24	5.96	6.74	8.48	45	20
46	10.85	13.07	14.56	14.85	13.63	10.90	7.86	5.57	4.07	4.04	5.46	7.84	10.63	13.64	15.83	16.64	16.01	13.87	10.90	8.00	6.17	5.46	5.74	7.26	46	20
47	9.70	12.25	14.42	15.50	15.15	13.08	9.90	6.94	4.75	3.92	4.66	6.62	9.46	12.60	15.08	16.60	16.64	15.00	11.93	8.96	6.76	5.63	5.06	5.54	47	20
48	7.84	10.54	13.30	15.12	15.66	14.46	11.76	8.44	5.86	4.26	4.25	5.52	7.84	10.68	13.68	15.84	16.68	15.86	13.15	10.22	7.36	5.65	4.23	4.46	48	20
49	6.97	8.56	11.57	14.06	15.54	15.51	13.57	10.53	7.47	5.38	4.52	5.04	6.70	9.14	12.18	14.74	16.36	16.26	14.64	11.74	8.68	6.28	4.54	4.14	49	20
50	5.97	7.06	9.74	12.44	14.55	15.46	14.76	12.57	9.68	7.24	5.84	5.60	6.54	8.40	10.77	13.32	15.42	16.26	15.47	13.18	10.24	7.54	5.62	4.54	50	20
51	4.69	5.80	7.87	10.40	12.80	14.50	15.06	14.03	11.86	9.36	7.58	6.64	6.76	7.86	9.60	11.66	13.73	15.08	15.32	14.12	11.86	9.24	6.90	5.18	51	20
52	4.38	5.06	6.46	8.24	10.33	12.41	13.86	14.34	13.44	11.46	7.58	6.05	7.40	7.66	8.58	9.92	11.68	13.36	14.16	14.12	12.82	10.83	8.73	6.87	52	20
53	5.45	4.92	5.44	6.63	8.23	10.14	11.77	12.96	13.40	12.76	11.56	10.24	9.04	8.45	8.28	8.67	9.76	11.20	12.50	13.18	13.06	11.88	10.35	8.57	53	20
54	6.98	5.77	5.38	5.64	6.37	7.82	9.54	11.17	12.38	13.02	12.10	12.96	12.16	11.07	10.02	8.94	8.44	8.48	9.27	10.44	11.57	12.34	12.34	11.70	54	19
55	10.50	8.90	7.32	5.96	5.24	5.12	5.86	7.17	8.50	10.63	12.10	13.16	13.56	13.13	11.86	10.27	8.88	8.08	7.87	8.42	9.56	10.87	11.93	12.44	55	19
56	12.26	11.27	9.76	7.96	6.27	5.06	4.55	5.02	6.47	8.52	10.67	12.72	14.14	14.86	14.44	12.70	10.66	8.80	7.60	7.21	7.64	9.18	11.00	12.40	56	19
57	13.36	13.52	12.60	10.86	8.63	6.40	4.63	4.06	4.70	6.46	8.84	11.30	13.80	15.56	16.25	15.33	12.96	10.26	7.95	6.54	6.18	7.03	8.83	11.00	57	19
58	12.96	14.40	14.74	13.76	11.70	8.84	6.08	4.05	3.42	4.14	6.18	8.80	12.06	14.93	16.76	17.15	15.84	12.87	9.66	7.00	5.18	5.12	6.26	8.52	58	19
59	11.16	13.67	15.38	15.86	14.57	11.93	8.26	5.48	3.42	2.92	4.14	6.52	9.58	13.16	16.04	17.62	17.34	15.27	11.66	8.27	5.56	4.16	4.32	5.84	59	19
60	8.66	11.92	14.74	16.46	16.54	14.66	11.26	7.66	4.94	3.20	3.27	4.70	7.52	10.86	14.63	17.06	17.98	16.96	13.90	10.20	6.96	4.47	3.56	4.02	60	19
61	6.04	9.40	12.86	15.55	16.86	16.36	13.86	10.44	6.92	4.54	3.37	3.90	5.80	8.56	12.33	15.44	17.27	17.40	15.46	12.03	8.50	5.70	3.74	3.27	61	19
62	4.33	7.10	10.34	13.76	15.97	16.76	15.76	12.96	9.44	6.74	4.67	4.23	5.26	7.43	10.37	13.82	16.13	17.08	16.40	13.86	10.50	7.26	4.94	3.56	62	19
63	3.86	5.60	8.27	11.55	14.34	16.02	16.28	14.66	11.66	8.60	6.46	5.26	5.46	6.56	8.86	11.44	14.36	15.97	16.18	14.88	12.00	8.86	6.28	4.57	63	19
64	4.06	4.86	6.67	9.40	12.24	14.39	15.64	15.33	13.25	10.46	8.22	6.76	6.34	7.00	8.36	10.22	12.44	14.42	15.27	14.71	12.72	10.14	7.72	5.93	64	19
65	4.86	5.00	6.10	8.03	10.30	12.47	13.97	14.58	13.92	12.03	10.14	8.54	7.56	7.56	8.42	9.82	11.34	12.96	14.04	14.24	13.22	11.36	9.36	7.56	65	19
66	6.27	5.84	6.34	7.46	9.00	10.76	12.44	13.56	13.74	12.74	11.40	10.07	9.16	8.96	9.27	9.77	10.46	11.36	12.44	13.07	13.03	12.12	10.46	8.86	66	19
67	7.68	7.02	7.02	7.66	8.54	9.66	10.96	12.24	12.88	12.88	12.24	11.43	10.66	10.24	10.16	10.24	10.47	10.86	11.44	12.02	12.40	12.24	11.36	10.18	67	19
68	8.87	7.97	7.67	7.94	8.50	9.00	9.78	10.74	11.76	12.46	12.67	12.27	11.74	11.26	10.87	10.56	10.36	10.22	10.36	10.76	11.26	11.56	11.38	10.86	68	19
69	9.96	9.14	8.40	7.98	7.80	7.86	8.34	9.30	10.46	11.44	12.08	12.36	12.27	12.03	11.50	10.78	10.20	10.20	9.73	9.58	9.87	10.35	10.89	11.10	69	18
70	11.10	10.78	10.32	9.72	8.86	7.97	7.28	7.26	7.87	8.97	10.32	11.56	12.46	13.04	13.10	12.54	11.68	10.56	9.64	9.08	8.82	9.16	9.88	10.74	70	18
71	11.40	11.75	11.70	11.14	10.07	8.84	7.56	6.74	6.70	7.63	8.94	10.62	12.06	13.26	13.78	13.68	12.86	11.34	9.88	8.86	8.16	8.03	8.46	9.64	71	18
72	10.86	12.06	12.78	12.56	11.57	9.92	8.17	6.67	5.98	6.16	7.20	8.87	10.76	12.70	14.08	14.61	14.06	12.53	10.68	8.96	7.55	6.88	7.05	8.07	72	18
73	9.84	11.76	12.97	13.54	13.03	11.46	9.42	7.27	5.74	5.30	5.90	7.44	9.66	11.92	14.02	15.17	15.16	13.87	11.66	9.44	7.56	6.34	6.07	6.86	73	18
74	8.68	10.80	12.96	14.26	14.55	13.37	11.16	8.45	6.26	5.16	5.12	6.24	8.10	10.63	13.22	15.15	15.86	15.17	13.22	10.40	7.86	6.06	5.52	5.54	74	18
Sum	733.67	769.74	798.21	798.65	762.13	720.27	665.02	622.68	607.77	627.02	667.96	738.10	843.55	919.95	973.32	986.21	945.71	867.75	817.96	736.38	671.32	637.88	629.45	666.34	No. of Days, 73° 19', 1837.01	

FORMS FOR SHORT-PERIOD TIDES.  
 SERIES K.—(Continued).

Day	1 <sup>h</sup>		2 <sup>h</sup>		3 <sup>h</sup>		4 <sup>h</sup>		5 <sup>h</sup>		6 <sup>h</sup>		7 <sup>h</sup>		8 <sup>h</sup>		9 <sup>h</sup>		10 <sup>h</sup>		11 <sup>h</sup>		12 <sup>h</sup>		13 <sup>h</sup>		14 <sup>h</sup>		15 <sup>h</sup>		16 <sup>h</sup>		17 <sup>h</sup>		18 <sup>h</sup>		19 <sup>h</sup>		20 <sup>h</sup>		21 <sup>h</sup>		22 <sup>h</sup>		23 <sup>h</sup>		Solar Hour d h
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet				
75	6.90	9.24	11.72	13.95	15.20	15.12	13.39	10.64	7.57	5.44	4.44	4.96	6.46	8.94	11.85	14.34	16.00	16.06	14.53	11.64	8.54	5.76	4.22	3.97	75 18																						
76	5.24	7.30	10.10	13.02	15.04	16.00	15.20	12.86	9.54	6.67	4.92	4.38	5.52	7.55	10.33	13.59	15.75	16.73	16.07	13.66	10.42	7.22	4.94	3.64	76 18																						
77	4.00	5.66	8.13	11.52	14.30	16.06	16.52	15.06	12.13	8.73	6.13	4.66	4.99	6.52	8.92	11.86	14.66	16.40	16.56	15.07	11.90	8.47	5.62	3.74	77 18																						
78	3.22	4.26	6.66	9.60	12.85	15.23	16.56	16.25	14.26	10.83	8.00	5.75	5.11	5.88	7.84	10.46	13.38	15.68	16.60	15.80	13.36	10.12	7.06	4.83	78 18																						
79	3.54	3.76	5.34	7.86	11.00	13.93	15.92	16.74	15.74	13.36	10.24	7.64	6.12	6.08	7.14	9.00	11.56	13.90	15.66	15.98	14.76	12.06	8.90	6.13	79 18																						
80	4.34	3.62	4.36	6.06	8.47	11.31	13.87	15.62	16.12	14.97	12.74	10.02	8.05	6.96	7.06	7.93	9.67	12.07	14.08	15.23	15.08	13.57	11.16	8.26	80 18																						
81	6.08	4.76	4.47	5.46	7.26	9.48	11.88	13.90	15.36	15.50	14.66	12.67	10.54	8.74	7.94	8.14	9.06	10.62	12.40	13.77	14.52	14.20	12.80	10.64	81 18																						
82	8.47	6.76	5.86	5.82	6.49	7.75	9.52	11.71	13.54	14.73	14.90	14.06	12.63	11.05	9.70	8.86	8.72	9.12	10.24	11.76	13.06	13.60	12.06	82 18																							
83	10.56	8.92	7.40	6.43	6.30	6.68	7.68	9.46	11.24	13.02	14.08	14.52	14.22	13.04	11.70	10.34	9.24	8.84	9.04	9.84	10.96	12.05	12.86	12.96	83 18																						
84	12.44	11.22	9.67	8.30	7.06	6.48	6.64	7.48	8.86	10.64	12.34	13.74	14.48	14.44	13.62	12.12	10.36	8.96	8.11	7.96	8.44	9.76	11.26	84 17																							
85	12.36	12.92	12.78	11.94	10.50	8.78	7.20	6.06	5.92	6.72	8.34	10.26	12.20	13.86	15.00	15.14	14.16	12.20	9.88	8.00	6.90	6.56	7.46	9.22	85 17																						
86	11.16	12.56	13.57	14.06	13.37	11.72	9.38	7.17	5.72	5.38	6.17	7.82	10.00	12.50	14.54	15.84	15.94	14.64	12.14	9.36	6.97	5.74	5.63	6.67	86 17																						
87	8.88	11.24	13.46	14.86	15.36	14.34	12.05	9.44	6.93	5.38	5.00	5.82	7.83	10.50	13.30	15.60	16.72	16.28	14.37	11.37	8.36	6.00	4.67	4.80	87 17																						
88	6.40	9.20	12.06	14.62	16.12	16.16	14.90	12.22	9.12	6.60	5.05	4.86	5.87	8.10	11.14	14.15	16.35	17.15	16.24	13.58	10.14	7.06	4.83	3.96	88 17																						
89	4.70	6.72	9.92	13.30	15.64	17.04	16.75	14.92	11.81	8.56	6.27	5.14	5.64	6.94	9.43	12.61	15.44	17.03	17.08	15.36	11.92	8.64	6.18	4.48	89 17																						
90	4.35	5.24	7.57	11.00	14.10	16.43	17.34	16.56	14.28	10.82	7.84	5.95	5.42	6.12	7.87	10.62	13.66	16.10	17.14	16.46	13.96	10.44	7.12	4.80	90 17																						
91	3.83	4.41	6.43	8.78	12.04	14.74	16.66	17.13	15.64	12.86	9.53	7.16	5.81	5.93	7.22	9.26	12.02	14.66	16.44	16.67	15.06	12.02	8.56	5.84	91 17																						
92	4.04	4.22	4.76	6.40	8.73	11.37	14.00	15.82	16.34	15.34	13.10	10.40	8.36	7.32	7.28	8.03	9.50	11.53	13.48	14.74	14.92	13.67	11.34	8.76	92 17																						
93	5.16	5.40	5.22	6.16	7.85	9.97	12.30	14.30	15.48	15.46	14.27	12.24	10.20	8.78	8.26	8.47	9.24	10.52	12.04	13.48	14.16	13.84	12.27	10.16	93 17																						
94	6.67	6.47	5.74	6.22	7.44	9.20	10.85	12.64	14.05	14.67	14.27	12.97	11.44	10.04	9.16	8.84	9.16	9.84	10.95	11.96	12.80	12.96	10.94	8.76	94 17																						
95	8.14	6.47	5.74	6.22	7.44	9.20	10.85	12.64	14.05	14.67	14.27	12.97	11.44	10.04	9.16	8.84	9.16	9.84	10.95	11.96	12.80	12.96	10.94	8.76	95 17																						
96	9.24	7.80	6.78	6.70	7.30	8.37	9.54	10.90	12.34	13.52	13.80	13.26	12.13	10.96	10.04	9.60	9.33	9.54	9.90	10.56	11.44	11.92	12.05	11.54	96 17																						
97	10.36	9.16	8.12	7.47	7.44	7.97	8.52	9.46	10.73	11.93	12.74	12.98	12.60	11.86	11.07	10.34	9.94	9.77	9.97	10.02	10.36	10.81	11.14	11.27	97 17																						
98	10.92	10.30	9.34	8.36	7.74	7.58	7.98	8.76	9.87	11.04	11.96	12.50	12.66	12.42	11.96	11.34	10.55	9.91	9.47	9.34	9.52	9.94	10.53	10.94	98 17																						
99	11.12	11.02	10.62	10.00	9.22	8.40	8.01	8.13	8.63	9.70	10.66	11.77	12.66	13.06	12.94	12.40	11.47	10.50	9.62	8.94	8.54	8.74	9.48	10.45	99 17																						
100	11.36	11.88	11.89	11.44	10.50	9.40	8.46	7.84	7.76	8.43	9.46	10.66	11.77	12.66	13.06	12.94	12.40	11.47	10.50	9.62	8.94	8.54	8.74	9.48	10.45	100 16																					
101	9.47	10.86	11.90	12.70	12.87	12.44	11.06	9.52	8.12	7.40	7.47	8.36	9.54	11.08	12.70	14.06	14.56	14.22	12.80	10.96	8.88	7.46	6.81	6.84	101 16																						
102	7.92	9.62	11.52	13.00	13.97	14.12	13.00	11.02	9.05	7.48	6.74	6.92	7.97	9.72	11.72	13.58	14.86	15.12	14.21	12.35	9.67	7.47	5.98	5.58	102 16																						
103	6.14	7.76	9.84	12.16	14.02	15.18	15.06	13.40	10.95	8.28	6.66	6.02	6.46	7.88	10.06	12.53	14.55	15.72	15.49	13.80	11.08	8.22	5.93	4.52	103 16																						
104	4.32	5.47	7.72	10.54	13.27	15.36	16.20	15.32	13.00	9.88	7.34	5.76	5.40	6.24	8.22	10.70	13.40	15.52	16.25	15.36	12.80	9.46	6.56	4.47	104 16																						
105	3.42	3.91	5.74	8.31	11.40	14.40	16.28	16.72	15.47	12.68	9.44	6.81	5.47	5.38	6.52	8.91	11.80	14.40	15.97	16.08	14.35	11.30	7.80	4.97	105 16																						
106	2.93	2.46	3.76	6.21	9.51	12.97	15.58	17.14	17.04	14.94	11.68	8.36	6.14	5.06	5.57	7.24	10.07	13.10	15.40	16.44	15.82	13.44	9.74	6.67	106 16																						
107	4.03	2.50	2.77	4.44	7.50	10.96	14.33	16.70	17.72	16.91	14.37	10.87	8.10	6.15	5.71	6.50	8.36	11.33	14.12	15.97	16.50	15.10	12.22	8.67	107 16																						
108	5.34	3.17	2.56	3.47	5.74	8.64	12.02	15.12	16.94	17.54	16.24	13.40	10.32	7.53	6.17	6.07	7.04	9.13	12.00	14.47	15.69	15.54	13.66	10.74	108 16																						
109	7.44	4.88	3.28	3.04	4.36	6.67	9.40	12.47	15.00	16.74	16.94	15.60	13.03	10.03	7.87	6.76	6.80	7.71	9.70	12.44	14.15	15.02	14.50	12.53	109 16																						



110	9'92	7'24	5'36	4'17	4'16	5'20	7'26	9'89	12'40	14'57	15'77	15'74	14'47	12'12	9'90	8'07	7'14	7'11	7'83	9'54	11'58	13'16	13'74	13'28	110 16
111	11'76	9'56	7'60	5'96	4'93	5'02	5'86	7'52	9'74	12'00	13'87	14'87	14'77	13'76	12'06	10'26	8'74	7'82	7'54	8'00	9'34	11'00	12'36	12'96	111 16
112	12'72	11'58	10'14	8'48	6'94	6'06	5'96	6'60	7'87	9'72	11'62	13'34	14'34	14'44	13'66	12'26	10'62	9'10	8'03	7'66	7'76	8'68	10'20	11'63	112 16
113	12'43	12'66	12'10	10'96	9'47	8'14	7'03	6'54	6'88	7'94	9'57	11'42	13'00	14'07	14'44	13'93	12'76	11'00	9'18	7'74	6'96	6'96	7'85	9'40	113 16
114	10'96	12'36	13'06	13'12	12'22	10'65	8'87	7'52	6'74	6'84	7'66	9'26	11'04	12'88	14'12	14'66	14'30	12'64	10'64	8'60	6'78	5'94	5'93	7'08	114 16
115	9'00	11'04	12'64	13'72	13'87	12'97	11'36	9'32	7'66	6'62	6'47		7'28	8'88	10'96	12'96	14'54	15'17	14'54	12'77	10'22	7'74	5'76	4'88	115 15
116	5'14	6'58	8'88	11'33	13'36	14'66	14'94	13'86	11'70	9'34	7'26	6'22	6'20	7'24	9'00	11'22	13'36	14'86	15'37	14'44	12'10	9'16	6'48	4'70	116 15
117	4'20	4'74	6'70	9'17	11'77	14'02	15'57	15'54	14'03	11'54	8'80	6'96	6'07	6'34	7'48	9'44	11'96	14'10	15'48	15'44	13'84	10'92	7'66	5'31	117 15
118	3'77	3'70	5'12	7'30	10'10	12'94	15'14	16'26	15'76	13'86	11'00	8'24	6'47	5'97	6'54	7'98	10'16	12'70	14'64	15'66	14'96	12'70	9'46	6'57	118 15
119	4'32	3'42	4'04	5'80	8'48	11'42	14'32	16'17	16'57	15'46	12'94	10'06	7'64	6'36	6'16	6'82	8'40	10'90	13'45	15'07	15'35	13'81	11'00	7'70	119 15
120	5'15	3'44	3'36	4'67	6'96	9'52	12'56	14'92	16'36	16'28	14'70	11'93	9'06	7'20	6'40	6'70	7'74	9'37	11'47	13'86	15'04	15'06	12'96	9'73	120 15
121	7'17	4'24	3'42	4'04	5'68	8'27	10'68	13'46	15'48	16'25	15'62	13'50	10'52	8'22	6'72	6'40	7'02	8'34	10'44	12'60	14'08	14'45	13'26	10'82	121 15
122	7'87	5'57	3'94	3'86	4'88	6'80	9'18	11'76	14'24	15'56	15'54	14'30	11'86	9'46	7'76	6'94	7'06	7'86	9'36	11'24	13'06	13'96	13'66	11'90	122 15
123	9'20	6'72	5'07	4'36	4'90	6'32	8'22	10'36	12'80	14'56	15'43	14'76	13'04	10'84	8'96	7'76	7'44	7'76	8'80	10'26	11'94	13'06	13'30	12'28	123 15
124	10'40	8'28	6'46	5'35	5'20	6'00	7'54	9'26	11'42	13'34	14'60	14'86	13'86	12'06	10'14	8'84	8'15	8'06	8'40	9'36	10'62	11'94	12'68	12'46	124 15
125	11'36	9'58	7'94	6'74	6'04	6'20	7'12	8'46	10'24	12'10	13'38	14'08	13'92	12'90	11'41	10'00	8'90	8'46	8'56	9'00	9'74	10'55	11'36	11'86	125 15
126	11'68	10'72	9'26	7'86	6'96	6'92	7'44	8'22	9'26	10'47	12'10	13'34	13'78	13'40	12'16	10'87	9'94	9'24	8'96	8'94	9'17	9'58	10'34	10'96	126 15
127	11'44	11'34	10'58	9'56	8'46	7'76	7'66	7'97	8'66	9'74	10'97	12'22	13'24	13'54	13'24	12'12	10'96	9'98	9'27	8'94	8'74	8'80	9'24	10'03	127 15
128	10'80	11'26	11'29	10'79	10'06	9'26	8'46	8'06	8'04	8'56	9'72	10'94	12'20	12'96	13'22	12'94	12'14	11'17	9'96	8'96	8'20	7'92	8'00	8'62	128 15
129	9'56	10'46	11'34	11'77	11'44	10'76	9'74	8'78	8'17	8'10	8'66	9'60	10'93	12'30	13'21	13'50	13'18	12'36	11'16	9'68	8'30	7'26	6'90	7'45	129 15
130	8'52	10'00	11'40	12'36	12'92	12'66	11'62	10'20	8'85	8'06	7'83	8'24	9'37	10'96	12'50	13'57	14'02	13'54		12'37	10'74	8'97	7'34	6'24	130 14
131	5'98	6'71	8'26	10'20	12'12	13'50	14'22	13'67	12'20	10'16	8'55	7'53	7'27	7'93	9'36	11'30	13'16	14'26	14'66	13'94	12'24	9'97	7'60	5'85	131 14
132	4'92	5'06	6'42	8'60	10'95	13'28	14'84	15'34	14'46	12'38	10'01	8'14	6'95	6'90	8'01	9'74	11'84	13'66	14'84	15'16	14'10	11'76	8'83	6'14	132 14
133	4'18	3'66	4'53	6'46	9'08	11'92	14'30	15'96	16'28	14'95	12'41	9'36	7'14	6'17	6'50	7'92	10'02	12'44	14'46	15'64	15'47	13'76	10'66	7'20	133 14
134	4'46	2'86	2'74	4'17	6'63	9'77	13'00	15'72	17'16	16'96	15'18	11'90	8'78	6'57	5'95	6'52	7'94	10'30	12'84	15'02	15'97	15'24	12'56	8'86	134 14
135	5'70	3'17	1'97	2'43	4'23	7'22	10'62	13'96	16'50	17'69	17'06	14'58	10'90	8'02	5'94	5'46	6'30	8'25	10'90	13'74	15'64	16'06	14'62	11'54	135 14
136	7'86	4'52	2'14	1'42	2'56	5'03	8'20	11'45	14'68	16'97	17'83	16'77	14'06	10'36	7'60	5'84	5'52	6'20	8'20	11'20	14'02	15'72	15'74	13'76	136 14
137	10'48	6'92	4'07	2'24	1'86	3'24	5'60	8'58	12'24	15'14	17'16	17'74	16'33	13'21	10'00	7'30	5'76	5'60	6'58	8'80	11'97	14'34	15'47	15'07	137 14
138	12'82	9'66	6'56	4'08	2'67	2'88	4'46	6'78	9'71	12'92	15'50	17'10	17'16	15'40	12'67	9'57	7'36	6'16	6'11	7'20	9'40	12'06	14'14	14'98	138 14
139	14'36	12'18	9'28	6'58	4'76	3'86	4'30	5'66	7'78	10'44	13'15	15'36	16'54	16'23	14'86	11'94	9'56	7'54	6'48	6'38	7'36	9'30	11'76	13'38	139 14
140	13'98	13'42	11'66	9'36	7'30	5'74	4'98	5'26	6'33	8'08	10'42	12'87	14'66	15'72	15'46	14'00	11'78	9'46	7'72	6'96	6'82	7'44	8'91	10'74	140 14
141	12'30	13'13	12'92	11'76	10'08	8'18	6'84	6'28	6'46	7'26	8'54	10'38	12'48	14'22	14'94	14'74	13'52	11'62	9'46	7'84	6'86	6'52	6'83	8'02	141 14
142	9'54	11'12	12'28	12'53	12'07	10'86	9'35	7'86	6'87	6'74	7'36	8'54	10'16	11'86	13'27	14'14	13'98	12'92	11'14	9'14	7'48	6'36	5'86	5'93	142 14
143	7'12	8'94	10'74	12'22	12'86	12'65	11'60	10'06	8'56	7'47	7'24	7'70	8'44	10'00	11'62	13'06	13'93	13'82	12'68	10'82	9'01	7'20	5'72	5'17	143 14
144	5'56	6'97	8'92	10'90	12'46	13'44	13'42	12'46	10'72	9'12	8'02	7'47	7'63	8'26	9'76	11'56	13'14	14'05	13'96	12'62	10'76	8'52	6'66	5'32	144 14
145	4'84	5'46	7'38	9'67	11'66	13'40	14'34	14'36	13'24	11'36	9'64	8'16	7'52	7'50	8'44	10'16	11'93	13'46	14'20	13'97	12'62	10'50	7'84	5'72	145 14
146		4'46	4'54	5'90	7'82	10'17	12'67	14'36	15'22	14'76	13'34	11'12	9'16	7'84	7'36	7'72	8'72	10'32	12'06	13'66	14'36	13'76	11'92	9'27	146 13
147	6'82	4'82	3'97	4'57	6'16	8'40	11'03	13'46	15'10	15'52	14'67	12'94	10'67	8'77	7'60	7'38	7'93	9'10	10'86	12'73	14'28	14'53	13'00	10'66	147 13
148	7'86	5'58	4'22	4'13	5'24	7'24	9'70	12'30	14'40	15'74	15'70	14'12	12'14	9'74	8'36	7'64	7'54	8'20	9'70	11'80	13'62	14'54	14'16	12'22	148 13
Sum	570'44	551'64	568'43	618'93	680'36	756'30	830'55	870'19	879'69	860'79	823'73	771'49	742'30	726'11	737'09	770'45	815'94	858'86	874'14	890'72	859'37	798'26	718'33	626'24	No. of Days. 73 <sup>19</sup> 18210'25
No.	73	74	74	74	74	73	74	74	74	74	74	73	74	74	74	74	74	74	73	74	74	74	74	73	78

FORMS FOR SHORT-PERIOD TIDES.

SERIES K.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
140	9.68	6.84	4.84	3.94	4.50	6.00	8.33	10.94	13.60	15.42	16.13	15.62	13.90	11.47	9.28	7.84	7.40	7.74	8.92	10.62	12.60	14.02	14.77	13.22	149 13	
150	10.78	8.10	5.76	4.27	4.17	5.26	7.20	9.70	12.28	14.66	15.94	16.04	14.86	12.64	10.27	8.44	7.54	7.34	8.10	9.52	11.55	13.36	14.27	13.92	150 13	
151	13.06	9.48	6.90	5.12	4.32	4.97	6.54	8.70	11.00	13.46	15.32	16.07	15.67	14.17	11.77	9.56	8.16	7.68	7.83	8.74	10.50	12.26	13.66	14.02	151 13	
152	12.96	10.86	8.34	6.24	5.04	4.82	5.84	7.60	9.46	11.87	14.10	15.30	15.60	14.66	12.78	10.74	9.03	7.96	7.73	8.24	9.44	11.07	12.62	13.44	152 13	
153	13.16	11.96	9.94	7.67	6.16	5.18	5.56	6.86	8.64	10.66	12.74	14.30	15.12	15.06	13.65	11.84	10.00	8.46	7.75	7.78	8.46	9.92	11.36	12.37	153 13	
154	12.84	12.22	10.98	9.18	7.32	6.03	5.94	6.87	8.17	9.67	11.58	13.28	14.64	14.97	14.22	12.62	11.08	9.47	8.38	8.08	8.30	9.20	10.24	11.40	154 13	
155	12.12	12.46	11.72	10.38	8.77	7.37	6.70	6.93	7.78	8.83	10.30	11.90	13.54	14.68	14.80	13.77	12.16	10.50	9.20	8.47	8.28	8.60	9.36	10.36	155 13	
156	11.26	11.83	12.05	11.56	10.60	9.20	8.14	7.72	7.83	8.62	9.82	11.10	12.64	13.94	14.46	14.16	13.26	11.74	10.42	9.26	8.54	8.34	8.46	9.23	156 13	
157	10.10	10.93	11.70	11.97	11.72	11.06	9.98	8.86	8.32	8.36	9.00	10.04	11.54	12.92	13.86	14.25	13.85	12.88	11.48	10.08	8.98	8.20	8.20	8.37	157 13	
158	9.12	10.03	11.29	12.14	12.38	12.36	11.84	11.02	10.06	9.23	8.78	9.20	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	10.03	8.74	7.92	7.54	158 13	
159	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	9.64	10.17	11.38	12.77	13.98	14.67	15.14	14.88	13.86	12.46	10.48	8.82	7.82	159 13	
160	7.50	8.19	9.46	11.28	13.22	14.76	15.82	15.76	14.97	13.34	11.70	10.67	10.27	10.56	11.52	12.90	14.12	15.30	15.05	15.48	14.17	12.02	9.86	8.00	160 13	
161	7.09	6.85	7.72	9.34	11.40	13.77	15.84	16.86	16.85	15.70	13.60	11.52	11.52	10.97	9.95	9.55	9.80	10.84	12.57	14.21	15.47	16.06	15.22	13.50	10.84	161 12
162	8.22	6.16	4.95	5.15	6.50	8.61	11.37	14.18	16.48	17.54	17.17	15.60	12.50	10.97	8.34	8.17	8.96	10.27	12.23	14.24	15.74	16.29	15.33	13.77	162 12	
163	9.46	6.32	4.44	3.62	4.30	6.30	8.54	11.95	15.02	17.28	17.95	17.20	15.02	11.76	9.04	7.44	7.22	7.81	9.55	12.08	14.54	16.07	16.21	14.76	163 12	
164	11.97	8.16	5.07	3.07	2.74	3.80	5.94	9.24	12.80	15.92	18.07	18.53	17.65	14.65	10.90	8.00	6.62	6.55	7.50	9.65	12.45	14.89	16.40	16.14	164 12	
165	14.28	10.90	7.10	4.31	2.62	2.37	3.68	6.30	9.76	13.48	16.44	18.12	18.40	17.00	13.80	10.17	7.55	6.20	6.18	7.30	9.66	12.79	15.16	16.42	165 12	
166	15.96	13.80	10.33	6.77	4.00	2.23	2.54	4.18	7.11	10.40	13.95	16.74	17.85	17.95	16.07	12.81	9.60	7.05	5.72	5.77	7.00	9.56	12.80	15.12	166 12	
167	16.05	15.26	12.76	9.20	6.14	3.95	2.88	3.47	5.52	7.93	11.04	14.21	16.44	17.72	17.40	15.44	12.07	9.02	6.70	5.67	5.93	7.41	10.07	13.02	167 12	
168	14.92	15.57	14.68	12.28	9.20	6.52	4.77	4.20	4.94	6.52	8.80	11.67	14.34	16.42	17.20	16.60	14.54	11.30	8.66	6.74	6.05	6.16	7.65	10.05	168 12	
169	12.50	14.32	14.85	14.05	11.96	9.47	7.26	6.06	5.80	6.39	7.66	9.64	11.92	14.25	15.90	16.46	15.74	13.76	10.84	8.61	6.86	6.32	6.58	7.86	169 12	
170	9.82	12.04	13.55	14.17	13.54	12.03	10.34	8.60	7.57	7.26	7.62	8.44	9.92	12.12	14.20	15.46	15.54	14.58	12.66	10.40	8.31	7.04	6.60	6.77	170 12	
171	7.78	9.32	11.22	12.80	13.58	13.46	12.40	10.90	9.62	8.66	8.31	8.49	9.03	10.30	12.04	13.70	14.74	14.75	13.73	12.02	10.10	8.46	7.12	6.53	171 12	
172	6.70	7.50	9.03	10.90	12.32	13.20	13.38	12.92	11.94	10.67	9.66	8.94	8.82	9.44	10.33	11.90	13.24	14.06	14.10	13.34	11.84	10.05	8.26	6.94	172 12	
173	6.44	6.67	7.49	9.06	10.86	12.50	13.66	14.10	13.63	12.46	11.06	10.06	9.30	9.05	9.33	10.22	11.60	12.90	13.82	13.85	13.08	11.64	9.76	8.00	173 12	
174	6.70	6.08	6.22	7.28	9.00	10.94	12.77	14.05	14.63	14.17	12.86	11.33	10.04	9.14	8.86	9.20	10.08	11.26	12.44	13.30	13.32	12.80	11.00	8.85	174 12	
175	7.06	5.67	5.05	5.60	7.15	9.26	11.30	13.28	14.45	14.84	13.95	12.40	10.90	9.46	8.62	8.24	8.56	9.64	11.12	12.55	13.40	13.37	12.07	10.07	175 12	
176	8.20	6.17	4.94	4.74	5.62	7.74	9.76	12.14	14.01	15.00	14.86	13.77	12.06	10.27	8.84	8.10	7.94	8.52	9.68	11.18	12.64	13.37	13.37	13.05	176 11	
177	11.52	9.17	6.76	5.11	4.16	4.64	6.10	8.00	10.50	12.90	14.56	15.33	14.70	13.32	11.14	9.44	8.17	7.54	7.57	8.34	9.81	11.65	13.20	13.60	177 11	
178	12.56	10.40	7.97	5.83	4.38	4.04	4.96	6.82	9.02	11.57	13.86	15.24	15.44	14.56	12.56	10.36	8.63	7.62	7.30	7.74	8.86	10.67	12.47	13.67	178 11	
179	13.60	12.02	9.66	6.93	4.96	3.94	4.22	5.70	7.84	10.40	12.82	14.74	15.56	15.33	13.80	11.44	9.35	7.79	7.04	7.03	7.90	9.44	11.66	13.22	179 11	
180	13.92	13.00	10.74	8.00	5.64	4.04	3.83	4.76	6.70	9.02	11.37	13.67	15.12	15.46	14.48	12.44	9.96	8.10	6.86	6.42	6.94	8.42	10.44	12.57	180 11	
181	13.67	13.68	12.22	9.64	6.86	4.96	3.98	4.36	5.65	7.72	10.02	12.26	14.33	15.28	15.12	13.77	11.30	9.01	7.37	6.64	6.56	7.46	9.06	11.01	181 11	
182	12.70	13.51	13.01	11.07	8.44	6.12	4.72	4.42	5.32	6.94	8.97	11.17	13.22	14.74	15.17	14.22	13.16	9.74	7.86	6.74	6.51	7.07	8.16	9.92	182 11	
183	11.66	12.82	13.10	11.86	9.72	7.36	5.70	5.02	5.34	6.42	8.07	10.12	11.98	13.73	14.86	14.72	13.40	11.17	9.22	7.55	6.51	6.57	7.34	8.72	183 11	

184	10.61	12.04	12.77	12.64	11.27	9.34	7.48	6.30	5.87	6.54	7.66	9.24	10.97	12.94	14.38	14.88	14.20	12.50	10.34	8.44	7.22	6.77	6.97	7.87	184 11
185	9.34	10.94	12.19	12.66	12.27	10.84	9.25	7.90	6.96	6.92	7.56	8.50	10.00	11.48	13.23	14.36	14.44	13.38	11.42	9.60	8.02	6.94	6.56	6.92	185 11
186	7.79	9.26	10.80	11.92	12.43	12.16	11.12	9.70	8.48	7.63	7.56	8.14	9.04	10.41	11.98	13.30	13.98	13.72	12.51	10.84	8.96	7.47	6.70	6.48	186 11
187	6.84	7.86	9.16	10.52	11.71	12.36	12.28	11.46	10.38	9.16	8.34	8.14	8.38	9.04	10.37	11.82	13.16	13.66	13.27	11.87	10.24	8.57	7.05	6.14	187 11
188	5.87	6.26	7.22	8.72	10.36	11.70	12.56	12.86	12.14	11.14	9.86	8.86	8.32	8.34	9.02	10.46	11.88	13.12	13.48	12.96	11.86	10.30	8.58	7.00	188 11
189	5.74	5.32	5.74	6.86	8.67	10.62	12.30	13.47	13.96	13.31	12.10	10.48	9.04	8.28	8.37	8.98	10.28	11.72	13.02	13.62	13.24	12.02	10.14	8.20	189 11
190	6.16	4.76	4.31	4.90	6.40	8.62	10.94	13.04	14.57	15.22	14.64	12.87	10.58	8.66	7.68	7.62	8.40	10.00	11.70	13.12	13.97	13.69	12.32	10.27	190 11
191	7.76	5.44	3.88	3.19	3.88	5.80	8.60	11.46	13.90	15.54	16.06	15.08	12.92	10.40	8.23	7.07	6.90	7.82	9.54	—	11.60	13.35	14.38	14.34	191 10
192	12.76	10.16	7.15	4.46	2.56	2.27	3.49	5.92	8.80	12.36	15.04	16.76	17.06	15.90	13.27	10.08	7.42	6.03	6.04	7.17	9.30	11.84	13.92	15.05	192 10
193	14.90	13.08	9.91	6.43	3.53	1.84	1.84	3.58	6.20	9.54	13.00	15.92	17.60	17.55	15.88	12.54	9.04	6.46	5.24	5.54	6.76	9.24	12.48	14.76	193 10
194	16.12	15.46	13.17	9.32	5.65	2.96	1.56	1.90	3.97	6.70	10.13	13.94	16.80	18.22	17.87	15.72	12.00	8.47	5.86	4.66	4.98	6.66	9.72	13.12	194 10
195	15.46	16.44	15.54	12.76	8.60	5.17	2.76	1.62	2.37	4.50	7.60	11.14	14.80	17.30	18.38	17.46	14.77	11.14	7.30	5.12	4.24	4.66	6.66	9.96	195 10
196	13.24	15.56	16.37	15.10	12.10	8.47	5.36	3.22	2.47	3.46	5.71	8.66	12.13	15.36	17.38	17.97	16.76	13.80	10.58	7.04	4.79	4.26	5.04	7.14	196 10
197	10.42	13.85	15.77	16.14	14.53	11.60	8.45	5.84	4.20	3.82	5.12	6.97	9.80	13.00	15.56	17.04	17.17	15.44	12.60	9.26	6.86	5.22	4.84	5.76	197 10
198	8.06	10.85	13.97	15.36	15.40	13.86	11.04	8.20	6.43	5.40	5.54	6.64	7.95	10.24	12.80	15.30	16.34	15.86	14.11	11.28	8.50	6.30	5.34	5.40	198 10
199	6.24	8.00	10.50	12.97	14.30	14.44	12.94	10.92	9.08	7.74	7.24	7.56	8.14	9.16	11.11	13.10	14.71	15.40	14.72	12.96	10.60	8.38	6.86	5.92	199 10
200	6.05	6.82	8.26	10.28	12.30	13.38	13.40	12.62	11.34	10.16	9.24	8.58	8.59	8.86	9.62	10.96	12.55	13.78	14.07	13.40	11.92	10.10	8.37	6.87	200 10
201	6.38	6.51	7.24	8.41	9.82	11.28	12.52	12.68	11.87	10.93	10.01	9.34	9.14	9.27	9.97	10.90	12.12	13.14	13.41	12.71	11.34	9.77	8.47	201 10	
202	7.34	6.76	6.86	7.36	8.56	10.06	11.46	12.50	13.02	12.96	12.57	11.86	10.96	10.04	9.53	9.52	9.76	10.73	11.74	12.78	13.04	12.50	11.42	10.20	202 10
203	8.76	7.52	6.90	6.76	7.25	8.50	10.20	11.86	13.24	13.87	13.87	13.28	12.22	11.04	10.07	9.54	9.50	9.87	10.64	11.70	12.60	12.94	12.66	11.70	203 10
204	10.10	8.56	7.16	6.24	6.28	7.14	8.62	10.44	12.07	13.40	14.20	14.14	13.28	12.08	10.74	9.52	8.94	8.94	9.48	10.50	11.72	12.63	13.06	12.60	204 10
205	11.28	9.36	7.66	6.38	5.86	6.06	7.07	8.94	10.96	13.07	14.58	15.07	14.54	13.34	11.84	10.26	9.14	8.46	8.46	9.16	10.36	11.74	13.14	13.52	205 10
206	12.81	11.24	9.13	7.31	5.74	5.33	6.10	7.65	9.76	12.02	14.00	15.20	15.33	14.58	12.97	11.01	9.35	8.37	8.18	8.73	9.62	10.95	12.64	13.76	206 10
207	13.92	—	12.56	10.36	8.02	6.14	5.26	5.24	6.52	8.36	10.60	12.96	14.83	16.05	15.68	14.35	12.14	9.94	8.56	8.04	8.20	8.78	9.99	11.82	207 9
208	13.73	14.66	14.04	11.84	8.90	6.50	5.04	4.74	5.78	7.22	9.33	11.77	14.22	15.86	16.07	15.15	13.18	10.77	8.67	7.57	7.18	7.78	8.96	10.77	208 9
209	12.83	14.27	14.50	13.28	10.70	7.76	5.53	4.56	4.86	6.26	8.20	10.44	13.14	15.37	16.51	16.11	14.47	11.94	9.36	7.58	6.88	7.16	8.00	9.72	209 9
210	11.80	13.84	14.90	14.32	12.37	9.57	6.78	5.10	4.56	5.42	7.13	9.26	11.96	14.36	15.96	16.14	15.17	12.96	10.25	8.01	6.67	6.34	6.89	8.16	210 9
211	10.14	12.46	14.24	14.84	13.50	10.90	8.02	5.86	4.76	5.04	6.52	8.34	10.66	13.15	15.27	16.14	15.82	14.14	11.47	8.96	7.02	6.16	6.33	7.34	211 9
212	9.23	11.44	13.54	14.58	14.24	12.42	9.84	7.44	5.64	5.14	5.97	7.54	9.60	11.76	13.95	15.50	15.83	14.93	12.72	10.10	7.72	6.16	5.77	6.54	212 9
213	7.96	9.86	12.04	13.74	14.37	13.56	11.51	8.97	7.02	5.96	5.96	7.12	8.61	10.53	12.64	14.44	15.55	15.26	13.84	11.46	8.86	6.95	5.97	6.05	213 9
214	7.05	8.56	10.54	12.48	13.67	13.96	12.84	10.98	9.00	7.60	6.88	7.24	8.26	9.66	11.37	13.15	14.57	15.10	14.32	12.72	10.34	8.27	6.67	6.12	214 9
215	6.40	7.34	8.74	10.52	12.26	13.26	13.32	12.36	10.84	9.38	8.24	7.77	8.12	8.86	10.16	11.76	13.33	14.29	14.38	13.46	11.64	9.64	7.76	6.48	215 9
216	6.10	6.50	7.54	9.00	10.63	12.05	12.96	13.18	12.64	11.47	10.24	9.16	8.76	9.04	9.66	10.72	12.02	13.24	14.10	14.04	13.02	11.29	9.63	7.96	216 9
217	6.84	6.50	6.73	7.66	9.04	10.52	12.10	13.14	13.55	13.28	12.50	11.34	10.26	9.52	9.35	9.67	10.59	11.83	12.88	13.62	13.44	12.54	11.15	9.50	217 9
218	7.86	6.50	5.94	6.16	7.10	8.50	10.20	11.94	13.44	14.14	14.16	13.42	12.16	10.76	9.56	9.05	9.15	9.96	11.33	12.62	13.38	13.55	12.96	11.68	218 9
219	9.90	7.96	6.26	5.30	5.46	6.46	8.25	10.24	12.44	14.18	15.26	15.50	14.64	12.94	10.78	9.16	8.56	8.76	9.78	11.16	12.57	13.70	14.26	14.02	219 9
220	12.80	10.52	8.01	5.84	4.76	4.81	5.98	7.77	10.32	13.02	15.24	16.66	16.76	15.58	13.24	10.54	8.38	7.60	7.78	8.76	10.54	12.56	14.24	15.18	220 9
221	14.86	13.21	10.40	7.41	4.97	3.62	3.84	5.16	7.44	10.44	13.54	16.14	17.54	17.44	15.84	12.90	9.72	7.44	6.60	6.85	8.10	10.22	12.92	15.15	221 9
222	16.26	15.72	13.66	10.33	6.96	4.40	3.04	—	3.33	5.32	7.86	11.08	14.56	17.20	18.37	18.04	16.16	12.38	8.82	6.46	5.54	5.05	7.72	10.60	222 8
Sum	769.73	738.35	721.10	680.42	642.70	620.46	605.70	645.71	699.54	763.58	829.96	887.21	914.17	945.43	935.76	904.46	859.81	810.17	766.70	727.42	726.17	733.12	751.00	768.07	No. of Days 73d 19h 18.46m 9.3s
No.	74	73	74	74	74	74	73	73	74	74	74	74	73	74	74	74	74	74	73	74	74	74	74	74	74

FORMS FOR SHORT-PERIOD TIDES.

SERIES K.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
223	13.60	16.07	17.04	16.38	13.96	10.25	6.47	3.74	2.56	3.20	5.12	8.18	11.74	15.30	17.66	18.90	14.76	10.60	7.27	5.06	4.48	5.07	7.18	223 8		
224	10.36	13.04	16.34	17.16	16.04	13.12	9.20	5.80	3.36	2.56	3.60	5.73	9.03	12.78	15.94	17.78	18.04	16.74	13.32	9.36	6.05	4.18	3.80	4.90	224 8	
225	7.56	11.01	14.46	16.66	16.88	15.39	12.15	8.23	5.44	3.52	3.32	4.58	7.04	10.14	13.35	16.16	17.52	17.26	15.28	11.80	8.22	5.32	3.80	4.02	225 8	
226	5.58	8.40	11.50	14.52	16.18	16.06	14.38	11.26	7.98	5.62	4.54	4.80	6.25	8.27	11.00	13.96	16.32	17.26	16.42	14.32	10.85	7.62	5.16	4.10	226 8	
227	4.64	6.45	8.92	12.05	14.70	15.80	15.18	13.36	10.62	7.94	6.32	5.74	6.44	7.77	9.72	12.07	14.12	15.66	15.72	14.46	12.06	9.36	6.96	5.40	227 8	
228	5.07	3.84	7.33	9.54	11.87	13.60	14.46	13.96	12.48	10.40	8.65	7.45	7.28	8.00	9.26	10.72	12.27	13.74	14.47	14.18	12.78	10.82	8.78	6.78	228 8	
229	5.83	5.86	6.74	8.34	10.14	12.02	13.26	13.57	12.85	11.76	10.70	9.74	9.12	8.90	9.34	10.06	10.94	12.10	12.88	13.72	13.38	11.88	10.06	8.17	229 8	
230	7.02	6.68	7.00	7.70	8.77	10.10	11.44	12.33	13.66	12.46	12.00	11.36	10.62	10.07	9.67	9.77	10.12	10.82	11.54	12.43	12.67	12.12	11.23	9.96	230 8	
231	8.64	7.77	7.46	7.69	8.30	9.04	10.10	11.17	12.34	12.90	12.90	12.34	11.72	11.15	10.62	10.30	10.00	10.14	10.50	11.34	11.96	12.26	11.97	11.38	231 8	
232	10.53	9.44	8.35	7.66	7.57	8.12	9.06	10.48	11.57	12.72	13.42	13.56	13.18	12.30	11.45	10.72	10.26	9.92	9.63	10.00	10.71	11.62	12.32	12.18	232 8	
233	11.42	10.36	9.08	8.15	7.53	7.24	7.70	8.54	9.82	11.43	12.72	13.64	13.66	13.26	12.36	11.22	10.18	9.34	8.97	9.08	9.88	10.76	11.64	12.26	233 8	
234	12.35	11.85	10.40	8.78	7.36	6.44	6.28	7.14	8.37	10.20	11.94	13.38	14.40	14.54	13.58	12.17	10.70	9.34	8.82	8.84	9.26	10.00	11.16	12.50	234 8	
235	13.30	13.42	12.06	10.16	8.40	6.86	6.06	6.14	7.20	8.95	10.80	12.76	13.96	14.91	14.84	13.64	11.84	9.97	8.77	8.36	8.48	8.96	10.06	11.56	235 8	
236	13.12	13.97	13.64	12.06	9.70	7.27	5.96	5.56	6.35	7.80	9.76	11.70	13.66	15.10	15.46	14.62	12.86	10.57	8.64	7.46	7.31	7.76	8.84	10.72	236 8	
237	12.64	14.21	14.62	13.44	11.00	8.24	6.24	5.17	5.36	6.54	8.54	10.66	13.00		15.02	15.96	15.50	14.08	11.60	8.97	7.34	6.70	6.84	7.80	237 7	
238	9.62	11.70	13.76	14.95	14.67	12.76	10.00	7.37	5.56	4.97	5.74	7.38	9.36	11.94	14.36	16.04	16.27	15.32	13.08	10.11	7.72	6.36	6.10	6.94	238 7	
239	8.63	10.83	13.20	15.21	15.71	14.43	11.89	8.54	6.26	4.97	5.06	6.36	8.22	10.64	13.40	15.80	16.62	16.16	14.21	11.38	8.34	6.35	5.46	5.74	239 7	
240	7.13	9.22	11.84	14.36	15.71	15.48	13.64	10.66	7.60	5.70	4.96	5.70	7.24	9.54	12.02	14.56	16.24	16.56	15.34	12.80	9.60	7.06	5.50	5.18	240 7	
241	5.94	7.72	10.28	13.04	15.14	15.90	14.88	12.52	9.63	7.07	5.74	5.64	6.67	8.36	10.62	13.17	15.30	16.38	15.97	14.06	11.04	8.16	6.11	5.05	241 7	
242	5.41	6.72	8.83	11.26	13.77	15.36	15.38	14.00	11.90	8.72	6.86	5.97	6.34	7.52	9.30	11.47	13.80	15.46	15.84	14.77	12.44	9.37	7.06	5.37	242 7	
243	4.85	5.64	7.12	9.24	11.64	13.96	15.06	14.75	13.17	10.76	8.64	7.30	6.86	7.44	8.64	10.38	12.36	14.06	15.24	15.10	13.64	11.26	8.61	6.50	243 7	
244	5.32	5.38	6.34	7.85	9.86	11.96	13.64	14.58	14.07	12.68	10.68	8.97	8.02	7.81	8.36	9.26	10.60	12.24	13.73	14.44	13.86	12.25	10.02	8.06	244 7	
245	6.46	5.62	5.78	6.47	7.80	9.63	11.38	12.97	13.74	13.44	12.44	11.04	11.92	10.73	9.67	9.16	9.18	9.63	10.54	11.48	12.46	12.92	12.66	11.74	245 7	
246	8.36	6.87	6.17	6.26	7.02	8.17	9.66	11.26	12.55	13.37	13.57	12.94	13.67	12.68	11.26	10.02	9.22	8.90	9.14	9.86	10.86	12.02	12.84	12.98	246 7	
247	10.42	8.87	7.44	6.44	6.21	6.66	7.76	9.20	10.76	12.36	13.54	14.05	13.67	12.68	11.26	10.02	9.22	8.90	9.14	9.86	10.86	12.02	12.84	13.98	247 7	
248	12.36	11.16	9.5	7.60	6.24	5.63	5.97	7.17	8.80	10.66	12.80	14.28	14.96	14.74	13.66	11.85	10.04	8.66	8.02	8.14	9.04	10.38	12.00	13.14	248 7	
249	13.74	13.40	12.04	10.04	7.64	5.76	4.78	5.02	6.24	8.16	10.78	13.20	15.04	15.98	15.74	14.33	11.96	9.30	7.37	6.55	6.70	8.06	9.98	12.06	249 7	
250	13.93	14.86	14.44	12.80	10.18	7.37	5.17	3.90	4.03	5.50	7.96	10.88	13.80	16.04	17.04	16.46	14.44	11.04	8.24	6.27	5.15	5.63	7.24	9.64	250 7	
251	12.32	14.74	15.98	15.46	13.29	9.94	6.63	4.34	3.17	2.53	5.38	8.20	11.40	14.56	16.82	17.44	16.36	13.83	9.98	6.70	4.46	3.84	4.58	6.80	251 7	
252	10.06	13.28	15.76	16.64	15.75	12.94	9.26	6.06	3.66	2.67	3.72	5.66	8.70	12.20	15.53	17.33	15.87	12.42								252 6
253	4.55	7.26	10.87	14.22	16.50	17.05	15.47	12.37	8.44	5.52	3.48	3.10	4.46	6.74	9.94	13.47	16.22	17.47	17.02	14.77	10.84	7.23	4.52	3.00	253 6	
254	3.30	5.07	8.06	11.72	14.94	16.86	16.90	14.94	11.54	8.00	5.38	3.90	4.20	5.52	7.95	11.06	14.30	16.51	17.04	15.88	12.99	9.17	5.97	3.70	254 6	
255	2.94	3.94	6.16	9.14	12.45	15.42	16.68	16.10	13.81	10.56	7.46	5.47	4.87	5.60	7.04	9.54	12.25	14.81	16.16	16.06	14.44	11.07	7.87	5.34	255 6	
256	3.84	3.92	5.16	7.43	10.36	13.44	15.47	16.04	14.92	12.66	9.98	7.74	6.47	6.36	7.02	8.54	10.58	12.80	14.58	15.36	14.73	12.82	9.86	7.17	256 6	
257	5.31	4.44	5.02	6.44	8.50	11.04	13.56	14.79	14.77	13.46	11.46	9.44	8.00	7.36	7.56	8.36	9.51	11.10	12.60	13.73	13.94	12.90	11.02	8.73	257 6	

258	5.90	5.70	5.63	6.34	7.60	9.36	11.36	13.14	13.88	13.60	12.43	10.94	9.64	8.76	8.44	8.70	9.18	9.95	10.88	12.06	12.76	12.71	11.64	9.87	258	6
259	8.26	7.04	6.44	6.67	7.34	8.36	9.74	11.16	12.22	12.70	12.20	11.38	10.60	9.88	9.34	9.16	9.13	9.34	9.87	10.66	11.30	11.62	11.37	10.56	259	6
260	9.48	8.44	7.52	7.14	7.33	7.86	8.66	9.84	10.90	11.62	11.97	11.87	11.54	11.08	10.42	9.92	9.60	9.42	9.54	9.86	10.24	10.70	10.91	10.80	260	6
261	10.34	9.74	9.06	8.35	7.72	7.46	7.67	8.44	9.64	10.73	11.52	11.88	12.06	11.88	11.53	10.97	10.23	9.48	9.04	9.01	9.38	10.01	10.64	11.05	261	6
262	11.18	10.94	10.46	9.52	8.56	7.74	7.42	7.64	8.34	9.42	10.67	11.65	12.46	12.82	12.62	12.04	10.96	9.85	8.96	8.54	8.42	8.86	9.64	10.44	262	6
263	11.23	11.67	11.60	10.92	9.74	8.36	7.26	6.68	6.86	7.74	9.24	10.86	12.34	13.24	13.55	13.17	12.08	10.64	9.21	8.06	7.54	7.74	8.74	9.92	263	6
264	11.30	12.38	12.82	12.42	11.17	9.62	7.86	6.55	6.10	6.54	7.88	9.68	11.56	13.16	14.03	14.06	13.18	11.60	9.86	8.07	6.97	6.64	7.14	8.38	264	6
265	10.20	11.92	13.16	13.44	12.50	10.70	8.70	6.90	5.75	5.50	6.36	8.04	10.20	12.32	13.87	14.64	14.36	12.87	10.73	8.45	6.71	5.90	6.17	7.29	265	6
266	9.02	11.07	13.02	14.14	14.04	12.68	10.30	7.96	6.07	5.14	5.48	6.87	9.06	11.46	13.68	15.18	15.37	14.28	12.24	9.67	7.34	5.74	5.30	6.12	266	6
267	7.84	9.97	12.54	14.50	15.33	14.46	12.23	9.34	6.94	5.36	4.94	5.94	8.06	10.08	12.62	14.76	15.76	15.26	13.46	10.67	7.88	5.74	4.48	4.66	267	6
268	6.00	8.44	11.24	13.97	15.67	15.66	14.20	11.46	8.47	6.20	4.97	5.22	6.65	8.86	11.54	14.06	15.76	16.07	14.86	12.14	9.06	6.37	4.56	268	5	
269	3.93	4.93	6.93	9.67	12.77	15.34	16.35	15.80	13.61	10.52	7.73	5.58	4.88	5.77	7.56	10.04	12.74	14.90	15.94	15.62	13.71	10.64	7.47	5.10	269	5
270	3.54	3.83	5.50	7.97	11.14	14.16	16.01	16.37	15.04	12.33	9.34	6.97	5.54	5.42	6.51	8.50	11.14	13.77	15.60	15.98	14.86	12.14	8.87	6.16	270	5
271	4.30	3.67	4.60	6.44	9.03	12.27	14.84	16.21	15.96	14.09	11.42	8.56	6.75	5.80	6.17	7.42	9.65	12.22	14.26	15.46	15.24	13.48	10.57	7.65	271	5
272	5.42	3.96	4.06	5.34	7.30	9.97	12.69	14.83	15.87	15.16	13.24	10.76	8.47	7.04	6.68	7.20	8.44	10.38	12.56	14.16	14.83	14.05	12.07	9.24	272	5
273	7.02	5.32	4.44	4.61	5.87	7.97	10.37	13.07	14.81	15.06	14.13	12.37	10.44	8.86	7.87	7.56	7.92	8.94	10.67	12.44	13.74	13.97	12.81	10.83	273	5
274	8.83	7.10	5.78	5.25	5.76	6.66	8.34	10.76	12.86	14.16	14.44	13.68	12.40	10.86	9.52	8.53	8.21	8.56	9.40	10.68	12.08	13.04	13.08	11.93	274	5
275	10.54	9.05	7.64	6.61	6.06	6.30	7.07	8.81	10.63	12.30	13.68	14.16	13.66	12.66	11.46	10.12	9.18	8.77	8.56	9.10	10.17	11.30	12.30	12.61	275	5
276	12.14	11.16	9.92	8.44	7.14	6.37	6.38	7.34	8.76	10.57	12.10	13.44	13.92	13.88	13.56	12.37	11.18	9.72	8.32	7.60	7.94	9.26	10.84	12.04	276	5
277	12.52	12.48	11.98	11.16	9.77	7.94	6.58	6.06	6.50	7.97	9.84	11.56	13.26	14.17	14.66	14.52	13.27	11.34	9.06	7.37	6.82	7.46	8.74	10.60	277	5
278	12.11	13.20	14.04	13.84	12.76	10.92	8.58	6.74	5.94	6.30	7.68	9.72	11.97	13.90	15.26	15.99	15.54	13.97	11.26	8.63	6.70	5.98	6.37	7.97	278	5
279	10.25	12.66	14.44	15.38	15.04	13.48	11.07	8.36	6.38	5.47	5.87	7.36	9.62	12.14	14.54	16.28	16.98	16.37	13.80	10.49	7.50	5.61	5.14	5.74	279	5
280	7.77	10.54	13.45	15.71	16.85	16.30	14.16	10.84	7.77	5.85	5.07	5.66	7.50	9.87	12.74	15.25	16.92	17.15	15.62	12.54	8.66	5.94	4.14	3.96	280	5
281	5.28	7.85	11.15	14.38	16.70	17.32	16.33	13.48	9.84	7.20	5.47	4.98	5.96	7.74	10.58	13.66	16.26	17.40	16.86	14.56	10.89	7.40	4.72	3.37	281	5
282	3.98	5.86	8.86	12.43	15.47	17.34	17.64	16.26	12.76	9.26	6.56	5.24	5.38	6.54	8.77	11.76	14.62	16.82	17.12	15.72	12.71	9.14	6.06	3.77	282	5
283	3.17	4.42	6.67	9.72	13.44	16.25	17.55	17.22	15.06	11.70	8.40	6.26	5.44	6.06	7.47	10.01	12.74	15.12	16.37	16.06	14.21	11.04	7.42	283	4	
284	4.80	3.12	3.62	5.50	8.04	11.13	14.40	16.50	17.22	16.16	13.58	10.36	7.77	6.24	6.04	6.91	8.53	10.52	13.06	15.02	15.64	14.36	11.93	8.64	284	4
285	6.01	4.31	3.47	4.52	6.20	8.94	11.94	14.56	16.24	16.32	14.74	12.13	9.47	7.47	6.58	6.90	7.84	9.30	11.26	13.26	14.41	14.26	12.74	10.35	285	4
286	7.88	5.80	4.44	4.58	5.92	7.85	10.30	12.70	14.67	15.54	15.01	13.36	11.14	9.11	7.80	7.42	7.74	8.64	10.04	11.80	13.04	13.64	13.06	11.36	286	4
287	9.07	7.14	5.84	5.47	6.20	7.44	9.04	10.97	13.06	14.36	14.36	13.40	11.83	10.44	9.16	8.44	8.24	8.54	9.26	10.30	11.46	12.12	12.22	11.46	287	4
288	10.00	8.37	7.08	6.36	6.44	7.32	8.34	9.60	11.24	12.72	13.46	13.28	12.32	11.06	10.10	9.27	8.97	8.94	9.08	9.61	10.14	11.01	11.52	11.46	288	4
289	10.73	9.52	8.47	7.66	7.41	7.56	8.04	8.76	9.91	11.17	12.30	12.88	12.66	11.92	11.04	10.37	9.76	9.36	9.12	9.08	9.27	9.86	10.44	10.68	289	4
290	10.66	10.30	9.78	9.22	8.56	8.06	7.74	8.02	8.86	10.06	11.16	12.02	12.40	12.34	12.06	11.48	10.82	9.97	9.24	8.77	8.68	8.96	9.55	10.22	290	4
291	10.70	10.88	10.82	10.57	10.03	9.26	8.44	7.90	8.07	8.80	9.84	10.90	11.78	12.36	12.58	12.54	12.07	11.12	9.97	8.90	8.23	8.12	8.56	9.27	291	4
292	10.10	10.90	11.50	11.78	11.53	10.67	9.30	8.14	7.56	7.77	8.55	9.74	11.07	12.15	12.94	13.28	13.04	12.24	10.77	9.14	7.88	7.18	7.36	8.12	292	4
293	9.26	10.62	11.94	12.78	12.88	12.06	10.48	8.86	7.70	7.28	7.65	8.65	10.02	11.54	12.81	13.77	14.04	13.50	12.16	10.00	8.34	6.96	6.50	6.88	293	4
294	7.96	9.76	11.52	13.07	13.96	13.77	12.48	10.52	8.76	7.36	6.77	7.26	8.52	10.36	12.17	13.66	14.56	14.48	13.40	11.12	8.84	6.87	5.64	5.46	294	4
295	6.30	8.06	10.30	12.80	14.34	15.00	14.16	12.26	9.96	7.92	6.50	6.22	7.10	8.82	10.86	13.12	14.54	15.07	14.56	12.60	9.98	7.47	5.46	4.56	295	4
296	4.96	6.60	9.03	11.80	14.15	15.84	15.96	14.52	12.00	9.24	7.24	6.16	6.40	7.67	9.66	11.93	14.14	15.62	15.76	14.36	11.76	8.61	6.02	4.24	296	4
Sum	617.23	654.72	698.28	764.60	807.84	825.07	812.56	780.34	723.32	704.58	688.28	691.72	722.35	755.99	828.47	884.66	921.14	927.27	897.33	832.70	770.54	696.55	637.83	603.82	No. of Days, 73 <sup>d</sup> 20 <sup>h</sup> 18.24 <sup>m</sup> 10 <sup>s</sup>	
No.	74	74	73	74	74	74	74	74	73	74	74	74	74	73	74	74	74	74	74	74	73	74	74	74	74	

**FORMS FOR SHORT-PERIOD TIDES.**  
**SERIES K.—(Continued).**

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour		
297	3.86	5.14	7.31	10.15	13.10	15.67	16.78	16.26	14.16	11.00	8.32	6.36	5.84	6.47	8.16	10.16	12.84	15.02	16.10	15.46	13.28	9.87	6.84	4.45	297	4	
298	3.04	3.57	5.44	8.15	11.37	14.60	16.81	17.35	16.28	13.64	10.44	7.71	6.07	5.84	6.88	8.87	11.47	14.12	15.94	16.22	14.81	11.87	8.55	298	3		
299	5.46	3.46	2.87	4.17	6.35	9.32	13.00	15.95	17.47	17.44	15.72	12.68	9.66	7.28	5.94	6.04	7.36	9.64	12.45	14.84	16.04	15.60	13.70	10.52	299	3	
300	7.15	4.66	2.92	3.10	4.72	7.47	10.55	13.92	16.35	17.36	16.74	14.57	11.67	8.85	6.76	5.94	6.28	7.70	9.92	12.68	14.78	15.38	14.78	12.36	300	3	
301	9.26	6.36	4.20	3.07	3.72	5.55	8.04	11.05	14.10	16.17	16.96	16.12	14.06	11.35	8.82	7.14	6.57	7.02	8.46	10.56	13.14	14.64	15.04	13.76	301	3	
302	11.47	8.74	6.42	4.70	4.22	5.00	6.80	9.02	11.88	14.60	16.14	16.22	15.16	13.36	10.86	8.96	7.58	7.14	7.44	8.84	10.92	12.84	13.84	13.86	302	3	
303	12.57	10.68	8.54	6.84	5.56	5.27	5.98	7.33	9.36	11.72	14.00	15.22	15.38	14.58	12.88	11.01	9.42	8.12	7.64	7.92	8.94	10.40	11.85	12.91	303	3	
304	13.12	12.26	10.75	9.22	7.66	6.68	6.30	6.72	7.86	9.44	11.50	13.34	14.46	14.66	13.96	12.74	11.30	9.76	8.54	7.93	7.84	8.40	9.60	10.88	304	3	
305	12.66	12.64	12.40	11.47	10.10	8.76	7.68	7.01	7.06	7.90	9.22	10.97	12.56	13.72	14.38	14.04	13.04	11.45	9.76	8.15	7.22	7.02	7.48	8.84	305	3	
306	10.31	11.48	13.55	12.87	12.46	11.36	9.70	8.28	7.14	6.80	7.40	8.84	10.74	12.56	13.87	14.54	14.38	13.40	11.67	9.60	7.53	6.30	5.98	6.50	306	3	
307	8.20	10.07	11.93	13.36	14.04	13.66	12.30	10.26	8.61	7.37	6.86	7.24	6.77	8.02	10.14	12.62	14.56	15.53	15.25	13.56	10.92	8.12	5.82	4.22	307	3	
308	5.86	7.79	10.12	12.66	14.54	15.37	14.86	13.04	10.66	8.56	7.12	6.44	6.77	8.02	10.14	12.62	14.56	15.53	15.25	13.56	10.92	8.12	5.82	4.22	308	3	
309	4.10	5.32	7.79	10.85	13.60	15.51	16.05	15.06	12.86	10.40	8.16	6.53	5.96	6.51	8.24	10.85	13.27	15.16	15.84	15.03	12.98	9.78	7.04	4.71	309	3	
310	3.46	3.86	5.60	8.44	11.74	14.64	16.50	16.72	15.38	12.86	9.98	7.70	6.25	5.93	6.71	8.67	11.25	13.84	15.52	15.84	14.55	11.68	8.46	5.64	310	3	
311	3.63	3.01	4.08	6.50	9.62	13.08	15.81	17.12	16.72	14.87	12.03	9.20	7.26	6.32	6.37	7.46	9.60	12.20	14.35	15.67	15.28	13.15	10.15	7.00	311	3	
312	4.47	3.03	3.22	5.03	7.60	10.76	14.05	16.38	17.05	16.14	13.92	11.10	8.66	6.87	6.16	6.46	8.00	10.44	13.10	14.76	15.16	13.92	11.40	8.36	312	3	
313	5.66	3.69	3.94	3.94	6.18	9.01	12.24	14.92	16.53	16.56	15.16	12.66	10.06	7.96	6.74	6.60	7.35	9.00	11.24	13.43	14.50	14.50	12.66	313	2		
314	9.94	7.20	4.97	3.56	3.77	5.34	7.72	10.56	13.46	15.64	16.34	15.71	13.92	11.46	9.28	7.66	6.86	6.98	7.98	9.96	12.00	13.52	14.02	13.37	314	2	
315	11.18	8.81	6.52	4.86	4.33	5.20	6.90	9.14	11.80	14.20	15.72	15.81	14.66	12.72	10.71	8.96	7.82	7.56	7.92	9.16	10.68	12.24	13.56	13.56	315	2	
316	13.06	10.17	8.00	6.25	5.31	5.50	6.66	8.34	10.52	12.80	14.44	15.18	14.68	13.32	11.56	10.02	8.76	8.10	8.00	8.60	9.65	10.96	12.18	11.58	316	2	
317	13.23	11.04	9.16	7.62	6.54	6.20	6.84	7.96	9.38	11.14	12.91	14.18	14.40	13.64	12.37	10.90	9.58	8.78	8.46	8.68	9.30	10.00	10.94	11.57	317	2	
318	11.80	11.36	10.28	8.94	7.84	7.18	7.20	7.86	8.82	9.98	11.46	12.86	13.86	13.83	12.96	11.72	10.53	9.66	9.14	8.92	8.96	9.17	9.66	10.40	318	2	
319	11.10	11.37	11.01	10.20	9.26	8.46	8.10	8.14	8.66	9.44	10.56	11.74	12.76	13.34	13.26	12.61	11.72	10.86	9.76	9.04	8.80	8.85	9.16	9.64	319	2	
320	10.14	10.74	11.18	11.32	11.06	10.38	9.58	8.94	8.71	8.90	9.50	10.42	11.46	12.48	13.10	13.15	12.64	11.84	10.76	9.71	8.88	8.35	8.19	8.42	320	2	
321	9.04	9.96	10.86	11.50	11.80	11.55	10.96	9.98	9.08	8.64	8.75	9.38	10.38	11.46	12.41	13.07	13.16	12.84	11.84	10.56	9.24	8.13	7.50	7.43	321	2	
322	7.86	8.83	10.03	11.16	12.23	12.80	12.64	11.66	10.25	9.04	8.36	8.34	8.96	10.02	11.20	12.46	13.23	13.47	13.00	11.72	10.14	8.38	7.03	6.27	322	2	
323	6.31	7.08	8.52	10.23	11.92	13.17	13.63	13.10	11.86	10.18	8.76	7.98	7.96	8.75	10.13	11.64	13.14	13.94	13.94	13.04	11.34	9.30	7.45	5.86	323	2	
324	5.13	5.46	6.76	8.80	11.15	13.20	14.66	14.98	13.87	11.76	9.58	8.10	7.96	8.75	10.13	11.64	13.14	13.94	13.94	13.04	11.34	9.30	7.45	5.86	324	2	
325	4.14	3.74	4.67	6.71	9.27	12.02	14.40	15.66	15.44	13.71	11.16	8.74	7.02	6.40	6.78	8.22	9.82	11.76	13.33	14.28	14.14	12.87	10.56	9.36	6.51	325	2
326	4.12	2.75	2.94	4.56	7.03	10.05	13.27	15.05	16.62	15.90	13.76	10.86	8.17	6.45	5.84	6.36	8.12	10.37	12.25	13.88	14.74	14.20	12.26	9.36	6.51	326	2
327	4.96	2.57	1.63	2.58	4.74	7.64	11.12	14.22	16.47	17.07	15.75	12.96	8.86	7.26	5.65	5.46	6.44	8.40	11.20	13.57	15.11	15.17	13.27	9.96	327	2	
328	6.40	3.62	1.76	1.54	3.26	6.02	9.25	12.97	15.66	17.40	17.35	15.37	12.23	9.00	6.75	5.63	6.43	8.40	11.20	13.57	15.11	15.17	13.27	9.96	328	2	
329	8.84	5.46	3.00	1.66	2.20	2.20	4.15	6.95	10.46	13.81	16.44	17.54	16.82	14.56	11.38	8.50	6.32	5.44	5.74	7.26	10.06	12.76	14.67	15.26	329	1	
330	14.06	11.32	8.05	5.16	2.94	2.16	3.11	5.16	7.96	11.23	14.30	16.57	17.22	16.23	13.81	10.68	8.07	6.16	5.50	5.88	7.64	10.25	12.77	14.29	330	1	
331	14.72	13.33	10.74	7.81	5.32	3.60	3.26	4.42	6.34	8.86	11.67	14.58	16.33	16.57	15.28	12.84	9.93	7.47	6.23	5.72	6.26	7.94	10.30	12.30	331	1	
332	13.76	13.96	12.68	10.56	8.18	6.28	4.97	4.83	5.73	7.34	9.58	12.05	14.37	15.76	15.80	14.56	13.28	9.94	8.13	6.64	6.14	6.54	8.04	10.04	332	1	

TIDAL OBSERVATIONS

[PLAN VII.]

333	11.78	12.86	13.16	12.24	10.73	8.96	7.30	6.24	5.96	6.50	7.80	9.84	12.15	13.88	14.87	14.84	13.77	11.77	10.06	8.23	6.86	6.34	6.56	7.70	333	1	
334	9.30	10.84	12.16	12.76	12.53	11.48	10.14	8.60	7.52	7.06	7.44	8.47	10.17	11.91	13.34	14.21	14.40	13.72	12.30	10.42	8.41	6.88	6.14	6.37	334	1	
335	7.32	8.81	10.45	11.84	12.86	13.08	12.42	11.25	9.75	8.54	7.84	7.88	8.64	10.02	11.65	13.16	14.14	14.30	13.64	12.17	10.31	8.37	6.68	5.72	335	1	
336	5.86	6.88	8.64	10.40	12.07	13.31	13.88	13.62	12.36	10.67	9.06	8.12	7.90	8.54	9.72	11.26	12.78	13.82	14.20	13.74	12.14	10.05	7.76	6.00	336	1	
337	5.04	5.23	6.52	8.50	10.56	12.60	14.12	14.40	13.86	12.58	10.80	8.97	7.94	7.68	8.24	9.50	11.14	12.75	13.98	14.44	13.73	11.85	9.10	6.84	337	1	
338	5.06	4.41	5.04	6.57	8.66	11.20	13.52	15.24	15.84	15.08	13.13	10.86	9.00	7.82	7.54	8.05	9.36	11.14	12.94	14.20	14.46	13.36	11.28	8.58	338	1	
339	5.98	4.22	3.96	5.07	6.97	9.54	12.26	14.54	16.11	16.34	15.17	12.88	10.26	8.38	7.53	7.40	8.14	9.77	11.52	13.36	14.60	14.56	12.94	10.26	339	1	
340	7.33	5.11	3.87	4.05	5.64	7.81	10.61	13.20	15.47	16.54	16.21	14.70	12.20	9.81	8.08	7.33	7.37	8.31	10.05	12.02	13.86	14.76	14.17	12.16	340	1	
341	8.93	6.32	4.31	3.72	4.64	6.56	9.06	11.87	14.55	16.23	16.72	15.97	13.94	11.34	8.98	7.71	7.36	7.70	9.02	10.97	12.94	14.40	14.70	13.44	341	1	
342	10.64	7.77	5.58	4.12	4.16	5.63	7.85	10.36	13.16	15.34	16.56	16.48	15.11	12.72	10.27	8.26	7.37	7.26	8.12	9.82	11.91	13.58	14.48	14.07	342	1	
343	12.12	9.32	6.72	4.74	3.96	4.91	6.70	9.02	11.70	14.07	15.87	16.56	15.80	13.96	11.44	9.32	7.80	7.24	7.44	8.72	10.57	12.55	14.00	14.24	343	1	
344	13.24	10.72	8.06	5.93	4.58	4.74	6.03	8.20	10.34	—	12.88	15.05	16.23	16.28	14.89	12.63	10.30	8.54	7.57	7.44	8.17	9.64	11.50	13.03	344	0	
345	13.80	13.45	11.78	9.47	7.26	5.64	5.07	5.86	7.43	9.20	11.48	13.56	15.17	15.82	15.18	13.58	11.42	9.46	7.98	7.36	7.62	8.50	10.02	11.60	345	0	
346	12.67	13.00	12.14	10.36	8.34	6.54	5.59	5.67	6.77	8.43	10.27	12.17	13.90	14.96	14.86	13.76	12.00	10.22	8.66	7.73	7.38	7.80	8.82	10.22	346	0	
347	11.48	12.26	12.24	11.15	9.47	8.01	6.87	6.45	6.75	7.83	9.14	10.75	12.56	13.86	14.46	14.06	12.87	11.31	9.72	8.40	7.76	7.73	8.27	9.36	347	0	
348	10.54	11.48	12.02	11.81	10.84	9.56	8.46	7.76	7.56	8.00	8.95	10.05	11.60	13.13	14.20	14.42	13.83	12.50	10.98	9.76	8.76	8.24	8.24	8.80	348	0	
349	9.62	10.53	11.27	11.70	11.62	11.14	10.38	9.49	8.78	8.48	8.71	9.47	10.70	12.04	13.16	13.78	13.79	13.14	11.94	10.54	9.17	8.30	7.83	8.04	349	0	
350	8.58	9.36	10.22	11.00	11.54	11.74	11.57	10.96	10.14	9.44	9.04	9.10	9.74	10.90	12.24	13.16	13.57	13.38	13.14	12.44	11.22	9.78	8.36	7.04	350	0	
351	7.36	7.86	8.85	10.11	11.13	11.95	12.42	12.30	11.78	10.77	9.72	9.06	9.91	9.55	10.76	11.97	12.94	13.38	13.14	12.44	11.22	9.78	8.36	7.04	351	0	
352	6.26	6.15	6.82	8.20	9.97	11.56	12.90	13.50	13.36	12.36	10.92	9.68	8.84	8.68	9.14	10.18	11.57	12.76	13.30	13.22	12.46	11.00	9.17	7.18	352	0	
353	5.75	4.90	4.92	6.07	7.94	10.07	12.03	13.66	14.48	14.16	12.76	10.77	9.04	7.98	7.73	8.23	9.70	11.40	12.74	13.42	13.45	12.54	10.80	8.50	353	0	
354	6.30	4.47	3.64	4.12	5.82	8.20	10.84	13.27	14.95	15.70	14.97	13.05	10.60	8.64	7.50	7.36	8.16	9.80	11.80	13.38	14.33	14.26	13.00	10.50	354	0	
355	7.72	5.17	3.42	2.93	4.16	6.37	9.00	12.12	14.97	16.74	16.96	15.68	13.11	10.34	8.06	6.98	7.04	8.06	10.00	12.15	14.04	15.14	15.03	13.10	355	0	
356	10.20	7.00	4.27	2.40	2.20	3.93	6.57	9.77	13.27	16.13	17.72	17.51	15.78	12.57	9.74	7.27	6.14	6.36	7.56	9.86	12.72	14.77	15.81	15.20	356	0	
357	12.64	9.26	5.91	3.10	1.55	1.93	4.00	7.06	10.68	14.30	17.04	18.34	17.72	15.47	12.00	8.88	6.58	5.67	6.00	7.50	10.14	13.10	15.24	16.17	357	0	
358	14.94	12.16	8.55	5.06	2.64	1.50	2.57	5.14	8.44	11.93	15.00	17.66	18.34	17.37	14.51	10.92	7.77	5.66	5.14	5.64	7.65	10.63	13.44	15.46	358	0	
359	15.86	14.14	10.98	7.68	4.48	2.36	1.77	3.30	5.83	8.90	12.30	15.56	17.50	17.88	16.62	—	13.58	9.97	6.94	5.14	4.70	5.52	7.63	10.73	359	23	
360	13.70	15.36	15.32	13.24	9.92	6.64	4.73	3.07	3.08	4.74	6.97	9.86	13.01	15.80	17.38	17.48	15.95	12.86	9.53	6.72	5.22	4.90	5.87	8.03	360	23	
361	10.96	13.30	14.68	14.83	13.24	10.55	7.68	5.43	4.33	4.63	5.97	8.02	10.57	13.25	15.58	16.60	16.14	14.11	11.13	8.76	6.38	5.17	5.13	6.30	361	23	
362	8.60	10.76	12.74	13.74	13.62	12.37	10.30	8.14	6.53	5.84	6.14	7.14	8.74	10.77	13.13	14.96	15.71	15.12	13.32	10.86	8.44	6.53	5.48	5.27	362	23	
363	6.00	7.78	9.85	11.62	12.84	13.10	12.28	10.74	9.22	7.96	7.33	7.28	7.93	9.16	10.97	13.12	14.54	14.68	13.66	12.28	10.12	8.24	6.78	5.82	363	23	
364	5.70	6.37	7.72	9.40	11.06	12.32	12.86	12.50	11.47	10.24	9.12	8.42	8.24	8.54	9.54	11.12	12.64	13.57	13.57	12.88	11.44	9.87	8.24	6.74	364	23	
365	5.77	5.52	6.12	7.27	8.94	10.64	12.10	13.01	13.12	12.46	11.26	10.02	9.06	8.58	8.66	9.44	10.68	11.96	12.92	13.14	12.66	11.54	10.06	8.36	365	23	
366	6.86	5.72	5.37	5.87	7.17	9.14	11.00	12.70	13.68	13.81	12.94	11.57	10.28	9.14	8.62	8.63	9.20	10.44	11.66	12.53	12.92	12.58	11.64	9.77	366	23	
367	7.86	6.12	5.05	4.78	5.62	7.06	9.15	11.26	13.23	14.30	14.32	13.36	11.78	10.34	9.17	8.44	8.24	8.62	9.76	11.04	12.36	13.08	12.90	11.65	367	23	
368	9.64	7.34	5.52	4.45	4.52	5.76	7.66	9.97	12.43	14.27	15.18	14.97	13.73	11.82	10.16	8.86	8.24	8.26	8.96	10.32	11.70	12.96	13.58	13.16	368	23	
369	11.26	8.91	6.66	4.96	4.33	4.86	6.36	8.55	11.00	13.44	15.21	15.84	15.17	13.56	11.44	9.66	8.38	7.80	7.97	9.00	10.56	12.24	13.46	13.82	369	23	
370	12.72	10.52	7.90	5.74	4.34	4.11	5.34	7.23	9.78	12.44	14.65	15.93	15.94	14.74	12.37	10.23	8.53	7.47	7.31	7.97	9.38	11.36	13.14	14.17	370	23	
371	14.00	12.18	9.43	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	370	2
Sum	670.87	618.09	583.62	568.88	596.11	647.59	715.26	823.36	840.22	865.32	889.31	881.87	858.64	828.38	792.71	765.16	776.25	780.49	792.29	804.99	795.42	798.40	770.62	724.27	No. of Days. 73 <sup>d</sup> 22 <sup>h</sup> 18 <sup>m</sup> 47 <sup>s</sup> 12		
No.	75	75	75	73	74	74	74	74	74	73	74	74	74	74	73	73	74	74	74	74	73	74	74	74	74		

FORMS FOR SHORT-PERIOD TIDES.

BOMBAY—Commencing 0 hours, Astronomical Time, 1st January, 1885.

SERIES P.

Motion per mean Solar hour = 14° 9589314.

Argument ( $\gamma - 2\eta$ ).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour		
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d	h	
1	15.52	12.96	9.13	5.76	3.03	1.68	2.28	4.80	7.90	11.70	15.50	18.00	18.85	18.08	15.14	11.54	8.50	6.21	5.53	6.08	8.20	11.31	14.16	16.06	1	23	
2	16.66	15.40	12.16	8.40	4.86	2.56	1.71	2.90	5.56	8.82	12.94	16.44	18.58	18.97	17.67	14.24	10.56	7.53	5.57	5.16	6.10	8.63	11.84	14.68	2	23	
3	16.63	16.96	15.24	11.92	8.00	4.87	2.80	2.57	4.24	6.84	10.20	14.07	17.26	18.86	18.84	17.06	13.20	9.77	6.90	5.23	4.96	6.16	8.86	12.14	3	23	
4	14.87	16.40	16.40	14.28	11.00	7.63	4.88	3.55	3.86	5.55	8.01	11.36	14.83	17.16	18.38	17.93	15.80	12.16	8.68	6.10	5.05	5.25	6.68	9.24	4	23	
5	12.28	14.51	15.96	15.58	13.48	10.47	7.54	5.76	5.07	5.67	7.22	9.17	12.11	15.02	17.02	17.55	16.63	14.11	10.96	8.16	6.22	5.47	5.84	7.18	5	23	
6	9.67	12.12	14.04	15.00	14.45	12.62	10.24	8.07	7.04	6.84	7.54	8.67	10.60	12.84	15.06	16.36	16.35	15.24	12.76	10.11	8.00	6.64	6.17	6.55	6	23	
7	7.86	9.76	11.80	13.27	14.00	13.64	12.22	10.47	9.05	8.44	8.46	9.03	9.97	11.20	13.05	14.64	15.46	15.18	13.87	11.68	9.76	8.10	7.16	7.03	7	23	
8	7.40	8.29	9.82	11.16	12.55	13.24	13.07	12.20	11.16	10.27	9.64	9.60	9.90	10.60	11.70	14.02	14.44	13.75	12.27	10.82	9.20	7.93	7.24	7.06	8	0	
9	7.34	8.07	9.14	10.55	11.74	12.48	12.66	12.27	11.60	10.93	10.34	9.98	9.86	10.17	11.07	12.14	13.06	13.36	12.72	11.71	10.43	9.14	7.97	7.14	9	0	
10	6.75	6.94	7.74	8.96	10.26	11.64	12.67	13.14	12.97	12.20	11.24	10.48	10.12	10.05	10.23	10.84	11.64	12.27	12.68	12.37	11.53	10.42	8.97	7.80	10	0	
11	6.96	6.38	6.44	7.28	8.73	10.47	12.14	13.23	13.84	13.63	12.58	11.38	10.27	9.77	9.62	9.89	10.44	11.24	11.97	12.52	12.50	11.87	10.54	8.76	11	0	
12	7.34	6.16	5.74	6.34	7.62	9.54	11.46	13.22	14.24	14.58	13.94	12.72	11.24	10.02	9.32	9.14	9.46	10.37	11.48	12.46	13.04	12.84	11.88	10.23	12	0	
13	8.20	6.52	5.62	5.56	6.50	8.14	10.17	12.34	14.10	15.20	15.17	13.97	12.27	10.58	9.35	8.75	8.76	9.26	10.34	11.68	12.96	13.64	13.36	11.80	13	0	
14	9.66	7.32	5.82	5.14	5.44	6.74	8.86	11.26	13.66	15.38	15.87	15.24	13.66	11.54	9.82	8.71	8.16	8.36	9.30	10.74	12.46	13.64	13.98	13.00	14	0	
15	10.84	8.24	6.20	4.76	4.46	5.40	7.36	9.78	12.57	14.82	16.13	15.97	14.56	12.25	10.05	8.46	7.82	7.74	8.41	9.71	11.76	13.30	14.26	14.09	15	0	
16	13.44	9.76	7.00	5.12	4.20	4.63	6.12	8.44	11.24	14.04	15.74	16.36	15.71	13.82	11.22	8.94	7.54	6.94	7.15	8.40	10.27	12.44	14.06	14.68	16	0	
17	13.84	11.50	8.60	5.94	4.37	4.02	5.06	7.26	9.66	12.72	15.20	16.55	16.63	15.27	12.77	9.97	7.86	6.84	6.68	7.56	9.32	11.40	13.55	14.80	17	0	
18	14.78	13.22	10.43	7.48	5.34	4.30	4.66	6.25	8.54	11.38	14.15	16.15	16.88	16.08	14.04	11.02	8.54	6.76	6.12	6.34	7.60	9.84	12.14	14.06	18	0	
19	14.84	14.14	12.06	9.06	6.46	4.67	4.24	5.16	7.15	9.68	12.56	14.87	16.44	16.45	15.00	12.42	9.50	7.22	5.80	5.43	6.26	8.16	10.65	12.88	19	0	
20	14.28	14.56	13.33	10.92	8.30	6.04	4.87	5.06	6.54	8.66	11.04	13.64	15.62	16.36	15.76	13.82	11.00	8.37	6.37	5.54	5.64	6.83	8.93	11.40	20	0	
21	13.32	14.42	14.25	12.47	10.10	7.91	6.34	5.70	6.30	7.70	9.76	12.17	14.36	15.74	15.96	14.86	12.76	10.13	7.78	6.17	5.70	6.11	7.62	9.70	21	0	
22	11.76	13.36	14.14	13.72	12.06	9.94	8.32	7.22	7.01	7.74	8.97	10.80	12.97	14.62	15.50	15.17	13.80	11.46	9.14	7.34	6.17	6.00	6.68	8.02	22	0	
23	9.76	11.65	13.04	13.76	13.34	12.14	10.65	9.07	8.15	8.14	8.68	9.86	11.56	13.36	14.56	15.02	14.37	12.76	10.76	8.71	6.96	6.23	6.09	6.68	7.86	23	1
24	9.46	11.24	12.66	13.36	13.34	12.38	11.08	9.94	9.11	8.88	9.28	10.22	11.70	13.06	14.14	14.41	13.60	12.06	10.26	8.46	7.10	6.25	6.08	6.56	24	1	
25	7.64	9.14	10.84	12.34	13.44	13.81	13.33	12.18	10.75	9.76	9.24	9.34	10.07	11.16	12.40	13.38	13.66	13.03	11.87	10.24	8.47	7.00	5.83	5.38	25	1	
26	5.68	6.78	8.55	10.33	12.22	13.56	14.30	14.16	13.05	11.56	10.06	9.11	8.87	9.40	10.46	11.87	12.94	13.44	13.33	12.40	10.74	8.86	6.83	5.22	26	1	
27	4.41	4.77	6.10	8.10	10.50	12.63	14.53	15.56	15.33	13.76	11.64	9.52	8.28	7.92	8.25	9.53	11.24	12.70	13.80	14.14	13.30	11.34	8.72	6.20	27	1	
28	4.24	3.38	3.76	5.30	7.76	10.55	13.50	15.72	16.74	16.12	14.36	11.40	8.83	7.24	6.86	7.53	9.20	11.11	12.97	14.55	15.08	14.17	11.84	8.82	28	1	
29	5.79	3.60	2.56	3.06	5.04	7.88	11.48	14.56	17.04	17.86	17.00	14.36	10.96	8.07	6.27	5.77	6.57	8.62	11.25	13.92	15.74	16.28	14.96	12.18	29	1	
30	8.44	5.42	3.22	2.16	3.07	5.52	8.75	12.46	16.01	18.10	18.47	17.26	13.80	10.14	7.09	5.27	5.02	6.02	8.40	11.85	14.65	16.52	16.84	15.28	30	1	
31	11.68	7.88	4.80	2.74	2.38	4.00	6.66	10.10	13.98	17.01	18.64	18.38	16.30	12.42	8.97	6.01	4.46	4.57	6.12	9.14	12.56	15.46	17.00	16.86	31	1	
32	14.76	11.06	7.36	4.34	2.72	2.99	4.86	7.74	11.40	14.94	17.54	18.47	17.66	14.67	11.08	7.54	5.01	3.93	4.32	6.55	9.62	13.04	15.80	16.84	32	1	
33	16.08	13.73	10.16	6.82	4.54	3.58	4.44	6.36	9.36	12.84	15.86	17.74	17.94	16.48	13.27	9.84	6.84	4.96	4.33	5.26	7.44	10.66	13.70	15.74	33	1	
34	16.43	15.42	12.82	9.66	6.90	5.42	5.14	6.20	8.06	10.66	13.66	16.02	17.12	16.74	14.88	11.68	8.76	6.34	4.92	4.74	5.86	8.26	11.07	13.60	34	1	
35	15.16	15.34	14.06	11.68	9.04	7.34	6.56	6.94	8.04	9.56	11.76	14.24	15.60	16.04	15.34	13.02	10.16	7.86	6.27	5.54	5.86	7.18	9.07	11.36	35	1	

TIDAL OBSERVATIONS.

[Cont. M.]





FORMS FOR SHORT-PERIOD TIDES.  
 SERIES P.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
75	4.44	4.96	6.46	8.94	11.85	14.34	16.00	16.06	14.53	11.64	8.54	5.76	4.22	3.97	5.24	7.30	10.10	13.02	15.04	16.00	15.20	12.86	9.54	6.67	76 4	
76	4.93	4.38	5.52	7.55	10.33	13.50	15.75	16.73	16.07	13.66	10.42	7.22	4.92	3.64	4.00	5.66	8.33	11.52	14.30	16.06	16.52	15.06	12.13	8.73	77 4	
77	6.13	4.66	4.99	6.52	8.92	11.86	14.66	16.40	16.56	15.07	11.90	8.47	5.62	3.74	3.22	4.26	6.60	9.60	12.85	15.23	16.56	16.25	14.26	10.83	78 4	
78	8.00	5.75	5.11	5.88	7.84	10.46	13.38	15.68	16.60	15.80	13.36	10.12	7.06	4.83	3.54	3.76	5.34	7.86	11.00	13.93	15.92	16.74	15.74	13.36	79 4	
79	10.24	7.64	6.12	6.08	7.14	9.00	11.56	13.90	15.66	15.98	14.76	12.06	8.90	6.13	4.34	3.62	4.36	6.06	8.47	11.31	13.87	15.62	16.12	14.97	80 4	
80	12.74	10.02	8.05	6.96	7.06	7.93	9.67	12.07	14.08	15.23	15.08	13.57	11.16	8.26	6.08	4.76	4.47	5.46	7.26	9.48	11.88	13.90	15.36	15.50	81 4	
81	14.66	12.67	10.54	8.74	7.94	8.14	9.06	10.63	12.40	13.77	14.52	14.20	12.80	10.64	8.47	6.76	5.86	5.82	6.49	7.75	9.52	11.71	13.54	14.73	82 4	
82	14.90	14.06	12.63	11.05	9.70	8.86	8.72	9.12	10.24	11.76	13.06	13.06	13.34	12.06	10.56	8.92	7.40	6.43	6.30	6.68	7.68	9.46	11.24	13.02	83 4	
83	14.08	14.52	14.22	13.04	11.70	10.34	9.24	8.84	9.04	9.84	10.96	12.05	12.86	12.96	12.44	11.22	9.67	8.30	7.06	6.48	6.64	7.48	8.86	10.64	84 4	
84	12.34	13.74	14.48	14.44	13.62	12.12	10.36	8.96	8.11	7.96	8.44	9.76	11.26	12.92	12.78	11.94	10.50	8.78	7.20	6.06	5.92	6.72	8.34	10.26	85 5	
85	12.20	13.86	15.00	15.14	14.16	12.20	9.88	8.00	6.90	6.56	7.46	9.22	11.16	12.56	13.57	14.06	13.37	11.72	9.38	7.17	5.72	5.38	6.17	7.82	86 5	
86	10.00	12.50	14.54	15.84	15.94	14.64	12.14	9.36	6.97	5.74	5.63	6.67	8.88	11.24	13.46	14.86	15.36	14.34	12.05	9.44	6.93	5.38	5.00	5.82	87 5	
87	7.83	10.50	13.30	15.60	16.72	16.28	14.37	11.37	8.36	6.00	4.67	4.80	6.40	9.20	12.06	14.62	16.12	16.16	14.90	12.22	9.12	6.60	5.05	4.86	88 5	
88	5.87	8.10	11.14	14.15	16.35	17.15	16.24	13.58	10.14	7.06	4.83	3.96	4.70	6.72	9.92	13.20	15.64	17.04	16.75	14.92	11.81	8.56	6.27	5.14	89 5	
89	5.64	6.94	9.43	12.61	15.44	17.03	17.08	15.36	11.02	8.64	6.18	4.48	4.55	5.24	7.57	11.00	14.10	16.43	17.34	16.56	14.28	10.82	7.84	5.95	90 5	
90	5.42	6.12	7.87	10.62	13.66	16.10	17.14	16.46	13.96	10.44	7.12	4.80	3.83	4.41	6.43	8.78	12.04	14.74	16.66	17.13	15.64	12.86	9.53	7.16	91 5	
91	5.81	5.93	7.22	9.26	12.02	14.66	16.44	16.67	15.06	12.02	8.56	5.84	4.04	3.84	4.93	7.24	10.09	13.22	15.56	16.90	16.56	14.74	11.68	8.84	92 5	
92	7.02	6.48	7.04	8.26	10.50	13.00	14.94	15.83	15.12	12.94	9.87	7.14	5.16	4.22	4.76	6.40	8.73	11.37	14.00	15.82	16.34	15.34	13.10	10.40	93 5	
93	8.36	7.32	7.28	8.03	9.50	11.53	13.48	14.74	14.92	13.67	11.34	8.76	6.67	5.40	5.22	6.16	7.85	9.97	12.30	14.30	15.48	15.46	14.27	12.24	94 5	
94	10.20	8.78	8.26	8.47	9.24	10.52	12.04	13.48	14.16	13.84	12.27	10.16	8.14	6.47	5.74	6.22	7.44	9.20	10.85	12.64	14.05	14.67	14.27	12.97	95 5	
95	11.44	10.04	9.16	8.84	9.16	9.84	10.95	11.96	12.80	12.96	12.28	10.94	9.24	7.80	6.78	6.70	7.30	8.37	9.54	10.90	12.34	13.52	13.80	13.26	96 5	
96	12.13	10.96	10.04	9.60	9.33	9.54	9.90	10.56	11.44	11.92	12.05	11.54	10.36	9.16	8.12	7.47	7.44	7.87	8.52	9.46	10.73	11.93	12.74	12.98	97 5	
97	12.66	11.86	11.07	10.34	9.94	9.77	9.87	10.02	10.36	10.81	11.14	11.27	10.92	10.30	9.34	8.36	7.74	7.58	7.98	8.76	9.87	11.04	11.96	12.50	98 5	
98	12.66	12.42	11.96	11.34	10.55	9.91	9.47	9.34	9.52	9.94	10.53	10.94	11.12	11.02	10.62	10.00	9.22	8.40	8.01	8.13	8.63	9.70	10.66	11.77	99 5	
99	12.66	13.06	12.94	12.46	11.47	10.50	9.62	8.94	8.54	8.74	9.48	10.45	11.36	11.88	11.89	10.50	9.40	8.46	7.84	7.76	8.43	9.46	10.86	12.30	100 6	
100	13.36	13.82	13.66	13.66	11.42	10.02	8.72	7.96	7.82	8.36	9.47	10.86	11.90	12.70	12.87	12.44	11.06	9.52	8.12	7.40	7.47	8.26	9.54	11.08	101 6	
101	12.70	14.06	14.56	14.22	12.80	10.96	8.88	7.46	6.81	6.84	7.92	9.62	11.52	13.00	13.97	14.12	13.00	11.02	9.05	7.48	6.74	6.92	7.97	9.72	102 6	
102	11.72	13.58	14.86	15.12	14.21	12.35	9.67	7.47	5.98	5.58	6.14	7.76	9.84	12.16	14.02	15.18	15.06	13.40	10.95	8.28	6.66	6.02	6.46	7.88	103 6	
103	10.06	12.53	14.55	15.72	15.49	13.80	11.08	8.22	5.93	4.52	4.22	5.47	7.72	10.54	13.27	15.36	16.20	15.32	13.00	9.88	7.34	5.76	5.40	6.24	104 6	
104	8.22	10.70	13.40	15.52	16.25	15.36	12.80	9.46	6.56	4.47	3.42	3.91	5.74	8.31	11.40	14.40	16.28	16.72	15.47	12.68	9.44	6.81	5.47	5.38	105 6	
105	6.52	8.91	11.80	14.40	15.97	16.08	14.35	11.30	7.80	4.97	2.93	2.46	3.76	6.21	9.51	12.97	15.58	17.14	17.04	14.94	13.68	8.36	6.14	5.06	106 6	
106	5.57	7.24	10.07	13.10	15.40	16.44	15.82	13.44	9.74	6.67	4.03	2.50	2.77	4.44	7.50	10.96	14.33	16.70	17.72	16.91	14.37	10.87	8.10	6.15	107 6	
107	5.71	6.50	8.36	11.33	14.12	15.97	16.50	15.10	12.22	8.67	5.24	3.17	2.56	3.47	5.74	8.64	12.02	15.12	16.94	17.54	16.24	13.40	10.32	7.62	108 6	
108	6.17	6.07	7.04	9.13	12.00	14.47	15.60	15.54	13.66	10.74	7.44	4.88	3.28	3.04	4.36	6.67	9.40	12.47	15.00	16.74	16.94	15.60	13.03	10.01	109 6	
109	7.87	6.76	6.80	7.71	9.70	12.14	14.15	15.02	14.50	12.53	9.92	7.24	5.36	4.17	4.16	5.20	7.26	9.89	12.40	14.57	15.77	15.74	14.47	12.12	110 6	



FORMS FOR SHORT-PERIOD TIDES.  
SERIES P.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
149	13.60	14.02	14.37	13.23	10.78	8.10	5.71	4.37	4.17	5.26	7.20	9.70	12.28	14.66	15.94	16.04	14.86	12.64	10.27	8.44	7.54	7.34	8.10	9.52	150 9	
150	11.55	13.30	14.27	13.92	12.06	9.48	6.90	5.12	4.32	4.97	6.54	8.70	11.00	13.46	15.32	16.07	15.65	14.17	11.77	9.56	8.16	7.68	7.83	8.74	151 9	
151	10.50	12.25	13.66	14.02	12.96	10.86	8.34	6.21	5.04	4.82	5.84	7.60	9.46	11.87	14.10	15.30	15.60	14.66	12.78	10.74	9.03	7.96	7.73	8.24	152 9	
152	9.44	11.07	12.61	13.44	13.16	11.96	9.94	7.67	6.16	5.18	5.56	6.86	8.64	10.66	12.74	14.30	15.12	15.06	13.95	11.84	10.00	8.46	7.75	7.78	153 9	
153	8.46	9.92	11.36	12.37	12.84	12.22	10.98	9.18	7.32	6.03	5.94	6.87	8.17	9.67	11.58	13.28	14.64	14.97	14.22	12.62	11.08	9.47	8.38	8.08	154 9	
154	8.30	9.20	10.24	11.40	12.12	12.46	11.72	10.38	8.77	7.37	6.70	6.93	7.78	8.83	10.30	11.90	13.54	14.68	14.80	13.77	12.16	10.50	9.20	8.47	155 9	
155	8.28	8.60	9.36	10.36	11.26	11.83	12.05	11.56	10.60	9.20	8.14	7.72	7.83	8.62	9.82	11.10	12.64	13.94	14.46	14.16	13.26	11.74	10.44	9.26	156 9	
156	8.54	8.34	8.46	9.23	10.10	10.93	11.70	11.97	11.72	11.06	9.98	8.86	8.32	8.30	9.00	10.04	11.54	12.92	13.86	14.25	13.85	12.88	11.48	10.08	157 9	
157	8.98	8.20	8.20	8.37	9.12	10.03	11.29	12.14	12.58	12.36	11.84	11.02	10.06	9.23	8.78	9.20	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158 9	
158	10.03	8.74	7.92	7.51	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	9.64	10.17	11.38	12.77	13.98	14.67	15.14	14.88	13.86	159 9	
159	12.46	10.48	8.81	7.83	7.50	8.19	9.46	11.28	13.22	14.76	15.82	15.76	14.97	13.34	11.70	10.67	10.27	10.56	11.52	12.90	14.12	15.30	15.65	15.48	160 9	
160	14.17	12.02	9.86	8.00	7.09	6.85	7.72	9.34	13.77	15.84	16.86	16.85	15.70	13.60	11.52	9.95	9.55	9.80	10.84	12.57	14.21	15.47	16.06	15.22	161 10	
161	13.50	10.84	8.22	6.16	4.95	5.15	6.50	8.61	11.37	14.18	16.48	17.54	17.17	15.60	12.50	10.07	8.34	8.17	8.96	10.27	12.23	14.24	15.74	16.29	162 10	
162	15.33	12.77	9.46	6.31	4.41	3.62	4.30	6.30	8.54	11.95	15.02	17.28	17.95	17.20	15.02	11.76	9.04	7.44	7.22	7.81	9.55	12.08	14.54	16.07	163 10	
163	16.21	14.76	11.87	8.16	5.07	3.07	2.74	3.80	5.94	9.24	12.80	15.92	18.07	18.53	17.65	14.65	10.90	8.00	6.62	6.55	7.50	9.65	12.45	14.89	164 10	
164	16.40	16.14	14.28	10.90	7.10	4.31	2.62	2.37	3.68	6.30	9.76	13.48	16.44	18.12	18.40	17.00	13.80	10.17	7.55	6.20	6.18	7.30	9.00	12.79	165 10	
165	15.16	16.43	15.96	13.80	10.33	6.77	4.00	2.33	2.54	4.18	7.11	10.40	13.95	16.74	17.85	17.95	16.07	12.81	9.60	7.05	5.72	5.77	7.00	9.56	166 10	
166	12.80	15.12	16.05	15.26	12.75	9.20	6.14	3.95	2.88	3.47	5.52	7.93	11.04	14.21	16.44	17.72	17.40	15.44	12.97	9.02	6.70	5.67	5.93	7.41	167 10	
167	10.07	13.02	14.92	15.57	14.68	12.28	9.20	6.52	4.77	4.20	4.94	6.52	8.80	11.67	14.34	16.42	17.20	16.60	14.54	11.30	8.66	6.74	6.05	6.16	168 10	
168	7.65	10.05	13.50	14.32	14.85	14.05	11.96	9.47	7.26	6.06	5.80	6.39	7.66	9.64	11.92	14.25	15.90	16.46	15.74	13.76	10.84	8.61	6.86	6.32	169 10	
169	6.58	7.80	9.82	12.04	13.55	14.17	13.54	12.03	10.34	8.60	7.57	7.26	7.62	8.44	9.92	12.12	14.20	15.46	15.54	14.58	12.66	10.40	8.31	7.04	170 10	
170	6.60	6.77	7.78	9.32	11.22	12.80	13.58	13.46	12.40	10.90	9.62	8.66	8.31	8.49	9.03	10.30	12.04	13.70	14.74	14.75	13.73	12.02	10.10	8.46	171 10	
171	7.12	6.53	6.70	7.50	9.03	10.90	12.32	13.20	13.38	12.92	11.94	10.67	9.60	8.94	8.82	9.24	10.33	11.90	13.24	14.06	14.10	13.34	11.84	10.05	172 10	
172	8.26	6.94	6.44	6.67	7.49	9.06	10.86	12.50	13.66	14.10	13.63	12.46	11.06	10.66	9.30	9.05	9.33	10.22	11.60	12.90	13.82	13.85	13.08	11.64	173 10	
173	9.76	8.00	6.70	6.08	6.22	7.28	9.00	10.94	12.77	14.05	14.63	14.17	12.86	11.33	10.04	9.14	8.86	9.20	10.08	11.26	12.44	13.30	13.52	12.80	174 10	
174	11.00	8.85	7.06	5.67	5.05	5.60	7.15	9.26	11.30	13.28	14.45	14.84	13.95	12.40	10.90	9.46	8.62	8.24	8.56	9.64	11.12	12.55	13.40	13.37	175 10	
175	12.07	10.07	8.20	6.17	4.94	4.74	5.62	7.74	9.76	12.14	14.01	15.00	14.86	12.66	10.27	8.84	8.10	7.94	8.52	9.68	11.18	12.64	13.37	13.05	176 11	
176	11.52	9.17	6.76	5.11	4.16	4.64	6.10	8.00	10.50	12.90	14.56	15.33	14.74	13.32	11.14	9.44	8.17	7.54	7.57	8.34	9.81	11.65	13.20	13.00	177 11	
177	12.56	10.40	7.97	5.85	4.38	4.04	4.96	6.82	9.02	11.57	13.86	15.24	15.56	13.30	11.44	10.36	8.63	7.62	7.30	7.74	8.86	10.67	12.47	13.67	178 11	
178	13.60	12.02	9.66	6.93	4.96	3.91	4.22	5.70	7.84	10.40	12.82	14.74	15.36	13.80	11.44	9.35	7.79	7.04	7.03	7.90	9.44	11.66	13.22	13.22	179 11	
179	13.92	13.00	10.74	8.00	5.64	4.04	3.83	4.76	6.70	9.02	11.37	13.67	15.12	15.46	14.48	12.44	9.96	8.16	6.86	6.42	6.94	8.42	10.44	12.57	180 11	
180	13.67	13.68	12.22	9.64	6.86	4.96	3.98	4.36	5.65	7.72	10.02	12.26	14.31	15.28	15.12	13.77	11.30	9.01	7.37	6.64	6.56	7.46	9.06	11.01	181 11	
181	13.70	13.51	13.01	11.07	8.44	6.12	4.72	4.42	5.32	6.94	8.97	11.17	13.22	14.74	15.17	14.22	12.16	9.74	7.86	6.74	6.51	7.07	8.16	9.92	182 11	
182	11.66	12.82	13.10	11.86	9.72	7.36	5.70	5.02	5.24	6.42	8.07	10.12	11.98	13.73	14.86	14.72	13.40	11.17	9.22	7.55	6.51	6.57	7.34	8.72	183 11	
183	10.61	12.04	12.77	12.64	11.27	8.72	7.48	6.30	5.87	6.54	7.66	9.24	10.97	12.94	14.38	14.88	14.20	12.50	10.34	8.44	7.22	6.77	7.87	9.07	184 11	



FORMS FOR SHORT-PERIOD TIDES.

SERIES P.—(Continued).

Day	0 <sup>h</sup>		1 <sup>h</sup>		2 <sup>h</sup>		3 <sup>h</sup>		4 <sup>h</sup>		5 <sup>h</sup>		6 <sup>h</sup>		7 <sup>h</sup>		8 <sup>h</sup>		9 <sup>h</sup>		10 <sup>h</sup>		11 <sup>h</sup>		12 <sup>h</sup>		13 <sup>h</sup>		14 <sup>h</sup>		15 <sup>h</sup>		16 <sup>h</sup>		17 <sup>h</sup>		18 <sup>h</sup>		19 <sup>h</sup>		20 <sup>h</sup>		21 <sup>h</sup>		22 <sup>h</sup>		23 <sup>h</sup>		Solar Hour
	feet	d h	feet	d h	feet	d h	feet	d h	feet	d h	feet	d h	feet	d h	feet	d h	feet	d h	feet	d h	feet	d h	feet	d h	feet	d h	feet	d h	feet	d h	feet	d h	feet	d h	feet	d h	feet	d h	feet	d h	feet	d h	feet	d h	feet	d h	feet	d h	
222	6.47	3.74	3.20	5.12	8.18	11.74	15.30	17.06	18.50	17.76	14.76	10.60	7.27	5.06	4.48	5.07	7.18	10.36	13.94	16.34	17.16	16.04	13.12	223 14																									
223	9.20	5.80	3.36	3.60	5.73	9.03	12.78	15.94	17.78	18.04	16.74	13.32	9.36	6.05	4.18	3.80	4.90	7.56	11.10	14.46	16.66	16.88	15.39	224 14																									
224	12.15	8.23	5.44	3.52	4.58	7.04	10.14	13.35	16.16	17.52	17.26	15.28	11.80	8.22	5.32	3.80	4.02	5.58	8.40	11.50	14.52	16.18	16.06	225 14																									
225	14.38	11.26	7.98	5.62	4.80	6.25	8.27	11.00	13.96	16.32	17.20	16.42	14.32	10.85	7.62	5.16	4.10	4.64	6.45	8.92	12.05	14.70	15.80	226 14																									
226	15.18	13.36	10.62	7.94	6.32	5.74	6.44	7.77	12.07	14.12	15.66	15.72	14.46	12.06	9.36	6.96	5.40	5.07	5.84	7.33	9.54	11.87	13.60	227 14																									
227	14.46	13.96	12.48	10.40	8.65	7.45	7.28	8.00	9.12	8.90	9.34	10.06	10.94	12.10	12.88	13.72	13.38	11.88	10.06	8.17	7.02	6.68	7.00	10.10	229 14																								
228	13.26	13.57	12.85	11.76	10.70	9.74	9.12	8.90	9.34	10.06	10.94	12.10	12.88	13.72	13.38	11.88	10.06	8.17	7.02	6.68	7.00	7.77	8.77	10.10	229 14																								
229	11.44	12.33	12.66	12.46	12.00	11.36	10.62	10.07	9.67	9.77	10.12	10.82	11.54	12.43	12.67	12.12	11.23	9.96	8.64	7.77	7.46	7.69	8.30	9.04	230 14																								
230	10.10	11.17	12.34	12.90	13.90	12.34	11.72	11.15	10.62	10.30	10.00	10.14	10.50	11.34	11.96	12.26	11.97	11.38	10.53	9.44	8.35	7.66	7.57	8.12	231 14																								
231	9.06	10.48	11.57	12.72	13.42	13.56	13.18	12.30	11.45	10.72	10.26	9.92	9.63	10.00	10.71	11.62	12.32	12.18	11.42	10.36	9.08	8.15	7.53	7.24	232 14																								
232	7.70	8.54	9.82	11.43	12.72	13.64	13.38	14.40	14.54	13.58	12.17	10.70	9.34	8.97	9.08	9.88	10.76	11.64	12.26	12.35	11.85	10.40	8.78	7.36	6.44	233 14																							
233	6.28	7.14	8.37	10.20	11.94	13.38	14.40	14.54	13.58	12.17	10.70	9.34	8.97	9.08	9.88	10.76	11.64	12.26	12.35	11.85	10.40	8.78	7.36	6.44	233 14																								
234	6.06	6.14	7.20	8.95	10.80	12.76	13.96	14.91	14.84	13.64	11.84	9.97	8.77	8.36	8.48	8.96	10.06	11.36	13.12	13.97	13.64	12.06	9.70	7.27	235 14																								
235	5.96	5.56	6.35	7.80	9.76	11.70	13.66	15.10	15.46	14.62	12.86	10.57	8.64	7.46	7.31	7.76	8.84	10.72	12.64	14.21	14.62	13.44	11.00	8.24	236 14																								
236	6.24	5.17	5.36	6.54	8.54	13.00	15.02	15.96	15.30	14.08	11.60	8.97	7.34	6.70	6.84	7.80	9.62	11.70	13.76	14.95	14.67	12.76	10.00	7.37	237 15																								
237	5.56	4.97	5.74	7.38	9.36	11.94	14.36	16.04	16.27	15.32	13.08	10.11	7.72	6.36	6.10	6.94	8.63	10.83	13.20	15.21	15.71	14.43	11.89	8.54	238 15																								
238	6.26	4.97	5.06	6.36	8.22	10.64	13.40	15.80	16.62	16.16	14.21	11.38	8.34	6.35	5.46	5.74	7.13	9.22	11.84	14.56	15.71	15.48	13.64	10.66	239 15																								
239	7.60	5.70	4.96	5.70	7.24	9.54	12.02	14.56	16.24	16.56	15.34	12.80	9.60	7.06	5.50	5.18	5.94	7.72	10.28	13.04	15.14	15.90	14.88	12.52	240 15																								
240	9.63	7.07	5.74	5.64	6.67	8.36	10.62	13.17	15.30	16.38	15.97	14.06	11.04	8.16	6.11	5.05	5.41	6.72	8.83	11.26	13.77	15.36	15.38	14.00	241 15																								
241	11.50	8.72	6.86	5.97	6.34	7.52	9.30	11.47	13.80	15.46	15.84	14.77	12.44	9.37	7.06	5.37	4.85	5.64	7.12	9.24	11.64	13.96	15.06	14.75	242 15																								
242	13.17	10.76	8.64	7.30	6.86	7.44	8.64	10.38	12.36	14.06	15.24	15.10	13.64	11.26	8.61	6.50	5.32	5.38	6.34	7.85	9.86	11.96	13.64	14.58	243 15																								
243	14.97	12.68	10.68	8.97	8.02	7.81	8.36	9.26	10.60	12.24	13.73	14.44	13.86	12.25	10.02	8.06	6.46	5.62	5.78	6.47	7.80	9.63	11.38	12.97	244 15																								
244	13.74	13.44	12.44	11.04	9.83	8.84	8.57	8.87	9.67	10.67	11.96	13.06	13.46	13.08	11.68	9.86	8.26	6.87	6.17	6.26	7.02	8.17	9.66	11.26	245 15																								
245	12.55	13.37	13.57	12.94	11.92	10.73	9.67	9.16	9.18	9.63	10.54	11.48	12.46	12.92	12.66	11.74	10.42	8.97	7.44	6.44	6.21	6.66	7.76	9.20	246 15																								
246	10.76	12.36	13.54	14.05	13.67	12.68	11.26	10.02	9.22	8.90	9.14	9.86	10.86	12.02	12.84	12.98	12.36	11.16	9.57	7.60	6.24	5.63	5.97	7.17	247 15																								
247	8.80	10.66	12.80	14.28	14.96	14.74	13.66	11.85	10.04	8.66	8.02	8.14	9.04	10.38	12.00	13.14	13.74	13.40	12.04	10.04	7.64	5.76	4.78	5.02	248 15																								
248	6.24	8.16	10.78	13.20	15.04	15.98	15.74	14.33	11.96	9.30	7.37	6.55	6.70	8.06	9.98	12.06	13.93	14.86	14.44	12.80	10.18	7.37	5.17	3.90	249 15																								
249	4.93	5.50	7.06	10.88	13.80	16.04	17.04	16.46	14.44	11.04	8.24	6.37	5.15	5.63	7.24	9.64	12.52	14.74	15.98	15.46	13.29	9.94	6.63	4.34	250 15																								
250	3.17	2.53	5.38	8.20	11.40	14.56	16.82	17.44	16.36	13.83	9.98	6.70	4.46	3.84	4.58	6.80	10.06	13.28	15.76	16.64	15.75	12.94	9.26	6.06	251 15																								
251	3.66	2.67	3.72	5.66	8.70	12.20	15.53	17.33	15.87	12.42	8.56	5.32	3.44	3.17	4.55	7.26	10.87	14.22	16.50	17.05	15.47	12.37	8.44	5.52	252 16																								
252	3.48	3.10	4.46	6.74	9.94	13.47	16.22	17.47	17.02	14.77	10.84	7.23	4.32	3.00	3.30	5.07	8.06	11.72	14.94	16.86	16.90	14.94	11.54	8.00	253 16																								
253	5.38	3.90	4.20	5.52	7.95	11.06	14.30	16.51	17.04	15.88	12.99	9.17	5.97	3.70	2.94	3.94	6.16	9.14	12.45	15.42	16.68	16.10	13.81	10.56	254 16																								
254	7.46	5.47	4.87	5.60	7.04	9.54	12.25	14.81	16.16	16.06	14.44	11.07	7.87	5.34	3.84	3.92	5.16	7.43	10.36	13.44	15.47	16.04	14.92	12.66	255 16																								
255	9.98	7.74	6.47	6.36	7.02	8.34	10.58	12.80	14.58	15.36	14.73	12.52	9.86	7.17	5.31	4.44	5.02	6.44	8.50	11.04	13.56	14.70	14.77	13.46	256 16																								
256	11.46	9.44	8.00	7.36	7.56	8.36	9.51	11.00	12.60	13.73	13.94	12.90	11.02	8.73	6.90	5.70	5.63	6.34	7.60	9.36	11.36	13.44	13.88	13.60	257 16																								



FORMS FOR SHORT-PERIOD TIDES.

SERIES P.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h	
296	8.16	10.16	12.84	15.02	16.10	15.46	13.28	9.87	6.84	4.45	3.04	3.57	5.44	8.15	11.37	14.60	16.81	17.35	16.28	13.64	10.44	7.71	5.84	6.88	297 19	
297	8.87	11.47	14.12	15.94	16.22	14.81	11.87	8.55	5.46	3.46	2.87	4.17	6.35	9.32	13.00	15.95	17.47	17.44	15.72	12.68	9.66	7.28	5.94	6.04	298 19	
298	7.36	9.64	12.45	14.84	16.04	15.60	13.70	10.52	7.15	4.66	2.92	3.10	4.72	7.47	10.55	13.92	16.35	17.36	16.74	14.57	11.67	8.85	6.76	5.94	299 19	
299	6.28	7.70	9.92	12.68	14.78	15.58	14.78	12.36	9.26	6.36	4.20	3.07	3.72	5.55	8.04	11.05	14.10	16.17	16.96	16.12	14.06	11.35	8.82	7.14	300 19	
300	6.57	7.02	8.46	10.56	13.14	14.64	15.04	13.76	11.47	8.74	6.42	4.70	4.22	5.00	6.80	9.02	11.88	14.60	16.14	16.22	15.16	13.26	10.86	8.86	301 19	
301	7.58	7.14	7.44	8.84	10.92	12.84	13.84	13.86	12.57	10.68	8.54	6.84	5.56	5.27	5.98	7.33	9.36	11.72	14.00	15.22	15.38	14.58	12.88	11.01	302 19	
302	9.42	8.12	7.64	7.92	8.94	10.40	11.85	12.91	13.12	12.26	10.75	9.22	7.66	6.68	6.30	6.72	7.86	9.44	11.50	13.34	14.46	14.66	13.96	12.74	303 19	
303	11.30	9.76	8.54	7.93	7.84	8.40	9.60	10.88	12.06	12.64	12.40	11.47	10.10	8.76	7.68	7.01	7.06	7.90	9.22	10.97	12.56	13.72	14.38	14.04	304 19	
304	13.04	11.45	9.76	8.15	7.22	7.02	7.48	8.84	10.32	11.48	12.55	12.87	12.46	11.36	9.70	8.28	7.14	6.80	7.40	8.84	10.74	12.56	13.87	14.54	305 19	
305	14.38	13.40	11.67	9.60	7.53	6.30	5.88	6.50	8.20	10.07	11.93	13.36	14.04	13.66	12.30	10.26	8.61	7.37	6.86	7.24	8.35	10.36	12.50	14.13	306 19	
306	15.08	14.96	13.80	11.64	9.03	6.96	5.44	5.04	5.86	7.79	10.12	12.66	14.54	15.37	14.86	13.04	10.66	8.56	7.12	6.44	6.77	8.02	10.14	12.62	307 19	
307	14.56	15.55	15.25	13.56	10.92	8.12	5.82	4.22	4.10	5.32	7.70	10.85	13.60	15.51	16.05	15.06	12.86	10.40	8.16	6.53	5.96	6.51	8.24	10.85	308 19	
308	13.27	15.16	15.84	15.03	12.98	9.78	7.04	4.71	3.46	3.86	5.60	8.44	11.74	14.64	16.50	16.72	15.38	12.86	9.98	7.70	6.25	5.93	6.71	8.67	309 19	
309	11.25	13.84	15.52	15.84	14.55	11.68	8.46	5.64	3.63	3.01	4.08	6.50	9.62	13.08	15.81	17.12	16.72	14.87	12.03	9.20	7.26	6.32	6.37	7.46	310 19	
310	9.60	12.20	14.35	15.67	15.28	13.15	10.15	7.00	4.47	3.03	3.22	5.03	7.60	10.76	14.05	16.38	17.05	16.14	13.92	11.10	8.66	6.87	6.16	6.46	311 19	
311	8.00	10.44	13.10	14.76	15.16	13.92	11.40	8.36	5.66	3.69	2.94	3.94	6.18	9.01	12.24	14.92	16.53	16.56	15.16	12.66	10.06	7.96	6.74	6.60	312 19	
312	7.35	9.00	13.43	14.50	14.36	12.66	9.94	7.20	4.97	3.56	3.77	5.34	7.72	10.56	13.46	15.64	16.34	15.71	13.92	11.46	9.28	7.66	6.86	6.98	313 20	
313	7.98	9.96	12.00	13.52	14.02	13.37	11.18	8.81	6.52	4.86	4.33	5.20	6.90	9.14	11.80	14.20	15.72	15.81	14.66	12.72	10.71	8.96	7.82	7.56	314 20	
314	7.92	9.16	10.68	12.24	13.26	12.06	10.17	8.00	6.25	5.31	5.50	6.66	8.34	10.52	12.80	14.44	15.18	14.68	13.32	11.56	10.02	8.76	8.10	315 20		
315	8.00	8.60	9.65	10.96	12.18	12.58	12.23	11.04	9.16	7.62	6.54	6.20	6.84	7.96	9.38	11.14	12.91	14.18	14.40	13.64	12.37	10.90	9.58	8.78	316 20	
316	8.46	8.68	9.30	10.00	10.94	11.57	11.80	11.36	10.28	8.94	7.84	7.18	7.20	7.86	8.80	9.98	11.46	12.86	13.86	13.83	12.96	11.72	10.53	9.66	317 20	
317	9.14	8.92	8.96	9.17	9.66	10.40	11.10	11.37	11.01	10.20	9.26	8.46	8.10	8.14	8.66	9.44	10.56	11.74	12.76	13.34	13.26	12.61	11.72	10.86	318 20	
318	9.76	9.04	8.80	8.85	9.16	9.64	10.14	10.74	11.18	11.32	11.06	10.38	9.58	8.94	8.71	8.90	9.50	10.42	11.46	12.48	13.10	13.15	12.64	11.84	319 20	
319	10.76	9.71	8.88	8.35	8.19	8.42	9.04	9.96	10.86	11.50	11.80	11.55	10.96	9.98	9.08	8.64	8.75	9.38	10.38	11.46	12.41	13.07	13.16	12.84	320 20	
320	11.84	10.56	9.24	8.13	7.50	7.43	7.86	8.83	10.03	11.16	12.23	12.80	12.64	11.66	10.25	9.04	8.36	8.34	8.96	10.02	11.20	12.46	13.23	13.47	321 20	
321	13.00	11.72	10.14	8.38	7.03	6.27	6.31	7.08	8.52	10.23	11.92	13.17	13.63	13.10	11.86	10.18	8.76	7.98	7.96	8.75	10.13	11.64	13.14	13.94	322 20	
322	13.94	13.04	11.34	9.30	7.45	5.86	5.13	5.46	6.76	8.80	11.15	13.20	14.66	14.98	13.87	11.76	9.58	8.10	7.27	7.36	8.22	9.82	11.76	13.33	323 20	
323	14.28	14.14	12.87	10.56	7.98	5.77	4.14	3.74	4.67	6.71	9.27	12.02	14.40	15.66	15.44	13.71	11.16	8.74	7.02	6.40	6.78	8.22	10.37	12.25	324 20	
324	13.88	14.74	14.20	12.26	9.36	6.51	4.12	2.75	2.94	4.56	7.03	10.05	13.27	15.65	16.62	15.90	13.76	10.86	8.17	6.45	5.84	6.36	8.12	10.44	325 20	
325	12.84	14.46	15.08	13.97	11.41	8.07	4.96	2.57	1.63	2.58	4.74	7.64	11.12	14.22	16.47	17.07	15.75	12.96	9.86	7.26	5.65	5.46	6.44	8.40	326 20	
326	11.20	13.57	15.11	15.17	13.27	9.96	6.40	3.62	1.76	1.54	3.26	6.02	9.25	12.97	15.66	17.40	17.25	15.37	12.23	9.00	6.75	5.63	5.63	6.88	327 20	
327	9.32	12.22	14.44	15.50	14.80	12.31	8.84	5.46	3.00	1.66	2.20	4.15	6.95	10.46	13.81	16.44	17.54	16.82	14.56	11.38	8.50	6.32	5.44	5.74	7.26	328 21
328	10.06	12.76	14.67	15.26	14.06	11.32	8.05	5.16	2.94	2.16	3.11	5.16	7.96	11.23	14.30	16.57	17.22	16.23	13.81	10.68	8.07	6.16	5.50	5.88	329 21	
329	7.64	10.25	12.77	14.29	14.72	13.33	10.74	7.81	5.32	3.66	3.26	4.42	6.34	8.86	11.67	14.58	16.33	16.57	15.28	12.84	9.93	7.47	6.23	5.72	330 21	
330	6.26	7.94	10.30	12.38	13.76	13.96	12.68	10.56	8.18	6.28	4.97	4.83	5.73	7.34	9.38	12.05	14.37	15.76	15.80	14.56	12.28	9.94	8.13	6.64	331 21	







38	14.66	14.44	13.11	11.12	9.30	7.54	6.26	6.13	6.68	7.86	9.28	10.86	12.27	13.10	12.94	11.93	10.66	9.72	9.12	9.06	9.26	9.66	10.60	37 13	
39	11.82	12.86	13.34	12.82	11.45	10.03	8.74	7.48	6.86	6.78	7.17	7.94	9.05	10.30	11.34	11.97	11.92	11.42	10.84	10.34	10.07	9.97	9.77	38 12	
40	9.94	10.44	11.32	12.06	12.26	11.78	10.88	9.87	8.84	7.86	7.24	6.94	7.18	8.03	9.07	10.14	11.00	11.56	11.85	11.77	11.46	11.12	10.57	39 11	
41	10.07	9.70	9.70	10.13	10.80	11.27	11.45	11.25	10.76	9.97	9.00	8.00	7.11	6.58	6.74	7.44	8.51	9.84	10.90	11.76	12.34	12.55	12.30	40 10	
42	11.60	10.57	9.76	9.34	9.17	9.56	10.24	10.94	11.36	11.44	10.97	10.10	9.07	7.87	6.85	6.30	6.50	7.26	8.50	10.16	11.44	12.65	13.26	41 9	
43	13.32	12.56	11.36	10.08	9.16	8.67	8.64	9.01	9.76	10.58	11.25	11.66	11.34	10.36	8.82	7.36	6.12	5.54	5.82	6.94	8.54	10.36	12.06	42 8	
44	13.46	13.97	13.64	12.30	10.76	9.26	8.14	7.84	8.12	8.96	10.24	11.52	12.40	12.66	12.07	10.47	8.56	6.64	5.46	5.20	5.93	7.55	9.56	43 7	
45	11.72	13.53	14.67	14.84	13.98	12.14	10.00	8.54	7.66	7.53	8.16	9.56	11.03	12.66	13.62	13.60	12.30	10.24	7.77	5.88	4.84	4.96	6.33	44 6	
46	8.27	10.66	13.07	14.85	15.64	15.23	13.64	11.13	9.02	7.54	6.79	7.00	8.13	9.87	11.85	13.60	14.38	13.88	11.93	9.10	6.54	4.66	4.00	4.90	45 6
47	6.86	9.20	11.97	14.34	15.82	15.96	14.78	12.26	9.64	7.46	6.24	5.96	6.74	8.48	10.85	13.07	14.56	14.85	13.63	10.90	7.86	5.57	4.07	46 5	
48	4.04	5.46	7.84	10.63	13.64	15.83	16.64	16.01	13.87	10.90	8.00	6.17	5.46	5.74	7.26	9.70	12.25	14.42	15.50	15.15	13.08	9.90	6.94	47 4	
49	4.75	3.92	4.66	6.62	9.46	12.60	15.08	16.60	16.64	15.00	11.93	8.96	6.76	5.63	5.06	5.54	7.84	10.54	13.30	15.12	15.66	14.46	11.76	48 3	
50	8.44	5.86	4.26	4.25	5.52	7.84	10.68	13.68	15.84	16.68	15.86	13.15	10.22	7.36	5.65	4.23	4.46	6.07	8.56	11.57	14.06	15.54	15.51	49 2	
51	13.57	10.53	7.47	5.38	4.52	5.04	6.70	9.14	12.18	14.74	16.26	16.26	14.64	11.74	8.68	6.28	4.54	4.14	5.07	7.06	9.74	12.44	14.55	50 1	
52	15.46	14.76	12.57	9.68	7.24	5.84	5.60	6.54	8.40	10.77	13.32	15.42	16.26	15.47	13.18	10.24	7.54	5.62	4.54	4.69	5.80	7.87	10.40	51 0	
53	12.80	14.50	15.06	14.03	11.86	9.36	7.58	6.64	6.76	7.86	9.60	11.66	13.73	15.08	15.32	14.12	11.86	9.24	6.90	5.18	4.58	5.06	6.46	51 23	
54	8.24	10.33	12.41	13.86	14.34	13.44	11.46	9.53	8.05	7.40	7.66	8.58	9.92	11.68	13.36	14.16	14.12	12.82	10.83	8.73	6.87	5.45	4.92	52 22	
55	5.44	6.63	8.23	10.14	11.77	12.96	13.40	12.76	11.56	10.24	9.04	8.45	8.28	8.67	9.76	11.20	12.50	13.18	13.06	11.88	10.25	8.57	6.98	53 21	
56	5.77	5.38	5.64	6.37	7.82	9.54	11.17	12.38	13.02	12.96	12.16	11.07	10.02	8.94	8.44	8.48	9.27	10.44	11.57	12.34	12.34	11.70	10.50	54 21	
57	7.32	5.96	5.24	5.12	5.86	7.17	8.90	10.63	12.10	13.16	13.56	13.13	11.86	10.27	8.88	8.08	7.87	8.42	9.56	10.87	11.93	12.44	12.26	55 20	
58	11.27	9.76	7.96	6.27	5.06	4.55	5.02	6.47	8.52	10.67	12.72	14.14	14.86	14.44	12.70	10.66	8.80	7.60	7.21	7.64	9.18	11.00	12.40	56 19	
59	13.36	13.52	12.60	10.86	8.63	6.40	4.63	4.06	4.70	6.46	8.84	11.30	13.80	15.56	16.25	15.33	12.96	10.26	7.95	6.54	6.18	7.03	8.83	57 18	
60	11.00	12.96	14.40	14.74	13.76	11.70	8.84	6.08	4.05	3.42	4.14	6.18	8.80	12.06	14.93	16.76	17.15	15.84	12.87	9.66	7.00	5.18	5.12	58 17	
61	6.26	8.52	11.16	13.67	15.38	15.86	14.57	11.93	8.26	5.48	3.42	2.92	4.14	6.52	9.58	13.16	16.04	17.62	17.34	15.27	11.66	8.27	5.56	59 16	
62	4.16	4.32	5.84	8.66	11.92	14.74	16.46	16.54	14.66	11.26	7.66	4.94	3.20	3.27	4.70	7.52	10.86	14.63	17.06	17.98	16.96	13.90	10.20	60 15	
63	6.96	4.47	3.56	4.02	6.04	9.40	12.86	15.55	16.86	16.36	13.86	10.44	6.92	4.54	3.37	3.90	5.80	8.56	12.33	15.44	17.27	17.40	15.46	61 14	
64	12.03	8.50	5.70	3.74	3.27	4.33	7.10	10.34	13.76	15.97	16.76	15.76	12.96	9.44	6.74	4.67	4.23	5.26	7.43	10.37	13.82	16.13	17.08	62 13	
65	16.40	13.86	10.50	7.26	4.84	3.56	3.86	5.60	8.27	11.55	14.34	16.02	16.28	14.66	11.66	8.60	6.46	5.26	5.46	6.56	8.86	11.44	14.36	63 12	
66	15.97	16.18	14.88	12.00	8.86	6.28	4.57	4.06	4.86	6.67	9.40	12.24	14.39	15.64	15.33	13.25	10.46	8.22	6.76	6.34	7.00	8.36	10.22	64 12	
67	14.42	15.27	14.71	12.72	10.14	7.72	5.93	4.86	5.00	6.10	8.03	10.30	12.47	13.97	14.58	13.92	12.03	10.14	8.54	7.56	7.56	8.42	9.82	65 11	
68	11.34	12.96	14.04	14.24	13.22	11.36	9.36	7.56	6.27	5.84	6.34	7.46	9.00	10.76	12.44	13.56	13.74	12.74	11.40	10.07	9.16	8.96	9.27	66 10	
69	9.77	10.46	11.36	12.44	13.07	13.03	12.12	10.46	8.86	7.68	7.02	7.02	7.66	8.54	9.66	10.96	12.24	12.88	12.88	12.24	11.43	10.66	10.24	67 9	
70	10.16	10.24	10.47	10.86	11.44	12.02	12.40	12.24	11.36	10.18	8.87	7.97	7.67	7.94	8.50	9.00	9.78	10.74	11.76	12.46	12.67	12.27	11.74	68 8	
71	11.26	10.87	10.56	10.36	10.22	10.36	10.76	11.26	11.56	11.38	10.86	9.96	9.14	8.40	7.98	7.80	7.86	8.34	9.30	10.46	11.44	12.08	12.36	69 7	
72	12.27	12.03	11.50	10.78	10.20	9.73	9.58	9.87	10.35	10.89	11.10	11.10	10.78	10.32	9.72	8.86	7.97	7.28	7.26	7.87	8.97	10.32	11.56	70 6	
73	12.46	13.04	13.10	12.54	11.68	10.56	9.64	9.08	8.82	9.16	9.88	10.74	11.40	11.75	11.70	11.14	10.07	8.84	7.56	6.74	6.70	7.63	8.94	71 5	
74	10.62	12.06	13.26	13.78	13.68	12.86	11.34	9.88	8.86	8.16	8.03	8.46	9.64	10.86	12.06	12.78	12.56	11.57	9.92	8.17	6.67	5.98	6.16	72 4	
75	7.20	8.87	10.76	12.70	14.06	14.61	14.06	12.53	10.68	8.96	7.55	6.88	7.05	8.07	9.84	11.76	12.97	13.54	13.03	11.46	9.42	7.27	5.74	73 3	
76	5.30	5.90	7.44	9.66	11.92	14.02	15.17	15.16	13.87	11.66	9.44	7.56	6.34	6.07	6.86	8.68	10.80	12.96	14.26	14.55	13.37	11.16	8.45	74 3	
Sum	762.81	771.19	763.32	757.94	768.36	742.42	745.02	746.89	740.06	729.58	732.71	749.20	745.64	742.01	768.91	774.83	746.57	777.49	768.34	760.60	755.80	738.47	764.47	741.40	No. of Days.
No.	73	74	73	73	74	73	73	74	73	73	73	74	73	72	74	74	71	74	73	73	72	74	73	73	18094.03

No. of Days.  
73<sup>d</sup> 4<sup>h</sup>.  
18094.03









FORMS FOR SHORT-PERIOD TIDES.

SERIES J.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
231	13.60	16.07	17.04	16.38	13.96	10.25	6.47	3.74	2.56	3.20	5.12	8.18	11.74	15.30	17.66	18.50	17.76	14.76	10.60	7.27	5.06	4.48	5.07	223 7	
232	7.18	10.16	13.04	16.34	17.16	16.04	13.12	9.20	5.80	3.36	2.56	3.60	5.73	9.03	12.78	15.94	17.78	18.04	16.74	13.32	9.36	6.05	4.18	224 6	
233	3.80	4.90	7.56	11.10	14.46	16.66	16.88	15.39	12.15	8.23	5.44	3.52	3.32	4.58	7.04	10.14	13.35	16.16	17.52	17.26	15.28	11.80	8.22	225 5	
234	5.32	3.80	4.02	5.58	8.40	11.50	14.52	16.18	16.06	14.38	11.26	7.98	5.62	4.54	4.80	6.25	8.27	11.00	13.96	16.32	17.26	16.42	14.32	226 4	
235	10.85	7.62	5.16	4.10	4.64	6.45	8.92	12.05	14.70	15.80	15.18	13.36	10.62	7.94	6.32	5.74	6.44	7.77	9.72	12.07	14.12	15.66	15.72	227 3	
236	14.46	13.06	9.36	6.96	5.40	5.07	5.84	7.33	9.54	11.87	13.60	14.46	13.96	12.48	10.40	8.65	7.45	7.28	8.00	9.26	10.72	12.27	13.74	228 2	
237	14.47	14.18	12.78	10.82	8.78	6.78	5.83	5.86	6.74	8.34	10.14	12.02	13.26	13.57	12.85	11.76	10.70	9.74	9.12	8.90	9.34	10.06	10.94	229 1	
238	12.10	12.88	13.72	13.38	11.88	10.06	8.17	7.02	6.68	7.00	7.70	8.77	10.10	11.44	12.33	12.66	12.46	12.00	11.36	10.62	10.07	9.67	9.77	230 0	
239	10.12	10.82	11.54	12.43	12.67	12.12	11.23	9.96	8.64	7.77	7.46	7.69	8.30	9.04	10.10	11.17	12.34	12.90	12.90	12.34	11.72	11.15	10.62	10.30	231 0
240	10.00	10.14	10.50	11.34	11.96	12.26	11.97	11.38	10.53	9.44	8.35	7.66	7.57	8.12	9.06	10.48	11.57	12.72	13.42	13.56	13.18	12.30	11.45	231 23	
241	10.73	10.26	9.92	9.63	10.00	10.71	11.62	12.32	12.18	11.42	10.36	9.08	8.15	7.53	7.24	7.70	8.54	9.82	11.43	12.72	13.64	13.66	13.26	232 22	
242	12.36	11.22	10.18	9.34	8.97	9.08	9.88	10.76	11.64	12.26	12.35	11.85	10.40	8.78	7.36	6.44	6.28	7.14	8.37	10.20	11.94	13.38	14.40	233 21	
243	14.54	13.58	12.17	10.70	9.34	8.82	8.84	9.26	10.00	11.16	12.50	13.30	13.42	12.06	10.16	8.40	6.86	6.06	6.14	7.20	8.95	10.80	12.76	234 20	
244	13.96	14.91	14.84	13.64	11.84	9.97	8.77	8.36	8.48	8.96	10.06	11.56	13.12	13.97	13.64	12.06	9.70	7.27	5.96	5.56	6.35	7.80	9.76	235 19	
245	11.70	13.66	15.10	15.46	14.62	12.86	10.57	8.64	7.46	7.31	7.76	8.84	10.72	12.64	14.21	14.62	13.44	11.00	8.24	6.24	5.17	5.36	6.54	236 18	
246	8.54	10.66	13.00	15.02	15.96	15.50	14.08	11.60	8.97	7.34	6.70	6.84	7.80	9.62	11.70	13.76	14.95	14.67	12.76	10.00	7.37	5.56	4.97	237 17	
247	5.74	7.38	9.36	11.94	14.36	16.04	16.27	15.32	13.08	10.11	7.72	6.36	6.10	6.94	8.63	10.83	13.20	15.21	15.71	14.43	11.89	8.54	6.26	238 16	
248	4.97	5.06	6.36	8.22	10.64	13.40	15.80	16.62	16.16	14.21	11.38	8.34	6.35	5.46	5.74	7.13	9.22	11.84	14.36	15.71	15.48	13.64	10.66	239 15	
249	7.60	5.70	4.96	5.70	7.24	9.54	12.02	14.56	16.24	16.56	15.34	12.80	9.60	7.06	5.50	5.18	5.94	7.72	10.28	13.04	15.14	15.90	14.88	12.52	240 15
250	9.63	7.07	5.74	5.64	6.67	8.36	10.62	13.17	15.30	16.38	15.97	14.06	11.04	8.16	6.11	5.05	5.41	6.72	8.83	11.26	13.77	15.36	15.38	241 14	
251	14.00	11.50	8.72	6.86	5.97	6.34	7.52	9.30	11.47	13.80	15.46	15.84	14.77	12.44	9.37	7.06	5.37	4.85	5.64	7.12	9.24	11.64	13.96	242 13	
252	15.06	14.75	13.17	10.76	8.64	7.30	6.86	7.44	8.64	10.38	12.36	14.06	15.24	15.10	13.64	11.26	8.61	6.50	5.32	5.38	6.34	7.85	9.86	243 12	
253	11.96	13.64	14.58	14.07	12.68	10.68	8.97	8.02	7.81	8.36	9.26	10.60	12.24	13.73	14.44	13.86	12.25	10.02	8.06	6.46	5.62	5.78	6.47	244 11	
254	7.80	9.63	11.38	12.97	13.74	13.44	12.44	11.04	9.83	8.84	8.57	8.87	9.67	10.67	11.96	13.06	13.46	13.08	11.68	9.86	8.26	6.87	6.17	245 10	
255	6.26	7.02	8.17	9.66	11.26	12.55	13.37	13.57	12.94	11.92	10.73	9.67	9.16	9.18	9.63	10.54	11.48	12.46	12.92	12.66	11.74	10.42	8.87	246 9	
256	7.44	6.44	6.21	6.66	7.76	9.20	10.76	12.36	13.54	14.05	13.67	12.68	11.26	10.02	9.22	8.90	9.14	9.86	10.86	12.02	12.84	12.98	12.36	247 8	
257	11.16	9.57	7.60	6.24	5.63	5.97	7.17	8.80	10.66	12.80	14.28	14.96	14.74	13.66	11.85	10.04	8.66	8.02	8.14	9.04	10.38	12.00	13.14	248 7	
258	13.74	13.40	12.04	10.04	7.64	5.76	4.78	5.02	6.24	8.16	10.78	13.20	15.04	15.98	15.74	14.33	11.96	9.30	7.37	6.55	6.70	8.06	9.98	249 6	
259	12.06	13.93	14.86	14.44	12.80	10.18	7.37	5.17	3.90	4.03	5.50	7.96	10.88	13.80	16.04	17.04	16.46	14.44	11.04	8.24	6.27	5.15	5.63	7.24	250 6
260	9.64	12.52	14.74	15.98	15.46	13.29	9.94	6.63	4.34	3.17	2.53	5.38	8.20	11.40	14.56	16.82	17.44	16.36	13.83	9.98	6.70	4.46	3.84	251 5	
261	4.58	6.80	10.06	13.28	15.76	16.64	15.75	12.94	9.26	6.06	3.66	2.67	3.72	5.66	8.70	12.20	15.53	17.33	17.53	15.87	12.42	8.56	5.32	252 4	
262	3.44	3.17	4.55	7.26	10.87	14.22	16.50	17.05	15.47	12.37	8.44	5.52	3.48	3.10	4.46	6.74	9.94	13.47	16.22	17.47	17.02	14.77	10.84	253 3	
263	7.33	4.52	3.00	3.30	5.07	8.06	11.72	14.94	16.86	16.90	14.94	11.54	8.00	5.38	3.90	4.20	5.52	7.95	11.06	14.30	16.51	17.04	15.88	254 2	
264	12.99	9.17	5.97	3.70	2.94	3.94	6.16	9.14	12.45	15.42	16.68	16.10	13.81	10.56	7.46	5.47	4.87	5.60	7.04	9.54	12.25	14.81	16.16	255 1	
265	16.06	14.44	11.07	7.87	5.34	3.84	3.92	5.16	7.43	10.36	13.44	15.47	16.04	14.92	12.66	9.98	7.74	6.47	6.36	7.02	8.54	10.58	12.80	256 0	
266	14.58	15.36	14.73	12.52	9.86	7.17	5.31	4.44	5.02	6.44	8.50	11.04	13.56	14.79	14.77	13.46	11.46	9.44	8.00	7.36	7.56	8.36	9.51	256 23	
267	11.10	12.60	13.73	13.94	12.90	11.02	8.73	6.90	5.70	5.63	6.34	7.60	9.36	11.36	13.14	13.88	13.60	12.43	10.94	9.64	8.26	8.44	8.70	267 23	











33	7.54	6.26	6.13	6.68	7.86	9.28	10.86	13.10	12.94	11.93	10.66	9.72	9.12	9.06	9.26	10.60	11.82	12.86	13.34	12.82	11.45	10.03	8.74	7.48	37	22	
34	6.78	7.17	7.94	9.03	10.30	11.34	11.97	11.92	10.84	10.34	10.07	9.97	9.77	9.94	9.66	11.32	12.26	11.78	10.88	9.87	8.84	7.86	7.24	6.94	39	0	
35	7.18	9.07	10.14	11.00	11.56	11.85	11.77	11.42	10.84	10.07	9.70	9.70	10.13	10.80	11.27	11.45	11.25	10.76	9.90	8.00	7.11	6.58	6.74	7.44	40	3	
36	8.51	9.84	11.76	12.34	12.55	12.30	11.60	10.57	9.76	9.34	9.56	10.24	10.94	11.36	11.44	10.97	10.10	9.97	7.87	6.30	6.50	7.26	8.50	10.16	41	6	
37	11.44	12.65	13.26	12.56	11.36	10.08	9.16	8.67	8.64	9.01	9.76	11.25	11.66	11.34	10.36	8.82	7.36	6.12	5.54	6.85	5.82	5.46	7.46	13.46	42	9	
38	13.97	13.64	12.30	9.26	10.76	8.14	7.84	8.12	8.96	10.24	11.52	12.66	12.07	10.47	8.56	6.64	5.46	5.20	5.93	7.53	11.72	14.67	14.84	13.98	43	12	
39	12.14	10.00	8.54	7.66	7.53	9.56	11.03	12.66	13.62	13.60	12.30	10.24	7.77	5.88	4.96	6.33	8.27	10.66	13.07	14.58	15.23	15.23	9.02	44	15		
40	7.54	6.79	7.00	8.13	9.87	11.85	14.38	13.88	11.93	9.10	6.54	4.66	4.00	4.90	9.20	11.97	14.34	15.82	15.96	14.78	12.26	9.64	7.46	5.96	45	18	
41	6.74	8.48	10.85	13.07	14.56	14.85	12.90	7.86	5.57	4.07	4.04	5.46	7.84	10.63	13.64	16.64	15.00	13.87	10.90	8.00	6.17	5.46	5.74	7.26	46	21	
42	12.35	14.42	15.50	15.15	13.08	9.90	6.94	4.75	3.02	6.62	9.46	12.60	15.08	15.08	16.60	16.64	15.00	11.93	6.76	5.63	5.54	7.84	10.54	13.30	47	23	
43	15.12	14.46	11.76	8.44	5.86	4.26	4.25	5.52	7.84	10.68	15.84	16.68	15.86	13.15	10.22	7.36	5.65	4.23	4.40	9.74	14.55	15.46	15.54	15.51	48	2	
44	13.57	7.47	5.38	4.52	5.04	6.70	9.14	12.18	14.74	16.26	14.64	11.74	8.68	6.28	4.54	4.14	5.07	7.06	12.44	14.55	15.46	14.76	12.57	9.68	50	5	
45	7.24	5.84	6.54	8.40	10.77	13.32	15.42	16.26	15.47	13.18	10.24	7.54	4.54	4.69	5.80	7.87	10.40	12.80	14.34	15.06	11.86	9.36	7.58	6.64	51	8	
46	6.76	7.86	9.60	11.66	13.73	15.08	15.32	14.12	11.86	9.24	6.90	5.06	6.46	8.24	10.33	12.41	13.86	14.34	13.44	14.03	11.46	7.40	7.66	8.58	52	11	
47	9.92	11.68	13.36	14.16	14.12	10.83	8.57	5.77	6.98	5.64	5.44	6.63	8.23	11.77	12.96	13.40	12.76	11.56	10.24	9.04	8.05	8.28	9.76	11.20	53	14	
48	12.50	13.18	13.06	11.88	10.25	8.57	5.77	6.98	5.64	6.37	7.82	9.54	11.17	12.38	13.02	12.16	11.07	10.02	8.94	8.44	8.48	9.27	10.44	12.34	54	17	
49	12.34	11.70	10.50	8.90	7.32	5.96	5.24	5.12	7.17	8.90	10.63	12.10	13.16	13.56	13.13	10.37	7.60	7.64	9.18	11.00	12.40	13.36	12.60	12.60	56	22	
50	12.26	9.76	7.96	6.27	5.06	4.55	5.02	8.52	8.52	12.72	14.14	14.86	14.44	12.70	10.66	8.80	7.21	8.83	12.96	14.40	14.74	13.76	11.70	8.84	58	1	
51	10.86	8.63	4.63	4.06	4.70	6.46	8.84	11.30	13.80	15.56	15.33	12.96	10.26	7.95	6.54	6.18	7.03	11.00	13.67	15.38	14.57	8.26	5.48	3.42	59	4	
52	6.08	4.03	3.42	4.14	6.52	13.16	16.06	16.96	17.15	15.84	9.66	7.00	5.18	5.12	6.26	8.32	11.16	13.67	16.54	14.66	11.26	7.66	3.20	4.70	60	7	
53	2.92	4.14	6.52	9.58	16.04	17.62	17.34	15.27	11.66	8.27	5.56	4.16	5.84	8.66	11.92	14.74	16.46	16.54	14.66	11.26	7.66	3.20	3.27	4.70	60	7	
54	7.52	10.86	14.63	17.06	16.96	13.90	10.20	6.96	4.47	3.56	4.02	6.04	9.40	15.55	16.86	16.36	13.86	10.44	6.92	4.54	3.37	5.80	8.56	12.33	61	10	
55	15.44	17.27	17.40	15.46	12.03	8.50	3.74	3.27	4.33	7.10	10.34	13.76	15.97	15.76	12.96	9.44	6.74	4.67	4.23	5.26	7.43	5.80	13.82	17.08	62	13	
56	16.40	13.86	10.50	7.26	4.84	3.56	5.00	3.86	8.27	11.55	14.34	16.02	14.66	11.66	8.60	6.46	5.46	6.56	8.86	11.44	14.36	15.97	16.18	14.88	63	16	
57	8.86	6.28	4.57	4.06	4.86	6.67	9.40	12.24	13.97	14.58	13.25	10.46	8.22	6.76	6.34	7.00	8.36	12.44	14.42	15.27	14.71	12.72	10.14	7.72	64	18	
58	5.93	5.00	6.10	8.03	10.30	13.47	13.97	14.58	12.03	10.14	8.54	7.56	7.56	8.42	9.82	11.34	12.96	14.04	13.22	11.36	9.36	7.56	6.27	5.84	65	21	
59	6.34	7.46	10.76	12.44	13.56	13.74	12.74	11.40	10.97	9.16	8.96	9.77	10.46	11.36	12.44	13.07	13.03	12.12	8.86	10.46	7.68	7.02	7.66	8.54	67	0	
60	9.66	10.96	12.24	12.88	12.24	11.43	10.66	10.24	10.16	10.24	9.27	10.86	12.02	12.40	12.24	11.36	10.18	8.87	7.97	7.94	6.67	8.30	9.78	10.74	68	3	
61	11.76	12.46	12.67	11.74	11.26	10.87	10.56	10.36	10.22	10.36	10.76	11.26	11.56	10.86	9.96	9.14	8.40	7.98	7.80	7.86	9.30	10.46	11.44	12.08	69	6	
62	12.36	12.27	12.03	11.50	10.20	9.73	9.58	9.87	10.35	10.89	11.10	11.10	10.78	10.32	8.86	7.97	7.28	7.26	7.87	8.97	10.32	12.46	13.04	13.10	70	9	
63	12.54	11.68	10.56	9.64	9.08	8.82	9.88	12.06	12.56	11.57	9.92	8.17	6.67	5.98	6.16	7.20	10.76	12.70	14.08	14.61	14.06	12.53	10.68	8.96	72	15	
64	9.88	8.86	8.16	8.03	8.46	9.64	10.86	12.78	12.56	11.57	9.92	8.17	6.67	5.98	6.16	7.20	10.76	12.70	14.08	14.61	14.06	12.53	10.68	8.96	72	15	
65	6.88	7.95	8.07	9.84	11.76	12.97	13.54	13.03	11.46	7.27	5.74	5.30	5.90	7.44	9.66	11.92	14.02	15.16	13.87	11.66	9.44	7.56	6.34	6.07	73	17	
66	6.86	10.80	12.96	14.26	14.55	13.37	11.16	8.45	6.26	5.12	6.24	8.10	10.63	13.22	15.15	15.86	15.17	13.22	7.86	6.06	5.25	5.54	6.90	9.24	74	20	
Sum	747.98	740.35	747.10	742.53	763.46	739.17	764.06	778.00	780.85	765.81	754.39	746.88	750.22	787.54	746.59	773.31	769.37	783.82	751.20	779.06	757.21	777.05	774.22	733.98	No. of Days.		
No.	75	73	74	72	75	73	75	74	74	74	73	74	73	75	73	75	74	75	72	74	73	75	75	78	78	1823.15	

FORMS FOR SHORT-PERIOD TIDES.

SERIES Q.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
07	11.72	13.95	15.20	13.30	10.64	7.57	5.44	4.44	4.96	6.46	8.94	14.34	16.00	16.06	14.53	11.64	8.54	5.76	4.22	5.24	7.30	10.10	13.02	15.04	15.04	75.23
68	16.00	15.20	12.86	9.54	4.92	4.38	5.32	7.55	10.33	13.50	15.75	16.07	13.66	10.42	7.22	4.92	3.64	4.00	5.06	8.33	14.30	16.06	16.52	16.52	15.06	77.2
69	12.13	8.73	6.13	4.66	4.09	8.92	11.86	14.66	16.40	16.56	15.07	11.90	8.47	3.74	3.22	4.26	6.60	9.60	12.85	15.23	16.56	16.25	10.83	8.00	78.5	
70	5.75	5.11	5.88	7.84	10.46	13.38	16.60	15.80	13.36	10.12	7.06	4.83	3.54	3.76	7.86	11.00	13.93	15.92	16.74	15.74	13.36	10.24	7.64	6.08	79.8	
71	7.14	9.00	11.56	13.90	15.66	15.98	14.76	8.90	6.13	4.34	3.62	4.36	6.06	8.47	11.31	15.62	16.12	14.97	12.74	10.02	8.05	6.96	7.06	7.93	80.11	
72	12.07	14.08	15.33	15.08	13.57	11.16	8.36	4.76	6.40	5.46	7.26	9.48	11.88	13.90	15.36	15.50	14.66	12.67	10.54	8.74	7.94	8.14	9.06	10.62	81.13	
73	13.77	14.20	12.80	10.64	8.47	6.76	5.86	5.82	7.75	9.52	11.71	13.54	14.73	14.90	14.06	12.63	11.05	9.70	8.72	9.12	10.24	11.76	13.06	13.60	82.16	
74	14.53	13.06	8.93	7.40	6.43	6.30	6.68	7.68	9.46	11.24	14.08	14.52	14.22	13.04	11.70	10.34	9.24	8.84	9.04	10.96	12.05	12.86	12.96	12.44	83.19	
75	13.34	10.56	8.30	6.48	6.64	7.48	8.86	10.64	12.34	13.74	14.48	13.62	12.12	10.36	8.96	8.11	7.96	8.44	9.76	11.26	12.92	12.78	11.94	10.50	84.22	
76	11.23	9.67	7.06	6.18	6.44	7.48	8.86	10.44	12.34	13.74	14.44	13.62	12.12	10.36	8.96	8.11	7.96	8.44	9.76	11.26	12.92	12.78	11.94	10.50	84.22	
77	8.78	7.20	6.08	5.92	8.34	10.26	12.20	13.86	15.00	15.14	14.16	12.20	8.00	6.90	6.56	7.46	9.22	11.16	12.56	13.57	14.06	11.72	9.38	7.17	86.1	
78	17.03	17.08	15.36	11.92	8.64	6.18	4.48	4.25	5.24	11.00	14.10	16.43	12.86	9.53	7.16	5.81	5.93	7.22	12.02	14.66	16.44	16.67	15.06	12.02	91.15	
79	13.96	10.44	7.12	4.80	3.83	4.41	6.43	8.78	12.04	16.66	17.13	15.64	12.86	9.53	7.16	5.81	5.93	7.22	12.02	14.66	16.44	16.67	15.06	12.02	91.15	
80	8.56	5.84	3.84	4.93	7.24	10.09	13.22	15.56	16.90	16.56	14.74	8.84	7.02	6.48	7.04	8.26	10.50	13.00	14.94	15.12	12.94	9.87	7.14	5.16	92.18	
81	4.22	4.76	8.73	11.37	14.00	15.82	16.34	15.34	13.10	10.40	8.36	7.28	8.03	9.50	11.53	13.48	14.74	14.92	13.67	11.34	6.67	5.40	5.22	6.16	93.21	
82	7.85	9.97	12.30	14.30	15.46	14.27	12.24	10.20	8.78	8.26	8.47	9.24	10.52	13.48	14.16	13.84	12.27	10.16	8.14	6.47	6.22	7.44	9.20	10.85	95.0	
83	12.64	14.05	14.67	14.27	12.97	11.44	9.16	8.84	9.16	9.84	10.95	11.96	12.80	12.06	10.94	9.24	7.80	6.78	6.70	7.30	8.37	9.54	12.34	13.52	96.3	
84	13.80	13.26	12.13	10.96	10.04	9.60	9.33	9.00	10.56	11.44	11.92	12.05	11.54	10.36	8.12	7.47	7.48	8.76	8.52	9.46	10.73	10.90	12.74	12.98	97.6	
85	11.86	11.07	10.34	9.94	9.77	9.87	10.02	10.81	11.14	11.27	10.92	10.30	9.34	8.36	7.74	7.58	8.76	9.87	11.04	11.96	12.50	12.66	12.42	11.96	98.8	
86	11.34	9.91	9.47	9.34	9.52	9.94	10.53	10.94	11.12	10.62	10.00	9.22	8.40	8.01	8.13	8.63	10.66	13.36	13.66	13.66	11.42	10.02	8.72	7.96	100.14	
87	10.55	8.94	8.74	9.48	10.45	11.36	11.88	11.89	11.44	9.40	8.46	7.84	7.76	8.43	9.46	10.86	12.30	13.82	13.82	12.80	10.96	7.46	6.81	6.84	101.17	
88	9.62	8.54	9.47	11.00	12.70	12.87	12.44	11.06	9.52	8.12	7.49	8.26	9.54	11.08	12.70	14.06	14.56	14.22	12.80	8.88	6.18	6.54	5.58	5.14	102.20	
89	9.62	11.52	13.00	14.97	13.00	11.02	9.05	7.48	6.74	6.92	7.97	11.72	13.58	14.86	15.12	14.21	12.35	9.67	7.47	5.98	5.14	7.76	9.84	12.16	102.20	
90	14.02	15.18	15.06	13.40	8.28	6.66	6.02	6.46	7.88	10.06	12.53	14.55	15.72	13.80	11.08	8.22	5.93	4.52	4.22	5.47	7.72	13.37	15.36	16.20	103.23	
91	15.32	13.00	9.88	7.34	5.76	5.40	8.22	10.70	13.40	15.52	16.25	15.36	12.80	6.56	4.47	3.42	3.91	5.74	8.31	11.40	14.40	16.28	16.72	12.68	105.2	
92	9.44	6.81	5.47	5.38	6.52	8.91	11.80	15.07	16.08	14.35	11.30	7.80	4.97	2.93	2.46	3.76	9.51	12.97	15.58	17.14	17.04	14.94	11.68	8.36	106.5	
93	5.06	5.37	7.24	10.07	13.10	15.40	16.44	15.84	9.74	6.67	4.93	2.50	2.77	4.44	7.50	10.96	16.70	17.72	16.91	14.37	10.87	8.10	6.15	5.71	107.7	
94	6.50	11.33	14.12	15.97	16.50	15.10	12.22	8.67	5.14	2.56	3.47	5.74	8.64	12.02	15.12	16.94	17.54	13.40	10.32	7.62	6.17	6.07	7.04	9.13	108.10	
95	12.00	15.66	14.54	13.66	10.74	7.44	4.88	3.28	3.04	4.36	6.67	12.47	15.00	16.74	16.94	15.60	13.03	10.01	7.87	6.80	6.76	7.71	9.70	14.15	109.13	
96	15.04	14.50	9.92	7.24	5.36	4.17	4.16	5.20	7.26	9.80	12.40	15.74	15.74	14.47	12.12	9.90	8.07	7.14	7.11	7.83	11.88	13.16	13.74	13.28	110.16	

99	11.76	9.56	7.60	5.96	5.02	5.86	7.52	9.74	12.00	13.87	14.87	14.77	13.76	10.26	8.74	7.84	7.54	8.00	9.34	11.00	12.36	12.72	11.58	10.44	111 19	
100	8.48	6.94	6.06	5.06	6.60	9.72	11.62	13.34	14.34	14.44	13.66	12.26	10.62	8.03	7.66	7.76	8.68	10.20	11.63	12.43	12.66	12.10	9.47	8.14	112 22	
101	7.03	6.54	6.88	7.94	9.57	11.42	13.00	14.44	13.93	12.76	11.00	9.18	7.74	6.96	7.85	9.40	10.96	12.36	13.06	13.12	12.22	10.65	8.87	7.52	114 1	
102	6.84	7.66	9.26	11.04	12.88	14.12	14.66	12.64	10.64	8.60	6.78	5.94	5.93	7.08	9.00	11.04	13.72	13.87	12.97	11.36	9.32	7.66	6.62	6.47	115 4	
103	8.88	10.96	12.96	14.54	15.17	14.54	12.77	10.22	7.74	4.88	5.14	6.58	8.88	11.33	13.36	14.66	14.94	11.70	9.34	7.26	6.22	6.20	7.24	9.00	116 6	
104	13.22	14.86	15.37	13.44	12.10	9.16	6.48	4.70	4.20	6.70	9.17	11.77	14.02	15.57	15.54	14.03	11.54	8.80	6.07	6.34	7.48	9.44	11.96	14.10	117 9	
105	15.48	15.44	10.92	10.92	4.04	5.80	8.48	11.42	14.32	16.17	15.46	16.26	15.76	13.86	11.00	8.24	6.47	5.97	7.98	10.16	12.70	14.64	15.66	14.96	118 12	
106	12.70	9.46	6.57	3.42	6.96	12.56	14.92	16.36	16.36	14.70	11.93	9.06	7.20	6.70	7.74	9.37	11.47	13.86	15.04	15.06	12.96	9.73	4.24	3.42	120 18	
107	5.15	3.44	3.36	4.67	9.52	15.48	16.25	15.62	13.50	10.52	8.22	6.40	7.02	8.34	12.60	14.08	14.45	13.26	10.82	7.87	5.57	3.94	4.88	6.80	121 21	
108	4.04	5.68	8.27	10.68	13.46	16.25	14.30	11.86	7.76	6.94	7.06	7.86	9.36	11.24	13.06	13.66	10.40	6.46	5.20	6.00	7.54	9.26	8.22	10.36	122 0	
109	9.18	11.76	14.24	15.56	15.54	14.30	9.40	8.96	7.76	6.94	7.06	7.86	9.36	11.24	13.06	13.66	10.40	6.46	5.20	6.00	7.54	9.26	8.22	10.36	123 0	
110	14.56	15.43	14.76	13.04	10.84	8.96	7.76	7.44	8.80	10.26	11.94	13.06	13.06	12.28	10.40	6.74	6.04	6.20	7.12	5.97	4.36	4.90	6.32	8.22	124 2	
111	14.86	12.06	10.14	8.84	8.15	8.06	8.40	9.36	11.94	11.68	12.46	11.36	9.58	7.94	6.94	6.04	6.20	7.12	5.97	4.36	4.90	6.32	8.22	10.36	125 5	
112	11.41	8.90	8.46	8.56	9.00	9.74	10.55	11.36	11.86	10.72	8.46	7.66	7.97	8.66	9.74	10.97	12.22	13.24	13.54	12.12	10.96	9.98	9.27	8.94	126 8	
113	9.24	8.96	8.94	9.58	10.34	10.96	11.44	11.34	10.38	9.56	7.76	7.66	7.97	8.66	9.74	10.97	12.22	13.24	13.54	12.12	10.96	9.98	9.27	8.94	127 11	
114	8.74	8.80	9.24	10.80	11.26	11.29	10.79	10.06	9.26	8.46	8.06	8.04	9.72	10.94	12.20	12.96	13.22	12.94	12.14	11.17	9.06	8.20	7.92	8.00	128 14	
115	8.62	9.56	10.46	11.34	11.77	10.76	9.74	8.78	8.17	8.10	8.66	9.60	10.93	13.20	13.50	13.50	13.18	12.36	11.16	9.68	8.30	7.26	7.45	10.00	129 17	
116	11.40	12.36	12.92	12.66	11.62	8.85	7.83	8.24	9.37	10.96	14.26	14.66	13.94	12.24	9.97	7.60	4.92	5.06	6.42	8.60	10.93	13.28	14.84	14.16	130 20	
117	14.22	13.67	12.20	10.16	8.55	7.53	7.27	9.36	11.30	13.16	14.26	14.66	13.94	12.24	9.97	7.60	4.92	5.06	6.42	8.60	10.93	13.28	14.84	14.16	131 23	
118	12.38	10.01	8.14	6.95	6.90	8.01	9.74	11.84	13.66	15.16	14.10	11.76	8.83	6.14	4.18	3.66	4.36	4.92	5.06	6.42	8.60	10.93	13.28	14.84	132 1	
119	9.36	6.17	6.50	7.92	10.02	12.44	14.46	15.64	15.47	13.76	7.20	4.46	2.86	2.74	4.17	6.63	9.77	13.00	17.16	16.96	15.18	11.90	8.78	6.57	134 4	
120	5.95	7.94	6.52	10.30	12.84	15.02	15.97	15.24	12.56	8.86	5.70	3.17	2.43	4.23	7.22	10.62	13.96	16.50	17.69	14.58	10.90	8.02	5.94	6.30	135 7	
121	8.25	10.90	13.74	16.06	14.62	11.54	7.86	4.52	2.14	1.42	2.56	5.03	11.45	14.68	16.97	17.83	16.77	14.06	10.36	7.60	5.52	6.20	8.20	11.20	136 10	
122	14.02	15.72	15.74	13.76	6.92	2.67	4.46	6.78	9.71	12.92	15.50	17.10	17.16	15.40	9.57	7.36	6.16	6.11	7.20	9.40	12.06	14.14	14.36	12.18	137 13	
123	15.07	12.82	9.66	6.56	4.08	2.88	4.46	6.78	13.15	15.36	16.23	14.86	11.94	9.56	6.48	6.38	7.36	9.30	11.76	13.38	13.98	13.42	11.66	9.36	139 19	
124	9.28	6.58	4.76	3.86	4.30	5.66	10.44	14.66	15.46	14.00	11.78	9.46	7.72	6.96	6.82	7.44	10.74	12.30	13.13	12.92	11.76	10.08	8.18	6.84	140 21	
125	5.74	4.98	5.26	6.33	8.08	10.42	12.87	15.72	14.66	15.46	14.00	11.78	9.46	7.72	6.96	6.82	7.44	10.74	12.30	13.13	12.92	11.76	10.08	8.18	6.84	141 21
126	6.28	7.26	8.54	10.38	12.48	14.22	14.94	14.74	13.52	9.46	7.84	6.86	6.52	6.83	8.02	9.54	12.28	12.65	10.06	8.56	7.47	7.86	6.87	6.74	142 0	
127	7.36	10.16	11.86	13.27	14.14	13.98	12.92	11.14	9.14	6.36	5.86	5.93	7.12	8.94	10.74	12.22	12.86	11.60	10.06	8.56	7.47	7.24	7.70	8.44	143 3	
128	10.00	11.62	13.06	13.93	13.82	12.68	10.82	9.01	7.20	5.72	5.17	5.56	8.92	10.90	12.46	13.44	13.42	12.46	10.72	9.12	8.02	7.63	8.26	9.76	144 6	
129	13.14	14.05	13.96	10.76	8.52	6.66	5.32	4.84	5.46	7.38	9.67	11.66	14.34	14.36	13.24	11.36	9.64	8.16	7.32	7.50	10.16	13.46	14.20	145 9		
130	13.97	12.62	10.50	7.84	4.46	5.72	4.54	5.90	7.82	10.17	12.67	14.36	15.22	13.34	11.12	9.16	7.84	7.36	7.72	8.72	10.32	12.06	13.66	11.02	146 12	
131	9.27	6.82	4.82	3.97	4.57	8.40	6.16	11.03	13.46	15.10	15.52	14.67	12.94	10.67	8.77	7.60	7.93	9.10	10.86	12.73	14.28	14.53	13.00	10.66	5.58	147 15
132	4.22	4.13	5.24	7.24	9.70	12.30	14.40	15.74	15.70	14.12	12.14	9.74	8.36	7.64	7.54	8.20	9.70	13.62	14.54	14.16	12.22	9.68	6.84	4.84	3.94	148 18
Sum	769.00	740.33	773.60	721.18	740.99	745.29	768.76	735.74	742.12	749.25	764.15	771.41	788.42	756.35	763.27	769.01	749.10	775.62	761.21	780.98	756.63	702.66	743.04	765.72	No. of Days	
No.	74	73	75	73	74	75	74	72	74	73	75	73	75	74	74	75	72	74	73	75	73	75	73	75	75	1821.91

FORMS FOR SHORT-PERIOD TIDES. SERIES Q.—(Continued).

Table with 24 columns (Day, 0h to 23h) and 25 rows (133 to 164). Each cell contains a tidal height value in feet, often with a decimal point. The final column is labeled 'Solar Hour' and contains values 'd h' (e.g., 7:20 149 20).



165	12:19	12:26 12:22	10:84	9:25	7:90	6:96	6:92	7:56	8:50	10:00 11:48	13:23	14:36	14:44	13:38	11:42	9:60	8:02	6:94 6:56	6:92	7:79	9:26	10:80	11:92	12:43	185 16
166	12:16	11:12	9:70 8:48	7:63	7:56	8:14	9:04	10:41	11:98	13:30	13:98 13:72	12:51	10:84	8:96	7:47	6:70	6:48	6:84	7:86	9:16 10:52	11:71	12:36	12:28	11:46	186 19
167	10:38	9:16	8:34	8:14 8:38	9:04	10:37	11:82	13:16	13:66	13:27	11:87	10:24 8:57	7:05	6:14	5:87	6:26	7:22	8:72	10:36	11:70	12:56 12:86	12:14	11:14	9:86	187 22
168	8:86	8:32	8:34	9:02	10:46 11:88	13:12	13:48	12:96	11:86	10:30	8:58	7:00	5:74 5:32	5:74	6:86	8:67	10:62	12:30	13:47	13:96	13:31	12:10 10:48	9:04	8:28	189 1
169	8:37	8:98	10:28	11:72	13:02	13:62 13:24	12:02	10:14	8:20	6:16	4:76	4:31	4:90	6:40	8:62 10:94	13:04	14:57	15:22	14:64	12:87	10:58	8:66	7:68 7:62	8:40	190 4
170	10:00	11:70	13:12	13:97	13:69	12:32	10:27 7:76	5:44	3:88	3:19	3:88	5:80	8:60	11:46	13:90	15:54 16:06	15:08	12:92	10:40	8:23	7:07	6:90	7:82	9:54 11:60	191 7
171	13:35	14:38	14:34	12:76	10:16	7:15	4:46	2:56 2:27	3:49	5:92	8:80	12:36	15:04	16:76	17:06	15:90	13:27 10:08	7:42	6:03	6:04	7:17	9:30	11:84	13:92	192 9
172	15:05 14:90	13:08	9:91	6:43	3:53	1:84	1:84	3:58	6:20 3:54	13:00	15:92	17:60	17:55	15:88	12:54	9:04	6:46	5:24 5:54	6:76	9:24	12:48	14:76	16:12	15:46	193 12
173	13:17	9:32 5:65	2:96	1:56	1:90	3:97	6:70	10:13	13:94	16:80	18:22 17:87	15:72	12:00	8:47	5:86	4:66	4:98	6:66	9:72 13:12	15:46	16:44	15:54	12:76	8:60	194 15
174	5:17	2:76	1:62 2:37	4:50	7:60	11:14	14:80	17:30	18:38	17:46	14:77	11:14 7:30	5:12	4:24	4:66	6:66	9:96	13:24	15:56	16:37 15:10	12:10	8:47	5:36	3:22	195 18
175	2:47	3:46	5:71	8:66 12:13	15:36	17:38	17:97	16:76	13:80	10:58	7:04	4:79	4:26 5:04	7:14	10:42	13:85	15:77	16:14	14:53	11:60	8:45 5:84	4:20	3:82	5:12	196 21
176	6:97	9:80	13:00	15:56	17:04	17:17 15:44	12:60	9:26	6:86	5:22	4:84	5:76	8:06	10:85 13:97	15:36	15:40	13:86	11:04	8:20	6:43	5:40 6:64	7:95	10:24	198 0	
177	12:80	15:32	16:34	15:86	14:11	11:28	8:50 6:30	5:34	5:40	6:24	8:00	10:50	12:97	14:30	14:44 12:94	10:92	9:08	7:74	7:24	7:56	8:14	9:16	11:11 13:10	14:71	199 3
178	15:40	14:72	12:96	10:60	8:38	6:86	5:92	6:05 6:82	8:26	10:28	12:30	13:38	13:40	12:62	11:34	10:16	8:58	8:59	8:86	9:62	10:96	12:55	13:78	14:07 13:40	200 6
179	11:92	10:10	8:37	6:87	6:38	6:51	7:24	8:41	9:82 11:28	12:52	12:90	12:68	11:87	10:93	10:01	9:34	9:14 9:27	9:97	10:90	12:12	13:14	13:41	12:71	11:34	201 8
180	9:77	8:47 7:34	6:76	6:86	7:36	8:56	10:06	11:46	12:50	13:02 12:96	12:57	11:86	10:96	10:04	9:53	9:52	9:76	10:73 11:74	12:78	13:04	12:50	11:42	10:20	8:76	202 11
181	7:52	6:90	6:76 7:25	8:50	10:20	11:86	13:24	13:87	13:87	13:28	12:22 11:04	10:07	9:54	9:50	9:87	10:64	11:70	12:60	12:94 12:66	11:70	10:10	8:56	7:16	6:24	203 14
182	6:28	7:14	8:62	10:44 12:07	13:40	14:20	14:14	13:28	12:08	10:74	9:52	8:94 8:94	9:48	10:50	11:72	12:63	13:06	12:60	11:28	9:36 7:66	6:38	5:86	6:06	7:07	204 17
183	8:94	10:96	13:07	14:58	15:07 14:54	13:34	11:84	10:26	9:14	8:46	8:46	9:16	10:36 11:74	13:14	13:52	12:81	11:24	9:13	7:31	5:74	5:33	6:10 7:65	9:76	12:02	205 20
184	14:00	15:20	15:33	14:58	12:97	11:01 9:35	8:37	8:18	8:73	9:62	10:95	12:64	13:76	13:92 12:56	10:36	8:02	6:14	5:26	5:24	6:52	8:36	10:60	12:96 14:83	16:05	206 23
185	15:68	14:35	12:14	9:94	8:56	8:04	8:20 8:78	9:99	11:82	13:73	14:66	14:04	11:84	8:90	6:50 5:04	4:74	5:78	7:22	9:33	11:77	14:22	15:86	16:07	15:15 13:18	208 2
186	10:77	8:67	7:57	7:18	7:78	8:96	10:77 14:27	14:50	13:28	10:70	7:76	5:53	4:56	4:86	6:26	8:20 10:44	13:14	15:37	16:51	16:11	14:47	11:94	9:36	209 4	
187	7:58 6:88	7:16	8:00	9:72	11:80	13:84	14:90	14:32	12:37 9:57	6:78	5:10	4:56	5:42	7:13	9:26	11:96	14:36	15:96 16:14	15:17	12:96	10:25	8:01	6:67	6:34	210 7
188	6:89	8:16 10:14	12:46	14:24	14:84	13:50	10:90	8:02	5:86	5:04	6:52	8:34	10:66	13:15	15:27	16:14	15:82	14:14	11:47 8:96	7:02	6:16	6:33	7:34	9:23	211 10
189	11:44	13:54	14:58 14:24	12:42	9:84	7:44	5:64	5:14	5:97	7:54	9:60	11:76 13:95	15:50	15:83	14:93	12:72	10:10	7:72	6:16	5:77 6:54	7:96	9:86	12:04	13:74	212 13
190	14:37	13:56	11:51	8:97 7:02	5:96	5:96	7:12	8:61	10:53	12:64	14:44	15:55	15:26 13:84	11:46	8:86	6:95	5:97	6:05	7:05	8:56	10:54 12:48	13:67	13:96	12:84	213 16
191	10:98	9:00	7:60	6:88	7:24 8:26	9:66	11:37	13:15	14:57	15:10	14:32	12:72	10:34	8:27 6:67	6:12	6:40	7:34	8:74	10:52	12:26	13:26	13:32 12:36	10:84	9:38	214 19
192	8:24	7:77	8:12	8:86	10:16	11:76 13:33	14:29	14:38	13:46	11:64	9:64	7:76	6:48	6:10	6:50 7:54	9:00	10:63	12:05	12:96	13:18	12:64	11:47	10:24 9:16	8:76	215 22
193	9:04	9:66	10:72	12:02	13:24	14:10	14:04 13:02	11:29	9:63	7:96	6:84	6:50	6:73	7:66	9:04	10:52 12:10	13:14	13:55	13:28	12:50	11:34	10:26	9:52	9:35 9:67	217 1
194	10:59	11:83	12:88	13:62	13:44	12:54	11:15	9:50	7:86 6:50	5:94	6:16	7:10	8:50	10:20	11:94	13:44	14:14 14:16	13:42	12:16	10:76	9:56	9:05	9:15	9:96	218 3
195	11:33 12:62	13:38	13:55	12:96	11:68	9:90	7:96	6:26	5:30	5:46 6:46	8:25	10:24	12:44	14:18	15:26	15:50	14:64	12:94 10:78	9:16	8:56	8:76	9:78	11:16	12:57	219 6
196	13:70	14:26 14:02	12:80	10:52	8:01	5:84	4:76	4:81	5:98	7:77	10:32 13:02	15:24	16:66	16:76	15:58	13:24	10:54	8:38	7:60 7:78	8:76	10:54	12:56	14:24	15:18	220 9
197	14:86	13:21	10:40	7:41 4:97	3:62	3:84	5:16	7:44	10:44	13:54	16:14	17:54 17:44	15:84	12:90	9:72	7:44	6:60	6:85	8:10	10:22 12:92	15:15	16:26	15:72	13:66	221 12
198	10:33	6:96	4:40	3:04	3:33 5:32	7:86	11:08	14:56	17:20	18:37	18:04	16:16	12:38 8:82	6:46	5:54	5:95	7:72	10:60	13:60	16:07	17:04 16:38	13:96	10:25	6:47	222 15
Sum	764:31	787:43	750:82	777:22	768:42	755:54	742:48	728:93	770:21	759:73	787:09	779:64	772:88	772:18	780:18	771:08	776:86	776:52	774:13	790:96	779:33	775:94	776:29	792:73	No. of Days. 73 <sup>d</sup> 21 <sup>h</sup> .
No.	73	75	73	75	74	73	74	73	75	73	74	74	75	73	74	73	74	75	74	75	73	74	73	74	185 10 90

FORMS FOR SHORT-PERIOD TIDES.

SERIES Q.—(Continued).

Day	Solar Hour																									
	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
199	3.74	2.56	3.20	5.12	8.18	11.74	17.66	18.30	17.76	14.76	10.60	7.27	5.06	4.48	7.18	10.36	13.94	16.34	17.16	16.04	13.12	9.20	5.80	3.36	2.56	223 18
200	3.60	5.73	9.03	13.78	15.94	17.78	18.04	13.32	9.36	6.05	4.18	3.80	4.90	7.56	11.10	16.66	16.88	15.39	12.15	8.23	5.44	3.52	3.32	4.58	7.04	224 21
201	10.14	13.35	16.16	17.52	17.26	15.28	11.80	8.22	3.80	4.02	5.58	8.40	11.50	14.52	16.18	14.38	11.26	7.98	5.62	4.54	4.80	6.25	8.27	11.00	225 23	
202	13.06	17.36	16.42	14.32	10.85	7.62	5.16	4.10	4.64	8.92	12.05	14.70	15.80	15.18	13.36	10.62	7.94	5.74	6.44	7.77	9.72	12.07	14.12	15.66	227 2	
203	10.32	14.46	9.36	6.96	5.40	5.07	5.84	7.33	9.54	13.66	11.87	14.46	12.85	12.48	10.40	8.65	7.45	7.28	8.00	10.72	12.27	13.74	14.47	14.18	228 5	
204	15.72	12.06	6.78	5.86	6.74	8.34	10.14	12.02	13.26	13.57	11.76	10.70	9.74	9.12	8.90	9.34	10.06	10.94	12.10	12.88	13.38	11.88	10.06	8.17	229 8	
205	10.82	8.78	5.83	7.00	8.77	10.10	11.44	12.33	12.66	12.46	12.00	11.36	10.07	9.67	9.77	10.12	10.82	12.43	12.67	12.12	11.23	9.06	7.77	7.46	230 11	
206	7.02	6.68	7.00	8.70	10.10	11.44	12.33	12.66	12.46	12.00	11.36	10.07	9.67	9.77	10.12	10.82	12.43	12.67	12.12	11.23	9.06	7.77	7.46	7.46	231 14	
207	7.69	8.30	9.04	9.04	10.10	11.44	12.33	12.66	12.46	12.00	11.36	10.07	9.67	9.77	10.12	10.82	12.43	12.67	12.12	11.23	9.06	7.77	7.46	7.46	232 17	
208	9.06	10.48	11.57	12.72	13.42	13.56	13.18	12.30	11.45	10.72	10.26	9.92	10.00	10.71	11.62	12.18	11.42	10.36	9.08	8.15	7.53	7.24	7.70	9.82	233 17	
209	11.43	12.72	13.64	13.66	13.26	12.36	10.18	9.34	8.82	9.36	8.84	10.00	11.16	12.50	13.30	13.42	12.06	10.16	8.40	6.80	6.06	6.14	7.20	8.95	234 22	
210	14.40	14.54	13.58	12.17	10.70	9.34	8.82	9.36	8.84	10.00	11.16	12.50	13.30	13.42	12.06	10.16	8.40	6.80	6.06	6.14	7.20	8.95	10.80	12.76	13.96	236 1
211	14.81	11.84	9.97	8.77	8.36	8.48	8.96	10.06	11.56	13.64	12.06	6.24	5.17	5.36	6.54	8.54	10.66	13.00	15.02	15.06	14.08	11.60	8.97	7.34	237 4	
212	13.64	8.64	7.31	7.76	8.84	10.72	12.64	14.21	14.62	13.44	11.00	6.24	4.97	7.38	9.36	11.94	14.36	16.04	16.27	15.32	13.08	10.11	6.36	6.10	6.94	238 7
213	10.57	7.40	7.80	11.70	13.76	14.95	14.67	12.76	10.00	7.37	5.56	5.74	7.38	9.36	11.94	14.36	16.04	16.27	15.32	13.08	10.11	6.36	6.10	6.94	239 10	
214	8.63	10.83	13.20	15.21	14.43	11.89	8.54	6.26	4.97	5.06	6.36	8.22	13.40	15.80	16.62	16.16	14.21	11.38	8.34	6.35	5.74	7.13	9.22	11.84	240 13	
215	14.56	15.71	15.48	13.64	10.66	7.60	4.96	5.70	7.24	9.54	12.02	14.56	16.24	16.36	12.80	9.60	7.06	5.50	5.18	5.94	7.72	13.02	15.14	15.90	241 16	
216	14.88	12.32	9.63	7.07	5.74	5.64	8.36	6.67	10.62	13.17	15.30	16.38	15.97	14.05	11.34	8.16	5.05	5.41	6.72	8.83	11.26	13.77	15.36	14.00	11.50	242 19
217	8.72	6.86	5.97	6.34	7.52	9.30	11.47	13.80	15.84	14.77	12.44	9.37	7.06	5.37	4.85	5.64	9.24	11.64	13.96	15.06	14.75	13.17	10.76	8.64	243 21	
218	6.86	7.44	8.64	10.38	12.36	14.06	15.24	15.10	13.64	8.61	6.50	5.32	5.38	6.34	7.85	9.86	11.96	14.58	14.07	12.68	10.68	8.97	8.02	7.81	243 21	
219	8.36	9.26	12.24	13.73	14.44	13.86	12.25	10.02	8.06	6.46	5.78	6.47	7.80	9.63	11.38	12.97	13.74	13.44	11.04	9.83	8.84	8.57	8.81	9.67	245 0	
220	10.67	11.96	13.06	13.06	11.68	9.86	8.26	6.87	6.17	6.26	7.02	9.66	11.26	12.55	13.37	13.57	12.94	11.92	10.73	9.16	9.18	10.54	11.48	12.84	246 3	
221	12.46	12.92	12.66	10.42	8.87	7.44	6.44	6.21	6.66	7.76	9.20	10.76	13.54	14.95	13.67	12.68	11.26	10.02	9.22	8.90	9.14	10.86	12.02	12.84	247 6	
222	12.98	12.36	11.16	9.57	7.60	6.24	5.63	5.97	7.17	8.80	10.66	12.80	14.74	14.96	13.66	11.85	10.04	8.66	8.02	8.14	9.04	10.38	11.74	13.40	248 9	
223	12.04	10.04	7.64	5.76	4.78	6.24	5.02	8.16	10.78	13.20	15.04	15.98	15.74	14.33	11.96	9.30	7.37	6.55	6.70	8.06	9.98	12.06	13.93	14.44	10.18	249 12
224	7.37	5.17	3.90	4.03	5.50	7.96	10.88	13.80	16.04	17.04	16.46	14.44	11.04	8.24	6.27	5.15	7.24	9.64	12.52	14.74	15.98	15.46	13.29	9.94	6.63	250 15
225	3.17	2.53	5.38	8.20	11.40	14.56	16.82	17.44	13.93	9.98	6.70	4.46	3.84	4.58	6.80	10.06	15.76	16.64	15.75	12.94	9.26	6.06	3.66	2.67	251 17	
226	3.72	8.70	13.20	15.53	17.33	17.53	15.87	12.42	5.32	3.44	3.17	4.55	7.26	10.37	14.22	16.50	17.05	15.47	8.44	5.52	3.48	3.10	4.46	6.74	252 20	
227	9.94	13.47	17.47	17.02	14.77	10.84	7.23	4.52	3.00	3.06	8.06	11.72	14.94	16.86	16.90	14.94	11.54	8.00	5.98	4.20	5.52	7.95	11.06	14.30	253 23	
228	16.51	17.04	15.88	9.17	5.97	3.70	2.94	3.94	6.16	9.14	12.45	16.68	16.10	13.81	10.56	7.46	5.47	4.87	5.60	7.04	12.25	14.81	16.16	16.06	255 2	
229	14.44	11.07	7.87	5.34	3.02	5.16	7.43	10.36	13.44	15.47	16.04	14.92	12.66	7.74	6.47	6.36	7.02	8.54	10.58	12.80	14.58	14.73	12.52	9.86	256 5	
230	7.17	5.31	4.44	5.02	8.50	11.04	13.56	14.79	14.77	13.46	11.46	9.44	8.08	7.56	8.36	9.51	11.10	12.60	13.73	13.94	12.90	11.02	6.90	5.70	257 8	
231	5.63	6.34	7.60	9.36	11.36	13.88	15.63	16.24	13.88	10.94	8.76	8.44	8.70	9.48	10.86	12.06	12.76	12.76	12.71	11.64	9.87	8.46	7.04	6.67	7.34	258 11

231	8.36	9.74	11.16	12.22	12.70	12.20	11.38	10.60	9.34	9.13	9.34	9.16	9.13	9.34	9.87	10.66	11.30	11.63	10.56	9.48	8.44	7.52	7.14	7.33	7.86	8.66	8.66	289 14
232	10.90	11.62	11.97	11.87	11.54	11.08	10.42	9.22	9.66	9.54	9.86	10.24	10.70	10.91	10.91	10.80	10.34	9.66	9.74	8.35	7.72	7.46	7.67	8.44	9.64	10.73	10.73	290 16
233	11.52	12.06	11.88	11.53	10.97	10.23	9.48	9.04	9.38	9.38	10.64	11.05	11.18	10.94	10.46	9.52	8.56	7.74	7.42	7.42	7.04	8.34	9.42	10.67	11.65	12.46	12.46	291 19
234	12.82	12.04	10.90	9.85	8.96	8.54	8.42	8.86	10.44	11.23	11.67	11.60	10.92	9.74	8.36	7.26	6.68	7.74	7.42	7.42	7.04	10.86	12.34	13.24	13.55	13.17	13.17	292 22
235	12.08	10.61	9.21	8.06	7.74	8.74	9.92	11.30	12.38	12.82	12.42	11.17	7.86	6.53	6.10	6.54	7.88	9.68	11.56	13.16	14.06	13.18	11.60	11.60	9.86	9.86	284 1	
236	8.07	6.97	6.64	7.14	8.38	11.92	13.16	13.44	12.50	10.70	8.70	6.90	5.75	6.36	8.04	10.20	12.32	13.87	14.64	14.36	13.87	8.45	6.71	6.71	5.90	5.90	285 4	
237	6.17	7.29	9.02	11.07	13.02	14.14	12.68	10.30	7.96	6.07	5.14	5.48	6.87	9.06	13.68	15.18	15.37	14.28	12.24	9.67	7.34	5.74	6.12	6.12	7.84	7.84	286 7	
238	9.97	12.34	14.50	15.33	14.46	12.23	9.34	5.36	4.94	5.94	8.06	10.08	12.62	14.76	15.76	13.46	10.67	7.88	5.74	4.48	4.66	6.00	8.44	8.44	11.24	11.24	287 10	
239	15.67	15.66	14.20	11.46	8.47	6.20	4.97	6.65	8.86	11.54	14.06	15.76	16.97	14.86	12.14	9.06	4.56	3.93	4.93	6.93	9.67	12.77	15.34	15.34	16.35	16.35	288 12	
240	15.80	10.52	7.73	5.58	4.88	5.77	7.56	10.04	12.74	15.94	15.62	13.71	10.64	7.47	5.10	3.54	3.83	7.97	11.14	14.16	16.01	16.37	15.04	15.04	12.33	12.33	289 15	
241	9.34	6.07	5.42	6.51	8.50	11.14	13.77	15.60	15.98	12.14	8.87	6.16	4.30	3.67	4.60	6.44	9.03	12.27	14.84	15.96	14.09	11.42	8.56	8.56	6.75	6.75	270 18	
242	5.80	6.17	7.42	12.22	14.26	15.46	15.24	13.48	10.57	7.65	5.42	4.06	5.34	7.30	9.97	12.69	14.83	15.87	15.16	13.24	8.47	7.04	6.68	7.20	7.20	271 21		
243	8.44	10.38	12.56	14.83	14.95	12.07	9.24	7.02	5.32	4.44	4.61	5.87	10.37	13.07	14.81	15.06	14.13	12.37	10.44	8.86	7.56	7.92	8.94	10.67	10.67	273 0		
244	12.44	13.74	13.97	12.81	10.83	7.10	5.78	5.25	5.76	6.66	8.34	10.76	12.86	14.16	14.44	13.68	12.40	10.86	9.52	8.53	8.21	8.56	9.40	12.08	13.04	13.04	274 3	
245	13.08	11.93	10.54	9.05	7.64	6.06	6.30	7.07	8.81	10.63	12.30	13.68	14.16	13.66	11.46	9.74	7.60	7.94	9.26	10.84	12.04	12.52	12.48	11.98	11.98	276 6		
246	11.16	9.92	8.44	7.14	6.37	6.38	7.34	10.57	12.10	13.44	13.92	13.88	13.56	12.37	11.18	9.74	7.60	7.94	9.26	10.84	12.04	12.52	12.48	11.16	11.16	11.16	277 9	
247	9.77	7.94	6.58	6.06	6.50	7.97	9.84	13.26	15.99	13.97	14.52	13.27	11.34	9.06	7.37	6.82	7.46	10.60	12.11	13.20	14.04	13.84	12.76	10.92	10.92	277 11		
248	8.58	6.74	6.30	7.68	9.72	11.97	13.90	15.26	15.99	13.97	11.26	8.63	6.70	5.98	6.37	7.97	10.25	14.44	16.30	15.04	13.48	11.07	8.36	6.38	6.38	278 14		
249	5.47	7.36	9.62	12.14	14.54	16.28	16.98	16.37	13.80	10.49	7.50	5.14	5.74	7.77	10.54	13.45	15.71	16.85	14.16	10.70	7.77	5.85	5.07	5.66	5.66	279 17		
250	7.50	9.87	12.74	16.92	17.15	15.62	12.54	8.66	5.94	4.14	3.96	5.28	11.15	14.38	16.70	17.32	16.33	13.48	9.84	5.47	7.82	4.98	5.96	7.74	10.58	10.58	280 20	
251	13.66	16.26	17.30	14.56	10.89	7.40	4.72	3.37	3.98	5.86	8.86	12.43	17.34	17.64	16.26	12.76	9.26	6.56	5.24	5.38	8.77	11.76	14.62	16.82	16.82	281 23		
252	17.12	15.72	12.71	9.14	6.06	3.77	4.42	6.67	9.72	13.44	16.25	17.55	17.22	15.06	8.40	6.26	5.44	6.06	7.47	10.01	12.74	15.12	16.06	14.21	14.21	283 2		
253	11.04	7.42	4.80	3.12	3.62	5.50	11.13	14.40	16.50	17.22	16.16	13.58	10.36	7.77	6.24	6.91	8.53	10.52	13.06	15.02	15.64	14.36	11.93	6.01	6.01	284 5		
254	4.31	3.47	4.52	6.20	8.94	11.94	14.56	16.32	14.74	12.13	9.47	7.47	6.58	6.90	7.84	9.30	13.26	14.41	14.26	12.74	10.35	7.88	5.80	4.44	4.44	285 8		
255	5.92	7.85	10.30	12.70	14.67	15.54	15.01	13.36	9.11	7.80	7.42	7.74	8.64	10.04	11.80	13.04	13.06	11.36	9.07	7.14	5.84	5.47	6.20	7.44	7.44	286 10		
256	9.04	10.97	14.36	14.36	13.40	11.82	10.44	9.16	8.44	8.24	9.26	10.30	11.46	12.12	12.22	11.46	10.00	8.37	6.36	6.44	7.32	8.34	9.60	11.24	11.24	287 13		
257	12.72	13.46	13.28	12.32	11.06	10.10	9.27	8.97	8.94	9.08	9.61	10.14	11.52	11.46	10.73	9.52	8.47	7.66	7.41	8.04	8.76	9.91	11.17	12.30	12.30	288 16		
258	12.66	11.92	11.04	10.37	9.36	9.12	9.08	9.27	9.86	10.44	10.68	10.30	9.78	9.22	8.56	8.06	7.74	8.02	8.86	10.06	11.06	12.40	12.34	12.06	12.06	289 19		
259	11.48	10.82	9.97	9.24	8.77	8.96	8.77	8.96	9.55	10.22	10.88	10.82	10.57	9.26	8.44	7.90	8.07	8.80	9.84	10.90	11.78	12.36	12.07	11.12	11.12	290 22		
260	9.97	8.90	8.23	8.12	8.56	10.10	10.90	11.50	11.78	11.53	10.67	9.30	8.14	7.77	8.55	9.74	11.07	12.15	12.94	13.28	13.04	12.24	10.71	7.88	7.88	293 1		
261	7.18	7.36	8.12	9.26	10.62	11.94	12.78	12.06	10.48	8.86	7.70	7.28	7.65	8.65	11.54	12.81	13.77	14.04	13.50	12.16	10.00	8.34	6.96	6.50	6.50	293 4		
262	7.96	9.76	11.52	13.07	13.96	13.77	12.48	10.52	7.36	6.77	7.26	8.52	10.36	12.17	13.66	14.56	14.48	11.12	8.84	6.87	5.64	5.46	6.30	8.06	8.06	294 6		
263	10.30	14.34	15.00	14.16	12.26	9.96	7.92	6.50	6.22	8.82	10.86	13.12	14.54	15.07	14.56	12.60	9.98	7.47	4.56	4.96	6.60	9.03	11.80	14.15	14.15	295 9		
264	15.84	15.96	14.52	12.00	9.24	7.24	6.16	6.40	7.67	9.66	11.93	15.62	14.36	11.76	8.61	6.02	4.24	3.86	5.14	7.32	10.15	13.10	15.67	16.78	16.78	296 12		
Sum	750.39773	1758.51768	46732.67	767.55771	90785.69	755.65758	63752.33	740.08	780.04	756.52	779.19	758.40	775.27	752.88	772.08	740.38	731.69	746.32	748.12	No. of Days								
No.	73	75	73	74	72	75	74	75	74	74	74	73	74	73	75	73	75	73	75	73	75	74	75	73	75	75	18241.70	

FORMS FOR SHORT-PERIOD TIDES.  
SERIES Q.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
265	14.16	11.00	8.32	5.84	3.47	1.16	10.16	12.84	15.02	16.10	15.46	13.28	6.84	4.45	3.04	3.57	5.44	8.15	11.37	14.00	17.35	16.28	13.64	10.44	297 15	
266	7.71	6.07	5.84	6.88	11.47	14.13	15.94	16.22	14.81	11.87	8.55	5.46	3.46	4.17	6.35	9.32	13.00	15.95	17.47	17.44	15.72	9.66	7.28	5.94	298 18	
267	6.04	7.36	9.64	12.45	14.84	15.60	13.70	10.52	7.15	4.66	2.92	3.10	11.05	14.10	16.17	16.12	14.06	11.35	8.82	7.14	6.57	7.02	10.56	13.14	301 0	
268	9.92	12.68	14.78	15.58	14.78	12.36	6.36	4.20	3.07	3.72	5.55	8.04	11.05	14.10	16.22	15.16	10.86	7.58	7.14	7.44	8.84	10.92	12.84	13.86	302 3	
269	14.04	15.04	13.76	11.47	8.74	6.42	4.70	5.00	6.80	9.02	11.88	14.60	16.14	16.22	15.16	10.86	8.86	7.58	7.14	7.44	8.84	10.92	12.84	13.86	303 5	
270	12.37	10.68	8.54	6.84	5.56	5.27	5.98	7.33	9.36	14.00	15.22	15.38	14.58	12.98	11.01	9.42	7.64	7.92	8.94	10.40	11.85	12.91	13.12	12.26	304 8	
271	9.22	7.66	6.68	6.30	6.72	7.80	9.44	11.50	13.34	14.66	13.96	12.74	11.30	9.76	8.54	7.92	7.84	9.60	10.88	12.06	12.64	12.40	11.47	10.10	304 8	
272	8.76	7.68	7.06	7.90	9.22	10.97	12.56	13.72	14.38	14.04	13.04	9.76	8.15	7.22	7.02	7.48	8.84	10.32	11.48	12.87	12.46	11.36	9.70	8.28	305 11	
273	7.14	6.80	7.40	8.74	10.74	12.56	14.54	14.38	13.40	11.67	9.60	7.53	5.88	6.50	8.20	10.07	11.93	13.36	14.04	13.66	10.26	8.61	7.37	6.86	306 14	
274	7.24	8.35	10.36	12.50	14.13	14.96	13.80	11.64	9.03	6.96	5.44	5.04	5.86	10.12	12.66	14.54	15.37	14.86	13.04	10.66	8.56	6.44	6.77	8.02	307 17	
275	10.14	12.62	14.56	15.55	15.35	13.56	8.12	5.82	4.22	4.10	5.32	7.70	10.85	13.60	16.05	15.06	12.86	10.40	8.16	6.53	5.96	6.51	8.24	13.27	308 20	
276	15.16	15.84	15.01	12.98	9.78	7.04	4.71	3.86	5.60	8.44	11.74	14.64	16.50	16.72	12.86	9.98	7.70	7.46	9.60	12.20	14.35	15.67	15.28	13.15	311 1	
277	14.55	11.68	8.46	5.64	3.63	3.01	4.08	6.50	13.08	15.81	17.12	16.72	14.87	12.03	9.20	7.26	6.37	7.46	9.60	12.20	14.35	15.67	15.28	13.15	311 1	
278	10.15	4.47	3.03	3.22	5.03	7.60	10.76	14.05	16.38	16.14	13.92	11.10	8.66	6.73	5.00	6.16	6.46	10.44	14.36	15.16	13.92	11.40	8.36	5.66	312 4	
279	3.69	2.94	6.18	9.01	12.24	14.92	16.53	16.56	15.16	10.66	7.96	6.74	6.60	7.35	9.00	11.24	13.43	14.50	12.66	9.94	7.20	4.97	3.56	3.77	313 7	
280	5.34	7.72	13.46	15.64	16.34	15.71	13.92	11.46	9.28	7.66	6.98	7.98	9.96	12.00	13.52	14.02	13.37	11.18	8.81	6.52	4.33	5.20	6.90	9.14	314 10	
281	11.80	14.20	15.72	14.66	12.72	10.71	8.96	7.82	7.56	7.92	9.16	12.24	13.26	13.26	12.06	10.17	8.00	6.25	5.31	5.50	8.34	10.52	12.80	14.44	315 13	
282	15.18	14.68	13.32	11.56	8.76	8.68	10.00	10.94	11.57	11.80	11.36	10.28	8.94	7.84	7.18	7.86	8.80	9.98	11.46	12.86	13.86	13.83	11.72	10.86	9.04	316 16
283	12.37	10.90	9.58	8.78	8.46	9.30	10.00	10.94	11.57	11.80	11.36	10.28	8.94	7.84	7.18	7.86	8.80	9.98	11.46	12.86	13.86	13.83	11.72	10.86	9.04	317 19
284	9.66	9.14	8.92	8.96	9.17	9.66	10.40	11.37	11.01	10.20	9.26	8.46	8.10	8.14	8.66	9.44	10.42	12.48	13.15	12.64	11.84	10.76	9.71	8.88	8.35	320 0
285	8.86	8.85	9.16	9.64	10.14	10.74	11.18	11.06	10.38	9.58	8.94	8.71	8.90	9.50	10.42	11.46	12.48	13.15	12.64	11.84	10.76	9.71	8.88	8.35	320 0	
286	8.42	9.04	9.96	10.86	11.50	11.80	11.55	10.96	9.98	8.64	8.75	9.38	10.38	11.46	12.41	13.07	13.16	11.84	10.56	9.24	8.13	7.50	7.43	7.86	321 3	
287	8.81	10.03	12.23	12.80	12.64	11.66	10.23	9.04	8.36	8.34	8.96	11.20	12.46	13.23	13.47	13.00	11.72	10.14	8.03	6.27	6.31	7.08	8.52	10.23	322 6	
288	11.92	13.17	13.10	11.86	10.18	8.76	7.98	7.96	8.75	10.13	11.64	13.14	13.94	13.04	11.34	9.30	7.45	5.86	5.13	5.46	8.80	11.15	13.20	14.66	323 9	
289	14.98	13.87	11.76	9.58	7.27	7.36	8.22	9.82	11.76	13.33	14.28	14.14	12.81	10.56	5.77	4.14	3.74	4.67	6.71	9.27	14.40	15.66	15.44	13.71	324 12	
290	11.16	8.74	7.02	6.40	6.78	8.22	12.25	13.88	14.74	14.20	12.26	9.36	6.51	4.12	2.94	4.56	7.03	10.05	13.27	15.65	16.62	15.76	10.86	8.17	325 15	
291	6.45	5.84	6.36	8.12	10.44	12.84	14.46	13.97	11.41	8.07	4.96	2.57	1.63	2.58	4.74	11.12	14.22	16.47	17.07	15.75	12.96	9.86	7.26	5.46	326 18	
292	6.44	8.40	11.20	13.57	15.11	15.17	13.27	9.96	3.62	1.76	1.54	3.26	6.02	9.25	12.97	15.66	17.25	15.37	12.23	9.00	6.75	5.63	6.88	8.88	327 21	
293	13.22	14.44	15.50	14.80	12.31	8.84	5.46	3.00	1.66	4.15	6.95	10.46	13.81	16.44	17.54	16.82	10.68	8.07	6.16	5.88	7.64	10.25	12.77	14.29	328 23	
294	14.07	15.36	14.06	11.32	8.05	5.16	2.94	2.16	3.11	5.16	14.30	16.57	17.22	16.33	13.81	10.68	8.07	6.16	5.88	7.64	10.25	12.77	14.29	14.72	330 2	
295	13.33	10.74	7.81	3.66	3.26	4.42	6.34	8.86	11.67	14.58	16.33	15.28	12.84	9.03	7.47	6.23	5.72	6.36	7.04	12.38	13.76	13.96	12.68	10.56	331 5	
296	8.18	6.28	4.97	5.23	4.83	7.34	9.38	12.05	14.37	15.76	15.56	12.28	8.13	6.64	6.14	6.54	8.04	10.04	11.78	12.86	13.24	10.14	8.96	7.50	333 8	
297	6.24	5.96	6.50	7.80	12.15	14.87	14.87	13.77	10.66	6.86	6.34	8.23	6.86	6.56	7.70	9.30	10.84	12.16	12.76	12.53	11.48	8.60	7.52	7.06	333 11	

298	7.44	8.47	10.17	11.91	13.34	14.231	13.72	12.30	10.42	8.41	6.88	6.14	6.37	7.32	10.45	11.84	12.86	13.08	12.42	11.25	9.75	8.54	7.83	8.64	334 14	
299	10.02	11.65	13.16	14.14	14.30	13.64	12.17	8.37	6.68	5.72	5.86	6.88	8.04	10.12	13.07	13.88	13.62	12.36	10.67	9.06	8.12	7.90	7.88	9.72	335 17	
300	12.78	13.82	14.20	13.74	12.14	10.05	7.76	6.00	5.23	6.52	8.50	10.56	12.60	14.12	14.40	13.86	12.58	8.97	7.94	7.68	8.24	9.50	11.14	12.75	336 19	
301	13.98	13.73	11.85	9.10	6.84	5.06	4.41	5.04	6.57	11.20	13.52	15.24	15.84	15.08	13.13	10.86	9.00	7.54	8.05	9.36	11.14	12.94	14.20	14.46	337 22	
302	13.36	8.58	11.28	5.98	4.22	3.96	6.97	9.54	12.26	14.54	16.34	15.20	12.88	10.26	8.38	7.53	7.40	8.14	11.52	13.36	14.60	14.56	12.94	10.26	339 1	
303	7.33	5.11	4.95	9.06	7.81	10.61	13.20	15.47	16.54	16.21	14.70	12.10	8.08	7.33	7.37	8.31	10.05	12.02	13.86	14.76	12.16	8.93	6.32	4.31	340 4	
304	3.72	4.64	6.56	11.87	16.56	16.48	11.44	8.26	7.37	8.98	9.81	7.71	7.70	9.02	10.97	12.94	14.40	14.70	13.41	10.64	7.77	4.16	4.16	5.63	341 7	
305	7.85	10.36	13.16	15.34	16.48	11.44	7.80	7.24	7.44	8.72	10.57	12.55	14.00	14.24	10.72	8.06	5.93	4.58	4.74	6.03	8.20	10.34	12.88	16.23	343 13	
306	14.97	15.87	16.56	15.80	13.96	9.32	11.44	9.32	7.44	8.72	10.57	12.55	14.00	14.24	10.72	8.06	5.93	4.58	4.74	6.03	8.20	10.34	12.88	16.23	343 13	
307	16.28	14.89	12.63	10.30	8.54	7.57	7.44	9.64	12.26	14.54	16.34	15.20	12.88	10.26	8.38	7.53	7.40	8.14	11.52	13.36	14.60	14.56	12.94	10.26	344 16	
308	11.42	9.46	7.98	7.36	7.62	8.50	10.02	11.60	12.67	12.14	10.36	8.34	6.54	5.59	5.67	6.77	10.57	12.55	14.00	14.24	10.72	8.06	6.32	4.31	340 4	
309	8.66	7.38	7.80	8.82	10.22	11.48	12.26	12.24	11.15	9.47	6.87	6.45	6.75	7.83	9.14	10.75	12.56	14.46	14.46	12.87	11.31	9.72	8.40	7.76	346 21	
310	7.73	8.27	10.54	11.48	12.02	11.81	10.84	9.56	8.46	7.76	7.56	8.00	9.17	7.18	4.90	4.92	6.07	7.94	10.07	12.03	13.66	14.48	14.16	10.77	352 12	
311	9.62	10.53	11.27	11.70	11.14	10.38	9.49	8.78	8.48	8.71	9.47	10.70	13.16	13.78	13.79	13.14	11.94	10.54	9.17	8.30	8.04	8.58	9.36	10.22	349 3	
312	11.00	11.54	11.74	11.57	10.96	9.44	9.04	9.10	9.74	10.90	12.24	13.16	13.57	12.64	11.55	10.26	8.86	7.83	7.22	7.36	7.86	10.11	11.13	11.95	350 6	
313	12.42	12.30	11.78	10.77	9.72	9.06	9.55	10.76	11.97	13.94	13.38	13.14	12.44	9.78	8.75	8.20	6.15	6.82	8.20	9.07	11.56	12.90	13.36	13.50	351 9	
314	12.36	10.92	9.68	8.84	8.68	9.14	11.57	12.76	13.30	13.22	12.46	11.00	9.17	7.18	4.90	4.92	6.07	7.94	10.07	12.03	13.66	14.48	14.16	10.77	352 12	
315	9.04	7.98	7.73	8.23	9.70	11.40	12.74	13.45	10.50	5.17	3.42	2.93	4.16	6.37	9.00	12.12	16.74	16.96	15.68	13.11	10.34	8.06	6.98	7.04	354 17	
316	7.50	8.16	9.80	11.80	13.38	14.33	14.26	13.00	7.72	7.50	8.50	6.30	4.47	4.16	6.37	9.00	12.12	16.74	16.96	15.68	13.11	10.34	8.06	6.98	7.04	354 17
317	8.06	12.15	14.04	15.14	15.03	13.10	10.20	7.00	4.27	2.20	7.06	14.30	17.04	18.34	17.72	15.47	12.00	8.88	6.38	5.67	7.30	10.14	13.10	15.24	356 23	
318	12.72	14.77	15.20	12.64	9.26	5.91	3.10	1.55	1.93	4.00	10.68	17.66	17.37	14.51	10.92	7.77	5.66	5.14	5.64	7.65	13.44	10.63	15.46	15.86	14.14	358 2
319	16.17	14.94	12.16	8.55	2.64	1.50	2.57	5.14	8.44	11.93	15.00	18.34	17.37	14.51	10.92	7.77	5.66	5.14	5.64	7.65	13.44	10.63	15.46	15.86	14.14	358 2
320	10.98	7.68	4.48	2.36	3.30	1.77	5.83	8.90	12.30	15.56	17.50	17.88	13.58	6.94	5.14	4.70	5.34	7.63	10.73	13.70	15.36	13.24	9.92	6.64	359 5	
321	4.73	3.07	3.08	4.74	6.97	13.01	15.80	17.38	17.48	15.95	12.86	9.53	6.72	5.22	4.90	8.03	10.96	13.30	14.68	14.83	13.24	10.55	5.43	6.14	361 11	
322	4.63	5.97	8.02	10.57	13.25	15.58	16.60	14.11	11.13	8.76	6.38	5.17	5.13	6.30	8.60	10.76	13.74	13.62	12.37	10.30	8.14	6.53	5.84	7.14	361 11	
323	8.74	10.77	13.13	14.96	15.71	15.12	13.32	8.44	6.78	5.82	5.27	6.00	7.78	9.85	11.62	12.84	13.10	10.74	9.22	7.96	7.33	7.28	7.93	9.16	362 13	
324	10.97	14.54	14.68	13.66	12.28	10.12	8.24	6.78	5.82	5.70	7.72	9.40	11.06	12.32	12.86	12.50	11.47	9.12	8.42	8.24	8.54	9.54	11.12	12.64	363 16	
325	13.57	13.88	11.44	9.87	8.24	6.74	5.77	5.52	6.12	7.27	10.64	12.10	13.01	13.12	12.46	11.26	10.02	9.06	8.58	9.44	10.68	11.96	12.92	13.14	364 19	
326	12.66	11.54	10.06	6.86	5.72	5.37	5.87	7.17	9.14	11.00	12.70	13.68	12.94	11.57	10.28	9.14	8.62	8.63	9.20	10.44	12.53	12.92	12.58	11.64	365 22	
327	9.77	7.86	6.12	5.05	5.62	7.06	9.15	11.26	13.23	14.30	14.32	13.36	11.78	9.17	8.44	8.24	8.62	9.76	11.04	12.36	13.08	11.65	9.64	7.34	367 1	
328	5.52	4.45	4.52	5.76	7.66	12.43	14.27	15.18	14.97	13.73	11.82	10.16	8.86	8.26	8.06	10.32	11.70	12.96	13.58	13.16	11.26	6.66	4.96	4.33	368 4	
329	4.86	6.36	8.55	11.00	13.44	15.21	15.84	13.56	11.44	9.66	8.38	7.80	7.97	9.00	10.56	13.46	13.82	12.72	10.52	7.90	5.74	4.34	4.11	7.23	369 7	
330	9.78	12.44	14.65	15.93	15.94	14.74	12.37	8.53	7.14	7.47	9.38	10.23	11.36	13.14	14.17	14.00	9.43	6.77	4.83	3.98	4.52	6.17	8.54	11.10	370 10	
331	15.49	16.36	15.78	13.85	11.34	9.14	7.57	7.01	8.33	10.10	12.14	13.77	14.42	13.51	11.13	8.22	5.94	...	...	...	...	...	...	...	371 4	
Sum	750.90	757.95	743.99	755.91	761.36	782.39	766.39	756.46	743.89	757.48	757.41	707.17	756.01	759.53	781.47	777.74	790.50	749.28	770.69	763.27	776.03	744.37	749.23	770.16	No. of Days 74 1/2	
No.	74	75	74	76	74	74	74	74	75	74	74	76	75	75	76	75	75	72	74	74	75	73	75	75	75	

FORMS FOR SHORT-PERIOD TIDES.  
BOMBAY—Commencing 0 hours, Astronomical Time, 1st January, 1885.

SERIES L. Motion per mean Solar hour =  $14^{\circ}76'42.994''$ .

Argument  $(\gamma - \frac{1}{2}\sigma - \frac{1}{2}\omega)$ .

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
1	15.32	12.96	9.13	5.76	3.03	1.68	2.28	4.80	7.00	11.70	15.50	18.00	18.85	18.08	15.14	11.54	8.50	6.21	5.53	6.08	6.08	8.20	11.31	14.16	16.06	1 23
2	16.66	15.40	12.16	8.40	4.86	2.56	1.71	2.90	8.82	12.94	16.44	18.48	18.97	17.67	14.24	10.56	7.53	5.57	5.16	6.10	6.10	8.65	11.84	14.68	16.53	3 0
3	16.96	15.24	11.92	8.00	4.87	2.80	2.57	4.24	6.84	10.20	14.07	17.26	18.86	18.84	17.06	13.20	9.77	6.90	5.23	4.96	4.96	6.16	8.86	12.14	14.87	4 0
4	16.40	16.40	14.28	11.00	7.63	4.88	3.55	3.86	5.55	8.01	11.36	14.83	17.16	18.58	17.93	15.80	12.16	8.68	6.10	5.05	5.05	5.25	6.68	12.28	14.51	5 1
5	15.96	15.88	13.48	10.47	7.54	5.76	5.07	5.67	7.22	9.17	12.11	15.02	17.02	17.32	16.63	14.11	10.96	8.16	6.22	5.47	5.47	5.84	7.18	9.67	12.12	6 1
6	14.04	15.00	14.45	12.62	10.24	8.07	7.04	6.84	7.54	8.67	10.60	12.84	15.06	16.36	16.35	15.24	12.76	10.11	8.00	6.64	6.64	6.17	6.55	7.86	9.76	7 1
7	11.80	13.27	14.00	13.64	12.22	10.47	9.05	8.44	8.46	9.03	9.97	11.20	13.05	15.46	15.18	13.87	11.68	9.76	8.10	7.16	7.16	7.03	7.40	8.29	9.82	8 2
8	11.16	12.55	13.24	13.07	12.20	11.16	10.27	9.64	9.60	9.90	10.60	11.70	12.96	14.02	14.44	13.75	12.27	10.82	9.20	7.93	7.93	7.24	7.06	7.34	8.07	9 2
9	9.14	10.55	11.74	12.48	12.66	12.27	11.60	10.93	10.34	9.98	9.86	10.17	11.07	12.14	13.06	13.36	12.72	11.71	10.43	9.14	9.14	7.97	7.14	6.75	6.94	10 2
10	7.74	8.96	10.26	11.64	13.14	12.97	12.20	11.24	10.48	10.12	10.05	10.23	10.84	11.64	12.27	12.68	12.37	11.33	10.42	8.97	8.97	7.80	6.96	6.38	6.44	11 3
11	7.28	8.73	10.47	12.14	13.23	13.84	13.63	13.94	12.72	11.24	10.02	9.62	9.89	10.44	11.24	11.97	12.52	12.50	11.87	10.54	10.54	8.76	7.34	6.16	5.74	12 3
12	6.34	7.62	9.54	11.46	13.22	14.24	14.58	13.94	12.72	11.24	10.02	9.32	9.14	9.46	10.37	11.48	12.46	13.04	11.88	10.23	10.23	8.20	6.52	5.62	5.66	13 4
13	6.50	8.14	10.17	12.34	14.10	15.20	15.17	13.97	12.27	10.58	9.35	8.75	8.76	9.26	10.34	11.68	12.96	13.64	13.36	11.80	11.80	9.66	7.32	5.82	5.14	14 4
14	5.44	6.74	8.86	11.26	13.66	15.38	15.87	15.24	13.66	11.54	9.82	8.71	8.16	8.36	9.30	10.74	12.46	13.64	13.98	13.00	13.00	10.84	8.24	6.20	4.76	15 4
15	4.46	5.40	7.36	9.78	12.57	14.82	16.13	15.97	14.56	10.05	8.46	7.82	7.74	8.41	9.71	11.76	13.30	14.26	14.09	12.44	12.44	9.76	7.00	5.12	4.20	16 5
16	4.63	6.12	8.44	11.24	14.04	15.74	16.36	15.71	13.82	11.22	8.94	7.54	6.94	7.15	8.40	10.27	12.44	14.06	14.68	13.84	13.84	11.50	8.60	5.94	4.37	17 5
17	4.02	5.06	7.26	9.66	12.72	15.20	16.55	16.63	15.27	12.77	9.97	7.86	6.84	6.68	7.56	9.32	11.40	13.32	14.42	14.25	14.25	12.47	10.10	7.91	6.34	18 6
18	4.66	6.35	8.54	11.38	14.15	16.15	16.88	16.08	14.04	11.02	8.54	6.76	6.12	6.34	7.60	9.84	12.14	14.06	14.84	14.14	14.14	12.06	9.06	6.46	4.67	19 6
19	4.24	5.16	7.15	9.68	12.56	14.87	16.44	16.45	15.00	12.42	9.50	7.22	5.86	5.43	6.26	8.16	10.65	12.88	14.28	14.50	14.50	13.33	10.92	8.30	6.04	20 6
20	4.87	5.66	6.54	8.66	11.04	13.64	15.62	16.36	15.76	13.82	11.00	8.37	6.37	5.64	6.83	8.93	11.40	13.32	14.42	14.25	14.25	12.47	10.10	7.91	6.34	21 7
21	5.70	6.30	7.70	9.76	12.17	14.36	15.74	15.96	14.86	12.76	10.13	7.78	6.17	5.70	6.11	7.62	9.70	11.76	13.36	14.14	14.14	13.72	12.06	9.94	8.32	22 7
22	7.22	7.01	7.74	8.97	10.80	12.97	14.62	15.50	15.17	13.80	11.46	9.14	7.34	6.17	6.00	6.68	8.02	9.76	11.65	13.04	13.04	13.76	13.34	12.14	10.65	23 7
23	9.07	8.15	8.14	8.68	9.86	13.36	14.56	15.02	14.37	12.76	10.76	8.71	6.96	6.23	6.09	6.68	7.86	9.46	11.24	12.66	12.66	13.36	13.34	12.14	10.65	24 8
24	9.94	9.11	8.88	9.28	10.22	11.70	13.06	14.14	14.41	13.60	12.06	10.26	8.46	7.10	6.25	6.08	6.56	7.64	9.14	10.84	10.84	12.34	13.44	13.38	11.08	25 8
25	12.18	10.75	9.76	9.24	9.34	10.07	11.16	12.40	13.38	13.66	13.03	11.87	10.24	8.47	7.00	5.83	5.38	5.68	6.78	8.55	8.55	10.33	12.22	13.56	14.30	26 9
26	13.05	11.56	10.06	9.11	8.97	9.40	10.46	11.87	12.94	13.44	13.33	12.40	10.74	8.86	6.83	5.22	4.41	4.77	6.10	8.10	8.10	10.50	12.63	14.53	15.56	27 9
27	15.33	13.76	11.64	9.52	8.28	7.92	8.25	9.53	11.24	12.70	13.80	14.14	13.30	11.34	8.82	5.70	3.60	3.38	3.76	5.30	5.30	7.76	10.55	13.50	15.72	28 9
28	16.74	16.12	14.36	11.40	8.83	7.24	6.86	7.53	9.20	11.11	14.55	15.08	14.17	11.84	8.82	5.70	3.60	3.38	3.06	5.04	5.04	7.88	11.48	14.56	17.04	29 10
29	17.86	17.00	14.36	10.96	8.07	6.27	5.77	6.57	8.62	11.25	13.92	15.74	16.28	14.96	12.18	8.44	5.42	3.22	2.16	3.07	3.07	5.52	8.75	12.46	16.01	30 10
30	18.10	18.47	17.26	13.80	10.14	7.09	5.27	5.02	6.02	8.40	11.85	14.65	16.52	16.84	15.28	11.68	7.88	4.80	2.74	2.38	2.38	4.00	6.66	10.10	13.98	31 10
31	17.01	18.38	16.30	12.42	8.97	6.01	4.46	4.37	6.12	9.14	12.56	15.46	17.00	16.86	14.76	11.06	7.36	4.34	2.72	2.99	2.99	4.86	7.74	11.40	14.94	32 11
32	17.54	18.47	17.66	14.67	11.08	7.54	5.01	3.93	4.32	6.55	9.62	13.04	15.80	16.84	16.08	13.73	10.16	6.82	4.54	3.38	3.38	4.44	6.30	9.36	12.84	33 11
33	15.86	17.74	17.94	16.48	13.27	9.84	6.84	4.96	4.33	5.26	7.44	10.66	13.70	15.74	15.42	12.82	9.66	6.90	5.42	5.14	5.14	6.20	8.06	10.66	13.66	34 12
34	16.02	17.12	16.74	14.88	11.68	8.76	6.34	4.92	4.74	5.86	8.26	11.07	13.60	15.16	15.34	14.06	11.68	9.04	7.34	6.56	6.56	6.94	8.56	9.36	11.76	35 12
35	14.24	15.60	16.04	15.34	13.02	10.16	7.86	6.27	5.54	5.86	7.18	9.07	11.36	13.26	14.34	14.26	13.88	11.00	9.30	8.26	8.26	7.97	8.30	9.05	10.36	36 12

36	12-08	13-76	14-44	14-66	14-44	13-11	11-12	7-54	6-24	6-13	6-68	7-86	9-28	10-86	12-27	13-10	12-94	11-93	10-66	9-74	9-12	9-06	9-26	9-66	10-60	37 18
37	11-82	12-86	13-34	12-82	11-45	10-03	8-74	7-48	6-86	6-78	7-17	7-94	9-05	10-50	11-34	11-97	11-92	11-42	10-84	10-34	10-07	9-97	9-77	9-94	38 13	
38	10-44	11-32	12-06	12-26	11-78	10-88	9-87	8-84	7-86	7-24	6-94	7-18	8-03	9-07	10-14	11-00	11-56	11-85	11-77	11-46	10-57	10-07	9-70	9-70	39 14	
39	10-13	10-80	11-27	11-45	11-25	10-76	9-97	9-00	8-00	7-11	6-58	6-74	7-44	8-51	9-84	10-90	11-76	12-34	12-55	12-30	11-60	10-57	9-76	9-34	40 14	
40	9-17	9-56	10-24	10-94	11-36	11-44	10-97	10-10	9-07	7-87	6-85	6-30	6-50	7-26	8-50	10-16	11-44	12-65	13-26	13-32	12-56	11-36	10-08	9-16	41 14	
41	8-67	8-64	9-01	9-76	10-58	11-25	12-66	12-07	10-47	8-56	6-64	5-46	5-20	5-93	7-55	9-56	11-72	13-53	14-67	14-84	13-98	12-14	10-00	8-54	42 15	
42	7-84	8-12	8-96	10-24	11-52	12-40	13-62	13-60	12-30	10-24	7-77	5-88	4-84	4-90	6-86	9-20	11-97	14-34	15-83	15-96	14-78	12-26	9-64	7-46	43 15	
43	7-66	7-53	8-16	9-56	11-03	12-66	13-62	13-88	11-93	9-10	6-54	4-66	4-00	4-90	6-86	9-20	11-97	14-34	15-83	15-64	14-86	12-26	9-02	7-46	44 15	
44	7-54	7-00	8-13	9-87	11-85	13-60	14-38	14-38	13-63	10-90	7-86	5-57	4-97	4-04	5-46	7-84	10-63	13-64	15-83	16-64	16-01	13-87	10-90	8-00	45 16	
45	6-24	5-96	6-74	8-48	10-85	13-07	14-56	14-85	13-63	10-90	7-86	5-57	4-97	4-04	5-46	7-84	10-63	13-64	15-83	16-64	16-01	13-87	10-90	8-00	46 16	
46	6-17	5-46	5-74	7-26	9-70	12-25	14-42	15-50	15-15	13-08	9-90	6-94	4-75	3-92	4-66	6-62	8-27	10-66	13-07	14-85	15-23	13-64	11-13	9-02	47 17	
47	5-63	5-06	5-54	7-84	10-54	13-30	15-12	15-66	14-46	11-76	8-44	5-86	4-26	4-25	5-52	7-84	10-68	13-68	15-84	16-68	15-86	13-15	10-22	7-36	48 17	
48	5-65	4-23	4-46	6-07	8-56	11-57	14-06	15-54	15-51	13-57	10-53	7-47	5-38	4-52	5-94	6-70	9-14	12-18	14-74	16-26	16-26	14-64	11-74	8-68	49 17	
49	6-38	4-54	4-14	5-07	7-06	9-74	12-44	15-46	14-76	12-57	9-68	7-24	5-84	5-60	6-54	8-40	10-77	13-32	15-42	16-26	15-47	13-18	10-24	7-54	50 18	
50	5-62	4-54	4-69	5-80	7-87	10-40	12-86	14-50	15-06	14-03	11-86	9-36	7-58	6-64	6-76	7-86	9-60	11-66	13-73	15-08	15-32	14-12	11-86	9-24	51 18	
51	6-90	5-18	4-58	5-06	6-46	8-24	10-33	12-41	13-86	14-34	13-44	11-46	10-24	8-45	8-28	8-67	9-76	11-20	12-50	13-18	13-06	11-88	10-25	8-73	52 19	
52	6-87	5-45	4-92	5-44	6-63	8-23	10-14	11-77	12-96	13-40	12-76	11-56	10-24	8-45	8-28	8-67	9-76	11-20	12-50	13-18	13-06	11-88	10-25	8-73	53 19	
53	8-57	6-98	5-77	5-38	5-64	6-37	7-82	9-54	11-17	12-38	13-02	12-96	12-16	11-07	10-02	8-94	8-44	8-44	8-44	8-44	11-57	12-34	12-34	11-70	54 19	
54	10-50	8-90	7-32	5-96	5-24	5-12	5-86	7-17	8-90	10-63	12-10	13-16	13-13	11-86	10-27	8-88	8-08	7-87	8-42	9-56	10-87	11-93	12-44	12-26	55 20	
55	11-27	9-76	7-96	6-27	5-06	4-55	5-02	6-47	8-32	10-67	12-72	14-14	14-86	14-44	12-70	10-66	8-80	7-60	7-21	7-64	9-18	11-00	12-40	13-36	56 20	
56	13-52	12-60	10-86	8-63	6-40	4-63	4-06	4-70	6-46	8-84	11-30	13-80	15-56	16-25	15-33	12-96	10-26	7-95	6-54	6-18	7-03	8-83	11-00	12-96	57 20	
57	14-40	14-74	13-76	11-70	8-84	6-08	4-05	3-42	4-14	6-18	8-80	12-06	14-93	16-76	17-15	15-84	12-87	9-56	7-00	5-18	5-12	6-26	8-52	11-16	58 21	
58	15-38	15-86	14-57	11-93	8-26	5-48	3-42	2-92	4-14	6-18	8-80	12-06	14-93	16-76	17-15	15-84	12-87	9-56	7-00	5-18	5-12	6-26	8-52	11-16	58 21	
59	14-74	16-46	16-34	14-66	11-26	7-66	4-94	3-20	3-27	4-70	7-52	10-86	14-03	17-06	17-98	16-96	13-90	10-20	6-96	4-47	3-56	4-02	6-04	9-40	60 22	
60	15-55	16-86	16-36	13-86	10-44	6-92	4-54	3-37	3-90	5-80	8-56	12-33	15-44	17-27	17-40	15-46	12-93	8-50	5-70	3-74	3-27	4-33	7-10	10-34	61 22	
61	13-76	15-97	16-76	15-76	12-96	9-44	6-74	4-67	4-23	5-26	7-43	10-37	13-82	16-13	17-08	16-40	13-86	10-50	7-26	4-84	3-56	3-86	5-60	8-27	62 22	
62	11-55	14-34	16-02	16-28	14-66	11-66	8-60	6-46	5-46	6-56	8-86	11-44	14-36	15-97	16-18	14-88	12-00	8-86	6-28	4-57	4-06	4-86	6-67	9-40	63 23	
63	12-24	14-39	15-64	15-33	13-25	10-46	8-22	6-76	6-34	7-00	8-36	10-22	12-44	14-42	15-27	14-71	12-72	10-14	7-72	5-93	4-86	5-00	6-10	8-03	64 23	
64	10-30	12-47	13-97	14-58	13-92	12-03	10-14	8-54	7-56	7-56	8-42	9-82	11-34	12-96	14-04	14-24	13-22	11-36	9-36	7-56	6-27	5-84	6-34	9-00	66 0	
65	10-76	12-44	13-56	13-74	12-74	11-40	10-07	9-16	8-96	9-27	9-77	10-46	11-36	12-44	13-07	13-03	12-12	10-46	8-86	7-68	7-02	7-02	7-06	8-54	67 0	
66	9-66	10-96	12-24	12-88	12-88	12-24	11-43	10-66	10-24	10-16	10-24	10-47	10-86	11-44	12-02	12-40	12-24	11-36	10-18	8-87	7-97	7-67	7-94	8-50	68 0	
67	9-00	9-78	10-74	11-76	12-46	12-67	12-27	11-74	11-26	10-87	10-56	10-36	10-26	10-76	11-26	11-56	11-38	10-86	9-96	9-14	8-40	7-98	7-86	7-86	69 1	
68	8-34	9-30	10-46	11-44	12-08	12-36	12-27	12-03	11-50	10-78	10-20	9-75	9-58	9-87	10-35	10-89	11-10	10-78	10-32	9-72	8-80	7-97	7-38	7-38	70 1	
69	7-26	7-87	8-97	10-32	11-56	12-46	13-94	13-10	12-54	11-68	10-56	9-64	9-08	8-82	9-16	9-88	10-74	11-40	11-75	11-70	11-14	10-07	8-84	7-56	71 1	
70	6-74	6-70	7-63	8-94	12-06	13-26	13-78	13-68	12-86	11-34	9-88	8-86	8-16	8-03	8-46	9-64	10-86	12-06	12-78	12-56	11-57	9-92	8-17	6-67	72 2	
71	5-98	6-16	7-20	8-87	10-76	12-70	14-08	14-61	14-06	12-53	10-68	8-96	7-55	6-88	7-95	8-07	9-84	11-76	12-97	13-54	13-03	11-46	9-42	7-27	73 2	
72	5-74	5-30	5-90	7-44	9-66	11-92	14-02	15-17	15-16	13-87	11-66	9-44	7-56	6-34	6-07	6-86	8-08	10-80	12-96	14-55	13-37	11-16	8-45	6-26	74 3	
73	5-16	5-12	6-24	8-10	10-63	13-22	15-15	15-86	15-17	13-22	10-40	7-86	6-06	5-25	5-34	6-90	9-24	11-72	13-95	15-20	15-12	13-10	10-64	7-57	75 3	
Sum	767-45	775-49	790-38	795-81	775-44	765-23	765-55	762-71	764-99	758-26	754-06	771-84	800-60	796-45	810-02	790-80	763-78	766-14	754-43	735-41	726-65	726-00	711-50	720-83	10340-74	
No.	74	74	74	74	74	74	74	74	75	74	74	74	75	74	74	74	74	73	75	73	74	74	74	74	74	

No. of Days. 7<sup>th</sup> day.

FORMS FOR SHORT-PERIOD TIDES.

SERIES L.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour		
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d	h	
74	5'44	4'44	4'96	6'46	8'94	11'85	14'34	16'00	16'06	14'53	11'64	8'54	5'76	4'22	3'97	5'24	7'30	10'10	13'02	15'04	16'00	15'20	12'86	9'54	76	3	
75	6'67	4'92	4'38	5'52	7'55	10'33	13'50	15'75	16'73	16'07	13'66	10'42	7'22	4'92	3'64	4'00	5'66	8'33	11'52	14'30	16'06	16'52	15'06	12'13	8'73	77	4
76	6'13	4'66	4'90	6'52	8'92	11'86	14'66	16'40	16'56	15'07	11'90	8'47	5'62	3'74	3'22	4'26	6'00	9'60	12'85	15'23	16'56	16'25	14'26	10'83	78	4	
77	8'00	5'75	5'11	5'88	7'84	10'46	13'38	15'68	16'60	15'80	13'36	10'12	7'06	4'83	3'54	3'76	5'34	7'86	11'00	13'93	15'92	16'74	15'74	13'36	10'24	79	5
78	7'64	6'12	6'08	7'14	9'00	11'56	13'90	15'66	15'98	14'76	12'06	8'90	6'13	4'34	3'62	4'36	6'06	8'47	11'31	13'87	15'62	16'12	14'97	12'74	80	5	
79	10'02	8'05	6'96	7'06	7'93	9'67	12'07	14'08	15'23	15'08	13'57	11'16	8'26	6'08	4'76	4'47	5'46	7'26	9'48	11'88	13'90	15'36	15'50	14'66	81	5	
80	12'67	10'54	8'74	7'94	8'14	9'06	10'62	12'40	13'77	14'52	14'20	12'80	10'64	8'47	6'76	5'86	5'82	6'49	7'75	9'52	11'71	13'54	14'73	14'90	14'06	82	6
81	12'63	11'05	9'70	8'86	8'72	9'12	10'24	11'76	13'06	13'60	13'34	12'06	10'56	8'92	7'40	6'43	6'30	6'68	7'68	9'46	11'24	13'02	14'08	14'52	83	6	
82	14'22	13'04	11'70	10'34	9'24	8'84	9'04	9'84	10'96	12'05	12'86	12'96	12'44	11'22	9'67	8'30	7'06	6'48	6'64	7'48	8'86	10'64	12'34	13'74	84	6	
83	14'48	14'44	13'62	12'12	10'36	8'96	8'11	7'96	8'44	9'76	11'26	12'36	12'92	12'78	11'94	10'50	8'78	7'20	6'06	5'92	6'72	8'34	10'26	12'20	13'86	85	7
84	15'00	15'14	14'16	12'20	9'88	8'00	6'90	6'56	7'46	9'22	11'16	12'56	13'57	14'06	13'37	11'72	9'38	7'17	5'72	5'38	6'17	7'82	10'00	12'50	86	7	
85	14'54	15'84	15'94	14'64	12'14	9'36	6'97	5'74	5'63	6'67	8'88	11'24	13'46	14'86	15'36	14'34	12'05	9'44	6'93	5'38	5'00	5'82	7'83	10'50	13'30	87	8
86	15'60	16'72	16'28	14'37	11'37	8'36	6'00	4'67	4'80	6'40	9'20	12'06	14'62	16'12	16'16	14'90	12'22	9'12	6'60	5'05	4'86	5'87	8'10	11'14	88	8	
87	14'15	16'35	17'15	16'24	13'58	10'14	7'06	4'83	3'96	4'70	6'72	9'92	13'20	15'64	17'04	16'75	14'92	11'81	8'56	6'27	5'14	5'64	6'94	9'43	89	8	
88	12'61	15'44	17'03	17'08	15'36	11'92	8'64	6'18	4'48	4'25	5'24	7'57	11'00	14'10	16'43	17'34	16'56	14'28	10'82	7'84	5'95	5'42	6'12	7'87	10'62	90	9
89	13'66	16'10	17'14	16'46	13'96	10'44	7'12	4'80	3'83	4'41	6'43	8'78	12'04	14'74	16'66	17'13	15'64	12'86	9'53	7'16	5'81	5'93	7'22	9'26	91	9	
90	12'02	14'66	16'44	16'67	15'06	12'02	8'56	5'84	4'04	3'84	4'93	7'24	10'09	13'22	15'56	16'90	16'56	14'74	11'68	8'84	7'02	6'48	7'04	8'26	92	9	
91	10'50	14'94	15'83	15'12	12'94	9'87	7'14	5'16	4'22	4'76	6'40	8'73	11'37	14'00	15'82	16'34	15'34	13'10	10'40	8'36	7'32	7'28	8'03	9'50	93	10	
92	11'53	13'48	14'74	14'92	13'67	11'34	8'76	6'67	5'40	5'22	6'16	7'85	9'97	12'30	14'30	15'48	15'46	14'27	12'24	10'20	8'78	8'26	8'47	9'24	94	10	
93	10'52	12'04	13'48	14'16	13'84	12'27	10'16	8'14	6'47	5'74	6'22	7'44	9'20	10'85	12'64	14'05	14'67	14'27	12'97	11'44	10'04	9'16	8'84	9'16	9'84	95	11
94	10'95	11'96	12'80	12'96	12'28	10'94	9'24	7'80	6'78	6'70	7'30	8'37	9'54	10'90	12'34	13'52	13'80	13'26	12'13	10'96	10'04	9'60	9'33	9'54	96	11	
95	9'90	10'56	11'44	11'02	12'05	11'54	10'36	9'16	8'12	7'47	7'44	7'87	8'52	9'46	10'73	11'93	12'74	12'98	12'60	11'86	11'07	10'34	9'94	9'77	97	11	
96	9'87	10'02	10'36	10'81	11'14	11'27	10'92	10'30	9'34	8'36	7'74	7'58	7'98	8'76	9'87	11'04	11'96	12'50	12'66	12'42	11'96	11'34	10'55	9'91	9'47	98	12
97	9'34	9'52	9'94	10'53	10'94	11'12	11'02	10'62	10'00	9'22	8'40	8'01	8'13	8'63	9'70	10'66	11'77	12'66	13'06	12'94	12'40	11'47	10'50	9'62	99	12	
98	8'94	8'54	8'74	9'48	10'45	11'36	11'88	11'89	11'44	10'50	9'40	8'46	7'84	7'76	8'43	9'46	10'86	12'30	13'36	13'82	13'66	12'66	11'42	10'02	8'72	100	13
99	7'96	7'82	8'36	9'47	10'86	11'90	12'70	12'87	12'44	11'06	9'52	8'12	7'40	7'47	8'26	9'54	11'08	12'70	14'06	14'56	14'22	12'80	10'96	8'88	101	13	
100	7'46	6'81	6'84	7'92	9'62	11'52	13'00	13'97	14'12	13'00	11'02	9'05	7'48	6'74	6'92	7'97	9'72	11'72	13'58	14'86	15'12	14'21	12'35	9'67	102	13	
101	7'47	5'98	5'58	6'14	7'76	9'84	12'16	14'02	15'18	15'06	13'40	10'95	6'66	6'02	6'46	7'88	10'06	12'53	14'55	15'72	15'49	13'80	11'08	8'22	103	14	
102	5'93	4'52	4'32	5'47	7'72	10'54	13'27	15'36	16'20	15'32	13'00	9'88	7'34	5'76	5'40	6'24	8'22	10'70	13'40	15'52	16'25	15'36	12'80	9'46	104	14	
103	6'56	4'47	3'42	3'91	5'74	8'31	11'40	14'40	16'28	16'72	15'47	12'68	9'44	6'81	5'47	5'38	6'52	8'91	11'80	14'40	15'97	16'08	14'35	11'30	105	14	
104	7'80	4'97	2'93	3'46	3'76	6'21	9'51	12'97	15'58	17'14	17'04	14'94	11'68	8'36	6'14	5'06	5'57	7'24	10'07	13'10	15'40	16'44	15'82	13'44	9'74	106	15
105	6'67	4'03	2'50	2'77	4'44	7'50	10'96	14'33	16'70	17'72	16'91	14'37	10'87	8'10	6'15	5'71	6'50	8'36	11'33	14'12	15'97	16'50	15'10	12'22	107	15	
106	8'67	5'24	3'17	2'56	3'47	5'74	8'64	12'02	15'12	16'94	17'54	16'24	13'40	10'32	7'62	6'17	6'07	7'04	9'13	12'00	14'47	15'69	15'54	13'66	10'74	108	16
107	7'44	4'88	3'28	3'04	4'36	6'67	9'40	12'47	15'00	16'74	16'94	15'60	13'03	10'01	7'87	6'76	6'80	7'71	9'70	12'14	14'15	15'02	14'50	12'53	109	16	
108	9'92	7'24	5'36	4'17	4'16	5'20	7'26	9'89	12'40	14'57	15'77	15'74	14'47	12'12	9'90	8'07	7'14	7'11	7'83	9'54	11'58	13'16	13'74	13'28	110	16	





FORMS FOR SHORT-PERIOD TIDES.

SERIES L.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
147	8.92	10.62	12.60	14.02	14.27	13.22	10.78	8.10	5.76	4.27	4.17	5.26	7.20	9.70	12.28	14.66	15.94	16.04	14.86	12.64	10.27	8.44	7.54	7.34	150 7	
148	8.10	9.52	11.55	13.36	14.27	13.92	12.06	9.48	6.90	5.12	4.32 4.97	6.54	8.70	11.00	13.46	15.32	16.07	15.67	14.17	11.77	9.56	8.16	7.68	7.83	151 8	
140	8.74	10.50	12.26	13.66	14.02	12.96	10.86	8.34	6.24	5.04	4.82	5.84	7.60	9.46	11.87	14.10	15.30	15.60	14.66	12.78	10.74	9.03	7.96	7.73	152 8	
150	8.24	9.44	11.07	12.62	13.44	13.16	11.96	9.94	7.67	6.16	5.18	5.56	6.86	8.64	10.66	12.74	14.30	15.12	15.06	13.65	11.84	10.00	8.46	7.75	153 8	
151	7.78 8.46	9.92	11.36	12.37	12.84	12.22	10.98	9.18	7.32	6.03	5.94	6.87	8.17	9.67	11.58	13.28	14.64	14.97	14.22	12.62	11.08	9.47	8.38	8.08	154 9	
152	8.30	9.20	10.24	11.49	12.12	12.46	11.72	10.38	8.77	7.37	6.70	6.93	7.78	8.83	10.30	11.90	13.54	14.68	14.80	13.77	12.16	10.50	9.20	8.47	155 9	
153	8.28	8.60	9.36	10.36	11.26	11.83	12.05	11.56	10.60	9.20	8.14	7.72	7.83	8.62	9.82	11.10 12.64	13.94	14.46	14.16	13.26	11.74	10.42	9.26	8.54	156 10	
154	8.34	8.46	9.23	10.10	10.93	11.70	11.97	11.72	11.06	9.98	8.86	8.32	8.36	9.00	10.04	11.54	12.92	13.86	14.25	13.85	12.88	11.48	10.08	8.98	157 10	
155	8.20	8.20	8.37	9.12	10.03	11.29	12.14	12.58	12.36	11.84	11.02	10.06	9.23	8.78	9.20	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	10.03	158 10	
156	8.74	7.92	7.54	7.76	8.67	9.96	11.54 12.84	13.87	13.86	13.28	12.03	10.56	9.66	9.64	10.17	11.38	12.77	13.98	14.67	15.14	14.88	13.86	12.46	10.48	159 11	
157	8.82	7.82	7.50	8.19	9.46	11.28	13.22	14.76	15.82	15.76	14.97	13.34	11.70	10.67	10.27	10.56	11.52	12.90	14.12	15.30	15.65	15.48	14.17	12.02	160 11	
158	9.86	8.00	7.09	6.85	7.72	9.34	11.40	13.77	15.84	16.86	16.85	15.70	13.60	11.52	9.95	9.55	9.80	10.84	12.57	14.21	15.47 16.06	15.22	13.50	10.84	161 12	
159	8.22	6.16	4.95	5.15	6.50	8.61	11.37	14.18	16.48	17.54	17.17	15.60	12.50	10.07	8.34	8.17	8.96	10.27	12.23	14.24	15.74	16.29	15.33	12.77	162 12	
160	9.46	6.32	4.44	3.62	4.30	6.30	8.54	11.95	15.02	17.28	17.95	17.20	15.02	11.76	9.04	7.44	7.22	7.81	9.55	12.08	14.54	16.07	16.21	14.76	163 12	
161	11.87	8.16	5.07	3.07	2.74	3.80	5.94	9.24	12.80	15.92	18.07	18.53 17.65	14.65	10.90	8.00	6.62	6.55	7.50	9.65	12.45	14.89	16.40	16.14	14.28	164 13	
162	10.90	7.10	4.31	2.62	2.37	3.68	6.30	9.76	13.48	16.44	18.12	18.40	17.00	13.80	10.17	7.55	6.20	6.18	7.30	9.60	12.79	15.16	16.42	15.96	165 13	
163	13.80	10.33	6.77	4.00	2.33	2.54	4.18	7.11	10.40	13.95	16.74	17.85	17.95	16.07	12.81	9.60	7.05	5.72	5.77	7.00	9.56	12.80	15.12	16.05	166 13	
164	15.26	12.76 9.20	6.14	3.95	2.88	3.47	5.52	7.93	11.04	14.21	16.44	17.72	17.40	15.44	12.07	9.02	6.70	5.67	5.93	7.41	10.07	13.02	14.92	15.57	167 14	
165	14.68	12.28	9.20	6.52	4.77	4.20	4.94	6.52	8.80	11.67	14.34	16.42	17.20	16.60	14.54	11.30	8.66	6.74	6.05	6.16	7.65	10.05	12.50	14.32	168 14	
166	14.85	14.05	11.96	9.47	7.26	6.06	5.80	6.39	7.66	9.64	11.92	14.25	15.90	16.46	15.74	13.76 8.61	6.86	6.32	6.58	7.80	9.82	12.04	13.55	169 15		
167	14.17	13.54	12.03	10.34	8.60	7.57	7.26	7.62	8.44	9.92	12.12	14.20	15.46	15.54	14.58	12.66	10.40	8.31	7.04	6.60	6.77	7.78	9.32	11.22	170 15	
168	12.80	13.58	13.46	12.40	10.90	9.62	8.66	8.31	8.49	9.05	10.30	12.04	13.70	14.74	14.75	13.73	12.02	10.10	8.46	7.12	6.53	6.70	7.50	9.03	171 15	
169	10.90	12.32	13.20	13.38	12.92	11.94	10.67 8.94	9.60	8.82	9.24	10.33	11.90	13.24	14.06	14.10	13.34	11.84	10.05	8.26	6.94	6.44	6.67	7.49	9.06	172 16	
170	10.86	12.50	13.66	14.10	13.63	12.46	11.06	10.06	9.30	9.05	9.33	10.22	11.60	12.90	13.82	13.85	13.08	11.64	9.76	8.00	6.70	6.08	6.22	7.28	173 16	
171	9.00	10.94	12.77	14.05	14.63	14.17	12.86	11.33	10.04	9.14	8.86	9.20	10.08	11.26	12.44	13.30	13.52	12.80	11.00	8.85	7.06	5.67 5.05	5.60	7.15	174 17	
172	9.26	11.30	13.28	14.45	14.84	13.95	12.40	10.90	9.46	8.62	8.24	8.56	9.64	11.12	12.55	13.40	13.37	12.07	10.07	8.20	6.17	4.94	4.74	5.62	175 17	
173	7.74	9.76	12.14	14.01	15.00	14.86	13.77	12.06	10.27	8.84	8.10	7.94	8.52	9.68	11.18	12.64	13.37	13.05	11.52	9.17	6.76	5.11	4.16	4.64	176 17	
174	6.10	8.00	10.50	12.90	14.56	15.33	14.70	13.32	11.14	9.44	8.17	7.54	7.57 8.34	9.81	11.65	13.20	13.60	12.56	10.40	7.97	5.83	4.38	4.04	4.96	177 18	
175	6.82	9.02	11.57	13.86	15.24	15.44	14.56	12.56	10.36	8.63	7.62	7.30	7.74	9.86	10.67	12.47	13.67	13.60	12.02	9.66	6.93	4.96	3.94	4.22	178 18	
176	5.70	7.84	10.40	12.82	14.74	15.56	15.33	13.80	11.44	9.35	7.79	7.04	7.03	7.90	9.44	11.66	13.22	13.92	13.00	10.74	8.00	5.64	4.04	3.83	179 18	
177	4.76	6.70	9.02	11.37 13.67	15.12	15.46	14.48	12.44	9.96	8.16	6.86	6.42	6.94	8.42	10.44	12.57	13.67	13.68	12.22	9.64	6.86	4.96	3.98	4.36	180 19	
178	5.65	7.72	10.02	12.26	14.31	15.28	15.12	13.77	11.30	9.01	7.37	6.64	6.56	7.46	9.06	11.01	12.70	13.51	13.01	11.07	8.44	6.12	4.72	4.42	181 19	
179	5.32	6.94	8.97	11.17	13.22	14.74	15.17	14.22	12.16	9.74	7.86	6.74	6.51	7.07	8.16	9.92	11.66	12.82 13.10	11.86	9.72	7.36	5.70	5.02	5.24	182 20	
180	6.42	8.07	10.12	11.98	13.73	14.86	14.72	13.40	11.17	9.22	7.55	6.51	6.57	7.34	8.72	10.61	12.04	12.77	12.64	11.27	9.34	7.48	6.30	5.87	183 20	
181	6.54	7.66	9.24	10.97	13.94	14.38	14.88	14.20	12.50	10.34	8.44	7.22	6.77	6.97	7.87	9.34	10.94	12.19	12.66	12.22	10.84	9.35	7.90	6.96	184 20	



FORMS FOR SHORT-PERIOD TIDES.  
SERIES L.—(Continued).

Day	0 <sup>h</sup>		1 <sup>h</sup>		2 <sup>h</sup>		3 <sup>h</sup>		4 <sup>h</sup>		5 <sup>h</sup>		6 <sup>h</sup>		7 <sup>h</sup>		8 <sup>h</sup>		9 <sup>h</sup>		10 <sup>h</sup>		11 <sup>h</sup>		12 <sup>h</sup>		13 <sup>h</sup>		14 <sup>h</sup>		15 <sup>h</sup>		16 <sup>h</sup>		17 <sup>h</sup>		18 <sup>h</sup>		19 <sup>h</sup>		20 <sup>h</sup>		21 <sup>h</sup>		22 <sup>h</sup>		23 <sup>h</sup>		Solar Hour
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet		
219	16.18	13.96	6.47	3.74	2.56	3.20	5.12	8.18	11.74	15.30	17.66	18.50	17.76	14.76	10.60	7.27	5.06	4.48	5.07	7.18	10.36	13.94	16.34	223 11																									
220	17.16	16.94	13.12	9.20	5.80	3.36	2.56	3.60	5.73	9.03	12.78	15.94	17.78	18.04	16.74	13.32	9.36	6.05	4.18	4.90	7.56	11.10	14.46	224 11																									
221	16.66	16.98	15.39	12.15	8.23	5.44	3.52	3.32	4.58	7.04	10.14	13.35	17.52	17.26	15.28	11.80	8.22	5.32	3.80	5.58	8.40	11.50	14.52	225 12																									
222	16.18	16.06	14.38	11.26	7.98	5.62	4.54	4.80	6.25	8.27	11.00	13.96	16.32	17.26	16.42	14.32	10.85	7.62	5.16	4.64	7.02	12.05	15.05	226 12																									
223	14.70	15.80	15.18	13.36	10.62	7.94	6.32	5.74	6.44	7.77	9.72	12.07	14.12	15.66	15.72	14.46	12.06	9.36	6.96	5.07	5.84	7.33	9.54	227 12																									
224	11.87	13.60	14.46	13.96	10.40	8.65	7.45	7.28	8.00	9.26	10.72	12.27	13.74	14.47	14.18	12.78	10.82	8.78	6.78	5.86	6.74	8.34	10.14	228 13																									
225	12.02	13.36	13.57	12.85	11.76	10.70	9.74	9.12	8.90	9.34	10.06	10.94	12.10	12.88	13.72	13.38	11.88	10.06	8.17	7.02	6.68	7.00	8.77	229 13																									
226	10.10	11.44	12.33	12.66	12.46	12.00	11.36	10.62	10.07	9.67	9.77	10.12	10.82	11.54	12.43	12.67	11.33	9.96	8.64	7.77	7.46	7.69	9.04	230 14																									
227	10.10	11.17	12.34	12.90	12.90	12.34	11.72	11.15	10.62	10.30	10.00	10.14	10.50	11.34	11.96	12.26	11.97	11.38	10.53	9.44	8.35	7.66	8.12	231 14																									
228	9.06	10.48	11.57	12.72	13.42	13.56	13.18	12.30	11.45	10.72	10.26	9.92	9.63	10.00	10.71	11.62	12.32	12.18	11.42	10.36	9.08	8.15	7.53	232 14																									
229	7.70	8.54	9.82	11.43	12.72	13.66	13.66	13.26	11.22	10.18	9.34	8.97	9.08	9.88	10.76	11.64	12.26	12.35	11.85	10.40	8.78	7.36	6.44	233 15																									
230	7.14	8.37	10.20	11.94	13.38	14.40	14.54	13.58	12.17	10.70	9.34	8.82	8.84	9.26	10.00	11.16	12.50	13.30	13.42	12.06	10.16	8.40	6.86	234 15																									
231	6.14	7.20	8.95	10.80	12.76	13.96	14.91	14.84	13.64	11.84	9.97	8.77	8.36	8.48	8.96	10.06	11.36	13.12	13.97	13.64	12.06	9.70	7.27	235 16																									
232	6.35	7.80	9.76	11.70	13.66	15.10	15.46	14.62	12.86	10.57	8.64	7.46	7.31	7.76	8.84	10.72	12.64	14.21	14.62	13.44	11.00	8.24	5.17	236 16																									
233	5.36	6.54	8.54	10.66	13.00	15.02	15.96	15.50	14.08	11.60	8.97	7.34	6.70	6.84	7.80	9.62	11.70	13.76	14.95	14.67	12.76	10.00	7.37	237 16																									
234	4.97	5.74	7.38	9.36	11.94	14.36	16.04	16.27	15.32	13.08	10.11	7.72	6.36	6.94	8.63	10.83	13.20	15.21	15.71	14.43	11.89	8.54	6.26	238 17																									
235	5.06	6.36	8.22	10.64	13.40	15.80	16.62	16.16	14.21	11.38	8.34	6.35	5.46	5.74	7.13	9.22	11.84	14.36	15.71	15.48	13.64	10.66	7.60	239 17																									
236	4.96	5.70	7.24	9.54	12.02	14.56	16.24	16.56	15.34	12.80	9.60	7.06	5.50	5.18	5.94	7.72	10.28	13.04	15.14	15.90	14.88	12.52	9.63	240 17																									
237	5.74	5.64	6.67	8.36	10.62	13.17	15.30	15.97	14.06	11.04	8.16	6.11	5.05	5.41	6.72	8.83	11.26	13.77	15.36	15.38	14.00	11.50	8.72	241 18																									
238	5.97	6.34	7.52	9.30	11.47	13.80	15.46	15.84	14.77	12.44	9.37	7.06	5.37	4.85	5.64	7.12	9.24	11.64	13.96	15.06	14.75	13.17	10.76	242 18																									
239	7.30	6.86	7.44	8.64	10.38	12.36	14.06	15.24	15.10	13.64	11.26	8.61	6.50	5.32	5.38	6.34	7.85	9.86	13.64	14.58	14.07	12.68	10.68	243 19																									
240	8.02	7.81	8.36	9.26	10.60	12.24	13.73	14.44	13.86	12.25	10.02	8.06	6.46	5.62	5.78	6.47	7.80	9.63	11.38	12.97	13.74	13.44	12.44	244 19																									
241	9.83	8.84	8.57	8.87	9.67	10.67	11.96	13.06	13.46	13.08	11.68	9.86	8.26	6.87	6.17	6.26	7.02	8.17	9.66	11.26	12.55	13.37	13.57	245 19																									
242	11.92	10.73	9.67	9.16	9.18	9.63	10.54	11.48	12.02	12.66	11.74	10.42	8.87	7.44	6.44	6.21	6.66	7.76	9.20	10.76	12.36	13.54	14.05	246 20																									
243	12.68	11.26	10.03	9.22	8.90	9.14	9.86	10.86	12.02	12.84	12.98	13.14	13.40	12.04	10.04	7.64	5.76	4.78	5.02	6.24	8.16	10.78	14.28	247 20																									
244	14.74	13.66	11.85	10.04	8.66	8.02	8.14	9.04	10.38	12.06	13.14	14.86	14.44	12.80	10.18	7.37	5.17	3.90	3.34	5.50	7.96	10.88	13.80	248 21																									
245	15.74	14.33	11.96	9.30	7.37	6.55	6.70	8.06	9.98	12.06	13.93	15.74	15.08	14.44	12.80	10.18	7.37	5.17	3.90	5.50	7.96	10.88	13.80	249 21																									
246	17.04	16.46	14.44	11.04	8.24	6.27	5.15	5.63	7.24	9.64	12.52	14.74	15.98	15.46	13.29	9.94	6.63	4.34	3.17	5.53	8.20	11.40	14.56	250 21																									
247	16.82	17.44	16.36	13.83	9.98	6.70	4.46	3.84	4.58	6.80	10.06	13.28	15.76	16.64	13.29	9.94	6.26	6.06	3.66	3.72	5.66	8.70	12.20	15.53	251 22																								
248	17.33	17.53	15.97	12.42	8.56	5.32	3.44	3.17	4.55	7.26	10.87	14.22	16.50	17.05	15.47	12.37	8.44	5.52	3.48	3.10	4.46	6.74	9.94	13.47	252 22																								
249	16.22	17.47	17.02	14.77	10.84	7.23	4.52	3.00	3.30	5.07	8.06	11.72	14.94	16.86	16.90	14.94	11.54	8.00	5.38	3.90	4.20	5.52	7.95	11.06	253 22																								
250	14.30	16.51	17.04	15.88	9.17	5.97	3.70	2.94	3.94	6.16	9.14	12.45	15.42	16.68	16.10	13.81	10.56	7.46	5.47	4.87	5.60	7.04	9.54	12.25	254 23																								
251	14.81	16.16	16.06	14.44	11.07	7.87	5.34	3.84	3.92	5.16	7.43	10.36	13.44	15.47	16.04	14.92	12.66	9.98	7.74	6.47	6.36	7.02	8.54	10.58	255 23																								
252	12.80	14.58	15.36	14.73	12.53	9.86	7.17	5.31	4.44	5.02	6.44	8.50	11.04	13.56	14.79	14.77	13.46	11.46	9.44	8.00	7.56	8.36	9.51	11.10	257 0																								
253	12.60	13.73	13.94	12.90	11.02	8.73	6.96	5.70	5.63	6.34	7.60	9.36	11.36	13.14	13.88	13.60	12.43	10.94	9.64	8.76	8.44	8.70	9.95	258 0																									



FORMS FOR SHORT-PERIOD TIDES.  
SERIES L.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour		
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d	h
202	6.36	5.84	6.47	8.16	10.16	12.84	15.02	16.10	15.46	13.28	9.87	6.84	4.45	3.04	3.57	5.44	8.15	11.37	14.60	16.81	17.35	16.28	13.64	10.41	297	15	
203	7.71	6.07	5.84	6.88	8.87	11.47	14.12	15.94	16.22	14.81	11.87	8.55	5.46	3.46	2.87	4.17	6.35	9.32	13.00	15.95	17.47	17.44	15.72	12.68	298	15	
204	9.66	7.28	5.94	6.04	7.36	9.64	12.45	14.81	16.04	15.60	13.70	10.52	7.15	2.92	3.10	4.72	7.47	10.55	13.92	16.35	17.36	16.74	14.57	11.67	299	16	
205	8.85	6.76	5.94	6.28	7.70	9.92	12.68	14.78	15.58	14.78	12.36	9.26	6.36	4.20	3.07	3.72	5.55	8.04	11.05	14.10	16.17	16.96	16.12	14.06	300	16	
206	11.15	8.82	7.14	6.57	7.02	8.46	10.56	13.14	14.64	15.04	13.76	11.47	8.74	6.42	4.70	4.22	5.00	6.80	9.02	11.88	14.60	16.14	16.22	15.16	301	16	
207	13.26	10.86	8.80	7.58	7.44	8.84	10.92	12.84	13.84	13.86	12.57	10.68	8.54	6.84	5.56	5.27	5.98	7.33	9.36	11.72	14.00	15.22	15.38	14.58	302	17	
208	13.88	11.01	9.42	8.12	7.64	7.92	8.94	10.40	11.85	12.91	13.12	12.26	10.75	9.22	7.66	6.68	6.30	6.72	7.86	9.44	11.50	13.34	14.46	14.66	303	17	
209	13.96	13.74	11.30	9.76	8.54	7.93	7.84	8.40	9.60	10.88	12.06	12.64	12.40	11.47	10.10	8.76	7.68	7.01	7.06	9.22	10.97	12.56	13.72	14.38	304	18	
300	14.04	13.04	11.45	9.76	8.15	7.22	7.02	7.48	8.84	10.32	11.48	12.55	12.87	12.46	11.36	9.70	8.28	7.14	6.80	7.40	8.84	10.74	12.56	13.87	305	18	
301	14.54	14.38	13.40	11.67	9.60	7.53	6.30	5.88	6.50	8.20	10.07	11.93	13.36	14.04	13.66	12.30	10.26	8.61	7.37	6.86	7.24	8.35	10.36	12.50	306	18	
302	14.13	15.08	14.96	13.80	11.64	9.03	6.96	5.44	5.04	7.79	10.12	12.66	14.54	15.37	14.86	13.04	10.66	8.56	7.12	6.44	6.77	8.02	10.14	12.62	307	19	
303	14.56	15.55	15.25	13.56	10.92	8.12	5.82	4.22	4.10	5.32	7.70	10.85	13.62	15.51	16.05	15.06	12.86	10.40	8.16	6.53	5.96	6.51	8.24	10.85	308	19	
304	13.27	15.16	15.84	15.03	12.98	9.78	7.04	4.71	3.46	3.86	5.60	8.44	11.74	14.64	16.50	16.72	15.38	12.86	9.98	7.70	6.25	5.93	6.71	8.67	309	20	
305	13.84	15.32	15.84	14.55	11.68	8.46	5.64	3.63	3.01	4.08	6.50	9.62	13.08	15.81	17.12	16.72	14.87	12.03	9.20	7.26	6.32	6.37	7.46	9.60	310	20	
306	12.20	14.35	15.67	15.28	13.15	10.15	7.00	4.47	3.03	3.22	5.03	7.60	10.76	14.05	16.38	17.05	16.14	13.92	11.10	8.66	6.16	6.46	8.00	311	20		
307	10.44	13.10	14.76	15.16	13.92	11.40	8.36	5.66	3.69	2.94	3.94	6.18	9.01	12.24	14.92	16.56	15.16	12.66	10.06	7.96	6.74	7.35	9.00	312	21		
308	11.24	13.43	14.50	14.36	12.66	9.94	7.20	4.97	3.56	3.77	5.34	7.72	10.56	13.46	15.64	16.34	15.71	13.92	11.46	9.28	7.66	6.86	6.98	7.98	313	21	
309	9.96	12.00	13.52	14.02	13.37	11.18	8.81	6.52	4.86	4.33	5.20	6.90	9.14	11.80	14.20	15.72	15.81	14.66	12.72	10.71	8.96	7.82	7.56	7.92	314	21	
310	9.16	10.98	12.24	13.26	12.06	10.17	8.00	6.25	5.31	5.50	6.66	8.34	10.52	12.80	14.44	15.16	14.68	13.32	11.56	8.76	8.10	8.00	8.60	8.60	315	22	
311	9.65	10.96	12.18	13.58	12.23	11.04	9.16	7.62	6.54	6.20	6.84	7.96	9.38	11.14	12.91	14.18	14.40	13.64	12.37	10.90	9.58	8.78	8.46	8.68	316	22	
312	9.30	10.00	10.94	11.57	11.80	11.36	10.28	8.94	7.84	7.18	7.20	7.86	8.80	9.98	11.46	12.86	13.86	13.83	12.96	11.72	9.66	9.14	8.92	8.96	317	23	
313	9.17	9.66	10.40	11.10	11.37	11.01	10.20	9.26	8.46	8.10	8.14	8.66	9.44	10.56	11.74	12.76	13.34	13.26	12.61	11.72	10.86	9.76	9.04	8.80	318	23	
314	8.85	9.16	9.64	10.14	10.74	11.18	11.32	11.06	10.38	9.58	8.94	8.71	8.90	9.50	10.12	11.46	12.48	13.10	13.15	12.64	11.84	10.76	9.71	8.88	319	23	
315	8.35	8.19	8.42	9.04	9.96	10.86	11.50	11.80	11.55	10.96	9.98	8.64	8.75	9.38	10.38	11.46	12.41	13.07	13.16	12.84	11.84	10.56	9.24	8.13	320	0	
316	7.50	6.43	7.86	8.81	10.03	11.16	12.23	12.80	12.64	11.66	10.35	9.04	8.36	8.34	8.96	10.02	11.20	12.46	13.23	13.47	13.00	11.72	10.14	8.38	322	0	
317	7.03	6.27	6.31	7.08	8.52	10.23	11.92	13.17	13.63	13.10	11.86	10.18	8.76	7.98	7.96	8.75	10.13	11.64	13.14	13.94	13.04	11.34	11.34	9.30	323	0	
318	5.86	5.13	5.46	6.76	8.80	11.15	13.20	14.66	14.98	13.87	11.76	9.58	8.10	7.57	7.36	8.22	9.82	11.76	13.33	14.28	14.14	12.87	10.56	7.98	324	1	
319	5.77	4.14	3.74	4.67	6.71	9.27	12.02	14.40	15.66	15.44	13.71	11.16	8.74	7.02	6.40	6.78	8.22	10.37	12.95	13.88	14.74	14.20	12.26	9.36	325	1	
320	6.51	4.12	2.75	2.94	4.56	7.03	10.95	13.27	15.65	16.62	15.90	13.76	10.86	8.17	6.45	5.84	8.12	10.44	12.84	14.46	15.08	13.97	11.41	8.07	326	2	
321	4.96	2.57	1.63	2.58	4.74	7.64	11.12	14.22	16.47	17.07	15.75	12.96	9.86	7.26	5.65	5.46	6.44	8.40	11.20	13.57	15.11	15.17	13.27	9.96	327	2	
322	6.40	3.62	1.76	1.54	3.26	6.02	9.25	12.97	15.66	17.40	17.25	15.37	12.23	9.00	6.75	5.63	5.63	6.88	9.32	12.22	14.44	15.50	14.80	12.31	328	2	
323	8.84	5.46	3.00	1.66	2.20	4.15	10.46	13.81	16.44	17.54	16.82	14.56	11.38	8.50	6.32	5.44	5.74	7.26	10.06	12.76	14.67	15.26	14.06	11.32	329	3	
324	8.05	5.16	2.94	2.16	3.11	5.16	7.96	11.23	14.30	16.57	17.22	16.23	13.81	10.68	8.07	6.16	5.50	5.88	7.64	10.25	13.77	14.29	14.72	13.35	330	3	
325	10.74	7.81	5.32	3.66	3.26	4.42	6.34	8.86	11.67	14.39	16.33	16.57	15.28	12.84	9.93	7.47	6.23	5.72	6.26	7.94	10.58	13.76	13.96	12.68	331	4	
326	10.56	8.18	6.28	4.97	4.83	5.73	7.34	9.38	12.05	14.37	15.76	15.80	14.56	12.28	9.94	8.13	6.64	6.14	6.54	8.04	10.24	11.78	12.86	13.16	332	4	
327	12.24	10.73	8.96	7.30	6.24	5.96	6.50	7.80	9.84	12.15	13.88	14.87	14.84	13.77	11.77	10.06	8.23	6.86	6.34	7.70	9.90	10.84	12.16	12.86	333	4	







36	6.86	6.78	7.17	7.94	9.05	10.30	11.34	11.97	11.42	10.84	10.34	10.07	9.97	9.77	9.94	10.44	11.32	12.06	12.26	11.78	10.88	9.87	8.84	7.86	38 22	
37	7.24	6.94	8.03	9.07	10.14	11.00	11.56	11.85	11.77	11.46	11.12	10.57	10.07	9.70	9.70	10.13	10.80	11.27	11.45	11.25	10.76	9.00	8.00	7.11	40 0	
38	6.58	6.74	7.44	8.51	9.84	10.90	11.76	12.34	12.55	12.30	11.60	10.57	9.76	9.34	9.17	10.24	10.94	11.36	11.44	10.97	10.10	9.07	7.87	6.85	41 1	
39	6.30	6.50	7.26	8.50	10.16	11.44	12.65	13.26	13.32	11.36	10.08	9.16	8.67	8.64	9.01	9.76	10.58	11.25	11.66	11.34	10.36	8.82	7.36	6.12	42 2	
40	5.54	5.82	6.94	10.36	12.06	13.46	13.97	13.64	12.30	10.76	9.26	8.14	7.84	8.12	8.96	10.24	11.52	12.40	12.66	12.07	10.47	6.64	5.46	5.20	43 4	
41	5.93	7.55	9.56	11.72	13.53	14.67	14.84	13.98	12.14	10.00	8.54	7.66	7.53	8.16	9.56	11.03	13.62	13.60	12.30	10.24	7.77	5.88	4.84	4.96	44 5	
42	6.33	8.27	10.66	13.07	14.85	15.64	15.23	13.64	11.13	9.02	6.79	7.00	8.13	9.87	11.85	13.60	14.38	13.88	11.93	9.10	6.54	4.66	4.00	4.90	45 6	
43	6.86	9.20	11.97	14.34	15.96	14.78	12.26	9.64	7.46	6.24	5.96	6.74	8.48	10.85	13.07	14.56	14.85	13.63	10.90	7.86	5.57	4.07	5.46	7.84	46 8	
44	10.63	13.64	15.83	16.64	16.01	13.87	10.90	8.00	6.17	5.46	5.74	7.26	9.70	12.25	14.42	15.50	15.15	13.08	9.90	6.94	4.75	3.92	4.66	6.62	9.46	47 9
45	12.60	15.08	16.60	16.64	15.00	11.93	8.96	6.76	5.63	5.06	5.54	7.84	10.54	13.30	15.12	15.66	14.46	11.76	8.44	5.86	4.26	4.25	5.52	7.84	10.68	48 10
46	13.68	15.84	16.68	15.86	13.15	10.22	7.36	5.65	4.23	4.46	6.07	8.56	11.57	14.06	15.54	15.51	13.57	10.53	7.47	5.38	4.52	5.04	6.70	9.14	14.74	49 12
47	16.26	16.26	14.64	11.74	8.68	6.28	4.54	4.14	5.07	7.06	9.74	12.44	14.55	15.46	14.76	12.57	9.68	5.84	5.60	6.54	8.40	10.77	13.32	15.42	50 13	
48	16.26	15.47	13.18	10.24	7.54	5.62	4.54	4.69	5.80	7.87	10.40	12.80	15.06	14.03	11.86	9.36	7.58	6.64	6.76	7.86	9.60	11.66	13.73	15.08	51 14	
49	15.32	14.12	11.86	9.24	6.90	5.18	5.06	6.46	8.24	10.33	12.41	13.86	14.34	13.44	11.46	9.53	8.05	7.40	7.66	8.58	9.92	11.68	13.36	14.16	52 16	
50	12.82	10.83	8.73	6.87	5.45	4.92	5.44	6.63	8.23	10.14	11.77	12.96	13.40	12.76	11.56	10.24	9.04	8.28	8.67	9.76	11.20	12.50	13.18	13.06	53 17	
51	11.88	10.25	8.57	6.98	5.77	5.38	5.64	6.37	7.82	9.54	11.17	12.38	13.02	12.96	12.16	11.07	10.02	8.94	8.44	8.48	9.27	10.44	11.57	12.34	54 18	
52	11.70	10.50	8.90	7.32	5.96	5.24	5.12	7.17	8.90	10.63	12.10	13.16	13.56	13.13	11.86	10.27	8.88	8.08	7.87	8.42	9.56	10.87	11.93	12.44	55 19	
53	12.26	9.76	7.96	6.27	5.06	4.55	5.02	6.47	8.52	10.67	12.72	14.14	14.86	14.44	12.70	10.66	8.80	7.60	7.64	9.18	11.00	12.40	13.36	13.52	56 21	
54	12.60	10.86	8.63	6.40	4.63	4.06	4.70	6.46	8.84	11.30	13.80	15.56	16.25	15.33	12.96	10.26	7.95	6.54	6.18	7.03	8.83	11.00	12.96	14.40	57 22	
55	13.76	11.70	8.84	6.08	4.05	3.42	4.14	6.18	12.06	14.93	16.76	17.15	15.84	12.87	9.66	7.00	5.18	5.12	6.26	8.52	11.16	13.67	15.38	15.86	58 23	
56	14.57	11.93	8.26	5.48	3.42	2.92	4.14	6.52	9.58	13.16	16.04	17.62	17.34	15.27	11.66	8.27	5.56	4.16	4.32	5.84	8.66	14.74	16.46	16.54	59 1	
57	11.26	7.66	4.94	3.20	3.27	4.70	7.52	10.86	14.63	17.06	17.98	16.96	13.90	10.20	6.96	4.47	3.56	4.02	6.04	9.40	12.86	15.55	16.86	16.36	60 2	
58	10.44	6.92	4.54	3.37	3.90	5.80	8.56	12.33	15.44	17.40	15.46	12.03	8.50	5.70	3.74	3.27	4.33	7.10	10.34	13.76	15.97	16.76	15.76	12.96	62 3	
59	9.44	6.74	4.67	5.26	7.43	10.37	13.82	16.13	17.08	16.40	13.86	10.50	7.26	4.84	3.56	3.86	5.60	8.27	11.55	14.34	16.02	14.66	11.66	8.60	63 5	
60	6.46	5.26	5.46	6.56	8.86	11.44	14.36	15.97	16.18	14.88	12.00	8.86	6.28	4.57	4.06	6.67	9.40	12.24	14.39	15.64	15.33	13.25	10.46	8.22	64 6	
61	6.76	6.34	7.00	8.36	10.22	12.44	14.42	15.27	14.71	12.72	7.72	5.93	4.86	5.00	6.10	8.03	10.30	12.47	13.97	14.58	13.92	12.03	10.14	8.54	65 7	
62	7.56	7.56	8.42	9.82	12.96	14.04	14.24	13.22	11.36	9.36	7.56	6.27	5.84	6.34	7.46	9.00	10.76	12.44	13.56	13.74	12.74	11.40	9.16	8.96	66 9	
63	9.27	9.77	10.46	11.34	12.44	13.07	13.03	12.12	10.46	8.86	7.68	7.02	7.02	7.66	8.54	9.66	12.24	12.88	12.88	12.24	11.43	10.66	10.24	10.16	67 10	
64	10.24	10.47	10.86	11.44	12.02	12.40	12.24	11.36	10.18	8.87	7.67	7.94	8.50	9.00	9.78	10.74	11.76	12.46	12.67	12.27	11.74	11.26	10.87	10.56	68 11	
65	10.36	10.22	10.36	10.76	11.26	11.56	11.38	10.86	9.96	9.14	8.40	7.98	7.80	7.86	8.34	9.30	10.46	11.44	12.08	12.36	12.27	12.03	11.50	10.78	69 13	
66	9.58	9.87	10.35	10.89	11.10	11.10	10.78	10.32	9.72	8.86	7.97	7.28	7.26	7.87	8.97	10.32	11.56	13.04	13.10	12.54	11.68	10.56	9.64	9.08	70 14	
67	8.82	9.16	9.88	10.74	11.40	11.75	11.70	11.14	10.07	8.84	7.56	6.70	7.63	8.94	10.62	12.06	13.26	13.78	13.68	12.86	11.34	9.88	8.86	8.16	71 15	
68	8.03	8.46	9.64	10.86	12.06	12.78	11.57	9.92	8.17	6.67	5.98	6.16	7.20	8.87	10.76	12.70	14.08	14.61	14.06	12.53	10.68	8.96	7.55	6.88	72 17	
69	8.07	9.84	11.76	12.97	13.54	13.03	11.46	9.42	7.27	5.74	5.30	5.90	7.44	9.66	11.92	14.02	15.17	15.16	13.87	11.66	9.44	7.56	6.34	6.07	73 18	
70	8.68	10.80	12.96	14.26	14.55	13.37	11.16	8.45	6.26	5.16	5.12	6.24	8.10	10.63	13.22	15.15	15.86	15.17	13.22	10.40	7.86	6.06	5.25	5.54	74 19	
Sum	783.91	741.93	710.19	709.60	684.10	693.37	732.72	748.53	791.19	830.15	840.57	818.68	775.35	756.44	712.26	701.39	704.93	703.75	731.39	771.67	803.35	819.91	834.91	843.62	No. of Days.	
No.	73	73	73	75	74	74	74	73	73	75	75	74	73	74	73	74	75	74	73	73	74	74	74	75	18243.91	





FORMS FOR SHORT-PERIOD TIDES.  
SERIES N.—(Continued).

Day	0 <sup>a</sup>	1 <sup>a</sup>	2 <sup>a</sup>	3 <sup>a</sup>	4 <sup>a</sup>	5 <sup>a</sup>	6 <sup>a</sup>	7 <sup>a</sup>	8 <sup>a</sup>	9 <sup>a</sup>	10 <sup>a</sup>	11 <sup>a</sup>	12 <sup>a</sup>	13 <sup>a</sup>	14 <sup>a</sup>	15 <sup>a</sup>	16 <sup>a</sup>	17 <sup>a</sup>	18 <sup>a</sup>	19 <sup>a</sup>	20 <sup>a</sup>	21 <sup>a</sup>	22 <sup>a</sup>	23 <sup>a</sup>	Solar Hour
141	4.84	3.94	4.50	8.33	10.94	13.60	15.42	16.13	15.62	13.90	11.47	9.28	7.84	7.40	7.74	8.92	10.62	12.60	14.02	14.27	13.22	10.78	5.76	4.27	149 17
142	4.17	5.26	7.20	9.70	12.28	14.66	15.94	16.04	14.86	12.64	10.27	8.44	7.54	7.34	8.10	9.52	13.36	14.27	13.92	12.06	9.48	6.90	5.12	4.32	150 18
143	4.97	6.54	8.70	11.06	13.46	15.32	16.07	15.67	14.17	9.56	8.16	7.68	7.83	8.74	10.50	12.26	13.66	14.02	12.96	10.86	8.34	6.24	5.04	4.82	151 19
144	5.84	7.60	9.46	11.87	15.30	15.60	14.66	12.78	10.74	9.03	7.96	7.73	8.24	9.44	11.07	12.62	13.44	13.16	11.96	9.94	7.67	6.16	5.18	6.86	152 21
145	8.64	10.66	12.74	14.30	15.12	15.06	13.65	11.84	10.00	8.46	7.75	7.78	8.26	9.24	11.36	12.37	12.84	10.98	9.18	7.32	6.03	5.94	6.97	8.17	153 22
146	9.67	11.58	13.28	14.64	14.97	14.22	12.62	11.08	9.47	8.38	8.08	8.30	10.24	11.40	12.12	12.46	11.72	10.38	8.77	7.37	6.70	6.93	7.78	8.83	154 28
147	10.30	11.90	13.54	14.68	14.80	13.77	12.16	10.30	8.47	8.28	8.60	9.36	10.36	11.26	11.83	12.05	11.56	10.60	9.20	8.14	7.72	7.83	8.62	9.82	155 1
148	12.64	13.94	14.46	14.16	13.26	11.74	10.42	9.26	8.54	8.34	8.46	9.23	10.10	10.93	11.70	11.97	11.72	11.06	8.86	8.32	8.36	9.00	10.04	11.54	157 2
149	13.92	13.86	14.25	13.85	12.88	11.48	10.08	8.98	8.20	8.20	8.37	9.12	10.03	11.29	12.14	12.58	12.36	11.84	11.02	10.06	9.23	8.78	9.20	11.98	158 3
150	13.44	14.22	14.34	13.94	12.86	11.50	8.74	7.92	7.54	7.76	8.67	9.06	11.54	12.84	13.97	13.86	14.97	13.34	11.70	10.27	9.66	10.17	11.38	12.77	159 5
151	14.67	15.14	14.88	13.86	12.46	10.48	8.82	7.82	7.50	8.19	9.46	11.28	13.22	14.76	15.82	15.76	14.97	13.34	11.70	10.27	9.55	10.84	12.37	14.21	161 7
152	15.30	15.65	15.48	14.17	13.02	9.86	8.00	7.09	6.85	7.72	9.34	11.40	15.84	16.86	16.85	15.70	13.60	11.52	9.95	9.55	8.17	10.27	11.38	14.24	162 8
153	15.47	16.06	15.22	13.50	10.84	8.22	4.95	5.15	6.50	8.61	11.37	14.18	16.48	17.54	17.17	15.60	12.50	10.07	8.34	8.17	7.22	10.27	12.37	16.07	168 10
154	15.74	15.33	12.77	9.46	6.32	4.44	3.62	4.30	6.30	8.54	11.95	15.02	17.28	17.95	17.20	15.02	11.76	9.04	7.44	7.22	6.55	10.27	11.38	16.40	164 11
155	16.21	14.76	11.87	8.16	5.07	3.07	2.74	3.80	5.94	9.24	12.80	15.92	18.07	18.53	14.65	10.90	8.00	6.62	6.55	7.50	6.18	7.30	10.27	14.89	165 12
156	16.14	13.28	10.90	7.10	4.31	2.62	2.37	3.60	3.68	9.76	13.48	18.12	18.40	17.00	13.80	10.17	7.55	6.20	6.18	7.00	6.00	10.27	11.38	16.42	166 14
157	15.96	10.33	6.77	4.00	2.33	2.54	4.18	7.11	10.40	13.95	16.74	17.85	17.95	17.05	12.81	9.60	7.05	5.72	5.77	7.56	7.00	10.27	12.37	15.26	166 14
158	12.76	9.20	6.14	3.95	2.88	3.47	5.52	4.52	11.04	14.21	16.44	17.72	17.40	15.44	12.07	6.70	5.67	5.93	7.41	10.07	13.02	14.94	15.57	14.68	167 15
159	12.28	9.20	6.52	4.77	4.20	4.94	6.52	8.80	11.67	16.42	17.20	16.60	14.54	11.30	8.66	6.74	6.05	6.16	7.65	10.05	12.50	14.32	14.85	14.05	168 16
160	11.96	9.47	6.06	4.00	2.33	2.54	4.18	7.11	10.40	13.95	16.74	17.85	17.95	17.05	12.81	9.60	7.05	6.32	7.80	9.82	12.04	14.17	13.54	12.03	169 18
161	10.34	8.60	7.57	7.26	7.62	8.44	9.92	12.12	14.20	15.46	15.54	14.58	12.66	10.40	8.31	6.60	6.77	7.78	9.32	11.22	12.80	13.58	13.46	12.40	170 19
162	10.90	9.62	8.66	8.31	8.49	9.03	10.30	12.04	13.70	14.74	13.73	12.02	10.10	8.46	7.12	6.53	6.70	7.50	9.03	10.90	12.32	13.20	13.38	12.92	171 20
163	11.94	10.67	9.66	8.94	8.82	9.24	10.33	11.90	13.24	14.06	14.10	11.84	10.05	8.26	6.94	6.44	6.67	7.49	9.06	10.86	12.50	13.66	13.63	12.46	172 22
164	11.06	10.06	9.30	9.05	9.33	10.22	11.60	12.44	13.30	13.52	11.00	8.85	7.06	5.67	5.05	5.60	7.15	9.26	11.30	13.28	14.45	14.84	13.95	12.40	175 0
165	11.33	10.04	9.14	8.86	9.20	10.08	11.26	12.44	13.40	13.52	11.00	8.85	7.06	5.67	5.05	5.60	7.15	9.26	11.30	13.28	14.45	14.84	13.95	12.40	175 0
166	10.90	9.46	8.62	8.24	9.64	11.12	12.55	13.40	13.37	12.07	10.07	8.20	6.17	4.94	4.74	5.62	7.74	9.76	12.14	14.01	15.00	14.86	13.77	10.27	176 2
167	8.84	8.10	7.94	8.52	9.68	11.18	12.64	13.37	13.05	11.52	9.17	6.76	5.11	4.16	4.64	6.10	8.00	12.90	14.56	15.33	14.70	13.32	11.14	9.44	177 3
168	8.17	7.54	7.57	8.34	9.81	11.65	13.20	13.60	12.56	10.40	7.97	5.83	4.04	4.96	6.82	9.02	11.57	13.86	15.24	15.44	14.56	12.56	10.36	8.63	178 4
169	7.62	7.30	7.74	8.86	10.67	12.47	13.60	12.02	9.66	6.93	4.96	3.94	4.22	5.70	7.84	10.40	12.82	14.74	15.36	15.33	13.80	11.44	9.35	7.79	179 6
170	7.03	7.90	9.44	11.66	13.22	13.92	13.00	10.74	8.00	5.64	4.04	3.83	4.76	6.70	9.02	11.37	13.67	15.12	15.48	12.44	9.96	8.16	6.86	6.42	180 7
171	6.94	8.42	10.44	12.57	13.67	13.68	12.22	9.64	6.86	4.96	3.98	4.36	5.65	10.02	12.26	14.31	15.28	15.12	13.77	11.30	9.01	7.37	6.64	6.56	181 8
172	7.46	9.06	11.01	12.70	13.51	13.01	11.07	6.12	4.72	4.42	5.32	6.94	8.97	11.17	13.22	14.74	15.17	14.22	13.16	9.74	7.86	6.74	6.51	7.07	182 9
173	8.16	11.66	12.82	13.10	11.86	9.72	7.36	5.70	5.02	5.24	6.42	8.07	10.92	11.98	13.75	14.86	14.72	13.40	9.23	7.55	6.57	7.34	8.77	8.77	183 11
174	10.61	12.04	13.77	12.64	11.27	9.34	7.48	6.30	5.87	6.54	7.66	9.24	12.94	14.38	14.88	14.20	12.50	10.34	8.44	7.22	6.77	6.97	8.77	9.34	184 12
175	10.94	12.19	13.66	12.22	10.84	9.25	7.90	6.94	6.06	7.56	8.50	10.00	13.23	14.36	14.44	13.38	11.42	9.60	8.02	6.94	6.56	6.92	7.79	9.26	186 18

176	10.86	11.92	12.16	11.12	9.70	8.48	7.63	7.56	8.14	9.04	10.41	11.98	13.30	13.98	13.72	12.51	10.84	8.96	7.47	6.78	6.84	7.86	9.16	10.52	186 15	
177	11.71	12.36	12.28	11.46	10.38	9.16	8.34	8.14	8.38	9.04	10.37	11.82	13.16	13.66	11.87	10.24	8.57	7.05	6.14	5.87	6.26	7.22	8.72	10.36	187 16	
178	11.70	12.56	12.86	12.14	11.14	9.86	8.86	8.32	8.34	10.46	11.88	13.12	13.48	12.96	11.86	10.30	8.58	7.00	5.74	5.32	5.74	6.86	8.67	10.62	188 17	
179	12.30	13.47	13.96	12.10	10.48	9.04	8.28	8.37	8.98	10.28	11.72	13.02	13.62	13.24	12.02	10.14	8.20	6.16	4.76	4.31	4.90	6.62	10.94	13.04	189 19	
180	14.57	15.22	14.64	12.87	10.58	8.66	7.68	7.62	8.40	10.00	11.70	13.12	13.97	13.69	12.32	7.76	5.44	3.88	3.19	3.88	5.80	8.60	11.46	13.90	190 20	
181	15.54	16.06	15.08	12.92	10.40	8.23	7.07	6.90	7.82	9.54	11.60	14.38	14.34	12.76	10.16	7.15	4.46	2.56	2.27	3.49	5.92	8.80	12.36	15.04	191 21	
182	16.76	17.06	15.90	13.27	7.42	6.03	6.04	7.17	9.30	11.84	13.92	15.05	14.90	13.08	9.91	6.43	3.53	1.84	1.84	3.58	6.20	9.54	15.92	17.60	192 23	
183	17.55	15.88	12.54	9.04	6.46	5.24	6.04	7.17	9.30	11.84	13.92	15.05	14.90	13.08	9.91	6.43	3.53	1.84	1.84	3.58	6.20	9.54	15.92	17.60	192 23	
184	17.87	15.72	12.00	8.47	5.86	4.66	4.98	6.66	9.96	13.24	15.56	16.37	15.10	12.10	8.47	5.36	3.22	2.47	3.46	5.71	8.66	12.13	15.36	17.38	193 0	
185	17.46	14.77	11.14	7.30	4.24	4.66	6.66	9.96	13.24	15.56	16.37	15.10	12.10	8.47	5.36	3.22	2.47	3.46	5.71	8.66	12.13	15.36	17.38	17.97	194 0	
186	13.80	10.58	7.04	4.79	4.26	5.04	7.14	10.42	13.85	15.77	16.14	14.53	11.60	8.45	5.84	4.20	3.82	6.97	9.80	13.00	15.56	17.04	17.17	15.44	197 4	
187	12.60	9.26	6.86	5.22	4.84	5.76	8.06	10.85	13.97	15.36	15.40	13.86	11.04	8.20	6.43	5.40	5.54	6.64	7.95	10.24	12.80	15.30	16.34	15.86	198 5	
188	11.28	8.50	6.30	5.34	5.40	8.00	10.50	12.97	14.30	14.44	12.94	10.92	9.08	7.74	7.24	7.56	8.14	9.16	11.11	13.10	14.71	15.40	14.72	10.60	199 7	
189	8.38	6.86	5.92	6.05	6.82	8.20	10.28	12.30	13.38	13.40	12.62	11.34	10.16	9.24	8.58	8.59	8.86	10.96	12.55	13.78	14.97	13.40	11.92	10.10	200 8	
190	8.37	6.87	6.38	6.51	7.24	8.41	9.82	11.28	12.52	12.90	12.68	10.93	10.01	9.34	9.14	9.27	9.97	10.90	12.12	13.14	13.41	12.71	11.34	9.77	201 9	
191	8.47	7.34	6.76	6.86	7.36	8.56	10.06	11.46	12.50	13.02	12.96	12.57	11.86	10.04	9.53	9.52	9.76	10.73	11.74	12.78	13.04	12.50	11.42	10.20	202 10	
192	7.52	6.90	6.76	7.35	8.50	10.20	11.86	13.24	13.87	13.87	13.28	12.22	11.04	10.07	9.54	9.50	9.87	10.64	12.60	12.94	12.66	11.70	10.10	8.56	203 12	
193	7.16	6.24	6.28	7.14	8.62	10.44	12.07	13.40	14.20	14.14	13.28	12.08	10.74	8.94	8.94	9.48	10.50	11.72	12.63	13.06	12.66	11.28	9.36	7.66	204 13	
194	6.38	5.86	6.06	7.07	8.94	10.96	14.58	15.07	14.54	13.34	11.84	10.26	9.14	8.46	8.46	9.61	10.36	11.74	13.14	13.52	12.81	11.24	9.13	7.31	205 14	
195	5.74	5.33	7.65	9.76	12.02	14.00	15.20	15.33	14.58	13.34	11.84	10.26	9.14	8.46	8.46	9.61	10.36	11.74	13.14	13.52	12.81	11.24	9.13	7.31	205 14	
196	5.24	6.52	8.36	10.60	12.96	14.83	16.05	15.68	14.35	12.14	9.94	8.56	8.04	8.20	8.37	8.18	8.73	9.62	10.95	12.64	13.76	12.56	6.14	5.26	206 16	
197	5.78	7.22	9.33	11.77	14.22	15.86	16.07	15.15	10.77	8.67	7.57	7.18	7.78	8.96	10.77	12.83	14.27	14.50	13.28	10.70	7.76	5.53	4.56	4.86	208 18	
198	6.26	8.20	13.14	15.37	16.51	16.11	14.47	11.94	9.36	7.58	6.88	7.16	8.00	9.72	11.80	13.84	14.90	14.32	12.37	9.57	5.10	4.56	5.42	7.13	209 20	
199	9.26	11.96	14.36	15.96	16.14	15.17	12.96	10.25	8.01	6.67	6.34	6.89	8.16	10.14	12.46	14.84	13.50	10.90	8.02	5.86	4.76	5.04	6.52	8.34	210 21	
200	10.66	13.15	15.27	16.14	15.82	14.14	11.47	8.96	7.02	6.33	7.34	9.23	11.44	13.54	14.58	14.24	12.42	9.84	7.44	5.64	5.14	5.97	7.54	9.60	211 22	
201	11.76	13.95	15.83	15.50	14.93	12.72	10.34	8.27	6.67	6.16	6.34	9.23	11.44	13.54	14.58	14.24	12.42	9.84	7.44	5.64	5.14	5.97	7.54	9.60	211 22	
202	14.41	15.55	15.26	13.84	11.46	8.86	6.95	5.97	6.05	7.05	8.56	9.86	12.04	13.74	14.37	13.56	11.51	8.97	7.02	5.96	5.96	6.61	10.53	12.64	213 0	
203	14.57	15.10	14.32	12.72	10.34	8.27	6.67	6.16	6.40	7.24	10.52	12.26	13.20	13.32	12.36	10.84	9.38	8.24	7.77	8.12	8.86	10.16	11.76	13.33	215 2	
204	14.29	14.38	13.46	11.64	7.76	6.48	6.10	6.50	7.54	9.00	10.63	12.05	12.96	13.18	12.64	11.47	10.24	9.16	8.76	9.04	9.66	10.72	12.02	14.10	216 4	
205	14.04	13.02	11.29	9.63	7.96	6.84	6.50	6.73	7.66	9.04	10.52	12.10	13.14	13.55	13.28	12.50	11.34	10.26	9.52	9.35	9.67	10.59	11.83	13.62	217 5	
206	13.44	12.54	11.15	9.50	7.86	6.50	5.94	6.16	7.10	8.50	10.20	13.44	14.14	14.16	13.42	12.16	10.76	9.56	9.05	9.15	9.96	11.33	12.62	13.36	218 6	
207	13.55	12.96	11.68	9.90	6.26	5.46	6.46	8.25	10.24	12.44	14.18	15.26	15.50	14.64	12.94	10.78	9.16	8.56	8.76	9.78	11.16	13.70	14.26	219 8		
208	14.02	12.80	10.52	8.01	5.84	4.76	4.81	5.98	7.77	10.32	13.02	15.24	16.66	16.76	15.58	13.24	10.54	7.60	7.78	8.76	10.54	12.56	14.24	15.18	220 9	
209	14.86	13.21	10.40	7.41	4.97	3.62	3.84	5.16	7.44	10.44	13.54	17.44	17.44	15.84	12.90	9.72	7.44	6.60	6.85	8.10	10.22	12.92	15.15	16.26	221 10	
210	15.72	13.66	10.33	6.96	4.40	3.33	3.33	7.86	11.08	14.56	17.20	18.37	18.04	16.16	12.38	8.82	6.46	5.54	5.95	7.72	10.60	13.60	16.07	17.04	222 12	
Sum	824.98	806.89	800.14	756.21	712.03	703.03	690.51	703.39	737.45	805.95	824.51	839.99	848.43	833.50	795.99	733.48	729.70	709.59	603.46	709.14	727.67	786.15	841.37	859.94	No. of Days.	
No.	73	73	75	74	74	75	73	73	73	75	74	74	74	73	73	74	75	74	73	74	73	74	75	75	75	79 21 1/2





FORMS FOR SHORT-PERIOD TIDES.

SERIES N. -- (Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour d h	
281	13.10	15.67	16.78	16.36	14.16	11.00	8.32	6.36	5.84	6.47	8.16	10.16	12.84	15.02	16.10	15.46	9.87	6.84	4.45	3.04	3.57	5.44	8.15	11.37	287 9	
282	14.60	16.81	17.35	16.28	13.64	10.44	7.71	6.07	5.84	6.88	11.47	14.12	15.94	16.22	14.81	11.87	8.55	5.46	3.46	2.87	4.17	6.35	9.32	13.00	288 10	
283	15.95	17.47	17.44	12.68	15.72	12.68	5.94	6.04	7.36	9.64	14.45	14.84	16.04	15.66	13.70	10.52	7.15	4.66	2.92	3.10	4.72	7.47	13.92	16.35	289 12	
284	17.36	16.74	14.57	11.67	8.85	6.76	5.94	6.28	7.70	9.92	12.68	14.78	15.58	14.78	12.36	9.26	6.36	4.20	3.07	3.72	5.55	8.04	11.05	16.17	300 13	
285	16.96	16.12	14.06	11.35	8.82	7.14	6.57	7.02	8.46	10.56	13.14	15.04	13.76	11.47	8.74	6.42	4.70	4.22	5.00	6.86	9.02	11.88	14.60	16.14	301 14	
286	16.22	15.16	13.26	10.86	8.86	7.14	7.44	8.84	10.92	12.84	13.84	13.86	12.57	10.68	8.54	6.84	5.56	5.27	5.98	7.33	9.36	11.72	15.22	14.00	302 16	
287	14.58	12.88	11.01	9.42	8.12	7.64	7.92	8.94	10.40	11.85	12.91	13.12	12.26	10.75	9.22	7.66	6.30	6.72	7.86	9.44	11.50	13.34	14.46	14.66	308 17	
288	13.96	13.74	11.30	9.76	8.54	7.93	7.84	8.40	9.66	10.88	12.06	12.87	12.46	11.36	9.70	8.28	7.14	6.80	7.40	8.84	10.74	12.56	13.72	14.38	304 18	
289	14.04	13.04	11.45	9.76	8.15	7.02	7.22	8.84	10.32	11.48	12.55	13.04	13.66	12.30	10.26	8.61	7.37	6.86	8.35	10.36	12.50	14.13	15.08	14.54	305 20	
290	13.40	11.67	9.60	7.53	6.30	5.88	6.50	8.20	10.07	11.93	13.36	14.04	13.66	12.30	10.26	8.61	7.37	6.77	8.02	10.14	12.62	14.56	15.55	15.25	306 21	
291	13.80	11.64	9.03	6.96	5.44	5.04	5.86	7.79	10.12	12.66	14.54	15.37	13.04	10.66	8.56	7.12	6.44	6.77	8.02	10.14	12.62	14.56	15.55	15.25	307 22	
292	13.56	10.92	8.12	5.82	4.22	4.10	5.32	10.85	13.65	15.51	16.05	15.06	12.86	10.40	8.16	6.53	5.96	6.51	8.24	10.85	13.27	15.16	15.84	15.03	308 23	
293	9.78	7.04	4.71	3.46	3.86	5.60	8.44	11.74	14.64	16.50	16.72	14.87	12.03	9.26	6.32	6.37	7.46	9.60	11.25	13.84	15.52	15.84	14.55	11.68	310 1	
294	8.46	5.64	3.63	3.01	4.08	6.50	9.62	13.08	15.81	17.12	16.72	14.87	9.20	7.26	6.32	6.37	7.46	9.60	12.20	14.35	15.67	15.28	13.15	10.15	311 2	
295	7.00	4.47	3.03	3.22	5.03	7.60	10.76	14.05	17.05	16.14	13.92	11.10	8.66	6.87	6.16	6.46	8.00	10.44	13.10	14.76	15.16	13.92	11.40	8.36	312 3	
296	5.66	3.69	3.94	6.18	9.01	12.24	14.92	16.53	16.56	15.16	12.66	10.06	7.96	6.74	6.60	7.35	9.00	11.24	13.43	14.36	14.50	12.66	9.94	7.20	4.97	313 5
297	3.56	3.77	5.34	7.72	10.56	13.46	15.64	16.34	15.71	13.92	11.46	9.28	7.66	6.98	7.98	9.96	12.00	13.52	14.02	13.37	11.18	8.81	6.52	4.86	314 6	
298	4.33	5.20	6.90	9.14	11.80	14.20	15.72	15.81	14.66	10.71	8.96	7.82	7.56	7.92	9.16	10.68	12.24	13.26	13.26	12.06	10.17	8.00	6.25	5.31	315 7	
299	5.50	6.66	10.52	12.80	14.44	15.16	14.68	13.32	12.37	10.99	8.76	8.10	8.00	8.60	9.65	10.96	12.18	12.58	12.23	11.04	7.84	7.54	6.20	6.84	316 9	
300	7.96	9.38	11.44	12.91	14.18	14.40	13.64	12.37	10.99	9.58	8.78	8.46	8.68	9.30	10.00	11.57	11.80	11.36	10.28	8.94	7.84	7.20	8.14	8.66	318 11	
301	8.80	9.98	11.46	12.86	13.86	13.83	12.96	11.72	10.53	9.14	8.92	8.96	9.16	9.64	10.14	10.74	11.18	11.32	11.06	10.38	9.58	8.94	8.71	9.50	319 13	
302	9.44	10.56	11.74	13.34	13.76	13.26	12.61	11.72	10.86	9.76	8.80	8.85	9.16	9.64	10.14	10.86	11.30	11.55	11.06	10.96	9.98	8.64	8.75	9.38	320 14	
303	10.42	11.46	12.48	13.10	13.15	12.64	11.84	10.76	9.71	8.88	8.35	8.19	8.42	9.04	9.96	11.23	12.80	12.64	11.66	10.25	9.04	8.36	8.34	8.96	321 15	
304	10.38	11.46	12.41	13.07	13.16	12.84	11.84	10.56	9.24	8.13	7.43	7.86	8.83	10.03	11.16	12.53	12.80	12.64	11.66	10.18	8.76	8.36	8.34	8.96	321 15	
305	10.02	11.20	12.46	13.23	13.47	11.72	10.14	8.38	7.03	6.27	6.31	7.08	8.52	10.23	11.92	13.17	13.63	13.10	11.86	10.18	8.76	7.98	7.96	10.13	322 17	
306	11.64	13.14	13.94	13.94	13.04	11.34	9.30	7.45	5.86	5.13	5.46	6.76	8.80	11.15	13.20	14.66	14.08	11.76	9.58	8.10	7.27	7.36	8.75	9.82	323 18	
307	11.76	13.33	14.28	14.14	12.87	10.56	7.98	5.77	4.14	3.74	6.71	9.27	12.02	14.40	15.66	15.44	13.87	11.16	8.74	7.02	6.40	6.78	8.22	10.37	324 19	
308	12.25	13.88	14.74	14.20	12.26	6.51	4.12	2.75	2.94	4.56	7.03	10.05	13.27	15.65	16.62	15.90	13.76	10.86	8.17	6.45	5.84	6.36	8.12	10.44	325 21	
309	14.46	15.08	13.97	11.41	8.07	4.96	2.57	1.63	2.58	4.74	7.64	11.12	14.22	16.47	17.07	15.75	12.96	9.86	6.56	5.46	6.44	8.40	11.20	13.57	326 22	
310	15.11	15.17	13.27	9.96	6.40	3.62	1.76	1.34	3.26	6.02	9.25	12.97	17.40	17.25	15.37	12.23	9.00	6.75	5.63	5.63	6.88	9.32	12.22	14.44	327 23	
311	15.50	14.80	13.31	8.84	5.46	3.00	2.20	4.15	6.93	10.46	13.81	16.44	17.54	16.83	14.56	11.38	8.50	6.32	5.44	5.74	7.26	10.06	12.76	14.67	329 0	
312	15.26	11.32	8.05	5.16	2.94	2.16	3.11	5.16	7.96	11.23	14.30	16.57	17.22	16.23	13.81	10.68	8.07	6.16	5.80	7.64	10.23	12.77	14.59	14.72	330 2	
313	13.33	10.74	7.81	5.32	3.66	3.26	4.42	6.34	8.86	11.67	14.58	16.33	15.28	13.84	9.93	7.47	6.23	5.72	6.26	7.94	10.30	12.38	13.76	13.96	331 3	
314	13.68	10.56	8.18	6.28	4.97	4.83	7.34	9.38	12.05	14.37	15.76	15.80	14.56	13.28	9.94	8.13	6.64	6.14	6.54	8.04	10.04	11.78	12.86	13.16	332 4	
315	13.24	8.23	7.30	6.24	5.96	6.50	7.80	9.84	12.15	13.88	14.87	14.84	13.77	11.77	10.66	8.43	6.86	6.34	6.56	7.70	10.84	12.16	12.76	13.53	833 6	



316	11'48	10'14	8'60	7'52	7'06	7'44	8'47	10'17	11'91	13'34	14'21	14'40	13'72	12'30	10'42	8'41	6'88	6'14	6'37	7'32	8'81	10'45	11'84	12'86	13'08	334	7		
317	12'42	11'25	9'75	8'54	7'84	7'88	8'64	10'02	11'65	13'16	14'14	14'30	13'64	12'17	10'31	8'37	6'68	5'72	5'86	6'88	8'64	10'40	12'07	13'31	13'88	335	8		
318	13'62	12'36	9'06	8'12	7'90	8'54	9'72	11'26	12'78	13'82	14'20	13'74	12'14	10'05	7'76	6'00	5'04	5'23	6'52	8'50	10'56	12'60	14'12	14'40	13'86	336	10		
319	12'58	10'80	8'97	7'94	7'68	8'24	9'50	11'14	12'75	13'98	14'44	13'73	11'85	9'10	6'84	4'41	5'04	6'57	8'66	11'20	13'52	15'24	15'84	15'08	337	11			
320	13'13	10'86	9'00	7'82	7'54	8'05	9'36	11'14	12'94	14'20	14'66	13'36	11'28	8'58	5'98	4'22	3'96	5'07	6'97	9'54	12'26	14'54	16'11	16'34	15'17	338	12		
321	12'88	10'26	8'38	7'40	8'14	9'77	11'52	13'36	14'60	14'56	12'94	10'26	7'33	5'11	3'87	4'05	5'64	7'81	10'61	13'20	15'47	16'54	16'21	14'70	12'20	339	14		
322	9'81	8'08	7'33	7'37	8'31	10'05	12'02	13'86	14'76	14'17	12'16	8'93	6'32	4'31	3'72	4'64	6'56	9'06	11'87	14'55	16'23	16'72	15'97	13'94	11'34	340	15		
323	8'98	7'71	7'36	7'70	9'02	10'97	12'94	14'40	14'70	13'44	10'64	7'77	5'58	4'12	4'16	5'63	7'83	10'36	13'16	15'34	16'56	16'48	15'11	12'72	10'27	341	16		
324	8'26	7'37	7'26	8'12	11'91	13'58	14'48	14'07	12'12	9'32	6'72	4'74	3'96	4'91	6'70	9'02	11'70	14'07	15'87	16'56	15'80	13'96	11'44	9'32	7'80	342	18		
325	7'24	7'44	8'72	10'57	12'55	14'00	14'24	13'24	10'72	8'06	5'93	4'58	4'74	6'03	8'20	10'34	12'88	16'23	16'28	14'89	12'63	10'30	8'54	7'57	343	19			
326	7'44	8'17	9'64	11'50	13'03	13'80	13'45	11'78	9'47	7'26	5'64	5'86	7'43	9'20	11'48	13'56	15'17	15'82	15'18	13'58	11'42	9'46	7'98	7'36	344	20			
327	7'62	8'50	10'02	11'60	12'67	12'14	10'36	8'34	6'54	5'59	5'67	6'77	8'43	10'27	12'17	13'90	14'96	14'86	13'76	12'00	10'22	8'66	7'73	7'38	7'80	345	22		
328	8'82	10'22	11'48	12'26	12'24	11'15	9'47	8'01	6'87	6'45	6'75	7'83	9'14	10'75	12'56	13'86	14'46	14'06	12'87	11'31	9'72	8'40	7'76	7'73	8'27	346	23		
329	9'36	10'54	11'48	12'02	11'81	10'84	9'56	8'46	7'76	7'56	8'00	8'95	11'60	13'13	14'20	14'42	13'83	12'50	10'98	9'76	8'76	8'24	8'24	8'80	8'80	348	0		
330	9'62	10'53	11'27	11'70	11'62	11'14	9'49	8'78	8'48	8'71	9'47	10'70	12'04	13'16	13'78	13'79	13'14	11'94	10'54	9'17	8'30	7'83	8'04	8'58	9'36	349	2		
331	10'22	11'00	11'54	11'74	11'57	10'96	10'14	9'44	9'04	9'10	9'74	10'90	12'24	13'16	13'57	13'38	12'64	11'55	10'26	8'86	7'83	7'22	7'36	7'86	8'85	350	3		
332	10'11	11'13	11'95	12'42	12'30	11'78	10'77	9'72	9'06	9'01	9'55	10'76	11'97	12'94	13'38	13'14	12'44	11'22	9'78	8'36	7'04	6'26	6'15	6'82	8'20	351	4		
333	9'97	11'56	12'90	13'50	13'36	12'36	10'92	9'68	8'84	8'68	9'14	10'18	11'57	12'76	13'30	13'22	12'46	11'00	9'17	7'18	5'75	4'90	4'92	6'07	7'94	352	5		
334	10'07	12'03	13'66	14'48	14'16	12'76	10'77	9'04	7'98	7'73	8'23	9'70	11'40	12'74	13'42	13'45	12'54	10'80	8'50	6'30	4'47	3'64	4'12	5'82	8'20	10'84	353	7	
335	13'27	14'95	15'70	14'97	13'05	10'60	8'64	7'50	7'36	8'16	9'80	11'80	13'38	14'33	14'26	13'00	10'50	7'72	5'17	3'42	2'93	4'16	6'37	9'00	12'12	354	8		
336	14'97	16'74	16'90	15'68	13'11	10'34	8'06	6'98	6'08	8'06	10'00	12'15	14'04	15'14	15'03	13'10	10'20	7'00	4'27	2'40	2'20	3'93	6'57	9'77	13'27	355	9		
337	16'13	17'72	17'51	15'78	12'57	9'74	7'27	6'14	6'36	7'56	9'86	12'72	14'77	15'81	15'20	12'64	9'26	5'91	3'10	1'55	1'93	4'00	7'06	10'68	14'30	17'04	356	11	
338	18'34	17'72	15'47	12'00	8'88	6'58	5'67	6'00	7'50	10'14	13'10	15'24	16'17	14'94	12'16	8'55	5'06	2'64	1'50	2'57	5'14	8'44	11'93	15'00	17'66	357	12		
339	18'34	17'37	14'51	10'92	7'77	5'66	5'14	5'64	7'65	10'63	13'44	15'46	15'86	14'14	10'98	7'68	4'48	2'36	1'77	3'30	5'83	8'90	12'30	15'56	17'50	358	13		
340	17'88	16'62	13'58	9'97	6'94	5'14	4'70	5'52	7'63	10'73	13'70	15'36	15'32	13'24	9'92	6'64	.	.	.	.	.	.	.	.	.	.	359	15	
341	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	360	16
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350	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	370	2
Sum	744'70	732'90	684'61	651'26	620'19	564'80	561'73	592'35	640'28	659'68	694'11	747'68	733'94	700'42	653'34	615'20	575'45	545'14	543'44	561'20	593'16	651'90	698'64	722'63	.	.	No.	of Days.	
No. {	63	64	63	63	64	63	63	63	64	63	63	64	63	63	63	63	62	62	63	62	61	62	63	62	62	62 <sup>d</sup> 21 <sup>h</sup> .	.	.	
	73	74	73	74	75	74	73	73	74	74	74	75	73	73	73	76	74	74	74	73	73	74	74	74	73	73 <sup>d</sup> 18 <sup>h</sup> .	15488'75	.	.

FORMS FOR SHORT-PERIOD TIDES.

BOMBAY—Commencing 0 hours, Astronomical Time, 1st January, 1885.

SERIES λ.

Motion per mean Solar hour = 14°.7278127.

Argument ( $\gamma - \frac{1}{2}\sigma + \frac{1}{2}\omega - \eta$ ).

Table with columns for Day (1-35), Solar Hour (d h), and tidal heights in feet for hours 0h to 35h. The table contains numerical data for each row and column.

86	14.44	13.11	11.12	9.30	7.54	6.26	6.13	6.68	7.86	9.28	10.86	12.27	13.10	12.94	11.93	10.66	9.72	9.12	9.06	9.26	9.66	10.60	11.84	12.86	27.15	
37	13.34	12.82	11.45	10.03	8.74	7.48	6.86	6.78	7.17	7.94	9.03	10.30	11.34	11.97	11.92	11.42	10.84	10.34	10.07	9.97	9.77	9.94	10.44	11.32	38.15	
38	12.06	12.26	11.78	10.88	9.87	7.86	7.24	6.94	7.18	8.03	9.07	10.14	11.00	11.56	11.85	11.77	11.46	11.12	10.57	10.07	9.70	9.70	10.13	10.80	39.16	
39	11.27	11.45	11.25	10.76	9.97	9.00	8.00	7.11	6.58	6.74	7.44	8.51	9.84	10.90	11.76	12.34	12.55	12.30	11.60	10.57	9.76	9.34	9.17	9.56	40.16	
40	10.24	10.94	11.36	11.44	10.97	10.10	9.07	7.87	6.85	6.30	6.50	8.50	10.16	11.44	12.65	13.26	13.32	12.56	11.36	10.08	9.16	8.67	8.64	9.01	41.17	
41	9.76	10.58	11.35	11.66	11.34	10.36	8.82	7.36	6.12	5.54	5.82	6.94	8.54	10.36	12.06	13.46	13.97	13.64	12.30	10.76	9.26	8.14	7.84	8.12	42.17	
42	8.96	10.24	11.52	12.40	12.66	12.97	10.47	8.56	6.64	5.46	5.20	5.93	7.55	9.56	11.72	13.53	14.67	13.98	12.14	10.00	8.54	7.66	7.53	8.10	43.18	
43	9.56	11.03	12.66	13.62	13.60	12.30	10.24	7.77	5.88	4.84	4.96	6.33	8.27	10.66	13.07	14.85	15.82	15.96	14.78	12.26	9.64	7.54	6.79	7.00	44.18	
44	8.13	9.87	11.85	13.60	14.38	13.88	11.93	9.10	6.54	4.66	4.00	4.90	6.86	9.20	11.97	14.34	15.64	15.82	14.78	12.26	9.64	7.46	6.24	5.96	45.19	
45	8.48	10.85	13.07	14.56	14.85	13.63	10.90	7.86	5.57	4.07	4.04	5.46	7.84	10.63	13.64	15.83	16.64	16.01	13.87	10.90	8.00	6.17	5.46	5.74	46.19	
46	7.26	9.70	12.25	14.42	15.50	15.15	13.08	9.90	6.94	4.75	3.92	4.66	6.62	9.46	13.60	15.08	16.60	16.64	15.00	11.93	8.96	6.76	5.63	5.06	47.19	
47	5.54	7.84	10.54	13.30	15.12	15.66	13.08	9.90	6.94	4.75	4.25	5.52	7.84	10.68	13.68	15.84	16.68	15.86	13.15	10.22	7.36	5.65	4.23	4.46	48.20	
48	6.07	8.56	11.57	14.06	15.54	15.51	13.57	10.53	7.47	5.38	4.52	5.04	6.70	9.14	12.18	14.74	16.26	16.26	14.64	11.74	8.68	6.28	4.54	4.14	49.20	
49	5.07	7.06	9.74	12.44	14.55	15.46	14.76	12.57	9.68	7.24	4.58	5.60	8.40	10.77	13.32	15.42	16.26	15.47	13.18	10.24	7.54	5.62	4.54	4.69	50.21	
50	5.80	7.87	10.40	12.80	14.50	15.06	14.03	11.86	9.36	7.38	4.58	6.76	7.86	9.60	11.66	13.73	15.08	15.32	14.12	11.86	9.24	6.90	5.18	4.58	51.21	
51	5.06	6.46	8.24	10.33	12.41	13.80	14.34	13.41	11.46	9.33	8.05	7.40	7.66	8.58	9.92	11.68	13.36	14.16	12.82	10.83	8.73	6.87	5.45	4.92	52.22	
52	5.44	6.63	8.23	10.14	11.77	12.96	13.40	12.76	11.50	10.24	9.04	8.45	8.28	8.67	9.76	11.20	12.50	13.18	13.06	11.88	10.25	8.57	6.98	5.77	53.22	
53	5.38	5.64	6.37	7.82	9.54	11.17	12.38	13.02	12.96	12.16	11.07	10.02	8.94	8.44	8.48	9.27	10.44	11.57	12.34	12.34	11.70	10.50	8.90	7.32	54.23	
54	5.24	5.12	5.86	7.17	8.90	10.63	12.10	13.16	13.56	13.13	11.86	10.27	8.88	8.08	7.87	8.42	9.56	10.87	11.93	12.44	12.26	11.27	9.76	7.96	55.23	
55	6.27	5.06	4.55	5.02	6.47	8.52	10.67	12.72	14.14	14.86	14.44	12.70	10.66	8.80	7.60	7.21	7.64	9.18	11.00	12.40	13.36	13.52	12.60	10.86	56.23	
56	8.63	6.40	4.63	4.06	4.70	6.46	11.30	13.80	15.56	16.25	15.33	12.96	10.26	7.95	6.54	6.18	7.03	8.83	11.00	12.96	14.40	14.74	13.76	11.70	58.0	
57	8.84	6.08	4.05	3.42	4.14	6.18	8.80	12.06	14.93	16.76	17.15	15.84	12.87	9.66	7.00	5.18	5.12	6.26	8.52	11.16	13.67	15.38	15.86	14.57	59.0	
58	11.93	8.26	5.48	3.42	2.92	4.14	6.52	9.58	13.16	16.04	17.62	17.34	11.66	8.27	5.56	4.16	4.32	5.84	8.66	11.92	14.74	16.46	16.54	14.66	60.1	
59	11.26	7.66	4.94	3.20	3.27	4.70	7.52	10.86	14.63	17.06	17.98	16.96	13.90	10.20	6.96	4.47	3.56	4.02	6.04	9.40	12.86	15.55	16.86	16.36	61.1	
60	13.86	10.44	6.92	4.54	3.37	3.90	5.86	8.56	12.33	15.44	17.27	17.40	15.46	12.03	8.50	5.70	3.74	3.27	7.10	10.34	13.76	15.97	16.76	15.76	62.2	
61	12.96	9.44	6.74	4.67	4.23	5.26	7.43	10.37	13.82	16.13	17.08	16.40	13.86	10.50	7.26	4.84	3.56	3.86	5.60	8.27	11.55	14.34	16.02	16.28	63.2	
62	14.66	11.66	8.60	6.46	5.26	5.46	6.56	8.86	11.44	14.36	15.97	16.18	14.88	12.00	8.86	6.28	4.57	4.06	4.86	6.67	9.40	12.24	14.39	15.64	64.2	
63	15.33	10.46	8.22	6.76	6.34	7.00	8.36	10.22	12.44	14.42	15.27	14.71	12.72	10.14	7.72	5.93	4.86	5.00	6.10	8.03	10.30	12.47	13.97	14.58	65.3	
64	13.92	12.93	10.14	8.54	7.56	7.56	8.42	9.82	11.34	12.96	14.04	14.24	13.22	11.36	9.36	7.56	6.27	5.84	6.34	7.46	9.00	10.76	12.44	13.56	66.3	
65	13.74	12.74	11.40	10.07	9.16	8.96	9.77	10.46	11.36	12.44	13.07	13.03	12.12	10.46	8.86	7.68	7.02	7.02	7.66	8.54	9.66	10.96	12.24	13.88	67.4	
66	12.88	12.24	11.43	10.66	10.24	10.16	10.24	10.47	10.86	11.44	12.02	12.40	11.56	10.86	9.96	9.14	8.40	7.98	7.80	7.86	8.34	9.30	10.46	11.44	68.4	
67	12.46	12.67	12.27	11.74	11.26	10.87	10.56	10.36	10.22	10.36	10.76	11.26	11.38	11.10	11.10	10.78	10.32	8.86	7.97	7.28	7.26	7.87	8.97	10.32	69.5	
68	12.08	12.36	12.27	12.03	11.50	10.78	10.20	9.73	9.58	9.87	10.35	10.89	11.56	11.38	10.86	9.96	9.14	8.40	7.98	7.80	7.86	8.34	9.30	10.46	70.5	
69	11.56	12.46	13.04	13.10	12.54	11.68	10.56	9.64	9.08	8.82	9.16	9.88	11.10	11.10	11.10	10.78	10.32	8.86	7.97	7.28	7.26	7.87	8.97	10.32	71.6	
70	12.06	13.26	13.78	13.68	12.86	11.34	9.88	8.86	8.16	8.03	8.46	9.64	10.86	12.06	12.78	12.56	11.57	9.92	8.17	6.67	5.98	6.16	7.20	8.87	72.6	
71	10.76	12.70	14.08	14.61	14.06	12.53	10.68	8.96	7.55	6.88	7.05	8.07	9.84	11.76	12.97	13.54	13.03	11.46	9.42	7.27	5.74	5.30	6.44	7.44	73.6	
72	9.66	14.02	15.17	15.16	13.87	11.66	9.44	7.56	6.34	6.07	6.86	8.68	10.80	12.96	14.26	14.55	13.37	11.16	8.45	6.26	5.16	5.12	6.24	8.10	74.7	
73	10.63	13.22	15.15	15.86	15.17	13.22	10.40	7.86	6.06	5.25	5.54	6.90	9.24	11.72	13.95	15.20	15.12	13.39	10.64	7.57	5.44	4.44	4.96	6.46	75.7	
Sum	805.33	719.93	769.55	794.03	770.85	773.79	754.69	739.87	740.77	772.47	804.96	812.35	805.13	785.61	772.60	783.82	756.64	762.68	725.23	700.59	607.14	723.64	761.76	768.59	No. of Days. 749.81.	
No.	75	73	73	76	75	75	74	73	73	75	76	75	74	73	73	75	75	76	74	73	73	75	76	75	75	18362.04

FORMS FOR SHORT-PERIOD TIDES.  
 SERIES A.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
74	8.94	11.85	14.34	16.00	16.06	14.53	11.64	5.76	4.22	3.97	5.24	7.30	10.10	13.02	15.04	16.00	15.20	12.86	9.54	6.67	4.92	4.38	5.52	7.55	70 8	70 8
75	10.11	13.59	15.75	16.73	16.07	13.66	10.42	7.22	4.92	3.64	4.00	5.66	8.33	11.52	14.30	16.06	16.52	15.06	12.13	8.73	6.13	4.66	4.99	6.52	77 8	77 8
76	8.92	11.86	14.66	16.40	16.56	15.07	11.90	8.47	5.62	3.74	3.22	4.26	6.66	12.85	15.23	16.56	16.25	14.26	10.83	8.00	5.75	5.11	5.88	7.84	78 9	78 9
77	10.46	13.38	15.68	16.60	15.80	13.36	10.12	7.00	4.83	3.54	3.76	5.34	7.86	11.00	13.93	15.92	16.74	15.74	13.36	10.24	7.64	6.12	6.08	7.14	79 9	79 9
78	9.00	11.56	13.90	15.66	15.98	14.76	12.06	8.90	6.13	4.34	3.62	4.36	6.06	8.47	11.31	13.87	15.62	16.12	14.97	10.02	8.05	6.96	7.06	7.93	80 10	80 10
79	9.67	12.07	14.08	15.23	15.08	13.57	11.16	8.26	6.08	4.76	4.47	5.46	7.26	9.48	11.88	13.90	15.36	15.50	14.06	12.67	10.54	8.74	7.94	8.14	81 10	81 10
80	9.06	10.62	12.40	13.77	14.52	14.20	12.80	10.64	8.47	6.76	5.86	5.82	6.49	7.75	9.52	11.71	13.54	14.73	14.90	14.06	12.63	11.05	9.70	8.86	82 10	82 10
81	8.72	10.24	11.76	13.06	13.60	13.34	12.06	10.56	8.92	7.40	6.43	6.30	6.68	7.68	9.46	11.24	13.02	14.08	14.52	14.22	13.04	11.70	10.34	9.24	83 11	83 11
82	8.84	9.04	9.84	10.96	12.05	12.86	12.96	12.44	11.22	9.67	8.30	7.06	6.48	6.64	7.48	8.86	10.64	12.34	13.74	14.48	14.44	13.62	12.12	10.36	84 11	84 11
83	8.96	8.11	7.96	8.44	9.76	11.26	12.92	12.78	11.94	10.50	8.78	7.20	6.06	5.92	6.72	8.34	10.26	12.20	13.86	15.00	15.14	14.16	12.20	9.88	85 12	85 12
84	8.00	6.90	6.56	7.46	9.22	11.16	12.56	13.57	14.06	13.37	11.72	9.38	7.17	5.72	5.38	6.17	7.82	10.00	12.50	14.54	15.84	15.94	14.64	12.14	86 12	86 12
85	9.36	6.97	5.74	5.63	6.67	8.88	11.24	13.46	14.86	15.36	14.34	12.05	9.44	5.38	5.00	5.82	7.83	10.50	13.30	15.60	16.72	16.28	14.37	11.37	87 13	87 13
86	8.36	6.00	4.67	4.80	6.40	9.20	12.06	14.62	16.12	16.16	14.90	12.22	9.12	6.60	5.05	4.86	5.87	8.10	11.14	14.15	16.35	17.15	16.24	13.58	88 13	88 13
87	10.14	7.06	4.83	3.96	4.70	6.72	9.92	13.20	15.64	17.04	16.75	14.92	11.81	8.56	6.27	5.14	5.64	6.94	9.43	12.61	17.03	17.08	15.36	11.92	89 14	89 14
88	8.64	6.18	4.48	4.25	5.24	7.57	11.00	14.10	16.43	17.34	16.56	14.28	10.82	7.84	5.95	5.42	6.12	7.87	10.62	13.66	16.10	17.14	16.46	13.96	90 14	90 14
89	10.44	7.12	4.80	3.83	4.41	6.43	8.78	12.04	14.74	16.66	17.13	15.64	12.86	9.53	7.16	5.81	5.93	7.22	9.26	12.02	14.66	16.44	16.67	15.06	91 14	91 14
90	12.02	8.56	4.04	3.84	4.93	7.24	10.09	13.22	15.56	16.90	16.56	14.74	11.68	8.84	7.02	6.48	7.04	8.26	10.50	13.00	14.94	15.83	15.12	12.94	92 15	92 15
91	9.87	7.14	5.16	4.22	4.76	6.40	8.73	11.37	14.00	15.82	16.34	15.34	13.10	10.40	8.36	7.32	7.28	8.03	9.50	11.53	13.48	14.74	14.92	13.67	93 15	93 15
92	11.34	8.76	6.67	5.40	5.22	6.16	7.85	12.30	14.30	15.48	15.46	14.27	12.24	10.20	8.78	8.26	8.47	9.24	10.52	12.04	13.48	14.16	13.84	12.27	94 16	94 16
93	10.16	8.14	6.47	5.74	6.22	7.44	9.20	10.85	12.64	14.05	14.67	14.27	12.97	11.44	10.04	9.16	8.84	9.16	9.84	10.95	11.96	12.80	12.96	12.28	95 16	95 16
94	10.94	9.24	7.80	6.78	6.70	7.30	8.37	9.54	10.90	12.34	13.52	12.98	12.66	12.42	11.07	10.34	9.94	9.77	9.87	10.56	11.44	11.92	12.05	11.54	96 17	96 17
95	10.36	9.16	8.12	7.47	7.44	7.87	8.52	9.46	10.73	11.93	12.74	12.98	12.66	12.42	11.96	11.34	10.55	9.91	9.34	9.47	9.52	10.94	11.12	98 18	98 18	
96	10.92	10.30	9.34	8.36	7.74	7.58	7.98	8.76	9.87	11.04	11.96	12.50	12.66	12.42	12.40	11.47	10.50	9.62	8.94	8.54	8.74	9.48	10.45	11.36	99 18	99 18
97	11.02	10.62	10.00	9.22	8.40	8.01	8.13	8.63	9.70	10.66	11.77	12.66	13.06	13.82	13.66	12.66	11.42	10.02	8.72	7.96	7.82	8.36	9.47	10.86	100 18	100 18
98	11.88	11.89	11.44	10.50	9.40	8.46	7.84	7.76	8.43	9.46	11.08	12.70	14.00	14.86	14.22	12.80	10.96	8.88	7.46	6.81	6.84	7.92	9.62	11.52	101 19	101 19
99	11.90	12.70	12.87	12.44	11.06	9.52	7.48	6.74	6.92	7.97	9.72	11.72	13.58	14.86	15.12	14.21	12.35	9.67	7.47	5.98	5.58	6.14	7.76	9.84	102 19	102 19
100	13.00	13.97	14.12	13.00	11.02	9.05	7.48	6.66	6.46	7.88	10.06	12.53	14.55	15.72	15.49	13.80	11.08	8.22	5.93	4.52	4.32	5.47	7.72	10.54	103 20	103 20
101	12.16	14.02	15.18	15.06	13.40	10.95	8.28	6.02	5.40	6.24	8.22	10.70	13.40	15.52	16.25	15.36	12.80	9.46	6.56	4.47	3.91	5.74	7.74	10.54	104 20	104 20
102	13.27	15.36	16.20	15.32	13.00	9.88	7.34	5.76	5.40	6.24	8.22	10.70	13.40	15.52	16.25	15.36	12.80	9.46	6.56	4.47	3.91	5.74	7.74	10.54	105 20	105 20
103	11.40	14.40	16.28	16.72	15.47	12.68	9.44	6.81	5.47	5.38	6.52	8.91	11.80	14.40	16.08	14.35	11.30	7.80	4.97	2.93	2.46	3.76	6.21	9.51	105 21	105 21
104	12.97	15.38	17.14	17.04	14.94	11.68	8.36	6.14	5.06	5.57	7.24	10.97	13.10	15.40	16.44	15.82	13.44	9.74	6.67	4.03	2.50	2.77	4.44	7.50	106 21	106 21
105	10.96	14.33	16.70	17.72	16.91	14.37	10.87	8.10	6.15	5.71	6.50	8.36	11.33	14.12	15.97	16.50	15.10	12.22	8.67	5.24	2.56	3.47	5.74	8.64	107 22	107 22
106	12.02	13.12	16.94	17.54	16.24	13.40	10.32	7.62	6.17	6.07	7.04	9.13	12.00	14.47	15.69	15.54	13.66	10.74	7.44	4.88	3.28	3.04	4.36	6.67	108 22	108 22
107	9.40	12.47	15.00	16.74	16.94	15.60	13.03	10.01	7.87	6.76	6.80	7.71	9.70	12.14	14.15	15.02	14.50	12.53	9.92	7.24	5.36	4.17	4.16	5.20	108 22	108 22
108	7.36	9.86	12.40	14.57	15.77	15.74	14.47	13.12	9.90	8.07	7.14	7.11	9.54	11.58	13.16	13.74	13.28	11.76	9.56	5.96	4.93	5.02	5.86	110 23	110 23	

109	7.52	9.74	12.00	13.87	14.87	14.77	13.76	12.06	10.26	8.74	7.82	7.54	8.00	9.34	11.00	12.36	12.96	12.72	11.58	10.14	8.48	6.94	5.96	111	23	
110	6.60	7.87	9.72	11.62	13.34	14.34	14.44	13.66	12.26	9.10	8.03	7.66	7.76	8.68	10.20	11.63	12.43	12.66	12.10	10.96	9.47	8.14	7.03	6.54	113	0
111	6.88	7.94	9.57	11.42	13.00	14.07	14.44	13.93	12.76	11.00	9.18	7.74	6.96	6.96	7.85	9.40	10.96	12.36	13.66	13.12	12.22	10.65	8.87	7.52	114	0
112	6.74	6.84	7.66	9.26	11.04	12.88	14.12	14.66	14.30	13.64	10.64	8.60	6.78	5.94	5.93	9.00	11.04	12.64	13.72	13.87	12.97	11.36	9.32	7.66	115	1
113	6.62	6.47	7.28	8.88	10.96	12.96	14.54	15.17	14.54	12.77	10.22	7.74	5.76	4.88	5.14	6.58	8.88	11.33	13.36	14.66	14.94	13.86	11.70	9.34	116	1
114	7.26	6.22	6.20	7.24	9.00	11.22	13.36	14.86	15.37	14.44	12.10	9.16	6.48	4.70	4.20	4.74	6.70	9.17	11.77	14.02	15.54	14.03	11.54	9.34	117	2
115	6.96	6.07	6.34	7.48	9.44	11.96	14.10	15.28	15.44	13.84	10.92	7.66	5.31	3.77	3.70	5.12	7.30	10.10	12.94	15.14	16.26	15.76	13.86	11.00	118	2
116	8.24	6.47	5.97	6.34	7.98	10.16	12.70	14.64	15.66	14.96	12.70	9.46	6.57	4.32	3.42	4.04	5.80	8.48	11.42	14.32	16.17	16.57	15.46	12.94	119	2
117	10.06	7.64	6.16	6.36	6.82	8.40	10.90	13.45	15.07	15.35	13.81	11.00	7.70	5.15	3.44	3.36	4.67	6.96	9.52	12.56	14.92	16.36	16.28	14.70	120	3
118	9.06	7.20	6.40	6.70	7.74	9.37	11.47	13.86	15.04	15.06	12.96	9.74	7.17	4.24	3.42	4.04	5.68	8.27	10.68	13.46	15.48	16.25	15.62	13.50	121	3
119	10.32	8.22	6.72	6.40	7.02	8.34	10.44	12.60	14.45	14.53	13.26	10.82	7.87	5.57	3.94	3.86	4.88	6.80	9.18	11.76	14.24	15.56	15.54	14.30	122	4
120	9.46	7.76	6.94	7.06	7.86	9.36	11.24	13.06	13.96	13.66	11.90	9.20	6.72	5.07	4.36	4.90	6.32	8.22	10.36	12.80	14.56	15.43	14.76	13.04	123	4
121	10.84	8.96	7.76	7.44	7.76	8.80	10.26	11.94	13.06	13.30	12.28	10.40	8.28	6.46	5.35	6.00	7.54	9.26	11.42	13.34	14.60	14.86	13.86	12.06	124	5
122	10.14	8.84	8.15	8.06	8.40	9.36	10.62	11.94	12.68	12.46	11.36	9.58	7.94	6.74	6.04	6.20	7.12	8.46	10.24	12.10	13.38	14.08	13.92	12.90	125	5
123	11.41	10.00	8.90	8.46	8.56	9.00	9.74	10.55	11.36	11.86	11.68	10.72	9.26	7.86	6.96	6.92	7.44	8.22	9.26	10.47	12.10	13.78	13.40	12.16	126	6
124	10.87	9.94	9.24	8.96	8.94	9.17	9.58	10.34	10.96	11.44	11.34	10.58	9.56	8.46	7.76	7.66	7.97	8.66	9.74	10.97	12.22	13.24	13.54	13.24	127	6
125	12.12	10.96	9.98	9.27	8.94	8.74	8.80	9.24	10.03	10.80	11.26	11.29	10.79	10.06	9.26	8.46	8.06	8.04	8.56	9.72	10.94	12.20	12.96	13.22	128	6
126	12.94	12.14	11.17	8.96	8.20	7.92	8.00	8.62	9.56	10.46	11.34	11.77	11.44	10.76	9.74	8.58	8.17	8.10	8.66	9.60	10.93	12.30	13.21	13.50	129	7
127	13.18	12.36	11.16	9.68	8.30	7.26	6.90	7.45	8.52	10.00	11.40	12.36	12.92	12.66	11.62	10.20	8.85	8.06	7.83	8.24	9.37	10.96	12.50	13.57	130	7
128	14.02	13.54	12.37	10.74	8.97	7.34	6.24	5.98	6.71	10.20	12.12	13.50	14.22	13.67	12.20	10.16	8.55	7.53	7.27	7.93	9.36	11.30	13.16	14.36	131	8
129	14.66	13.94	12.24	9.97	7.60	5.85	4.92	5.06	6.42	8.00	10.95	13.28	14.84	15.34	14.46	12.38	10.01	8.14	6.95	6.90	8.01	9.74	11.84	13.66	132	8
130	14.84	15.16	14.10	11.76	8.83	6.14	4.18	3.66	4.53	6.46	9.08	11.92	14.30	15.96	16.28	14.95	9.36	7.14	6.17	6.50	7.92	10.02	12.44	14.46	133	9
131	15.64	15.47	13.76	10.66	7.20	4.46	2.86	2.74	4.17	6.63	9.77	13.00	15.72	17.16	16.96	15.18	11.90	8.78	6.57	5.95	6.52	7.94	10.30	12.84	134	9
132	15.02	15.97	15.24	12.56	8.86	5.70	3.17	1.97	2.43	4.23	7.22	10.62	13.96	16.30	17.09	17.06	14.58	10.90	8.02	5.94	5.46	6.30	10.90	13.74	135	10
133	15.64	16.06	14.62	11.54	7.86	4.52	2.14	1.42	2.56	5.03	8.20	11.45	14.68	16.97	17.83	16.77	14.06	10.36	6.60	5.84	5.52	6.20	11.20	13.60	136	10
134	14.02	15.72	15.74	13.76	10.48	6.92	4.07	2.24	1.86	3.24	5.60	8.58	12.24	15.14	17.10	17.74	16.33	13.21	10.00	7.30	5.76	5.60	6.58	8.80	137	10
135	11.97	14.34	15.47	12.82	9.66	6.56	4.08	2.67	2.88	4.46	6.78	9.77	12.92	15.50	17.10	17.16	15.40	12.67	9.57	7.36	6.16	6.11	7.20	9.40	138	11
136	12.06	14.14	14.98	14.36	12.18	9.28	6.58	4.76	3.86	4.30	5.66	7.78	10.44	13.15	15.36	16.23	14.86	11.94	9.56	7.54	6.48	6.38	7.36	10.91	139	11
137	9.30	11.76	13.38	13.98	13.42	11.66	9.36	7.30	5.74	4.98	6.33	8.08	10.42	12.87	14.66	15.72	15.46	14.00	11.78	9.46	7.72	6.96	6.82	7.44	140	12
138	8.91	10.74	12.30	13.13	12.92	11.76	10.08	8.18	6.84	6.28	6.46	7.26	8.54	10.38	12.48	14.22	14.94	14.74	13.52	11.62	9.46	7.84	6.86	6.52	141	12
139	6.83	8.02	9.54	11.12	12.28	12.53	12.07	10.86	9.35	7.86	6.87	6.74	7.36	8.54	10.16	11.80	14.14	13.98	12.92	11.14	9.14	7.48	6.36	5.86	142	13
140	5.93	7.12	8.94	10.74	12.22	12.86	12.65	11.60	10.06	8.56	7.47	7.24	7.70	8.44	10.00	11.62	13.06	13.93	13.82	12.68	10.82	9.01	7.20	5.72	143	13
141	5.17	5.56	6.97	8.92	10.90	12.46	13.44	13.42	12.46	10.72	9.12	8.02	7.47	7.63	8.26	9.76	11.56	13.14	14.02	13.96	12.62	10.76	6.66	5.32	144	14
142	4.84	5.46	7.38	9.67	11.66	13.40	14.34	14.36	13.24	11.36	9.64	8.16	7.52	7.50	8.44	10.16	11.93	13.46	14.20	13.97	12.62	10.50	7.84	5.72	145	14
143	4.46	4.54	5.90	7.82	10.17	12.67	14.36	15.22	14.76	13.34	11.12	9.16	7.84	7.36	7.72	8.72	10.32	12.06	13.66	14.36	13.76	11.92	9.27	6.82	146	14
144	4.82	3.97	4.57	6.16	11.03	13.46	15.10	15.52	14.67	12.94	10.67	8.77	7.60	7.38	7.93	9.10	10.86	12.73	14.28	14.53	13.00	10.66	7.86	5.58	147	15
145	4.22	4.13	5.24	7.24	9.70	12.30	14.40	15.74	15.70	14.12	12.14	9.74	8.36	7.64	7.54	8.20	9.70	11.80	13.62	14.54	14.16	12.22	9.68	6.84	148	15
Sum	729.58	750.10	763.88	784.78	781.80	743.68	751.85	738.00	744.66	730.62	713.40	709.54	723.28	764.02	763.26	798.01	779.57	774.97	780.57	784.90	788.60	766.78	739.39	724.67	No. of Days.	
No.	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	73d 8m.	

FORMS FOR SHORT-PERIOD TIDES.  
 SERIES λ.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
146	4.84	3.94	4.50	6.00	8.33	10.94	13.60	15.42	16.13	15.62	13.90	9.28	7.84	7.40	7.74	8.92	10.62	12.60	14.02	14.27	13.22	10.78	8.10	5.76	149 16	
147	4.57	4.17	5.26	7.20	9.70	12.28	14.66	15.94	16.04	14.86	12.64	10.27	8.44	7.54	7.34	8.10	9.52	11.55	13.36	14.27	13.92	12.06	9.48	6.90	150 16	
148	5.12	4.32	4.97	6.54	8.70	11.00	13.46	15.32	16.07	15.67	14.17	11.77	9.56	8.16	7.68	7.83	8.74	12.26	13.66	14.02	12.96	10.86	8.34	6.24	151 17	
149	5.04	4.82	5.84	7.60	9.46	11.87	14.10	15.30	15.60	14.66	12.78	10.74	9.03	7.96	7.73	8.24	9.44	11.07	12.62	13.44	13.16	11.96	9.94	7.67	152 17	
150	6.16	5.18	5.56	6.86	8.64	10.66	12.74	14.30	15.12	15.06	13.65	11.84	10.00	8.46	7.75	7.78	8.46	9.92	11.36	12.37	12.84	12.22	10.98	7.32	153 18	
151	6.03	5.94	6.87	8.17	9.67	11.58	13.28	14.64	14.97	14.22	12.62	11.08	9.47	8.38	8.08	8.30	9.20	10.24	11.40	12.12	12.46	11.72	10.38	8.77	154 18	
152	7.37	6.70	6.91	7.78	8.83	10.30	11.90	13.54	14.68	14.80	13.77	12.16	10.50	9.20	8.47	8.28	8.60	9.36	10.36	11.26	11.83	12.05	11.56	10.60	155 18	
153	9.20	8.14	7.72	7.83	8.62	11.10	12.64	13.94	14.46	14.16	13.26	11.74	10.42	9.26	8.54	8.34	8.46	9.23	10.10	10.93	11.70	11.97	11.72	11.06	156 19	
154	9.98	8.86	8.32	8.36	8.78	9.20	10.37	11.54	12.92	13.86	14.25	12.88	11.48	10.08	8.98	8.20	8.20	8.37	9.12	10.03	11.29	12.14	12.58	12.36	157 19	
155	11.84	11.02	10.06	9.23	8.78	9.20	10.37	11.54	12.92	13.86	14.25	12.88	11.48	10.08	8.98	8.20	8.20	8.37	9.12	10.03	11.29	12.14	12.58	12.36	158 20	
156	13.28	12.03	10.56	9.66	9.64	10.17	11.38	12.77	13.98	14.67	15.14	14.88	13.86	12.46	10.48	8.82	7.82	7.50	8.19	9.46	11.28	13.22	14.76	15.82	159 20	
157	15.76	14.97	13.34	11.70	10.67	10.27	10.56	11.52	12.90	14.12	15.30	15.65	15.48	14.17	12.02	9.86	8.00	6.85	7.72	9.34	11.40	13.77	15.84	16.86	160 21	
158	16.85	15.70	13.60	11.52	9.95	9.55	9.80	10.84	12.57	14.21	15.47	16.06	15.22	13.50	10.84	8.22	6.16	4.95	5.15	6.50	8.61	11.37	14.18	16.48	161 21	
159	17.54	17.17	15.60	12.50	10.07	8.34	8.17	8.96	10.27	12.23	14.24	15.74	16.29	15.33	12.77	9.46	6.32	4.44	3.62	4.30	6.30	8.54	11.95	17.28	162 22	
160	17.95	17.20	15.02	11.76	9.04	7.44	7.22	7.81	9.55	12.08	14.34	16.07	16.21	14.76	11.87	8.16	5.97	3.07	2.74	3.80	5.94	9.24	12.80	15.92	163 22	
161	18.07	18.53	17.65	14.65	10.90	8.00	6.62	6.55	7.50	9.65	12.45	14.89	16.40	16.14	14.28	10.90	7.10	4.31	2.62	2.37	3.68	6.30	9.76	13.48	164 22	
162	16.44	18.12	18.40	17.00	10.17	7.55	6.30	6.18	7.30	9.60	12.79	15.16	16.42	15.96	13.80	10.33	6.77	4.00	2.33	2.54	4.18	7.11	10.40	13.95	165 23	
163	16.74	17.85	17.95	16.97	12.81	9.60	7.05	5.72	5.77	7.00	9.56	12.80	15.12	16.05	15.26	12.76	9.20	6.14	3.95	2.88	3.47	5.52	7.93	11.04	166 23	
164	14.21	16.44	17.72	17.40	15.44	12.07	9.02	6.70	5.67	5.93	7.41	13.02	14.92	15.57	14.68	12.28	9.20	6.52	4.77	4.20	4.94	6.52	8.80	11.67	168 0	
165	14.34	16.42	17.20	16.60	14.54	11.30	8.66	6.74	6.05	6.16	7.65	10.05	12.50	14.32	14.85	14.05	11.96	9.47	7.26	6.06	5.80	6.39	7.66	9.64	169 0	
166	11.92	14.25	15.90	16.46	15.74	13.76	10.84	8.61	6.86	6.32	6.58	7.80	9.82	12.04	13.55	14.17	13.54	12.40	10.90	9.62	8.66	8.31	8.49	9.05	171 1	
167	12.12	14.20	15.46	15.44	14.58	12.66	10.40	8.31	7.04	6.60	6.77	7.78	9.32	11.22	12.80	13.58	13.46	12.40	10.90	9.62	8.66	8.31	8.49	9.05	171 1	
168	10.30	12.04	13.70	14.74	14.75	13.73	12.02	10.10	8.46	7.12	6.53	6.70	7.50	9.03	10.90	12.32	13.20	13.38	12.92	11.94	10.67	9.60	8.94	9.24	172 2	
169	10.33	11.90	13.24	14.06	14.10	13.34	11.84	10.05	8.26	6.94	6.44	6.67	7.49	9.06	10.86	12.50	13.66	14.10	13.63	12.46	11.06	10.06	9.30	9.05	173 2	
170	9.33	10.22	11.60	13.90	13.82	13.85	13.08	11.64	9.76	8.00	6.70	6.08	6.22	7.28	9.00	10.94	12.77	14.05	14.63	14.17	12.86	11.33	10.04	9.14	174 2	
171	8.86	9.20	10.08	11.26	12.44	13.30	12.80	11.60	8.85	7.06	5.67	5.05	5.60	7.15	9.26	11.30	13.28	14.45	14.84	13.95	12.40	10.90	9.46	8.62	175 3	
172	8.24	8.56	9.64	11.12	12.55	13.40	13.37	12.07	10.07	8.20	6.17	4.94	4.74	5.62	7.74	9.76	12.14	14.01	15.00	14.86	13.77	12.06	10.27	8.84	176 3	
173	8.10	7.94	8.52	9.68	11.18	12.64	13.37	13.05	11.52	9.17	6.76	5.11	4.64	6.10	8.00	10.50	12.90	14.56	15.33	14.70	13.32	11.14	9.44	8.17	177 4	
174	7.54	7.30	8.34	9.81	11.65	13.20	13.60	12.56	10.40	7.97	5.83	4.38	4.04	6.10	8.00	10.50	12.90	14.56	15.24	14.56	12.56	10.36	8.63	7.79	179 5	
175	7.62	7.30	7.74	8.86	10.67	12.47	13.67	13.60	12.02	9.66	6.93	4.96	3.94	4.22	5.70	7.84	10.40	12.82	15.56	15.33	13.80	11.44	9.35	7.79	179 5	
176	7.04	7.03	7.90	9.44	11.66	13.22	13.92	13.00	10.74	8.00	5.64	4.04	3.83	4.76	6.70	9.02	11.37	14.74	15.12	15.46	14.48	12.44	9.96	8.16	180 5	
177	6.86	6.42	6.94	8.42	10.44	12.57	13.67	13.68	12.22	9.64	6.86	4.96	3.98	4.36	5.65	7.72	10.02	12.26	14.31	15.28	15.12	13.77	11.30	9.01	181 6	
178	6.64	6.56	7.46	9.06	11.01	13.20	13.51	13.01	11.07	8.44	6.12	4.72	4.42	5.32	6.94	8.97	11.17	13.22	14.74	15.17	14.22	12.16	9.74	7.86	182 6	
179	6.74	6.51	7.07	8.16	9.92	11.66	12.82	13.10	11.86	9.72	7.36	5.70	5.02	5.24	6.42	8.07	10.12	11.98	13.73	14.86	14.72	13.40	11.17	9.22	183 6	
180	7.55	6.51	6.51	7.34	8.72	10.61	12.77	12.64	11.22	9.34	7.48	6.30	5.87	6.54	7.66	9.24	10.97	12.94	14.38	14.30	12.50	10.34	8.44	8.44	184 7	



FORMS FOR SHORT-PERIOD TIDES.  
 SERIES A.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
219	17.76	14.76	10.60	7.27	5.06	4.48	5.07	7.18	10.36	13.94	16.34	17.16	16.04	13.12	9.20	5.80	3.36	2.56	3.60	5.73	9.03	12.78	15.94	17.78	17.78	224 0
220	18.04	16.74	13.32	9.36	6.95	4.18	3.80	4.90	7.56	11.10	14.46	16.66	16.88	15.39	12.15	8.23	5.44	3.52	3.32	4.48	7.04	10.14	13.35	16.16	17.52	225 1
221	17.26	15.28	11.80	8.22	5.32	3.80	4.02	5.58	8.40	11.50	14.52	16.18	16.06	14.38	11.26	7.98	5.62	4.54	4.80	6.25	8.27	11.00	13.96	16.32	17.52	226 1
222	17.26	16.42	14.32	10.85	7.62	5.16	4.10	4.64	6.45	8.92	12.05	14.70	15.80	15.18	13.36	10.62	7.94	6.32	5.74	6.44	7.77	9.72	12.07	14.12	17.12	227 1
223	15.66	14.46	12.06	9.36	6.96	5.40	5.07	5.84	7.33	9.54	11.87	13.60	14.46	13.96	12.48	10.40	8.65	7.45	7.28	8.00	9.26	10.72	12.27	13.74	17.28	228 2
224	14.47	14.18	12.78	10.82	8.78	6.78	5.83	6.68	6.74	8.34	10.14	12.02	13.26	13.57	12.85	11.76	10.70	9.74	9.12	8.90	9.34	10.06	10.94	12.10	17.28	229 2
225	13.88	13.72	13.38	11.88	10.06	8.17	7.02	7.00	7.70	8.77	10.10	11.44	12.33	12.66	12.46	12.00	11.36	10.62	10.07	9.67	9.77	10.12	10.82	11.54	17.28	230 3
226	12.43	12.67	12.12	11.23	9.96	8.64	7.77	7.46	7.69	8.30	9.04	10.10	11.17	12.34	12.90	12.90	12.34	11.72	11.15	10.62	10.30	10.00	10.14	10.50	17.28	231 3
227	11.34	11.96	12.26	11.97	11.38	10.53	9.44	8.35	7.66	7.57	8.12	9.06	10.48	12.72	13.42	13.56	13.18	12.30	11.45	10.72	10.26	9.92	9.63	10.00	17.28	232 4
228	10.71	11.63	12.32	12.18	11.42	10.36	9.08	8.15	7.53	7.24	7.70	8.54	9.82	11.43	12.72	13.64	13.66	13.26	12.36	11.22	10.18	9.34	8.97	9.08	17.28	233 4
229	9.88	10.76	11.64	12.26	12.35	11.85	10.40	8.78	7.36	6.44	6.28	7.14	8.37	10.20	11.94	13.38	14.40	14.54	13.58	12.17	10.70	9.34	8.82	8.84	17.28	234 5
230	10.00	11.16	12.50	13.30	13.42	12.06	10.16	8.40	6.86	6.06	6.14	7.20	8.95	10.80	12.76	13.96	14.91	14.84	13.64	11.84	9.97	8.77	8.36	8.48	17.28	235 5
231	8.96	10.06	11.36	13.12	13.97	13.64	12.06	9.70	7.27	5.96	5.56	6.35	7.80	9.76	11.70	13.66	15.10	15.46	14.62	12.86	10.37	8.64	7.46	7.31	17.28	236 5
232	7.76	8.84	10.72	14.21	14.62	13.44	11.00	8.24	6.24	5.17	5.36	6.34	8.54	10.66	13.00	15.02	15.96	15.50	14.08	11.60	8.97	7.34	6.70	6.84	17.28	237 6
233	7.80	9.62	11.70	13.76	14.95	14.67	12.76	10.00	7.37	5.56	4.97	5.74	7.38	9.36	11.94	14.36	16.04	16.27	15.32	13.08	10.11	7.72	6.36	6.10	17.28	238 6
234	6.94	8.63	10.83	13.20	15.21	15.71	14.43	11.89	8.54	4.97	5.06	6.36	8.22	10.64	13.40	15.80	16.62	16.16	14.21	11.38	8.34	6.35	5.46	5.74	17.28	239 7
235	7.13	9.22	11.84	14.36	15.71	15.48	13.64	10.66	7.60	5.70	4.96	5.70	7.24	9.54	12.62	14.56	16.24	16.56	15.34	12.80	9.60	7.06	5.50	5.18	17.28	240 7
236	5.94	7.72	10.28	13.04	15.14	15.90	14.88	12.52	9.63	7.07	5.74	5.64	6.67	8.36	13.17	15.30	16.38	15.97	14.06	11.04	8.16	6.11	5.05	5.41	17.28	241 8
237	6.72	8.83	11.26	13.77	15.36	15.38	14.00	11.50	8.72	6.86	5.97	6.34	7.52	9.30	11.47	13.80	15.46	15.84	14.77	12.44	9.37	7.06	5.37	4.85	17.28	242 8
238	5.64	7.12	9.24	11.64	13.96	15.06	14.75	13.17	10.76	8.64	7.30	6.86	7.44	8.64	10.38	12.36	14.06	14.44	13.86	12.35	10.02	8.06	6.46	5.62	17.28	243 9
239	6.34	7.85	9.86	11.96	13.64	14.58	14.07	12.68	10.68	8.97	8.02	7.81	8.36	9.26	10.60	12.24	13.73	14.44	13.46	13.08	11.68	9.86	8.26	6.87	17.28	244 9
240	5.78	6.47	7.80	9.63	11.38	12.97	13.74	13.44	12.44	11.04	9.83	8.84	8.57	8.87	9.67	10.67	11.96	13.06	13.46	13.08	11.68	9.86	8.26	6.87	17.28	245 9
241	6.17	6.26	8.17	9.66	11.26	12.55	13.37	13.57	12.94	11.92	10.73	9.67	9.16	9.18	9.63	10.54	11.48	12.46	12.92	12.66	11.74	10.42	8.87	7.44	17.28	246 10
242	6.44	6.21	6.66	7.76	9.20	10.76	12.36	13.54	14.95	13.67	12.68	11.26	10.02	9.22	8.90	9.14	9.86	10.86	12.02	12.84	12.98	12.36	11.16	9.57	17.28	247 10
243	7.60	6.24	5.63	5.97	6.24	7.17	8.80	10.66	12.80	14.74	13.66	11.85	10.04	8.66	8.02	8.14	9.04	10.38	12.00	13.14	13.74	13.40	12.04	10.04	17.28	248 11
244	10.18	7.37	5.17	3.90	4.03	5.50	7.96	10.88	13.80	16.04	15.74	14.33	11.96	9.30	7.37	6.55	6.70	8.06	9.98	12.06	13.93	14.86	14.44	12.80	249 11	
245	9.94	6.63	4.34	3.17	2.53	5.38	8.20	11.40	14.56	16.82	17.44	16.36	13.83	9.98	6.20	4.46	3.84	4.58	6.80	10.06	13.28	15.76	16.64	15.75	250 12	
246	12.94	9.26	6.06	3.66	2.67	3.72	5.66	8.70	12.20	15.53	17.33	17.53	15.87	12.42	8.56	5.32	3.44	3.17	4.55	7.26	14.22	16.50	17.05	15.47	251 12	
247	12.37	8.44	5.52	3.48	3.10	4.46	6.74	9.94	13.47	16.22	17.47	17.02	14.77	10.84	7.23	4.52	3.00	3.30	5.07	8.06	11.72	14.94	16.86	16.90	252 13	
248	14.91	11.54	8.00	5.38	3.90	4.20	5.52	7.95	11.06	14.30	16.51	17.04	15.88	12.99	9.17	5.97	3.70	2.94	3.94	6.16	9.14	12.45	15.42	16.68	253 13	
249	16.10	13.81	10.56	5.47	4.87	5.60	7.04	9.54	12.25	14.81	16.16	16.06	14.44	11.97	7.87	5.34	3.84	3.92	5.16	7.43	10.36	13.44	15.47	16.04	254 14	
250	14.92	12.66	9.98	7.74	6.47	6.36	7.02	8.54	10.58	12.80	14.58	15.36	14.73	12.52	9.86	7.17	5.31	4.44	5.02	6.44	8.50	11.04	13.56	14.79	255 14	
251	14.71	13.46	11.46	9.44	8.00	7.36	7.56	8.36	9.51	12.60	13.73	13.94	12.90	11.02	8.73	6.90	5.70	5.63	6.34	7.60	9.14	11.36	13.14	14.88	256 15	
252	13.66	12.43	10.94	9.64	8.76	8.44	8.70	9.18	9.95	10.88	12.06	12.76	12.71	11.64	9.87	8.36	7.04	6.44	6.67	7.34	8.36	9.74	11.16	12.22	257 15	
253	13.66	12.43	10.94	9.64	8.76	8.44	8.70	9.18	9.95	10.88	12.06	12.76	12.71	11.64	9.87	8.36	7.04	6.44	6.67	7.34	8.36	9.74	11.16	12.22	258 15	



254	12.70	12.20	11.38	10.60	9.88	9.34	9.16	9.13	9.34	9.87	10.66	11.30	11.62	11.37	10.56	9.48	7.52	7.14	7.33	7.86	8.66	9.84	10.96	11.62	259 16	
255	11.97	11.87	11.54	11.08	10.42	9.92	9.60	9.42	9.54	9.86	10.24	10.70	10.91	10.80	10.34	9.74	9.06	8.35	7.72	7.46	7.67	7.84	8.44	9.64	10.73	260 16
256	11.52	11.88	12.06	11.88	11.53	10.97	10.23	9.48	9.04	9.01	9.38	10.01	10.64	11.03	11.18	10.94	10.46	9.52	8.56	7.74	7.42	7.42	8.34	9.42	10.67	261 17
257	11.65	12.46	12.82	12.62	12.04	10.96	9.85	8.96	8.34	8.42	8.86	9.64	10.44	11.23	11.67	11.60	10.92	9.74	8.36	7.26	6.68	6.86	7.74	9.24	262 17	
258	10.86	12.34	13.24	13.55	13.17	12.08	10.64	9.21	8.06	7.54	7.74	8.74	9.92	11.30	12.38	12.82	12.42	11.17	9.62	7.86	6.55	6.10	6.54	7.88	263 17	
259	9.68	11.56	13.16	14.06	13.18	11.60	9.86	8.07	6.91	6.64	7.14	8.38	10.20	11.92	13.16	13.44	12.50	10.70	8.70	6.90	5.75	5.50	6.36	8.04	264 18	
260	10.20	12.32	13.87	14.64	14.36	12.87	10.73	8.45	6.71	5.90	6.17	7.29	9.02	11.07	13.02	14.14	14.04	12.68	10.30	7.96	6.07	5.14	5.48	6.87	265 18	
261	9.06	11.46	13.68	15.18	15.37	14.28	12.24	9.67	7.34	5.74	6.12	7.84	9.97	12.54	14.50	15.33	14.46	12.23	9.34	6.94	5.36	4.94	5.94	8.06	266 19	
262	10.08	12.62	14.76	15.76	15.26	13.46	10.67	7.88	5.74	4.48	4.66	6.00	8.44	11.24	13.97	15.67	15.66	14.20	11.46	8.47	6.20	4.97	5.22	6.65	267 19	
263	8.86	11.34	14.06	15.76	16.07	14.86	12.14	9.06	6.37	4.56	3.93	4.93	6.93	9.67	12.77	15.34	15.80	13.61	10.52	7.73	5.38	4.88	5.77	7.56	268 20	
264	10.04	12.74	14.90	15.94	15.62	13.71	10.64	7.47	5.10	3.54	3.83	5.50	7.97	11.14	14.16	16.01	16.37	15.04	12.33	9.34	6.97	5.54	5.42	6.31	269 20	
265	8.50	11.14	13.77	15.60	15.98	14.86	12.14	8.87	6.16	4.30	3.67	4.60	6.44	9.03	12.27	14.84	16.21	15.96	14.09	11.42	8.56	5.80	6.17	7.42	270 21	
266	9.65	12.22	14.26	15.46	15.24	13.48	10.57	7.65	5.42	3.96	4.06	5.34	7.30	9.97	12.69	14.83	15.87	14.81	13.24	10.76	8.47	7.04	6.68	7.20	271 21	
267	8.44	10.38	12.56	14.16	14.83	14.05	12.07	9.24	7.02	5.32	4.44	4.61	5.97	7.97	10.37	13.07	14.81	15.06	14.13	12.37	10.44	8.86	7.87	7.56	272 21	
268	7.92	8.94	10.67	12.44	13.97	12.81	10.83	8.83	7.10	5.78	5.25	5.76	6.66	8.34	10.76	12.86	14.16	14.44	13.68	12.40	10.86	9.52	8.53	8.21	273 22	
269	8.56	9.40	10.68	12.08	13.04	13.08	11.93	10.54	9.05	7.64	6.61	6.06	6.30	7.07	8.81	10.63	12.30	13.68	14.16	13.66	12.66	11.46	10.12	9.18	274 22	
270	8.77	8.56	9.10	10.17	11.30	12.30	12.61	12.14	11.16	9.92	8.44	6.37	6.38	7.34	8.76	10.57	12.10	13.44	13.92	13.88	13.56	12.37	11.18	9.72	275 23	
271	8.32	7.60	7.94	9.26	10.84	12.04	12.52	12.48	11.98	11.16	9.77	7.94	6.58	6.06	6.50	7.97	9.84	11.56	13.26	14.17	14.66	14.52	13.27	11.34	276 23	
272	9.06	7.37	6.82	7.46	8.74	10.66	12.11	13.20	14.04	13.84	12.76	10.92	8.58	6.74	5.94	6.30	7.68	11.97	13.90	15.26	15.99	15.54	13.97	11.26	278 0	
273	8.63	6.70	5.98	6.37	7.97	10.23	12.66	14.44	15.38	15.04	13.48	11.07	8.36	6.38	5.47	5.87	7.36	9.62	12.14	14.54	16.38	16.98	16.37	13.80	279 0	
274	10.49	7.50	5.61	5.14	5.74	7.77	10.54	13.45	15.71	16.85	16.30	14.16	10.84	7.77	5.85	5.07	5.66	7.50	9.87	12.74	15.25	16.92	17.15	12.54	280 1	
275	8.66	5.94	4.14	3.96	5.28	7.85	11.15	14.38	16.70	17.32	16.13	13.48	9.84	7.20	5.47	4.98	5.96	7.74	10.58	13.66	16.26	17.40	16.86	14.56	281 1	
276	10.89	7.40	4.72	3.37	3.98	5.86	8.86	12.43	15.47	17.34	17.64	16.26	12.76	9.26	6.56	5.24	5.38	6.54	8.77	11.76	14.02	16.82	17.12	15.72	282 2	
277	12.71	9.14	6.06	3.77	3.17	6.67	9.72	13.44	16.25	17.55	17.22	15.06	11.70	8.40	6.26	5.44	6.06	7.47	10.01	12.74	15.12	16.37	16.06	14.21	283 2	
278	11.04	7.42	4.80	3.12	3.62	5.50	8.04	11.13	14.40	16.50	17.22	16.16	13.58	10.36	7.77	6.24	6.90	8.53	10.52	13.06	15.02	15.64	14.36	284 2		
279	11.93	8.64	6.01	4.31	3.47	4.32	6.20	8.94	11.94	14.56	16.24	14.74	12.13	9.47	7.47	6.58	7.42	7.74	9.64	11.26	13.26	14.41	14.26	12.74	285 3	
280	10.35	7.88	5.80	4.44	4.58	5.92	7.85	10.30	12.70	14.67	15.54	15.01	13.36	11.14	9.11	7.80	8.44	8.54	9.26	10.30	11.46	13.04	13.64	13.06	286 3	
281	11.36	9.07	7.14	5.84	5.47	6.20	7.44	9.04	10.97	13.06	14.36	14.36	13.40	11.82	10.44	9.16	8.24	8.54	9.26	10.30	11.46	13.04	13.64	13.06	287 4	
282	10.00	8.37	7.08	6.36	6.44	7.32	8.34	9.60	11.24	12.72	13.46	13.28	12.32	11.06	10.10	9.27	8.97	9.08	9.08	9.61	10.14	11.01	11.52	11.46	288 4	
283	10.73	9.52	8.47	7.66	7.41	7.56	8.04	8.76	9.91	11.17	12.30	12.88	12.66	11.92	11.04	10.37	9.76	9.36	9.12	9.08	9.27	9.86	10.44	10.66	289 5	
284	10.30	9.78	9.22	8.56	8.06	7.74	8.02	8.86	10.06	11.16	12.02	12.40	12.34	12.06	11.48	10.82	9.97	9.24	8.77	8.68	8.96	9.55	10.22	10.70	290 5	
285	10.88	10.82	10.57	10.03	9.26	8.44	7.90	8.07	8.86	9.84	10.90	11.78	12.36	12.58	12.54	12.07	11.12	9.97	8.90	8.23	8.12	8.56	9.27	10.10	291 5	
286	10.90	11.50	11.78	11.53	9.30	7.77	8.55	9.74	7.77	8.55	9.74	11.07	12.94	13.28	13.04	12.24	10.77	9.14	7.88	7.18	7.36	8.12	9.26	10.62	292 6	
287	11.94	12.78	12.88	12.06	10.48	8.86	7.70	7.28	7.65	8.65	10.62	11.54	12.81	13.77	14.04	13.50	12.16	10.00	8.34	6.96	6.50	6.88	7.96	9.76	293 6	
288	11.32	13.07	13.96	13.77	12.48	10.52	8.76	7.36	6.77	7.26	8.52	12.17	13.66	14.56	14.48	13.40	11.12	8.84	6.87	5.64	5.46	6.30	8.06	10.30	294 7	
289	12.80	14.34	15.00	14.16	12.26	9.96	7.92	6.50	6.22	7.10	8.82	10.86	13.12	14.54	15.07	14.56	12.60	9.98	7.47	5.46	4.56	4.96	6.00	9.01	295 7	
290	11.80	14.15	15.84	15.96	14.52	12.00	9.24	7.24	6.16	6.40	7.67	9.66	11.93	14.14	15.62	15.76	14.36	8.61	6.02	4.24	3.86	5.14	7.32	10.15	296 8	
Sum	767.08	766.59	757.45	761.02	729.94	707.88	695.14	698.96	735.36	744.78	791.32	778.57	782.39	787.15	787.51	788.20	771.89	750.72	745.21	723.00	753.41	751.06	783.80	765.56	No. of Days. 79 <sup>a</sup> 8 <sup>b</sup> .	
No.	72	73	74	75	74	72	72	73	74	74	75	72	72	73	74	74	74	73	72	73	75	74	74	73	73	18693.89

FORMS FOR SHORT-PERIOD TIDES.  
SERIES A.—(Continued).

Table with columns for Day, 0h, 1h, 2h, 3h, 4h, 5h, 6h, 7h, 8h, 9h, 10h, 11h, 12h, 13h, 14h, 15h, 16h, 17h, 18h, 19h, 20h, 21h, 22h, 23h, and Solar Hour. Each column contains two rows of data: 'feet' and 'h'. The 'feet' rows show tidal heights and the 'h' rows show corresponding times. The data is organized in rows corresponding to days 291 through 825.



FORMS FOR SHORT-PERIOD TIDES.  
BOMBAY—Commencing 0 hours, Astronomical Time, 1st January, 1885.

SERIES ν.

Motion per mean Solar hour = 14°25'62915".

Argument ( $\gamma - \frac{1}{2}\sigma - \frac{1}{2}\omega + \tau$ ).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	19 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
1	15.52	13.96	9.11	5.76	3.03	1.68	2.28	4.80	7.90	11.70	18.00	18.85	18.08	15.14	11.34	8.50	6.21	5.53	6.08	8.20	11.31	14.16	16.06	16.66	2 0	
2	15.40	12.16	8.40	4.86	3.56	2.90	5.56	8.82	12.94	16.44	18.38	18.97	17.67	14.24	10.56	7.53	5.57	5.16	6.10	8.63	11.84	14.68	16.63	15.24	3 2	
3	11.92	8.00	4.87	2.86	2.57	4.24	6.84	10.20	14.07	17.26	18.86	18.84	17.06	13.20	9.77	6.90	5.23	4.96	6.16	8.86	12.14	16.40	14.28	14.28	4 3	
4	11.00	7.63	4.88	3.55	3.86	5.55	8.01	11.36	14.83	17.16	18.38	17.93	15.80	12.16	6.10	5.05	5.25	6.68	9.24	12.28	14.51	15.96	15.58	13.48	5 4	
5	10.47	7.54	5.76	5.07	5.67	7.22	9.17	12.11	15.02	17.02	16.63	14.11	10.96	8.16	6.22	5.47	5.84	7.18	9.67	12.12	14.04	15.00	14.45	12.62	6 5	
6	10.24	8.07	7.04	6.84	8.67	7.54	10.66	15.06	16.36	16.35	15.24	12.76	10.11	8.00	6.64	6.17	6.55	7.86	9.76	11.80	13.27	14.00	13.64	10.47	7 7	
7	9.05	8.44	8.46	9.03	9.97	11.20	13.05	14.64	15.46	15.18	13.87	11.68	9.76	8.10	7.16	7.03	7.40	8.29	11.16	11.74	12.48	12.60	12.20	11.16	8 8	
8	10.27	9.64	9.66	9.00	10.60	11.70	13.96	14.02	14.44	13.75	12.27	10.82	9.20	7.93	7.06	7.34	8.07	9.14	10.55	11.74	12.48	12.60	12.27	11.60	9 9	
9	10.03	10.34	9.98	9.86	10.17	11.07	12.14	13.06	13.36	12.72	10.43	9.14	7.97	7.14	6.75	6.94	7.74	8.96	10.26	11.64	12.67	13.14	12.97	12.20	10.10	
10	11.24	10.48	10.12	10.05	10.84	11.64	12.27	12.68	12.37	11.53	10.42	8.97	7.80	6.96	6.38	6.44	7.28	8.73	10.47	12.14	13.23	13.84	13.63	11.38	11.12	
11	10.27	9.77	9.62	9.89	10.44	11.24	11.97	12.52	12.50	11.87	10.54	8.76	7.34	6.16	5.74	6.34	7.62	9.54	11.46	14.24	14.58	13.94	12.72	11.24	12.13	
12	10.02	9.32	9.14	9.46	10.37	11.48	12.46	13.04	12.84	11.88	10.23	8.20	6.52	5.62	5.56	6.14	10.17	12.34	14.10	15.26	15.17	13.97	12.27	10.58	13.14	
13	9.35	8.75	8.76	9.26	10.34	11.68	12.96	13.64	13.36	11.80	7.32	5.82	5.14	5.44	6.74	8.86	11.26	13.66	15.38	15.87	15.24	13.66	11.54	9.82	14.15	
14	8.71	8.16	8.36	9.30	10.74	13.64	13.08	13.00	10.84	8.24	6.20	4.76	4.46	5.40	7.36	9.78	12.57	14.82	16.13	15.97	14.56	12.35	10.05	8.46	15.17	
15	7.74	8.41	9.71	11.76	13.30	14.26	14.09	12.44	9.76	7.00	5.12	4.20	4.63	6.12	8.44	11.24	14.04	15.74	16.30	13.82	11.22	8.94	7.54	6.94	16.18	
16	7.15	8.40	10.27	12.44	14.06	14.68	13.84	11.50	8.60	5.91	4.37	4.02	5.06	7.26	9.66	12.72	15.20	16.55	16.63	13.27	12.77	9.97	7.86	6.68	17.19	
17	7.56	9.32	11.40	13.55	14.80	14.78	13.22	10.43	7.48	4.30	4.66	6.25	8.54	11.38	14.15	16.15	16.88	16.08	14.04	11.02	8.54	6.76	6.12	6.34	18.20	
18	7.60	9.84	12.14	14.06	14.14	12.06	9.06	6.46	4.64	4.74	5.16	7.15	9.68	12.56	14.87	16.44	16.45	15.00	12.42	9.50	7.22	5.80	5.43	8.16	19.22	
19	10.65	12.88	14.28	14.56	13.33	10.92	8.30	6.04	4.87	5.06	6.54	8.66	11.04	13.64	15.62	16.36	15.76	13.82	11.00	6.37	5.54	6.83	6.83	8.93	20.23	
20	11.40	13.32	14.42	14.25	12.47	10.10	7.91	6.34	5.70	6.30	7.70	9.76	12.17	14.36	15.74	15.96	14.86	12.76	10.13	7.28	6.17	5.70	6.11	7.62	9.70	22 0
21	11.76	13.36	14.14	13.72	12.06	9.94	8.32	7.22	7.01	8.97	10.80	12.97	14.62	15.50	15.17	13.80	11.46	6.17	6.06	6.68	6.00	6.68	8.02	9.76	23 1	
22	11.65	13.04	13.76	12.14	10.65	9.07	8.15	8.14	8.68	9.86	11.36	13.36	14.56	15.02	14.37	12.76	10.76	8.71	6.96	6.23	6.09	6.68	7.86	9.46	24 3	
23	12.66	13.36	13.34	13.38	11.08	9.94	9.11	8.88	9.28	10.22	11.70	13.06	14.14	14.41	13.60	12.06	10.26	8.46	7.10	6.08	6.08	6.68	7.86	11.24	25 4	
24	12.34	13.44	13.81	13.33	12.18	10.75	9.76	9.24	9.34	10.07	11.16	12.40	13.38	13.03	11.87	10.24	8.47	7.00	5.83	5.38	5.68	6.78	8.55	10.33	26 5	
25	12.22	13.56	14.30	14.16	13.05	11.56	10.06	9.11	9.40	9.40	11.87	12.94	13.44	13.33	12.40	10.74	8.86	6.83	5.22	4.41	4.77	6.10	8.10	10.50	27 6	
26	12.61	14.53	15.56	15.33	13.70	11.64	9.52	8.28	7.92	8.55	9.53	12.70	13.80	14.14	13.30	11.34	8.72	6.20	4.24	3.38	3.76	5.30	7.76	13.50	28 8	
27	15.72	16.74	16.12	14.36	11.40	8.83	7.24	6.86	7.53	9.20	11.11	12.97	14.55	15.08	14.17	11.84	8.82	5.70	3.60	3.06	5.04	7.88	11.48	14.56	29 9	
28	17.04	17.86	17.00	14.36	10.96	8.07	6.27	5.77	6.57	8.62	11.25	13.92	15.74	16.28	14.96	12.18	8.44	5.42	3.22	2.16	3.07	5.32	8.75	12.16	30.10	
29	18.10	18.47	17.26	13.80	10.14	7.09	5.27	5.02	6.02	8.40	11.25	16.52	16.84	15.28	11.68	7.88	4.86	2.74	2.38	4.00	6.66	10.10	13.98	17.01	31.11	
30	18.64	18.38	16.30	13.12	6.01	4.46	4.57	6.12	9.14	12.56	15.46	17.00	16.86	14.76	11.06	7.36	4.34	2.72	2.99	4.86	7.74	11.40	14.94	18.47	32.13	
31	17.66	14.67	11.08	7.54	5.01	3.93	4.32	6.55	9.62	13.04	15.80	16.94	16.08	13.73	10.16	6.82	4.54	3.38	4.44	9.36	12.84	15.86	17.74	17.94	33.14	
32	16.48	13.27	9.84	6.84	4.96	4.33	5.26	7.44	12.82	18.28	15.74	16.43	15.42	9.66	6.90	5.42	5.14	6.20	8.06	10.66	13.66	16.02	17.12	16.74	34.15	
33	14.88	11.68	8.76	6.34	4.92	4.74	5.86	8.20	11.97	13.60	15.34	14.08	14.08	9.04	7.34	6.56	6.94	8.04	9.56	11.76	14.24	15.60	16.04	15.34	35.16	
34	13.02	10.16	7.86	6.27	5.86	7.18	9.07	11.36	13.26	14.34	14.26	14.08	11.00	9.39	8.22	7.92	8.30	9.05	10.36	12.08	13.76	14.66	14.44	14.44	36.18	
35	9.30	7.54	6.26	6.13	6.68	7.86	9.28	10.86	12.27	13.10	12.94	11.93	10.66	9.72	9.12	9.06	9.26	10.60	11.82	12.86	13.34	13.82	13.82	13.82	37.19	

Table with 40 columns and 40 rows. The columns contain numerical data points for each row number (36 to 70). The final row (70) is labeled 'Sum' and contains a total sum of 791.287661. A final column on the right provides 'No. of Days' and '78° 16\"

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No.

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FORMS FOR SHORT-PERIOD TIDES.

SERIES v.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
71	6.06	5.35	5.54	6.90	9.24	11.72	13.95	15.20	15.12	13.39	10.64	7.57	5.44	4.44	4.96	6.46	8.94	14.34	16.00	16.06	14.53	11.64	8.54	5.76	75 16	
72	4.22	3.97	5.24	7.30	10.10	13.02	15.04	16.00	15.20	12.86	9.54	6.67	4.38	5.52	7.55	10.33	13.50	15.75	16.75	16.07	13.66	10.42	7.22	4.92	76 17	
73	3.64	4.00	5.66	8.33	11.52	14.30	16.06	16.52	15.06	12.13	8.73	4.66	4.99	6.52	8.92	11.86	14.66	16.40	16.5f	15.07	11.90	8.47	5.62	3.74	77 18	
74	3.22	4.26	6.06	9.60	12.85	15.23	16.56	16.25	14.26	10.83	8.00	5.75	5.11	5.88	7.84	10.46	13.38	15.68	16.60	15.8c	10.12	7.06	3.54	3.76	78 20	
75	5.34	7.86	11.00	13.93	15.92	16.74	15.74	14.36	10.24	7.64	6.12	6.08	7.14	9.00	11.56	13.90	15.66	14.76	12.06	8.90	6.13	4.34	3.62	4.36	79 21	
76	6.06	8.47	11.31	13.87	15.62	16.12	14.97	12.74	10.02	8.05	6.96	7.06	9.67	12.07	14.08	15.23	15.08	13.57	11.16	8.26	6.08	4.76	4.47	5.46	80 22	
77	7.26	9.48	11.88	13.90	15.36	15.50	14.66	12.07	10.54	8.74	7.94	8.14	9.06	10.62	12.40	13.77	14.52	12.80	10.64	8.47	6.76	5.86	6.49	6.49	81 23	
78	7.75	9.52	13.54	14.73	14.90	14.06	12.63	11.05	9.70	8.86	8.72	9.12	10.24	11.76	13.06	13.60	13.34	12.06	10.56	8.92	7.40	6.30	6.68	7.68	83 1	
79	9.46	11.24	13.02	14.08	14.52	14.22	13.04	11.70	10.34	9.24	8.84	9.04	9.84	10.96	12.05	12.86	12.96	11.22	9.67	8.30	7.06	6.48	6.64	7.48	84 2	
80	8.86	10.64	12.34	13.74	14.48	14.44	13.62	12.12	10.36	8.96	8.11	7.96	9.76	11.26	12.36	12.92	12.78	11.94	10.50	8.78	7.20	6.06	5.92	6.72	85 3	
81	8.34	10.28	12.20	13.86	15.00	15.14	14.16	12.20	9.88	8.00	6.56	7.46	9.22	11.16	12.56	13.57	14.06	13.37	11.72	9.38	7.17	5.72	5.38	6.17	86 4	
82	7.82	10.00	14.54	15.84	15.94	14.64	12.14	9.36	6.97	5.74	5.63	6.67	8.88	11.24	13.46	14.86	15.36	14.34	12.05	9.44	6.93	5.00	5.82	7.83	87 6	
83	10.50	13.30	15.60	16.72	16.28	14.37	11.37	8.36	6.00	4.67	4.80	6.40	9.20	12.06	14.62	16.12	16.16	12.22	9.12	6.60	5.05	4.86	5.87	8.10	88 7	
84	11.14	14.15	16.35	17.15	16.24	13.58	10.14	7.06	4.83	3.96	4.70	6.72	13.20	15.64	17.04	16.75	14.92	11.81	8.56	6.27	5.14	5.64	6.94	9.43	89 8	
85	12.61	15.44	17.03	17.08	15.36	11.92	8.64	4.48	4.25	5.24	7.57	11.00	14.10	16.43	17.34	16.56	14.28	10.82	7.84	5.95	5.42	6.12	7.87	10.62	90 9	
86	13.66	17.14	16.46	13.96	10.44	7.12	4.80	3.83	4.41	6.43	8.78	12.04	14.74	16.66	17.13	15.64	12.86	9.53	7.16	5.81	5.93	7.26	12.02	14.66	91 11	
87	16.44	16.67	15.06	12.02	8.56	5.84	4.04	3.84	4.93	7.24	10.09	13.22	15.56	16.90	16.56	11.68	8.84	7.02	6.48	7.04	8.26	10.50	13.00	14.94	92 12	
88	15.83	15.12	12.94	9.87	7.14	5.16	4.23	4.76	6.40	8.73	11.37	14.00	16.34	15.34	13.10	10.40	8.36	7.32	7.28	8.03	9.50	11.53	13.48	14.74	93 13	
89	14.92	13.67	11.34	8.76	6.67	5.40	6.16	7.85	9.97	12.30	14.30	15.82	15.46	14.27	12.24	10.20	8.78	8.26	8.47	9.24	10.52	12.04	13.48	14.16	94 14	
90	13.84	10.16	8.14	6.47	5.74	6.22	7.44	9.20	10.85	12.64	14.05	14.67	14.27	12.97	11.44	10.04	9.16	8.84	9.16	9.84	11.06	12.80	12.96	12.28	95 16	
91	10.94	9.24	7.80	6.78	6.70	7.30	8.37	9.54	10.90	12.34	13.52	13.80	13.26	12.13	10.96	9.60	9.33	9.54	9.90	10.56	11.44	11.92	12.05	11.54	96 17	
92	10.36	9.16	8.12	7.47	7.44	7.87	8.52	9.46	10.73	11.93	12.74	12.60	11.86	11.07	10.34	9.94	9.77	9.87	10.02	10.36	10.81	11.14	11.27	10.92	97 18	
93	10.30	9.34	8.36	7.74	7.58	7.98	8.76	11.04	11.96	12.50	12.66	12.42	11.96	11.34	10.55	9.91	9.47	9.34	9.52	9.94	10.53	10.94	11.12	11.02	98 19	
94	10.62	10.00	8.40	8.01	8.13	8.63	9.70	10.66	11.77	12.66	13.06	12.94	12.40	11.47	10.50	9.62	8.94	8.54	8.74	9.48	10.45	11.88	11.89	11.44	99 21	
95	10.50	9.40	8.46	7.84	7.76	8.43	9.46	10.86	12.30	13.36	13.82	13.66	12.66	11.42	10.02	8.72	7.82	8.36	9.47	10.80	11.90	12.70	12.87	12.44	100 22	
96	11.06	9.52	8.12	7.40	7.47	8.26	9.54	11.08	12.70	14.06	14.56	14.26	12.80	10.96	8.88	7.40	6.81	6.84	7.92	9.62	11.52	13.00	13.97	14.12	13.00	101 23
97	11.02	9.05	7.48	6.74	6.92	7.97	11.72	13.58	14.86	15.12	14.21	12.35	9.67	7.47	5.98	5.58	6.14	7.76	9.84	12.16	14.02	15.18	15.06	13.40	103 0	
98	10.95	8.28	6.60	6.02	6.46	7.88	10.06	12.53	14.55	15.72	15.49	13.80	11.08	8.22	5.95	4.52	4.32	5.47	7.72	10.54	13.27	15.36	15.32	9.88	104 2	
99	7.34	5.76	5.40	6.24	8.22	10.70	13.40	15.52	16.25	15.36	11.30	9.46	6.56	4.47	3.42	3.91	5.74	8.31	11.40	14.40	16.28	16.72	15.47	9.44	105 3	
100	6.81	5.47	5.38	6.52	8.91	11.80	14.40	15.97	16.08	14.35	7.80	4.97	2.93	2.46	3.76	6.21	9.51	12.97	15.58	17.14	17.04	14.94	11.68	8.36	106 4	
101	6.14	5.06	5.57	7.24	10.07	13.10	16.44	15.82	13.44	9.74	6.67	4.03	2.50	2.77	4.44	7.50	10.96	14.33	16.70	17.72	16.91	14.37	10.87	8.10	107 5	
102	6.15	6.50	8.36	11.33	14.12	15.97	16.50	15.10	12.22	8.67	5.24	3.17	2.36	3.47	5.74	8.64	12.02	15.12	16.94	17.54	13.40	10.32	7.62	6.17	108 7	
103	6.01	7.04	9.13	12.00	14.47	15.60	15.54	13.66	10.74	7.44	4.88	3.28	3.04	4.36	6.67	9.40	12.47	15.00	16.74	16.94	15.60	13.03	10.01	7.87	6.76	109 8
104	6.80	7.71	9.70	12.14	14.15	15.02	14.50	12.53	9.92	7.24	5.36	4.16	5.20	7.26	9.69	12.40	14.57	15.77	15.74	14.47	12.12	9.90	8.07	7.14	110 9	
105	7.11	7.83	9.54	11.58	13.16	13.28	11.76	9.56	7.60	5.96	4.93	5.02	5.86	7.52	9.74	12.00	13.87	14.87	14.77	13.76	12.06	10.26	8.74	7.82	111 10	

106	7.54	9.34	11.00	12.36	12.96	12.72	11.58	10.14	8.48	6.94	6.06	5.96	6.00	7.87	9.72	11.62	13.34	14.34	14.44	13.66	12.66	11.62	10.62	9.10	8.03	7.66	112 12		
107	7.76	8.68	10.20	11.63	12.43	12.66	12.10	10.96	9.47	8.14	7.03	6.54	6.88	7.94	9.57	11.42	13.34	14.44	14.44	13.93	12.76	11.62	10.64	9.18	7.74	7.96	113 13		
108	6.96	7.85	9.40	10.96	12.36	13.06	13.12	12.22	10.65	8.87	7.52	6.84	7.66	9.26	11.04	12.88	14.13	14.66	14.30	12.64	10.64	9.60	8.60	7.18	6.78	6.96	114 14		
109	5.93	7.08	9.00	11.04	12.64	13.72	12.97	11.36	9.32	7.66	6.62	6.47	7.28	8.88	10.96	12.96	14.54	15.17	14.54	12.77	10.22	7.74	5.76	4.88	4.88	4.88	115 15		
110	5.14	6.58	8.88	11.33	13.36	14.66	14.94	13.86	11.70	9.34	7.26	6.22	7.24	9.00	11.22	13.36	14.86	15.37	14.44	12.10	6.48	4.70	4.20	4.20	4.20	4.74	116 17		
111	6.70	9.17	11.77	14.02	15.57	15.54	14.03	11.54	8.80	6.96	6.07	6.34	7.48	9.44	11.06	15.48	15.44	13.84	10.92	7.66	5.31	3.77	3.70	3.70	3.70	3.70	5.12	117 18	
112	7.30	10.10	12.94	15.14	16.26	15.76	13.86	11.00	8.24	6.47	5.97	7.98	10.16	12.70	14.64	15.66	14.96	12.70	9.46	6.57	4.32	3.42	3.42	3.42	3.42	4.04	5.80	118 19	
113	8.48	11.42	14.32	16.17	16.57	15.46	10.06	7.64	6.36	6.16	6.82	8.40	10.90	13.45	15.07	15.35	13.81	11.00	7.70	5.15	3.44	3.36	3.36	3.36	3.36	4.67	6.96	119 20	
114	9.56	14.92	16.36	16.28	14.70	11.93	9.06	7.20	6.40	6.70	7.74	9.37	11.47	13.86	15.04	15.06	12.96	9.73	7.17	3.42	4.04	5.68	8.27	10.68	120 22	11.76	121 23		
115	13.46	15.48	16.25	15.62	13.50	10.52	8.22	6.72	6.40	7.02	8.34	10.44	12.60	14.08	13.26	10.82	7.87	5.57	3.94	3.86	4.88	6.80	9.18	11.76	121 23	12.80	123 0		
116	14.24	15.56	15.54	14.30	11.86	9.46	7.76	6.94	7.06	7.86	11.24	13.06	13.30	12.28	10.40	8.28	6.46	5.35	5.20	6.00	7.54	9.26	11.42	13.34	124 1	13.34	125 3		
117	14.56	15.43	14.76	13.04	10.84	8.96	7.44	7.76	8.80	10.26	11.94	13.06	12.46	11.36	9.38	7.94	6.74	6.04	6.20	7.12	10.24	12.10	13.38	14.08	125 3	13.78	126 4		
118	14.60	13.86	12.06	10.14	8.84	8.15	8.06	8.40	9.36	10.62	11.94	12.68	12.46	11.68	10.72	9.36	6.96	6.92	7.44	8.22	9.26	10.47	12.10	13.34	13.78	126 4	13.54	127 5	
119	13.92	12.90	11.41	10.00	8.90	8.46	8.56	9.00	9.74	10.55	11.36	11.86	10.38	9.56	8.46	7.76	7.66	7.97	8.66	9.74	10.97	12.22	13.24	13.54	127 5	13.22	128 6		
120	13.40	12.16	10.87	9.94	9.24	8.96	8.94	9.24	10.93	10.34	11.44	11.77	11.44	10.76	9.74	8.78	8.17	8.10	8.66	9.60	10.93	12.30	13.21	13.50	13.18	128 6	13.50	129 8	
121	13.24	12.12	10.96	9.98	9.27	8.74	8.80	9.24	10.93	10.80	11.26	11.29	10.79	10.06	9.26	8.46	8.06	8.04	8.56	9.72	10.94	12.20	12.96	13.22	12.96	13.22	128 6	13.50	130 9
122	12.94	11.17	9.96	8.96	8.20	7.92	8.00	8.62	9.56	10.46	11.34	11.97	12.06	11.62	10.20	8.95	8.24	8.24	9.37	10.96	12.50	13.57	14.02	13.54	130 9	14.02	13.54	130 9	
123	12.36	11.16	9.68	8.30	7.26	6.90	7.45	8.52	10.00	11.40	12.36	12.92	12.66	11.62	8.95	7.53	7.27	7.93	9.36	11.30	13.16	14.26	14.66	13.94	131 10	14.66	13.94	131 10	
124	12.24	9.97	7.60	5.85	4.92	4.64	6.42	8.60	10.95	13.28	15.34	14.46	12.38	10.16	8.14	6.95	6.90	8.01	9.74	11.84	13.66	14.84	15.16	11.76	132 12	15.16	11.76	132 12	
125	8.83	6.14	4.18	3.66	4.53	6.46	9.08	11.92	14.30	15.96	16.28	14.95	12.41	9.36	7.14	6.17	6.94	7.92	10.02	12.44	15.64	15.47	13.76	10.66	133 13	10.66	8.86	134 14	
126	7.20	4.46	2.86	2.74	4.17	6.63	9.77	13.00	15.72	17.16	16.96	15.18	11.90	8.78	6.57	6.52	7.50	8.30	10.90	13.74	15.64	16.06	14.62	12.56	8.86	134 14	8.86	134 14	
127	5.70	3.17	1.97	2.43	4.23	7.22	10.62	13.96	16.50	17.69	14.58	10.90	8.02	5.94	5.93	6.30	8.25	10.90	13.74	15.64	16.06	14.62	12.56	8.86	134 14	8.86	134 14		
128	4.52	2.14	1.42	2.56	5.03	8.20	11.45	14.68	16.97	17.83	16.77	14.06	7.60	5.84	5.32	6.20	8.25	10.90	13.74	15.64	16.06	14.62	12.56	8.86	134 14	8.86	134 14		
129	2.24	1.86	3.24	5.60	8.58	12.24	15.14	17.16	17.74	16.33	13.21	10.00	7.30	5.76	5.60	6.58	8.80	11.97	14.34	15.47	13.72	15.74	13.76	10.48	4.07	136 17	4.07	136 17	
130	2.67	2.88	4.46	6.78	9.71	12.92	15.50	17.10	17.16	15.40	12.67	9.57	7.30	5.76	6.16	7.20	9.40	12.06	14.14	14.98	14.36	12.18	9.28	6.58	4.76	138 19	4.76	138 19	
131	3.86	4.30	5.66	7.78	10.44	13.75	15.36	16.54	16.23	14.86	9.56	7.54	6.48	6.38	7.36	9.30	11.76	13.38	13.98	13.42	11.66	9.36	7.30	5.74	139 20	5.74	139 20		
132	4.98	5.26	6.33	8.68	12.87	14.66	15.72	15.46	14.00	11.78	9.46	7.72	6.96	6.82	7.44	8.91	10.74	12.30	13.13	12.92	11.76	10.08	8.18	6.28	140 22	6.28	140 22		
133	6.46	7.26	8.54	10.38	12.48	14.22	14.94	14.74	13.52	11.62	9.46	7.84	6.86	6.52	6.83	8.02	9.54	11.12	12.53	12.97	10.86	9.35	7.86	6.87	141 23	6.87	141 23		
134	6.74	7.36	8.54	10.16	11.86	13.27	14.14	13.98	12.92	11.14	9.14	7.48	6.36	5.86	7.12	8.94	10.74	12.22	12.86	12.65	11.60	10.06	8.56	7.47	143 0	7.47	143 0		
135	7.24	7.70	8.44	10.00	11.62	13.06	13.93	13.82	12.68	10.82	7.20	5.72	5.17	5.56	6.97	8.92	10.90	12.46	13.44	13.42	12.46	10.72	9.12	8.02	144 1	8.02	144 1		
136	7.47	7.63	8.26	9.76	11.56	13.14	14.05	13.96	12.62	10.76	8.52	6.66	5.32	4.84	5.46	7.38	9.67	11.66	13.40	14.34	14.36	13.24	11.36	9.64	8.16	145 8	9.64	145 8	
137	7.50	8.44	10.16	11.93	13.46	14.20	13.97	12.62	10.50	7.84	5.72	4.46	4.54	5.90	7.82	10.17	12.67	14.36	14.76	15.22	13.34	11.12	9.16	7.84	7.36	146 4	7.36	146 4	
138	7.72	8.72	10.32	12.06	13.66	14.36	13.76	11.92	9.27	6.82	4.82	3.97	4.57	6.16	11.03	13.46	15.10	15.24	14.67	12.94	10.67	8.77	7.60	7.38	147 5	7.38	147 5		
139	7.93	9.10	10.86	12.73	14.28	14.53	13.00	10.66	7.86	5.58	4.13	5.24	7.24	9.70	12.50	14.40	15.74	15.70	14.12	12.14	9.74	8.36	7.64	7.54	148 6	7.54	148 6		
Sum	682.71719	43.684	25.727	93.818	70.880	24.875	62.789	39.754	54.789	51.723	54.689	66.645	90.671	73.761	21.796	88.832	07.799	12.842	15.836	10.809	86.697	59.653	43.660	90.660	90.660	90.660	90.660	No. of Daye.	
No.	76	77	70	70	76	76	70	70	70	77	76	75	70	71	77	76	74	70	73	70	77	76	71	70	70	74	74	181.42	86

FORMS FOR SHORT-PERIOD TIDES.  
SERIES v.—(Continued).

Table with 24 columns (Day, 0h to 23h, Solar Hour) and 17 rows of data. Each row represents a day, with columns showing tidal heights in feet for each hour. The data is organized in a grid format with alternating 'feet' and 'h' labels for some columns.





FORMS FOR SHORT-PERIOD TIDES.  
SERIES v.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
212	18.50	17.76	14.76	10.60	7.37	5.06	4.48	7.18	10.36	13.94	16.34	17.16	16.04	13.12	9.20	5.80	3.36	2.56	3.60	5.73	9.03	12.78	15.94	17.78	224 0	
213	18.04	16.74	13.32	9.36	6.05	4.18	4.90	7.56	11.10	14.46	16.66	16.88	15.39	12.15	8.23	5.44	3.52	3.32	4.58	7.04	10.14	16.16	17.52	17.36	225 2	
214	15.28	11.80	8.22	5.32	3.80	4.02	5.58	8.40	11.50	14.52	16.18	16.06	14.38	11.36	7.98	4.54	4.80	6.25	8.27	11.00	13.96	16.32	17.26	16.42	226 3	
215	14.32	10.85	7.62	5.16	4.10	4.64	6.45	8.92	12.05	14.70	15.80	13.36	10.62	7.94	6.32	5.74	6.44	7.77	9.72	12.07	14.12	15.66	15.72	14.46	227 4	
216	13.06	9.36	6.96	5.40	5.07	5.84	7.33	11.87	13.60	14.46	13.96	12.48	10.40	8.65	7.45	7.28	8.00	9.26	10.72	12.27	13.74	14.47	14.18	12.78	228 5	
217	10.82	8.78	5.83	5.86	6.74	8.34	10.14	12.02	13.26	13.57	12.85	11.76	10.70	9.74	9.12	8.90	9.34	10.06	10.94	12.10	13.72	13.38	11.88	10.06	229 7	
218	8.17	7.02	6.68	7.00	7.70	8.77	10.10	11.44	12.33	12.66	12.46	12.00	11.36	10.62	10.07	9.67	10.12	10.82	11.54	12.43	12.67	12.12	11.23	9.96	230 8	
219	8.64	7.77	7.46	7.69	8.30	9.04	10.10	11.17	12.34	12.90	12.90	11.72	11.15	10.62	10.30	10.00	10.14	10.50	11.34	11.96	12.26	11.97	11.38	10.53	231 9	
220	9.44	8.35	7.66	7.57	8.12	9.06	11.57	12.72	13.42	13.56	13.18	12.30	11.45	10.72	10.26	9.92	9.63	10.00	10.71	11.62	12.32	12.18	11.42	10.36	232 10	
221	9.08	8.15	7.24	7.70	8.54	9.82	11.43	12.72	13.64	13.66	13.26	12.36	11.22	10.18	9.34	8.97	9.08	9.88	10.76	11.64	12.26	11.85	10.40	8.78	233 12	
222	7.36	6.44	6.28	7.14	8.37	10.20	11.94	13.38	14.40	14.54	13.58	12.17	10.70	9.34	8.82	8.84	10.00	11.16	12.50	13.30	13.42	12.06	10.16	8.40	234 13	
223	6.86	6.06	6.14	7.20	8.95	10.80	12.76	13.96	14.91	14.84	13.64	11.70	9.97	8.36	8.48	8.96	10.06	11.56	13.12	13.97	13.64	12.06	9.70	7.27	235 14	
224	5.96	5.56	6.35	7.80	9.76	13.66	15.10	15.46	14.62	13.86	10.57	8.64	7.46	7.31	7.76	8.84	10.72	12.64	14.21	14.62	13.44	11.00	8.24	6.24	236 15	
225	5.36	6.54	8.54	10.66	13.00	15.02	15.96	15.50	14.08	11.60	8.97	7.34	6.70	6.84	7.80	9.62	11.70	13.76	14.95	14.67	10.00	7.37	5.56	4.97	237 17	
226	5.74	7.38	9.36	11.94	14.36	16.04	16.27	15.32	13.08	10.11	7.72	6.36	6.10	6.94	8.63	10.83	15.21	15.71	14.43	11.89	8.54	6.26	4.97	5.06	238 18	
227	6.36	8.22	10.64	13.40	15.86	16.62	16.16	14.21	11.38	8.34	6.35	5.74	7.13	9.22	11.84	14.36	15.71	15.48	13.64	10.66	7.60	5.70	4.96	5.70	239 19	
228	7.24	9.54	12.02	14.56	16.24	15.34	12.80	9.60	7.06	5.50	5.18	5.94	7.72	10.28	13.04	15.14	15.00	14.88	12.52	9.63	7.07	5.74	5.64	6.67	240 20	
229	8.36	13.17	15.30	16.38	16.24	15.34	11.04	8.16	6.11	5.05	5.41	6.72	8.83	11.26	13.77	15.36	15.38	14.00	11.50	8.72	5.97	6.34	7.52	9.30	241 22	
230	11.47	13.80	15.46	15.84	14.77	12.44	9.37	7.06	5.37	4.85	5.64	7.12	9.24	11.64	13.96	15.06	13.17	10.76	8.64	7.30	6.86	7.44	8.64	10.38	242 23	
231	13.36	14.06	15.24	15.10	13.64	11.26	8.61	6.50	5.32	5.38	7.85	9.86	11.96	13.64	14.58	14.75	12.68	10.68	8.97	8.02	7.81	8.36	9.26	10.60	244 0	
232	12.24	13.73	14.44	13.86	12.25	10.02	8.06	6.46	5.62	5.78	6.47	7.80	9.63	11.38	12.97	13.74	13.44	12.44	9.83	8.84	8.57	8.87	9.67	10.67	245 1	
233	13.06	13.46	13.08	11.68	9.86	8.26	6.87	6.17	6.26	7.02	8.17	9.66	11.26	12.55	13.37	13.57	12.94	11.92	10.73	9.67	9.18	9.63	10.54	11.48	246 3	
234	12.46	12.92	12.66	11.74	10.12	8.87	7.44	6.44	6.21	6.66	7.76	9.20	10.76	12.36	14.05	13.67	12.68	11.26	10.02	9.22	8.90	9.14	9.86	10.86	247 4	
235	12.02	12.84	12.98	12.36	11.16	9.57	7.60	6.24	5.63	5.97	8.60	10.66	12.80	14.28	14.96	14.74	13.66	11.85	10.04	8.66	8.02	8.14	9.04	10.38	248 5	
236	12.06	13.14	13.74	13.40	12.04	10.04	8.76	4.78	5.02	6.24	8.16	10.78	13.20	15.04	15.98	15.74	14.33	11.96	9.30	7.37	6.55	6.70	8.06	9.98	249 6	
237	13.93	14.86	14.44	12.80	10.18	7.37	5.17	3.90	4.93	5.50	7.96	10.88	13.80	16.04	17.04	16.46	14.44	11.04	8.24	6.27	5.63	7.24	9.64	12.52	250 8	
238	14.74	15.98	15.46	13.20	9.94	6.63	4.34	3.17	2.53	3.38	8.20	11.40	14.56	16.82	16.36	13.83	9.98	6.70	4.46	3.84	4.58	6.80	10.06	13.28	251 9	
239	15.76	16.64	15.75	12.94	9.26	6.06	3.66	2.67	3.72	5.66	12.20	15.53	17.33	17.53	15.87	12.42	8.56	5.32	3.44	3.47	4.55	7.26	10.87	14.22	252 10	
240	16.50	17.05	15.47	12.37	8.44	5.52	3.10	4.46	6.74	9.94	13.47	16.22	17.47	17.02	14.77	10.84	7.23	4.52	3.00	3.30	5.07	8.06	11.72	14.94	253 11	
241	16.86	14.94	11.54	8.00	5.38	3.90	4.20	5.52	7.95	11.06	14.30	16.51	17.04	15.88	12.99	9.17	5.97	3.70	2.94	3.94	9.14	12.45	15.42	16.68	254 13	
242	16.10	13.81	10.56	7.46	5.47	4.87	5.00	7.04	9.54	12.25	14.81	16.16	16.06	14.41	11.07	5.34	3.84	3.92	5.16	7.43	10.36	13.44	15.47	16.04	255 14	
243	14.92	12.66	9.98	7.74	6.47	6.36	7.02	8.54	10.58	14.58	15.36	14.73	12.52	9.86	7.17	5.31	4.44	5.02	6.44	8.50	11.04	13.56	14.79	14.77	256 15	
244	13.46	11.46	9.44	8.00	7.36	7.56	9.51	11.10	12.66	13.73	13.94	12.90	11.02	8.73	6.90	5.70	5.63	6.34	7.60	9.36	11.36	13.14	13.88	13.60	257 16	
245	12.43	9.64	8.76	8.44	8.70	9.18	9.95	10.88	12.06	12.76	12.71	11.64	9.87	8.26	7.04	6.44	6.67	7.34	8.36	9.74	11.16	12.22	12.70	12.20	11.38	258 18
246	10.60	9.88	9.34	9.16	9.13	9.34	9.87	10.66	11.30	11.64	11.37	10.56	9.48	8.44	7.14	7.52	7.33	7.86	8.66	9.84	10.90	11.64	11.97	11.87	11.54	259 19

247	11.08	10.42	9.92	9.60	9.42	9.54	9.86	10.24	10.70	10.91	10.34	9.74	9.06	8.35	7.72	7.46	7.67	8.44	9.64	10.73	11.52	11.88	12.06	11.88	280 20
248	11.53	10.97	10.23	9.48	9.04	9.38	10.01	10.64	11.05	11.18	10.94	10.46	9.52	8.56	7.74	7.42	7.64	8.34	9.42	10.67	11.65	12.46	12.82	12.62	280 21
249	12.04	10.96	9.85	8.96	8.54	8.86	9.64	10.44	11.23	11.67	11.60	10.92	9.74	8.36	7.26	6.68	6.86	7.74	9.24	12.34	13.24	13.55	13.17	12.08	282 23
250	10.64	9.21	8.06	7.54	7.74	8.74	9.92	11.30	12.38	12.82	12.42	11.17	9.62	7.86	6.55	6.54	7.88	9.08	11.56	13.16	14.03	14.06	13.18	11.60	284 0
251	9.86	8.07	6.97	6.64	7.14	8.38	10.20	11.92	13.16	13.44	10.70	8.70	6.90	5.75	5.59	6.36	8.04	10.20	12.32	13.87	14.64	14.36	12.87	10.73	285 1
252	8.45	6.71	5.90	6.17	7.02	9.97	12.54	14.50	15.33	14.46	12.23	9.34	6.94	4.94	5.94	8.06	11.46	13.68	15.18	15.37	14.28	12.24	9.67	286 8	
253	5.74	5.30	6.12	7.84	9.97	12.54	14.50	15.33	14.46	12.23	9.34	6.94	4.94	5.94	8.06	11.46	13.68	15.18	15.37	14.28	12.24	9.67	286 8		
254	4.48	4.66	6.00	8.44	11.24	13.97	15.67	15.66	14.20	11.46	8.47	6.20	4.97	5.22	8.86	11.54	14.06	15.76	16.07	14.86	12.14	9.06	6.37	4.56	268 5
255	3.93	4.93	6.93	9.67	12.77	15.34	16.35	15.80	13.61	7.73	5.58	4.88	5.77	7.56	10.04	12.74	14.90	15.94	15.62	13.71	10.64	7.47	5.10	3.54	269 6
256	3.83	5.50	7.97	11.14	16.01	16.37	15.04	12.33	9.34	6.97	5.54	5.42	6.51	8.50	11.14	13.77	15.60	15.98	14.86	12.14	8.87	6.16	4.30	3.07	270 8
257	6.44	9.03	12.27	14.84	16.21	15.96	14.09	11.42	8.56	6.75	5.80	6.17	7.42	9.65	12.22	14.26	15.46	15.24	13.48	10.57	7.65	5.42	4.06	5.34	271 9
258	7.30	9.97	12.69	14.83	15.87	15.16	13.24	10.76	8.47	7.04	6.68	7.20	8.44	10.38	12.56	14.83	14.05	12.97	9.24	7.02	5.32	4.44	4.61	5.87	272 10
259	7.97	10.37	13.97	14.81	15.06	14.13	12.37	10.44	8.86	7.82	7.92	8.94	10.67	12.44	13.74	13.97	12.81	10.83	8.83	7.10	5.78	5.25	5.76	6.66	273 11
260	8.34	10.76	12.86	14.16	14.44	12.40	10.86	9.52	8.53	8.21	8.56	9.40	10.68	12.08	13.94	13.08	11.93	10.54	9.05	7.64	6.61	6.06	7.07	274 13	
261	10.63	12.30	13.68	14.16	13.66	12.66	11.46	10.12	9.18	8.77	8.56	9.10	10.17	11.30	12.30	12.61	12.14	11.16	9.02	7.14	6.37	6.38	7.34	8.76	275 14
262	10.57	12.10	13.44	13.92	13.88	13.56	12.37	11.18	9.72	8.32	7.60	7.94	9.26	10.84	12.52	12.48	11.98	11.16	9.77	7.94	6.58	6.06	6.50	7.97	276 15
263	9.84	11.56	13.26	14.17	14.66	14.52	13.27	11.34	9.06	7.37	7.46	8.74	10.60	12.11	13.20	14.44	13.84	12.76	10.92	8.58	6.74	5.94	6.30	7.68	277 16
264	9.72	11.97	13.90	15.26	15.99	13.97	11.26	8.63	6.70	5.98	6.37	7.97	10.25	12.66	14.44	15.38	15.04	13.48	11.07	8.36	6.38	5.47	5.87	7.36	278 18
265	12.14	14.54	16.28	16.98	16.37	13.80	10.49	7.50	5.61	5.14	5.74	7.77	10.54	13.45	15.71	16.85	15.30	14.16	10.84	5.85	5.07	5.66	7.50	9.87	279 19
266	12.74	15.25	16.92	17.15	15.62	12.54	8.66	5.94	4.14	3.96	5.28	7.85	11.15	16.70	17.32	16.33	13.48	9.84	7.77	5.47	4.98	5.96	7.74	10.58	280 20
267	13.66	16.26	17.40	16.86	14.56	10.89	7.40	4.72	3.37	3.98	8.86	12.43	15.47	17.34	17.64	16.26	12.76	9.26	6.56	5.24	5.38	6.54	8.77	11.76	281 21
268	14.62	16.82	17.12	15.72	12.71	6.06	3.77	3.17	4.42	6.67	9.72	13.44	16.25	17.55	17.22	15.06	11.70	8.40	6.26	5.44	6.06	7.47	10.01	12.74	282 23
269	16.37	16.06	14.21	11.04	7.42	4.80	3.12	3.62	5.50	8.04	11.13	14.40	16.50	17.22	16.16	13.58	10.36	7.77	6.24	6.91	8.53	10.52	15.12	15.02	284 0
270	15.64	14.36	11.93	8.64	6.01	4.31	3.47	4.52	6.20	8.94	11.94	14.56	16.24	14.74	13.36	11.44	9.11	7.80	7.42	7.74	8.61	10.04	14.41	14.41	285 1
271	14.26	12.74	10.35	7.88	5.80	4.44	4.58	5.92	7.85	10.30	14.67	15.54	15.01	13.36	11.44	9.11	7.80	7.42	7.74	8.61	10.04	11.80	13.04	13.64	286 2
272	13.06	11.36	9.07	7.14	5.47	6.20	7.44	9.04	10.97	13.06	14.36	14.36	13.40	11.82	10.44	9.16	8.44	8.24	8.54	9.26	10.30	11.46	12.22	11.46	287 4
273	10.00	8.37	7.08	6.36	6.44	7.32	8.34	9.60	11.24	12.72	13.46	13.28	12.32	11.06	10.10	9.27	8.97	8.94	9.08	9.61	10.14	11.52	10.73	288 5	
274	9.52	8.47	7.66	7.41	7.56	8.04	8.76	9.91	11.17	12.30	12.88	12.66	11.92	11.04	9.76	9.36	9.12	9.08	9.27	9.86	10.44	10.68	10.30	289 6	
275	9.78	9.22	8.56	8.06	7.74	8.02	8.86	10.06	12.02	12.40	12.54	12.07	11.12	11.12	9.97	8.90	8.23	8.12	8.56	9.27	10.10	10.70	10.88	290 7	
276	10.57	10.03	9.26	8.44	8.07	8.80	9.84	10.90	11.78	12.36	12.58	12.54	12.07	11.12	9.97	8.90	8.23	8.12	8.56	9.27	10.10	10.90	11.50	11.53	291 9
277	10.67	9.30	8.14	7.56	7.77	8.55	9.74	11.07	12.15	12.94	13.28	13.04	12.24	10.77	9.14	7.88	7.18	7.36	8.12	8.12	10.62	11.94	12.78	12.88	292 10
278	10.48	8.86	7.70	7.28	7.65	8.65	10.02	11.54	12.81	13.77	14.04	13.50	12.16	10.30	6.96	6.50	6.88	7.96	9.76	11.52	13.97	13.96	13.77	13.48	293 11
279	10.52	8.76	7.36	6.77	7.46	8.52	10.36	12.17	14.56	14.48	13.46	11.12	8.84	6.87	5.64	5.46	6.30	8.06	10.30	12.80	14.34	15.00	14.16	12.26	294 12
280	9.96	7.92	6.50	7.10	6.22	8.82	10.86	13.12	14.54	15.07	14.56	12.60	9.98	7.47	5.46	4.96	6.60	9.93	11.80	14.15	15.84	15.96	14.52	9.24	295 14
281	7.24	6.16	6.40	7.67	9.66	11.93	14.14	15.62	14.36	11.76	8.61	6.02	4.72	3.86	5.14	7.32	13.10	10.15	15.67	16.78	16.26	14.16	11.00	8.32	296 15
Sum	840.73	786.15	738.93	740.84	775.93	753.94	688.49	681.39	736.85	783.00	812.76	757.39	765.96	826.76	826.65	784.56	712.35	707.19	739.00	748.65	744.34	712.16	751.51	793.95	No. of Days.
No.	77	73	70	73	76	77	72	70	74	76	77	70	70	75	77	75	70	71	76	77	74	70	72	76	78 16.

FORMS FOR SHORT-PERIOD TIDES.  
SERIES v.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
282	6.36	5.84	6.47	8.16	10.16	12.84	15.02	16.10	15.46	13.28	9.87	6.84	4.45	3.04	5.44	8.15	11.37	14.60	16.81	17.35	16.28	13.64	10.44	7.71	297 16	
283	6.07	5.84	6.88	8.87	11.47	14.12	15.94	16.22	14.81	8.55	5.46	3.46	2.87	4.17	6.35	9.32	13.00	15.95	17.47	17.44	15.72	12.68	9.66	7.28	298 17	
284	5.94	6.04	7.36	9.64	14.84	16.04	15.60	13.70	10.52	7.15	4.06	2.02	3.10	4.72	7.47	10.55	13.92	16.35	17.36	16.74	14.57	11.67	8.85	5.94	299 19	
285	6.28	7.70	9.92	12.68	14.78	15.58	14.78	12.36	9.56	6.36	4.20	3.07	3.72	5.55	8.04	11.05	14.10	16.17	16.12	14.06	11.35	8.82	7.14	6.57	300 20	
286	7.02	8.46	10.56	13.14	14.64	15.04	13.76	11.47	8.74	6.42	4.70	4.22	5.00	9.02	11.88	14.60	16.14	16.22	15.16	13.56	10.86	8.86	7.58	7.14	301 21	
287	7.44	8.84	10.94	12.84	13.84	13.86	12.57	10.08	8.54	5.56	5.27	5.98	7.33	9.36	11.72	14.00	15.22	15.38	14.58	12.88	11.01	9.42	8.12	7.64	302 22	
288	7.92	8.94	10.40	11.85	13.12	12.56	10.75	9.22	7.66	6.68	6.30	6.72	7.86	9.44	11.50	13.34	14.46	14.66	13.96	12.74	11.30	9.76	8.54	7.84	304 0	
289	8.40	9.60	10.88	12.06	12.64	12.40	11.47	10.10	8.76	7.68	7.01	7.06	7.90	9.22	10.97	12.56	13.72	14.04	13.04	11.45	9.76	8.15	7.22	7.02	305 1	
290	7.48	8.84	10.32	11.48	12.55	12.87	12.46	11.36	9.70	8.28	7.14	6.80	7.40	10.74	12.56	13.87	14.54	14.38	13.40	11.67	9.60	7.53	6.30	5.88	306 2	
291	6.50	8.20	10.07	11.93	13.36	14.04	13.66	12.30	8.61	7.37	6.44	6.77	8.02	10.14	12.60	14.13	15.08	14.96	13.80	11.64	9.03	6.96	5.44	5.04	307 3	
292	5.86	7.79	10.12	12.66	15.37	14.86	13.04	10.66	8.56	7.12	6.44	6.51	8.24	10.85	13.27	15.16	15.84	15.03	13.56	10.92	8.12	5.82	4.22	5.32	308 5	
293	7.70	10.85	13.65	15.51	16.05	15.06	12.86	10.40	8.16	6.53	5.96	6.71	8.67	13.84	15.52	15.84	14.55	12.98	9.78	7.04	4.71	3.46	3.86	5.60	309 6	
294	8.44	11.74	14.64	16.50	16.72	15.38	12.86	9.98	7.70	6.25	5.93	6.71	11.25	14.35	15.67	15.28	13.15	10.15	8.46	5.64	3.63	3.01	4.08	6.50	310 7	
295	9.64	13.08	15.81	17.12	16.72	14.87	12.03	9.20	6.32	6.37	7.46	9.00	12.20	14.76	15.16	13.92	11.40	8.36	5.66	3.69	2.94	3.94	5.01	7.60	311 8	
296	10.76	14.05	16.38	16.14	13.92	11.10	8.66	6.87	6.16	6.46	8.00	10.44	13.14	13.43	14.50	14.36	12.66	9.94	7.20	3.56	3.77	5.34	7.72	12.24	312 10	
297	14.93	16.53	16.56	15.16	12.66	10.06	7.96	6.74	6.60	7.35	9.00	11.24	13.43	14.50	14.36	12.66	9.94	4.97	3.56	3.77	5.34	7.72	10.56	13.46	313 11	
298	15.64	16.34	15.71	13.92	11.46	9.28	7.66	6.86	6.98	7.98	9.96	12.00	13.52	13.37	11.18	8.81	6.52	4.86	4.33	5.20	6.90	9.14	11.80	14.20	314 12	
299	15.72	15.81	14.66	12.72	10.71	8.96	7.82	7.56	7.56	9.16	10.68	12.24	13.26	13.26	12.06	10.17	8.00	6.25	5.31	5.50	6.66	8.34	10.52	12.80	315 13	
300	15.18	14.68	13.32	11.56	10.02	8.76	8.10	8.00	8.60	9.65	10.96	12.58	12.23	11.04	9.16	7.62	6.54	6.20	6.84	7.96	9.38	11.14	12.91	14.40	316 15	
301	13.64	12.37	10.99	9.58	8.78	8.46	8.68	9.36	10.00	10.94	11.57	11.80	11.36	10.28	8.94	7.84	7.18	7.86	9.44	10.56	11.74	12.76	13.34	13.26	318 17	
302	12.96	11.72	10.53	9.06	9.14	8.92	8.96	9.17	9.66	10.40	11.10	11.37	10.20	9.26	8.46	8.10	8.14	8.66	9.50	10.42	11.46	12.48	13.10	13.15	319 18	
303	12.64	11.72	10.86	9.76	9.04	8.80	8.85	9.16	10.14	10.74	11.18	11.32	11.06	10.38	9.58	8.94	8.71	8.90	9.50	10.42	11.46	12.48	13.16	12.84	320 20	
304	12.64	11.84	10.76	8.88	8.35	8.10	8.42	9.04	9.96	10.86	11.50	11.80	11.86	10.96	10.25	9.04	8.36	8.34	10.02	11.20	12.46	13.33	13.47	13.00	321 21	
305	11.84	10.56	9.24	8.13	7.50	7.43	7.86	8.83	10.03	11.16	12.23	12.80	12.64	11.66	10.25	9.04	8.36	8.96	10.13	11.64	13.14	13.94	13.94	13.00	322 21	
306	11.72	10.14	8.38	7.03	6.27	6.31	7.08	8.52	10.23	11.92	13.17	13.63	13.10	10.18	8.76	7.98	7.96	8.22	9.82	10.37	12.25	13.88	13.94	13.00	322 22	
307	11.34	9.30	7.45	5.86	5.13	5.46	6.76	8.80	13.20	14.66	14.98	13.63	11.86	10.18	8.76	7.98	7.96	8.22	10.37	12.25	13.88	14.74	13.94	13.00	322 22	
308	10.56	7.98	4.14	3.74	4.67	6.71	9.27	12.02	14.40	15.66	15.44	13.71	11.76	9.38	8.10	7.27	7.36	8.22	10.37	12.25	13.88	14.74	13.94	13.00	322 23	
309	6.51	4.12	2.75	2.94	4.56	7.03	10.05	13.27	15.65	16.62	15.90	13.76	10.86	8.17	6.45	5.84	6.36	8.22	10.37	12.25	13.88	14.74	13.94	13.00	325 1	
310	4.96	2.57	1.63	2.38	4.74	7.64	11.12	14.22	16.47	17.07	15.75	12.96	9.86	7.26	5.65	5.46	6.44	8.40	11.20	13.57	15.11	15.17	13.27	9.96	6.40	327 3
311	3.62	1.76	1.54	3.26	6.02	9.25	12.97	15.66	17.25	15.37	12.23	9.00	7.26	5.65	5.63	6.88	9.32	12.22	14.44	15.50	14.80	12.31	8.84	5.46	328 4	
312	3.00	1.66	4.15	6.93	10.46	13.81	16.44	17.54	16.82	14.56	11.38	8.50	6.32	5.44	5.74	7.26	10.06	12.76	14.67	15.26	14.06	11.32	8.05	5.16	2.94	329 6
313	2.16	3.11	5.16	7.96	11.23	14.50	16.57	17.22	16.23	13.81	10.68	8.07	6.16	5.50	5.88	7.64	10.25	14.29	14.72	13.33	10.74	7.81	5.32	3.66	330 7	
314	3.26	4.42	6.34	8.86	11.67	14.58	16.33	16.57	15.28	12.84	9.93	7.47	5.72	6.26	7.94	10.30	12.38	13.76	13.96	12.68	10.56	8.18	6.28	4.97	331 8	
315	4.83	5.73	7.34	9.38	12.05	14.37	15.76	14.56	12.28	9.94	8.13	6.64	6.14	6.54	8.04	10.04	11.78	12.86	13.16	12.24	10.73	8.96	7.30	6.24	332 9	
316	5.96	6.50	9.94	12.15	13.88	14.87	14.84	13.77	11.77	10.66	8.23	6.86	6.34	6.56	7.70	9.30	10.84	12.16	12.76	12.53	11.48	8.60	7.52	7.06	823 11	

317	7.44	8.47	10.17	11.91	13.34	14.21	14.40	13.72	12.30	10.42	8.41	6.88	6.14	6.37	7.32	8.81	10.45	12.86	13.08	12.42	11.25	9.75	8.54	7.84	334 12
318	7.88	8.64	10.02	11.65	13.16	14.14	14.30	13.64	12.17	10.31	8.37	6.68	5.86	6.88	8.64	10.40	12.07	13.31	13.88	13.62	12.36	10.67	9.06	8.12	335 13
319	7.90	8.54	9.72	11.26	12.78	13.82	14.20	12.14	10.05	7.76	6.00	5.04	5.23	6.52	8.50	10.56	12.60	14.12	14.40	13.86	12.58	10.80	8.97	7.94	336 14
320	7.68	8.24	9.50	11.14	12.75	13.98	14.44	13.73	11.85	9.10	6.84	4.41	5.04	6.57	8.66	11.20	13.52	15.24	15.84	15.08	13.13	10.86	7.82	7.54	337 16
321	8.05	9.36	11.14	12.94	14.20	14.46	13.36	11.28	8.58	5.98	4.22	3.96	5.07	6.97	9.54	12.26	14.54	16.34	15.17	12.88	10.26	8.38	7.53	7.40	338 17
322	8.14	9.77	11.52	13.36	14.60	14.56	12.94	10.26	7.33	5.11	3.87	4.05	7.81	10.61	13.20	15.47	16.54	16.21	14.70	12.20	9.81	8.08	7.33	7.37	339 18
323	8.31	10.05	12.02	13.86	14.76	14.17	12.16	6.32	4.31	3.72	4.64	6.56	9.06	11.87	14.55	16.23	16.72	15.97	13.94	11.34	8.98	7.71	7.36	7.70	340 19
324	9.02	10.97	14.40	14.70	13.44	10.64	7.77	5.58	4.12	4.16	5.63	7.85	10.36	13.16	15.34	16.56	16.48	15.11	12.72	10.27	8.26	7.37	8.12	9.82	341 21
325	11.91	13.58	14.48	14.07	12.12	9.32	6.72	4.74	3.96	4.91	6.70	9.02	11.70	14.07	15.87	16.56	13.96	11.44	9.32	7.80	7.24	7.44	8.72	10.57	342 22
326	12.55	14.00	14.24	13.24	10.72	8.06	5.93	4.58	4.74	6.03	8.20	10.34	12.88	15.05	16.23	16.28	14.89	12.63	10.30	8.54	7.57	7.44	9.64	11.50	343 23
327	13.03	13.80	13.45	11.78	9.47	7.26	5.64	5.86	7.43	9.20	11.48	13.56	15.17	15.82	15.18	13.58	11.42	9.46	7.98	7.36	7.62	8.50	10.02	11.60	345 0
328	12.67	13.00	10.36	8.34	6.54	5.59	5.67	6.77	8.43	10.27	12.17	13.90	14.96	14.86	13.76	12.00	10.22	8.66	7.73	7.38	7.80	10.22	11.48	12.36	346 2
329	12.24	11.15	9.47	8.01	6.87	6.45	6.75	7.83	9.14	10.75	12.56	13.86	14.46	14.06	12.87	11.31	9.72	7.76	7.73	8.27	9.36	10.54	11.48	12.02	347 3
330	11.81	10.84	9.56	8.46	7.76	7.56	8.00	8.95	10.05	11.60	13.13	14.20	13.83	12.50	10.98	9.76	8.76	8.24	8.24	8.80	9.62	10.53	11.27	11.70	348 4
331	11.62	11.14	10.38	9.49	8.78	8.48	8.71	10.70	12.04	13.16	13.78	13.79	13.14	11.94	10.54	9.17	8.30	7.83	8.04	8.58	9.36	10.22	11.00	11.54	349 6
332	11.74	11.57	10.14	9.44	9.04	9.10	9.74	10.90	12.24	13.16	13.57	13.38	12.64	11.55	10.26	8.86	7.83	7.22	7.36	7.86	8.85	10.11	11.95	12.42	350 7
333	12.30	11.78	10.77	9.72	9.06	9.01	9.55	10.76	11.97	12.94	13.38	13.14	12.44	11.22											351 8
334																									352 9
335																									353 10
336																									354 12
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339																									357 15
340																									358 17
341																									359 18
342																									360 19
343																									361 20
344																									362 22
345																									363 23
346																									365 0
347																									366 1
348																									367 3
349																									368 4
350																									369 5
351																									370 2
Sum	479.15	635.61	575.11	611.05	577.86	584.12	613.64	623.08	557.65	499.96	483.21	522.49	560.63	516.09	530.96	559.39	621.65	665.82	64.559	175.46	275.58	67	512.06	465.31	No. of Days.
No. {	52	55	58	56	52	52	56	58	55	52	52	57	59	53	51	51	57	57	51	51	53	57	56	51	544 68
	70	77	76	74	70	73	76	76	73	70	74	76	77	71	70	75	76	76	70	70	75	75	74	69	73366.41

FORMS FOR SHORT-PERIOD TIDES.  
BOMBAY—Commencing 0 hours, Astronomical Time, 1st January, 1885.

Argument ( $\gamma - 2\sigma + \tau$ ). SERIES  $\mu$  or 2MS. Motion per mean Solar hour = 13°.9841042.

Table with 35 columns (Day 0h to 35h) and 12 rows of tidal data (feet, feet, feet, feet). Includes Solar Hour (d h) and Solar Hour (feet) values.









FORMS FOR SHORT-PERIOD TIDES.  
 SERIES  $\mu$  OF 2MS.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
130	15.63	13.90	11.47	9.28	7.84	7.40	7.74	8.02	10.62	12.60	14.02	14.27	13.22	8.10	5.76	4.17	5.26	7.20	9.70	12.28	14.66	15.94	16.04	150 1		
140	14.86	12.64	10.27	7.54	7.34	8.10	9.52	11.55	13.36	14.27	13.92	12.06	9.48	6.90	5.12	4.32	6.54	8.70	11.00	13.46	15.32	16.07	15.67	14.17	151 3	
141	11.77	9.56	8.16	7.68	7.83	10.50	13.26	13.66	14.02	12.96	10.86	8.34	6.24	5.04	4.82	5.84	7.60	9.46	11.87	14.10	15.60	14.66	12.78	10.74	152 5	
142	9.03	7.96	7.73	8.24	9.44	11.07	12.62	13.44	13.16	9.94	7.67	6.16	5.18	5.56	6.86	8.64	10.66	12.74	14.30	15.12	15.06	13.65	10.00	8.46	153 7	
143	7.75	7.78	8.46	9.92	11.36	12.37	12.84	12.22	10.98	9.18	7.32	6.03	5.94	8.17	9.67	11.58	13.24	14.64	14.97	14.22	12.62	11.08	9.47	8.38	154 8	
144	8.08	8.30	10.44	11.40	12.12	12.46	11.72	10.38	8.77	7.37	6.70	6.93	7.78	8.83	10.30	11.90	13.54	14.80	13.77	12.16	10.50	9.20	8.47	8.28	155 10	
145	8.60	9.36	10.36	11.26	11.83	12.05	10.60	9.20	8.14	7.72	7.83	8.62	9.82	11.10	12.64	13.94	14.46	14.16	13.26	11.74	9.26	8.54	8.34	8.46	156 12	
146	9.23	10.10	10.93	11.70	11.97	11.72	11.06	9.98	8.86	8.36	9.00	10.04	11.54	12.92	13.86	14.25	13.85	12.88	11.48	10.08	8.98	8.20	8.20	8.20	157 14	
147	10.03	11.29	12.14	12.58	12.36	11.84	11.02	10.06	9.23	8.78	9.20	10.37	11.98	13.41	14.22	14.34	13.94	12.86	11.59	10.03	8.74	7.92	7.54	7.76	158 15	
148	9.96	11.54	12.84	13.86	13.28	12.03	10.56	9.66	9.64	10.12	11.38	12.77	13.98	14.67	15.14	14.88	13.86	12.46	10.48	8.82	7.82	7.50	8.19	9.46	159 17	
149	13.22	14.76	15.83	15.76	14.97	13.34	11.70	10.27	10.56	11.52	12.90	14.12	15.30	15.65	15.48	14.17	12.02	9.86	8.00	7.09	7.72	9.34	11.40	13.77	160 19	
150	15.84	16.86	16.85	15.70	13.60	11.32	9.95	9.55	9.80	12.57	14.21	15.47	16.06	15.33	13.47	11.16	8.22	6.16	4.95	5.15	6.50	8.61	11.37	14.18	161 21	
151	17.54	17.17	15.66	12.50	10.07	8.34	8.17	8.96	10.27	12.23	14.24	15.74	16.29	12.77	9.46	6.32	4.44	3.62	4.30	6.30	8.54	11.95	15.02	17.28	162 22	
152	17.95	17.20	15.02	9.04	7.44	7.22	7.81	9.55	12.08	14.54	16.07	16.21	14.76	11.87	8.16	5.07	3.07	3.80	5.94	9.24	12.80	15.92	18.07	18.53	164 0	
153	17.65	14.65	10.90	8.00	6.62	6.55	7.50	12.45	14.89	16.40	15.16	14.28	10.90	7.10	4.31	2.54	4.18	7.11	10.40	13.95	16.74	17.85	17.40	15.44	167 5	
154	13.80	10.17	7.55	6.20	6.18	7.30	9.60	12.79	15.16	16.42	13.80	10.33	6.77	4.00	2.33	1.30	3.47	5.52	7.93	11.67	16.42	17.20	17.40	15.44	168 7	
155	9.60	7.05	5.72	5.77	7.00	9.56	12.80	15.12	16.05	15.26	12.76	9.20	6.14	2.88	3.47	5.52	7.93	11.67	16.42	17.20	16.60	14.54	11.30	8.66	168 7	
156	6.02	6.70	5.67	7.41	10.07	13.02	14.92	15.57	14.68	12.28	9.20	6.52	4.77	4.20	4.94	6.52	8.80	14.34	11.67	16.42	17.20	16.60	14.54	11.30	8.66	168 7
157	6.74	6.05	6.16	7.65	10.05	12.50	14.32	14.05	11.96	9.47	7.26	6.06	5.80	6.39	7.66	9.64	11.92	14.25	15.90	16.46	15.74	10.84	8.61	6.86	169 9	
158	6.32	6.58	7.80	9.82	12.04	13.55	14.17	13.54	12.03	10.34	7.57	6.66	7.26	7.62	8.44	9.92	12.12	14.20	15.46	15.54	14.58	12.66	10.40	8.31	7.04	170 10
159	6.60	7.78	9.32	11.22	12.80	13.58	13.46	12.40	10.90	9.62	8.66	8.31	8.49	9.03	10.30	13.70	14.74	14.75	13.73	12.02	10.10	8.46	7.12	6.53	171 12	
160	6.70	7.50	9.03	12.32	13.20	13.38	12.92	11.94	10.67	9.60	8.94	8.82	9.24	10.33	11.90	13.24	14.06	14.10	11.84	10.05	8.26	6.94	6.44	6.67	172 14	
161	7.49	9.06	10.86	12.50	13.66	14.10	13.63	12.46	11.06	9.30	9.05	9.33	10.22	11.60	12.90	13.82	13.85	13.08	11.64	9.76	8.00	6.08	6.22	7.28	173 16	
162	9.00	10.94	12.77	14.05	14.63	14.17	12.86	11.33	10.04	9.14	8.56	9.64	11.12	12.55	13.37	13.05	11.52	9.17	8.20	6.17	4.94	4.74	5.62	7.15	174 17	
163	11.30	13.28	14.45	14.84	13.95	12.40	10.90	9.46	8.62	8.24	8.86	10.08	11.26	12.44	13.30	13.52	12.80	11.00	8.85	7.06	5.67	5.05	5.60	7.15	174 17	
164	12.14	14.01	15.00	14.86	13.77	10.27	8.84	8.10	7.94	8.52	9.68	11.18	12.64	13.37	13.05	11.52	9.17	8.20	6.17	4.94	4.74	5.62	7.15	174 17		
165	14.56	15.33	14.70	13.32	11.14	9.44	8.17	7.54	8.34	9.81	11.65	13.20	13.60	12.56	10.40	7.97	5.83	4.38	4.04	4.96	6.82	6.10	8.00	10.50	12.90	176 21
166	15.44	14.56	12.56	10.36	8.63	7.62	7.30	7.44	8.86	10.67	12.47	13.67	13.06	12.02	9.66	6.93	4.96	3.94	4.22	5.70	7.84	10.40	12.82	14.74	15.56	179 0
167	15.33	13.80	11.44	9.35	7.79	7.04	7.03	7.90	9.44	11.66	13.22	13.02	13.06	10.74	8.00	5.64	3.83	4.76	6.70	9.02	11.37	13.67	15.12	15.46	180 2	
168	12.44	9.96	8.16	6.86	6.04	6.42	8.42	10.44	12.57	13.67	13.68	12.22	13.06	6.86	4.96	3.98	4.36	5.65	7.72	10.02	14.31	15.28	15.12	13.77	11.30	181 4
169	9.01	7.37	6.64	6.56	7.46	9.06	11.01	12.70	13.51	11.07	8.44	6.12	4.72	4.42	5.32	6.94	8.97	11.17	13.22	14.74	15.17	12.16	9.74	7.86	182 6	
170	6.74	6.51	7.07	8.16	9.93	11.66	12.82	13.10	11.86	9.72	7.36	5.70	5.24	6.42	8.07	10.12	11.98	13.73	14.86	14.72	13.40	11.17	9.22	7.55	183 7	
171	6.51	6.57	8.72	10.61	12.04	12.77	12.64	11.27	9.34	7.48	6.30	5.87	6.54	7.66	9.24	10.97	14.38	14.88	14.20	12.50	10.34	8.44	7.22	6.77	184 9	
172	6.97	7.87	9.34	10.94	12.10	12.22	10.82	9.25	7.90	6.96	6.92	7.56	8.50	10.00	11.48	13.23	14.36	14.44	11.42	9.60	8.02	6.94	6.56	6.92	185 11	
173	7.79	9.26	10.80	11.92	12.43	12.16	11.12	9.70	8.48	7.56	8.14	9.04	10.41	11.98	13.30	13.98	13.72	12.51	10.84	9.66	7.47	6.70	6.48	6.48	7.86	186 18

174	9.16	10.52	11.71	12.36	12.28	11.46	10.38	9.16	8.34	8.14	8.38	9.04	10.37	13.16	13.66	13.27	11.87	10.34	8.57	7.08	6.14	5.87	6.26	7.22	187.14	
175	8.72	10.36	12.56	12.86	12.14	11.14	9.86	8.86	8.32	8.34	9.02	10.46	11.88	13.12	13.48	12.86	10.30	8.58	7.00	5.74	5.32	5.74	6.86	8.67	188.16	
176	10.62	12.30	13.47	13.96	13.31	12.10	9.04	8.28	8.37	8.98	10.28	11.72	13.02	13.62	13.24	12.02	10.14	8.20	6.16	4.76	4.31	6.40	8.62	10.94	189.18	
177	13.04	14.57	15.22	14.64	12.87	10.58	8.66	7.68	7.62	10.00	11.70	13.12	13.97	13.69	12.32	10.27	7.76	5.44	3.88	3.19	3.88	5.80	8.60	13.90	190.20	
178	15.34	16.06	15.08	12.92	10.40	8.23	7.07	6.90	7.82	9.54	11.60	13.35	14.38	12.76	10.16	7.15	4.46	2.56	2.27	3.49	5.92	8.80	12.36	15.04	191.21	
179	16.76	17.06	15.90	10.08	7.42	6.03	6.04	7.17	9.30	11.84	13.92	15.05	14.90	13.08	9.91	6.43	3.81	1.84	3.58	6.20	9.54	13.00	15.92	17.60	192.23	
180	17.55	15.88	12.54	9.04	6.46	4.98	6.66	6.66	6.66	13.24	15.46	13.76	8.60	5.17	2.76	1.62	2.37	4.50	7.60	10.13	13.94	16.80	18.22	17.87	194.1	
181	15.72	12.00	8.47	5.86	4.66	4.66	6.66	6.66	6.66	13.24	15.46	13.76	8.60	5.17	2.76	1.62	2.37	4.50	7.60	10.13	13.94	16.80	18.22	17.87	195.3	
182	11.14	7.30	5.12	4.24	4.66	4.66	6.66	6.66	6.66	13.24	15.46	13.76	8.60	5.17	2.76	1.62	2.37	4.50	7.60	10.13	13.94	16.80	18.22	17.87	196.4	
183	10.38	7.04	4.76	5.04	7.14	10.42	13.85	15.77	16.14	14.53	11.60	8.45	5.84	4.20	3.82	5.12	9.80	10.24	12.80	15.30	15.86	14.11	11.28	8.50	198.8	
184	6.86	5.22	4.84	5.76	8.06	10.85	13.97	15.36	15.40	13.86	11.04	8.20	6.43	5.40	5.54	6.64	7.95	10.24	12.80	15.30	15.86	14.11	11.28	8.50	199.10	
185	5.34	5.40	6.24	8.00	10.50	12.97	14.30	14.44	12.94	10.92	7.74	7.24	7.56	8.14	9.16	11.11	13.10	14.71	15.40	14.72	12.96	10.60	8.38	5.92	200.11	
186	6.05	6.82	8.26	10.28	12.30	13.38	13.40	12.62	11.34	10.15	9.24	8.58	8.59	9.62	10.96	12.55	13.78	14.97	13.40	11.92	10.10	8.37	6.87	6.86	201.13	
187	6.51	7.24	8.41	11.28	12.52	12.90	12.68	11.87	10.93	10.01	9.34	9.14	9.27	9.97	10.90	12.12	13.14	12.71	11.34	9.77	8.47	7.34	6.76	6.86	202.15	
188	7.36	8.56	10.06	11.46	12.50	13.02	12.96	11.86	10.96	10.04	9.53	9.52	9.76	10.73	11.74	12.78	13.04	12.50	11.42	10.26	7.52	6.90	6.76	7.25	203.17	
189	8.50	10.20	11.86	13.24	13.87	13.87	13.28	12.22	11.04	10.07	9.50	9.87	10.64	11.70	12.60	12.94	12.66	11.70	10.10	8.56	7.16	6.24	6.28	8.62	204.19	
190	10.44	12.07	13.40	14.20	14.14	13.28	12.08	10.74	9.52	8.94	8.94	9.48	10.50	11.72	13.06	12.60	11.28	9.36	7.66	6.38	5.86	6.06	7.07	8.94	205.20	
191	10.96	13.07	14.58	15.07	13.34	11.84	10.26	9.14	8.46	8.46	9.16	10.36	11.74	13.14	13.52	12.81	11.24	7.31	5.74	5.33	6.10	7.65	9.76	13.02	206.22	
192	14.00	15.20	15.35	14.58	12.97	11.01	8.37	8.18	8.73	9.62	10.95	12.64	13.76	13.92	12.56	10.36	8.02	6.14	5.26	5.24	8.36	10.60	12.96	14.83	206.22	
193	16.05	15.68	14.35	12.14	9.54	8.56	8.04	8.20	8.78	9.99	11.82	14.66	14.04	11.84	8.90	6.50	5.04	4.74	5.78	7.22	9.33	11.77	14.22	15.86	207.23	
194	16.97	13.18	10.77	8.67	7.57	7.18	7.78	8.96	10.77	12.83	14.27	14.50	13.28	10.70	7.76	5.53	4.56	5.04	4.74	5.78	7.22	9.33	11.77	14.22	15.86	207.23
195	15.15	11.94	9.36	7.58	7.16	8.00	9.72	11.80	13.84	14.90	14.32	12.37	9.57	6.78	5.10	4.56	5.42	7.13	11.96	14.36	15.96	16.14	15.17	12.96	210.3	
196	10.25	8.01	6.67	6.34	6.89	8.16	10.14	12.46	14.84	13.50	10.90	8.02	5.86	4.76	5.04	6.52	8.34	10.66	13.15	15.27	16.14	11.47	8.96	211.5		
197	7.02	6.16	6.33	7.34	9.23	11.44	13.54	14.24	14.58	14.24	12.42	7.44	5.64	5.14	5.97	7.54	9.60	11.76	13.95	15.50	15.83	14.93	12.72	10.10	7.72	212.6
198	6.16	6.54	7.96	9.86	12.04	12.74	14.37	13.56	11.51	8.97	7.02	5.96	5.96	7.12	8.61	12.64	14.44	15.35	15.26	13.84	11.46	8.86	6.95	5.97	213.8	
199	6.05	7.05	8.56	12.48	13.67	13.96	12.84	10.98	9.00	7.60	6.88	7.24	8.26	9.66	11.37	13.15	14.57	15.10	12.72	10.34	8.27	6.67	6.12	6.40	214.10	
200	7.34	8.74	10.52	12.20	13.26	13.32	12.36	9.38	8.24	7.77	8.12	8.86	10.16	11.76	13.33	14.29	14.38	13.46	11.64	9.64	7.76	6.10	6.50	7.54	215.12	
201	9.00	10.63	12.05	12.96	13.18	12.64	11.47	10.84	9.16	8.76	9.04	10.72	12.02	13.24	14.10	14.04	13.02	11.59	9.63	7.96	6.84	6.50	6.73	7.66	216.13	
202	9.04	12.10	13.14	13.55	13.28	12.50	11.34	10.26	9.52	9.35	9.67	10.59	11.83	12.88	13.62	14.04	11.15	9.50	7.86	6.50	5.94	6.16	7.10	8.50	217.15	
203	10.52	11.94	13.44	14.14	13.42	12.16	10.76	9.56	9.05	9.15	9.96	11.33	12.62	13.38	13.44	12.54	11.68	9.90	7.96	6.26	5.46	6.46	8.25	10.24	218.17	
204	12.44	14.18	15.26	15.50	14.64	12.94	10.78	9.16	8.76	9.78	11.16	12.57	13.70	14.26	14.02	12.80	10.52	8.01	5.84	4.76	4.81	5.98	10.32	13.02	219.19	
205	15.24	16.66	16.76	15.58	13.24	10.54	8.38	7.60	7.78	8.76	10.54	12.56	13.70	14.86	13.21	10.40	7.41	4.97	3.62	3.84	5.16	7.44	10.44	13.54	220.20	
206	16.14	17.54	17.44	15.84	12.90	9.72	7.44	6.60	6.85	8.10	10.22	13.15	16.26	15.72	10.33	6.96	4.40	3.04	3.33	5.32	7.86	11.08	14.56	17.20	221.22	
207	18.37	18.04	16.16	12.38	8.82	6.46	5.95	7.72	10.60	13.60	16.07	17.04	16.38	13.96	10.25	6.47	3.74	2.96	3.20	5.12	8.18	11.74	15.30	17.66	18.50	223.0
Sum	806.79	860.60	812.33	806.72	792.57	775.12	796.98	810.81	774.19	807.97	796.20	756.78	762.42	753.69	737.14	694.92	718.68	717.71	707.38	744.73	779.56	769.99	790.25	806.93	No. of Days.	
No.	74	73	75	75	74	73	74	75	72	75	75	72	74	75	75	73	75	74	73	74	75	74	73	74	74	1856.48

FORMS FOR SHORT-PERIOD TIDES. SERIES μ OF 2MS. — (Continued).

Table with 24 columns (Day, 0h to 23h) and 2 rows (feet, Solar Hour). Contains tidal data for days 208 to 242, showing water levels in feet and corresponding solar hours.

243	8.44	9.64	10.73	11.57	11.88	11.53	10.23	9.48	9.04	9.01	9.38	10.01	10.64	11.05	11.18	10.94	10.46	9.53	8.56	7.74	7.64	8.34	261 15			
244	9.42	10.67	11.65	12.46	12.82	12.62	12.04	10.96	9.85	8.96	8.86	10.44	11.23	11.67	11.60	10.92	9.74	8.36	7.26	6.68	6.86	7.74	262 16			
245	9.24	10.86	13.24	13.55	13.17	12.08	10.64	9.21	8.06	7.54	8.74	11.30	12.38	12.42	11.17	9.62	7.86	6.55	6.10	6.54	7.88	9.68	263 18			
246	11.56	13.16	14.03	14.06	13.18	9.86	8.07	6.97	6.64	7.14	8.38	10.20	11.92	13.44	12.50	8.70	5.75	5.90	6.36	8.04	10.20	12.32	264 20			
247	13.87	14.64	14.36	12.87	10.73	8.45	6.71	5.90	7.29	9.02	11.07	13.02	14.14	14.04	12.68	10.30	7.96	6.07	5.14	5.48	6.87	13.68	265 22			
248	15.37	14.28	12.24	9.67	7.34	5.74	5.30	6.12	7.84	9.97	12.54	14.50	14.46	12.23	9.34	6.94	5.36	4.94	5.94	8.06	10.08	12.62	266 23			
249	15.26	13.46	10.67	7.88	5.74	4.48	4.66	6.00	8.44	11.24	13.97	15.67	14.20	11.46	8.47	4.97	5.22	6.65	8.86	11.54	14.06	15.76	268 1			
250	12.14	9.06	6.37	4.56	3.93	4.93	6.93	9.34	12.33	15.80	13.61	10.52	7.73	5.38	4.88	5.77	7.56	10.04	15.94	15.62	13.71	10.64	269 3			
251	7.47	5.10	3.54	3.83	5.50	7.97	11.14	14.16	16.01	15.04	12.33	9.34	6.75	5.54	5.42	6.51	8.50	11.14	13.77	15.60	15.98	14.86	270 5			
252	4.30	3.67	4.60	6.44	9.03	12.27	14.84	16.21	15.96	14.09	11.42	8.56	6.17	7.42	9.65	12.22	14.26	15.46	15.24	13.48	10.57	7.65	5.42	271 6		
253	3.96	5.34	7.30	9.97	12.69	14.83	15.87	15.16	13.24	10.76	8.47	7.04	6.68	7.20	8.44	12.56	14.16	14.83	14.05	12.07	9.24	7.02	5.32	4.44	272 8	
254	4.61	5.87	7.97	10.37	13.07	14.81	14.13	12.37	10.44	8.86	7.87	7.56	7.92	8.94	10.67	12.44	13.74	13.97	12.81	10.85	7.10	5.78	5.25	5.76	273 10	
255	6.66	8.34	10.76	12.86	14.16	14.34	13.68	12.40	9.52	8.53	8.21	8.56	9.40	10.68	12.08	13.04	13.08	11.93	10.54	9.05	7.64	6.61	6.06	7.07	274 12	
256	8.81	10.63	12.30	13.68	14.16	13.66	12.66	11.46	10.12	9.18	8.77	8.56	10.17	11.30	12.30	12.61	12.14	11.16	9.92	8.44	7.14	6.37	6.38	7.34	275 13	
257	8.76	10.57	12.10	13.92	13.88	13.56	12.37	11.18	9.72	8.32	7.60	7.94	9.26	10.84	12.04	12.52	11.98	11.16	9.77	7.94	6.58	6.06	6.50	7.97	276 15	
258	9.84	11.56	13.26	14.17	14.66	14.52	13.27	11.34	9.06	7.37	6.82	8.74	10.66	12.11	13.20	14.04	13.84	12.76	10.92	8.58	5.94	6.30	7.07	277 17		
259	11.97	13.90	15.26	15.99	15.54	13.97	11.26	8.63	6.70	5.98	7.97	10.25	12.66	14.44	15.38	15.04	13.48	11.07	8.36	6.38	5.47	5.87	7.36	9.62	278 19	
260	14.54	16.28	16.98	16.37	13.80	10.49	7.50	5.61	5.14	5.74	7.77	10.54	15.71	16.85	16.30	14.16	10.84	7.77	5.85	5.07	5.66	7.50	9.87	12.74	279 20	
261	15.25	16.92	17.15	12.54	8.66	5.94	4.14	3.96	5.28	7.85	11.15	14.38	16.70	17.32	16.33	13.48	7.20	5.47	4.98	5.96	7.74	10.58	13.66	16.26	280 22	
262	17.40	16.86	14.56	10.89	7.40	4.72	3.98	3.37	3.98	6.37	8.78	10.54	15.71	16.85	16.30	14.16	10.84	7.77	5.85	5.07	5.66	7.50	9.87	12.74	281 20	
263	15.72	12.71	9.14	6.06	3.77	3.17	4.42	6.67	9.72	16.25	17.55	17.22	15.06	11.70	8.40	6.26	5.44	6.06	7.47	10.01	12.74	15.12	16.37	16.06	282 2	
264	11.94	7.42	4.80	3.12	3.62	5.50	8.04	11.13	14.40	16.50	17.22	16.16	13.58	10.36	6.24	6.04	6.91	8.53	10.52	13.06	15.02	15.64	14.36	11.93	284 3	
265	8.64	6.01	4.31	4.52	6.20	8.94	11.94	14.56	16.24	16.32	14.74	12.13	9.47	7.47	6.58	6.90	7.84	11.26	13.26	14.41	14.26	13.74	10.35	7.88	285 5	
266	5.80	4.44	4.58	5.92	7.85	10.30	12.70	15.54	15.01	13.36	11.14	9.11	7.80	7.42	7.74	8.64	10.04	11.80	13.04	13.64	13.06	9.07	7.14	5.84	286 7	
267	5.47	6.20	7.44	9.04	10.97	13.06	14.36	14.36	13.40	10.44	9.16	8.44	8.24	8.54	9.20	10.30	11.46	12.12	12.22	11.46	10.00	8.37	7.08	6.36	287 9	
268	7.32	8.34	9.60	11.24	12.72	13.46	13.28	12.32	11.06	10.10	9.27	8.97	8.94	9.08	10.14	11.01	11.52	11.46	10.73	9.52	8.47	7.66	7.41	7.56	288 10	
269	8.04	8.76	9.91	12.36	12.06	12.40	12.34	11.06	10.82	9.97	9.24	8.77	8.68	8.96	9.55	10.22	10.88	10.82	10.57	10.03	9.22	8.56	8.06	8.06	289 12	
270	8.86	10.06	11.16	12.02	12.40	12.54	12.07	11.12	10.82	9.97	9.24	8.77	8.68	8.96	9.55	10.22	10.88	10.82	10.57	10.03	9.22	8.56	8.06	8.06	290 14	
271	9.84	10.90	11.78	12.36	12.58	12.54	12.07	11.12	10.82	9.97	9.24	8.77	8.68	8.96	9.55	10.22	10.88	10.82	10.57	10.03	9.22	8.56	8.06	8.06	291 15	
272	9.74	12.15	12.94	13.28	13.04	12.24	10.77	9.14	7.88	7.18	7.36	8.12	9.26	11.04	12.78	12.88	12.06	10.48	8.86	7.70	7.28	7.65	10.02	292 17		
273	11.54	12.81	13.77	13.50	12.16	10.00	8.34	6.96	6.50	6.88	7.96	9.76	11.52	13.07	13.96	13.77	12.48	10.52	7.36	6.77	7.26	8.52	10.36	12.17	293 19	
274	13.66	14.56	14.48	13.40	11.12	8.84	6.87	5.64	6.30	8.06	10.30	12.80	14.34	15.00	14.16	12.26	9.96	7.92	6.50	6.22	8.82	10.86	13.12	14.54	294 21	
275	15.07	14.56	12.60	9.98	7.47	5.46	4.56	6.00	9.03	11.80	15.84	15.96	14.52	12.00	9.24	7.24	6.16	6.40	7.67	9.66	11.93	14.14	15.62	205 22		
276	15.76	11.76	8.61	6.02	4.24	3.86	5.14	7.32	10.15	13.10	15.67	16.78	16.26	14.16	11.00	6.36	5.84	6.47	8.16	10.16	12.84	15.02	16.10	15.46	297 0	
Sum	772.62	751.66	767.12	757.22	732.52	765.92	777.83	762.45	808.90	813.02	803.52	799.98	806.10	791.47	744.97	751.18	718.14	720.00	728.12	723.87	739.64	741.67	751.35	756.37	No. of Days.	
No.	74	74	75	74	72	74	75	73	75	75	73	73	75	75	73	75	73	74	74	74	74	75	73	74	74	18285.59

FORMS FOR SHORT-PERIOD TIDES. SERIES μ or 2MS.—(Continued).

Table with columns for Day, Hour (0h to 23h), and Solar Hour. Each hour column contains a pair of values (feet and h). The table lists tidal data for days 277 through 311.

312	8.64	10.02	11.65	13.16	14.30	13.64	12.17	10.31	8.37	6.68	5.72	5.86	6.88	8.64	10.40	12.07	13.31	13.88	12.36	10.67	9.06	8.12	7.90	8.54	385 16		
313	9.72	11.20	12.78	13.82	14.20	13.74	12.14	10.03	6.00	5.04	5.23	6.52	8.50	10.56	12.60	14.12	14.40	13.86	12.58	10.80	8.97	7.68	8.24	9.50	386 17		
314	11.14	12.75	13.98	14.44	13.73	11.82	9.10	6.84	5.06	4.41	5.04	8.06	11.20	13.52	15.24	15.84	15.08	13.13	10.86	9.00	7.82	7.54	8.05	9.36	387 18		
315	11.14	14.20	14.46	13.36	11.28	8.58	5.98	4.22	3.96	5.07	6.97	9.54	12.26	14.54	16.11	15.17	12.88	10.26	8.38	7.53	7.40	8.14	9.77	11.52	388 20		
316	13.36	14.60	14.56	12.94	10.26	7.33	4.64	4.05	5.64	7.81	10.61	13.20	15.47	16.54	16.34	14.70	12.20	8.08	7.33	7.37	8.31	10.05	12.02	13.86	389 22		
317	14.70	14.17	12.16	8.03	6.32	4.31	3.72	4.64	9.06	11.87	14.55	16.23	16.72	15.97	13.94	11.34	8.98	7.71	7.36	7.70	9.02	10.97	14.40	14.70	391 0		
318	13.44	10.64	7.77	5.58	4.12	4.16	5.63	7.85	10.36	13.16	15.34	16.56	15.11	12.72	10.27	8.26	7.37	7.26	8.12	9.82	11.91	13.58	14.48	14.97	392 1		
319	12.12	6.72	4.74	3.96	4.91	6.70	9.02	11.70	14.97	15.87	16.56	16.56	13.96	11.44	9.32	7.24	7.44	8.72	10.57	12.55	14.00	14.24	13.24	10.72	393 3		
320	8.06	5.93	4.58	4.74	6.20	10.34	12.88	15.05	16.23	16.28	14.89	12.63	10.30	8.54	7.57	7.44	8.17	9.64	11.50	13.80	13.45	11.78	9.47	7.26	394 5		
321	5.64	5.07	5.86	7.43	9.20	11.48	13.56	15.17	15.18	13.58	11.42	9.46	7.98	7.36	7.62	8.50	10.02	11.66	12.67	13.00	12.14	10.36	6.54	5.59	395 7		
322	5.67	6.77	8.43	10.27	12.17	13.90	14.96	14.86	13.76	12.00	10.22	7.73	7.38	7.73	8.27	10.54	11.27	11.70	11.62	10.38	9.49	8.78	8.48	9.10	396 9		
323	6.75	9.14	10.75	12.56	13.86	14.46	14.06	12.87	11.31	9.72	8.40	7.76	7.73	8.27	9.36	11.48	12.02	11.81	10.84	9.56	8.46	7.76	7.56	8.00	397 10		
324	8.95	10.05	11.60	13.13	14.20	13.83	12.50	10.98	9.76	8.76	8.24	8.24	8.80	9.62	10.53	11.27	11.70	11.62	10.38	9.49	8.78	8.48	8.71	9.47	398 12		
325	10.70	12.04	13.16	13.78	13.79	13.14	11.94	10.54	9.17	7.83	8.04	8.58	10.11	11.13	11.93	12.42	12.30	11.78	10.77	9.72	9.06	9.01	9.55	10.76	399 15		
326	12.24	13.16	13.57	13.38	12.64	11.55	10.26	8.86	7.83	7.22	7.36	8.85	10.11	11.13	11.93	12.42	12.30	11.78	10.77	9.72	9.06	9.01	9.55	10.76	399 15		
327	11.97	12.91	13.38	13.14	12.44	11.22	9.78	8.36	7.04	6.26	6.15	8.20	9.97	11.56	12.90	13.50	12.36	10.92	9.68	8.84	8.68	9.14	10.18	11.57	351 17		
328	12.76	13.30	13.22	12.46	11.00	9.17	5.75	4.90	4.92	6.07	7.94	10.07	12.03	13.66	14.48	14.16	12.76	10.77	9.08	7.73	8.23	9.70	11.40	12.74	352 19		
329	13.42	13.45	12.54	10.80	8.50	6.30	4.47	3.64	5.82	8.20	10.84	13.27	14.95	15.70	14.97	13.95	10.60	8.64	7.50	7.36	8.16	9.80	11.80	14.33	353 21		
330	14.26	13.00	10.50	7.72	5.17	3.42	2.93	4.16	6.37	9.00	12.12	14.97	16.74	15.68	13.11	10.34	8.06	6.98	7.04	8.06	10.00	12.15	14.04	15.14	354 22		
331	15.03	13.10	7.00	4.27	2.40	2.20	3.93	6.57	9.77	13.27	16.13	17.72	17.31	15.78	12.57	7.27	6.14	6.36	7.56	9.86	12.72	14.77	15.81	15.20	356 0		
332	12.64	9.26	5.91	3.10	1.55	4.00	7.06	10.68	14.30	17.04	18.34	17.72	15.47	12.00	8.88	6.58	5.67	6.00	7.50	10.14	13.24	16.17	14.94	12.16	357 2		
333	8.55	5.06	2.64	1.50	2.57	5.14	8.44	11.93	17.66	18.34	17.37	14.51	10.92	7.77	5.66	5.14	5.64	7.65	10.63	13.44	15.40	15.86	14.14	7.68	358 4		
334	4.48	2.36	1.77	3.30	5.83	8.90	12.30	15.56	17.50	17.88	16.62	13.58	9.97	5.14	4.70	5.32	7.63	10.73	13.70	15.36	15.32	13.24	9.92	6.64	359 5		
335	4.73	3.07	4.74	6.97	9.86	13.01	15.80	17.38	17.48	15.95	12.86	9.53	6.72	5.22	4.90	5.87	8.03	13.30	14.68	14.83	13.44	10.55	7.68	5.43	360 7		
336	4.33	4.63	5.97	8.02	10.57	13.25	16.60	16.14	14.11	11.13	8.76	6.38	5.17	5.13	6.30	8.06	10.76	12.74	13.74	12.37	10.30	8.14	6.53	5.84	361 9		
337	6.14	7.14	8.74	10.77	13.13	14.96	15.71	15.12	13.32	8.44	6.53	5.48	5.27	6.00	7.78	9.85	11.62	12.84	13.10	12.28	10.74	9.22	7.96	7.33	362 11		
338	7.93	9.16	10.97	13.12	14.54	14.68	13.66	12.28	10.12	8.24	6.78	5.82	5.70	7.72	9.40	11.06	12.32	12.86	12.50	11.47	10.24	9.12	8.42	8.24	363 12		
339	8.54	9.54	11.12	13.37	13.57	12.88	11.44	9.87	8.24	6.74	5.77	5.52	6.37	7.72	9.94	10.64	12.10	13.12	12.46	11.26	10.02	9.06	8.58	8.66	364 14		
340	9.44	10.68	11.96	12.92	13.14	12.66	10.66	8.36	6.86	5.72	5.37	5.87	7.17	9.14	11.00	12.70	13.68	13.81	12.94	10.28	9.14	8.62	9.20	365 16			
341	10.44	11.66	12.53	12.92	12.58	11.64	9.77	7.86	6.12	5.05	5.62	7.06	9.15	11.26	13.23	14.30	14.32	13.36	11.78	10.34	9.17	8.44	8.24	9.76	366 18		
342	11.04	12.36	13.08	12.90	11.65	9.64	7.34	5.52	4.45	4.52	5.76	7.06	9.07	12.43	15.18	14.97	13.73	11.82	10.16	8.86	8.24	8.26	8.96	10.32	367 19		
343	11.70	12.96	13.58	13.16	11.26	8.91	6.66	4.96	4.33	4.86	6.36	8.55	11.00	13.44	15.21	15.84	15.17	13.56	9.66	8.38	7.80	7.97	9.00	10.56	368 21		
344	13.46	13.82	12.72	10.52	7.90	5.74	4.11	4.34	7.23	9.78	12.44	14.65	15.93	15.94	14.74	12.37	10.23	8.53	7.47	7.31	7.97	11.36	13.14	14.17	369 23		
345	14.00	12.18	9.43	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	370 2	
Sum	700.30	744.13	717.75	679.65	744.83	733.43	735.74	760.51	768.13	744.32	744.70	774.97	777.35	756.28	772.11	764.56	786.66	770.57	787.38	812.86	747.09	739.75	729.35	766.79	No. of Days.		
No.	73	75	71	73	74	73	74	73	74	72	71	74	74	72	73	72	74	72	74	74	74	72	73	73	73	79 <sup>a</sup> 2 <sup>b</sup>	
																										73	17948.95





36	7.18	9.07	11.36	13.26	14.34	14.26	12.88	11.00	9.39	8.26	7.92	8.30	9.05	10.36	12.08	13.76	14.66	14.44	13.11	11.12	9.30	7.54	6.26	6.13	36 22	
37	6.68	7.86	9.28	10.86	12.27	13.10	12.94	11.93	10.66	9.72	9.12	9.06	9.26	9.66	10.60	11.82	12.86	13.34	12.82	11.45	10.03	8.74	7.48	6.86	37 22	
38	6.78	7.17	7.94	9.05	10.30	11.34	11.97	11.92	11.42	10.84	10.34	10.07	9.97	9.77	9.94	10.44	11.32	12.06	12.26	11.78	10.88	9.87	8.84	7.86	38 22	
39	7.24	6.94	7.18	8.03	9.07	10.14	11.00	11.56	11.85	11.77	11.46	11.12	10.57	10.07	9.70	9.70	10.13	10.80	11.27	11.45	11.25	10.76	9.97	9.00	39 22	
40	8.00	7.11	6.58	6.74	7.44	8.51	9.84	10.90	11.76	12.34	12.55	12.30	11.60	10.57	9.76	9.34	9.17	9.56	10.24	10.94	11.36	11.44	10.97	10.10	40 22	
41	9.07	7.87	6.85	6.30	6.50	7.26	8.50	10.16	11.44	12.65	13.26	13.32	12.56	11.36	10.08	9.16	8.67	8.64	9.01	9.76	10.58	11.25	11.66	11.34	41 22	
42	10.36	8.82	7.36	6.12	5.54	5.82	6.94	8.54	10.36	12.06	13.46	13.97	13.64	12.30	10.76	9.26	8.14	7.84	8.12	8.96	10.24	11.52	12.40	12.66	42 22	
43	12.07	10.47	8.56	6.64	5.46	5.20	5.93	7.55	9.56	11.72	13.53	14.67	14.84	13.98	12.14	10.00	8.54	7.66	7.53	8.16	9.56	11.03	12.66	13.62	43 22	
44	13.60	12.30	10.24	7.77	5.88	4.84	4.96	6.33	8.27	10.66	13.07	14.85	15.64	15.23	13.64	11.13	9.02	7.54	6.79	7.00	8.13	9.87	11.85	13.60	44 22	
45	14.38	13.88	11.93	9.10	6.54	4.66	4.00	4.90	6.86	9.20	11.97	14.34	15.82	15.96	14.78	12.26	9.64	7.46	6.24	5.96	6.74	8.48	10.85	13.07	45 22	
46	14.56	14.85	13.63	10.90	7.86	5.57	4.07	4.04	5.46	7.84	10.63	13.64	15.83	16.64	16.01	13.87	10.90	8.00	6.17	5.46	5.74	7.26	9.70	46 21		
47	12.25	14.42	15.50	15.15	13.08	9.90	6.94	4.75	3.92	4.66	6.62	9.46	12.60	15.08	16.60	16.64	15.00	11.93	8.96	6.76	5.63	5.06	5.54	7.84	47 21	
48	10.54	13.30	15.12	15.66	14.46	11.76	8.44	5.86	4.26	4.25	5.52	7.84	10.68	13.68	15.84	16.68	15.86	13.15	10.22	7.36	5.65	4.23	4.46	6.07	48 21	
49	8.56	11.57	14.06	15.34	15.51	13.57	10.53	7.47	5.38	4.52	5.04	6.70	9.14	12.18	14.74	16.26	16.26	14.64	11.74	8.68	6.28	4.54	4.14	5.07	49 21	
50	7.06	9.74	12.44	14.55	15.46	14.76	12.57	9.68	7.24	5.84	5.60	6.54	8.40	10.77	13.32	15.42	16.26	15.47	13.18	10.24	7.54	5.62	4.54	4.69	50 21	
51	5.80	7.87	10.40	12.80	14.50	15.06	14.03	11.86	9.36	7.58	6.64	6.76	7.86	9.60	11.66	13.73	15.08	15.32	14.12	12.82	10.24	6.90	5.18	4.58	51 21	
52	5.06	6.46	8.24	10.33	12.41	13.86	14.34	13.44	11.46	9.53	8.05	7.40	7.66	8.58	9.92	11.68	13.36	14.16	14.12	12.82	10.83	8.73	6.87	5.45	52 21	
53	4.92	5.44	6.63	8.23	10.14	11.77	12.96	13.40	12.76	11.56	10.24	9.04	8.45	8.28	8.67	9.76	11.20	12.50	13.18	13.06	11.88	10.25	8.57	6.96	53 21	
54	5.77	5.38	5.64	6.37	7.82	9.54	11.17	12.38	13.02	12.96	12.16	11.07	10.02	8.94	8.44	8.48	9.27	10.44	11.57	12.34	12.34	11.70	10.50	8.90	54 21	
55	7.32	5.96	5.24	5.12	5.86	7.17	8.90	10.63	12.10	13.16	13.56	13.13	11.86	10.27	8.88	8.08	7.87	8.42	9.56	10.87	11.93	12.44	12.26	11.27	55 21	
56	9.76	7.96	6.27	5.06	4.55	5.02	6.47	8.52	10.67	12.72	14.14	14.86	14.44	12.70	10.66	8.80	7.60	7.21	7.64	9.18	11.00	12.40	13.36	13.52	56 21	
57	12.60	10.86	8.63	6.40	4.63	4.06	4.70	6.46	8.84	11.30	13.80	15.56	16.25	15.33	12.96	10.26	7.95	6.54	6.18	7.03	8.83	11.00	12.96	14.40	57 21	
58	14.74	13.76	11.70	8.84	6.08	4.05	3.42	4.14	6.18	8.80	12.06	14.93	16.76	17.15	15.84	12.87	9.66	7.00	5.18	5.12	6.26	8.52	11.16	13.67	58 21	
59	15.38	15.86	14.57	11.93	8.26	5.48	3.42	2.92	4.14	6.52	9.58	13.16	16.04	17.62	17.34	15.27	11.66	8.27	5.56	4.16	4.32	5.84	8.66	11.92	59 21	
60	14.74	16.46	16.54	14.66	11.26	7.66	4.94	3.20	3.27	4.70	7.52	10.86	14.63	17.06	17.98	16.96	13.90	10.20	6.96	4.47	3.56	4.02	6.04	9.40	60 21	
61	12.86	15.55	16.86	16.36	13.86	10.44	6.92	4.54	3.37	3.90	5.80	8.56	12.33	15.44	17.27	17.40	15.46	12.03	8.50	5.70	3.74	3.27	4.33	7.10	61 21	
62	10.34	13.76	15.97	16.76	15.76	12.96	9.44	6.74	4.67	4.23	5.26	7.43	10.37	13.82	16.13	17.08	16.40	13.86	10.50	7.26	4.84	3.56	3.86	5.60	62 21	
63	8.27	11.55	14.34	16.02	16.28	14.66	11.66	8.60	6.46	5.26	5.46	6.56	8.86	11.44	14.36	15.97	16.18	14.88	12.00	8.86	6.28	4.57	4.06	4.86	63 21	
64	6.67	9.40	12.24	14.39	15.64	15.33	13.25	10.46	8.22	6.76	6.34	7.00	8.36	10.22	12.44	14.42	15.27	14.71	12.72	10.14	7.72	5.93	4.86	5.00	64 21	
65	6.10	8.03	10.30	12.47	13.97	14.58	13.92	12.03	10.14	8.54	7.56	7.56	8.42	9.82	11.34	12.96	14.04	14.24	13.22	11.36	9.36	7.50	6.27	5.84	65 21	
66	6.34	7.46	9.00	10.76	12.44	13.56	13.74	12.74	11.40	10.07	9.16	8.96	9.27	9.77	10.46	11.36	12.44	13.07	13.03	12.12	10.46	8.86	7.68	7.02	66 21	
67	7.02	7.66	8.54	9.66	10.96	12.24	12.88	12.88	12.24	11.43	10.66	10.24	10.16	10.24	10.47	10.86	11.44	12.02	12.40	12.24	11.36	10.18	8.87	7.97	67 21	
68	7.67	7.94	8.50	9.00	9.78	10.74	11.76	12.46	12.67	12.27	11.74	11.26	10.87	10.56	10.36	10.22	10.36	10.76	11.26	11.56	11.38	10.86	9.96	9.14	68 21	
69	8.40	7.98	7.80	7.86	8.34	9.30	10.46	11.44	12.08	12.36	12.27	12.03	11.50	10.78	10.20	9.73	9.58	9.87	10.35	10.80	11.10	11.10	10.78	10.32	69 21	
70	9.72	8.86	7.97	7.28	7.26	7.87	8.97	10.32	11.56	12.46	13.04	13.10	12.54	11.68	10.56	9.64	9.08	8.82	9.16	9.88	10.74	11.40	11.75	11.70	70 21	
71	11.14	10.07	8.84	7.56	6.74	6.70	7.63	8.94	10.62	12.06	13.26	13.78	13.68	12.86	11.34	9.88	8.86	8.16	8.03	8.46	9.64	10.86	12.06	12.78	71 21	
72	12.56	11.57	9.92	8.17	6.67	5.98	6.16	7.20	8.87	10.76	12.70	14.08	14.61	14.06	12.53	10.68	8.96	7.55	6.88	7.05	8.07	9.84	11.76	12.97	72 21	
73	13.54	13.03	11.46	9.42	7.27	5.74	5.30	5.90	7.44	9.66	11.92	14.02	15.17	15.16	13.87	11.66	9.44	7.56	6.34	6.07	6.86	8.68	10.80	12.96	73 21	
74	14.26	14.55	13.37	11.16	8.45	6.26	5.16	5.12	6.24	8.10	10.63	13.22	15.15	15.86	15.17	13.22	10.40	7.86	6.06	5.25	5.54	6.90	9.24	11.72	74 21	
Sum	767.64	795.61	794.06	763.88	717.33	666.62	622.12	613.15	634.65	688.92	766.40	851.29	923.85	967.47	976.31	947.28	888.49	804.19	735.85	673.17	640.65	630.83	668.92	717.19	No. of Days.	
No.	74	74	74	74	74	74	73	74	74	74	74	74	74	74	74	74	74	73	74	74	74	74	74	74	74	73 <sup>1</sup> 22 <sup>8</sup> 18264.87

FORMS FOR SHORT-PERIOD TIDES.

SERIES R.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
75	13.95	15.20	15.12	13.39	10.64	7.57	5.44	4.44	4.96	6.46	8.94	11.85	14.34	16.00	16.06	14.53	11.64	8.54	5.76	4.22	3.97	5.24	7.30	10.10	75 21	
76	13.02	15.04	16.00	15.20	12.86	9.54	6.67	4.92	4.38	5.52	7.55	10.33	13.50	15.75	16.73	16.07	13.66	10.42	7.22	4.92	3.64	4.00	5.66	8.33	76 21	
77	11.52	14.30	16.06	16.52	15.06	12.13	8.73	6.13	4.66	4.99	6.52	8.92	11.86	14.66	16.40	16.56	15.07	11.90	8.47	5.62	3.74	3.22	4.26	77 20		
78	6.60	9.60	12.85	15.23	16.56	16.25	14.26	10.83	8.00	5.75	5.11	5.88	7.84	10.46	13.38	15.68	16.60	15.80	13.36	10.12	7.06	4.83	3.54	3.76	78 20	
79	5.34	7.86	11.00	13.93	15.92	16.74	15.74	13.36	10.24	7.64	6.12	6.08	7.14	9.00	11.56	13.90	15.66	15.98	14.76	12.06	8.90	6.13	4.34	3.62	79 20	
80	4.36	6.06	8.47	11.31	13.87	15.62	16.12	14.97	12.74	10.02	8.05	6.96	7.06	7.93	9.67	12.07	14.08	15.23	15.08	13.57	11.16	8.26	6.08	4.76	80 20	
81	4.47	5.46	7.26	9.48	11.88	13.90	15.36	15.50	14.66	12.67	10.54	8.74	7.94	8.14	9.06	10.62	12.40	13.77	14.52	14.20	12.80	10.64	8.47	6.76	81 20	
82	5.86	5.82	6.49	7.75	9.52	11.71	13.54	14.73	14.90	14.06	12.63	11.05	9.70	8.86	8.72	9.12	10.24	11.76	13.06	13.60	13.34	12.06	10.56	8.92	82 20	
83	7.40	6.43	6.30	6.68	7.68	9.46	11.24	13.02	14.08	14.52	14.22	13.04	11.70	10.34	9.24	8.84	9.04	9.84	10.96	12.05	12.86	12.96	12.44	11.22	83 20	
84	9.67	8.30	7.06	6.48	6.64	7.48	8.86	10.64	12.34	13.74	14.48	14.44	13.62	12.12	10.36	8.96	8.11	7.96	8.44	9.76	11.26	12.36	12.92	12.78	84 20	
85	11.94	10.50	8.78	7.20	6.06	5.92	6.72	8.34	10.26	12.20	13.86	15.00	15.14	14.16	12.20	9.88	8.00	6.90	6.56	7.46	9.22	11.16	12.56	13.57	85 20	
86	14.06	13.37	11.72	9.38	7.17	5.72	5.38	6.17	7.82	10.00	12.50	14.54	15.84	15.94	14.64	12.14	9.36	6.97	5.74	5.63	6.67	8.88	11.24	13.46	86 20	
87	14.86	15.36	14.34	12.05	9.44	6.93	5.38	5.00	5.82	7.83	10.50	13.30	15.60	16.72	16.28	14.37	11.37	8.36	6.00	4.67	4.80	6.40	9.20	12.06	87 20	
88	14.62	16.12	16.16	14.90	12.22	9.12	6.60	5.05	4.86	5.87	8.10	11.14	14.15	16.35	17.15	16.24	13.58	10.14	7.06	4.83	3.96	4.70	6.72	9.92	88 20	
89	13.20	15.64	17.04	16.75	14.92	11.81	8.56	6.27	5.14	5.64	6.94	9.43	12.61	15.44	17.03	17.08	15.36	11.92	8.64	6.18	4.48	4.25	5.24	7.57	89 20	
90	11.00	14.10	16.43	17.34	16.56	14.28	10.82	7.84	5.95	5.42	6.12	7.87	10.62	13.66	16.10	17.14	16.46	13.96	10.44	7.12	4.80	3.83	4.41	6.43	90 20	
91	8.78	12.04	14.74	16.66	17.13	15.64	12.86	9.53	7.16	5.81	5.93	7.22	9.26	12.02	14.66	16.44	16.67	15.06	12.02	8.56	5.84	4.04	3.84	4.93	91 20	
92	7.24	10.09	13.22	15.56	16.90	16.56	14.74	11.68	8.84	7.02	6.48	7.04	8.26	10.50	13.00	14.94	15.83	15.12	12.94	9.87	7.14	5.16	4.22	4.76	92 20	
93	6.49	8.73	11.37	14.00	15.82	16.34	15.34	13.10	10.40	8.36	7.32	7.28	8.03	9.50	11.53	13.48	14.74	14.92	13.67	11.34	8.76	6.67	5.40	5.22	93 20	
94	6.16	7.85	9.97	12.30	14.30	15.48	15.46	14.27	12.24	10.20	8.78	8.26	8.47	9.24	10.52	12.04	13.48	14.16	13.84	12.27	10.16	8.14	6.47	5.74	94 20	
95	6.22	7.44	9.20	10.85	12.64	14.05	14.67	14.27	12.97	11.44	10.04	9.16	8.84	9.16	9.84	10.95	11.96	12.80	12.96	12.28	10.94	9.24	7.80	6.78	95 20	
96	6.70	7.30	8.37	9.54	10.90	12.34	13.52	13.80	13.26	12.13	10.96	10.04	9.60	9.33	9.54	9.90	10.56	11.44	11.92	12.05	11.54	10.36	9.16	8.12	96 20	
97	7.47	7.44	7.87	8.52	9.46	10.73	11.93	12.74	12.98	12.60	11.86	11.07	10.34	9.94	9.77	9.87	10.02	10.36	10.81	11.14	11.27	10.92	10.30	9.34	97 20	
98	8.36	7.74	7.58	7.98	8.76	9.87	11.04	11.96	12.50	12.66	12.42	11.96	11.34	10.55	9.91	9.47	9.34	9.52	9.94	10.53	10.94	11.12	11.02	10.62	98 20	
99	10.00	9.22	8.40	8.01	8.13	8.63	9.70	10.66	11.77	12.66	13.06	12.94	12.40	11.47	10.50	9.62	8.94	8.54	8.74	9.48	10.45	11.36	11.88	11.89	99 20	
100	11.44	10.50	9.40	8.46	7.84	7.76	8.43	9.46	10.86	12.30	13.36	13.82	13.66	12.66	11.42	10.02	8.72	7.96	7.82	8.36	9.47	10.86	11.90	12.70	100 20	
101	12.87	12.44	11.06	9.52	8.12	7.40	7.47	8.26	9.54	11.08	12.70	14.06	14.56	14.22	12.80	10.96	8.88	7.46	6.81	6.84	7.92	9.62	11.52	13.00	101 20	
102	13.97	14.12	13.00	11.02	9.05	7.48	6.74	6.92	7.97	9.72	11.72	13.58	14.86	15.12	14.21	12.35	9.67	7.47	5.98	5.58	6.14	7.76	9.84	12.16	102 20	
103	14.02	15.18	15.06	13.40	10.95	8.28	6.66	6.02	6.46	7.88	10.06	12.53	14.55	15.72	15.49	13.80	11.08	8.22	5.93	4.52	4.32	5.47	7.72	10.54	103 20	
104	13.27	15.36	16.20	15.32	13.00	9.88	7.34	5.76	5.40	6.24	8.22	10.70	13.40	15.52	16.25	15.36	12.80	9.46	6.56	4.47	3.42	3.91	5.74	8.31	104 20	
105	11.40	14.40	16.28	16.72	15.47	12.68	9.44	6.81	5.47	5.38	6.52	8.91	11.80	14.40	15.97	16.08	14.35	11.30	7.80	4.97	2.93	2.46	3.76	6.21	105 20	
106	9.51	12.97	15.58	17.14	17.04	14.94	11.68	8.36	6.14	5.06	5.57	7.24	10.07	13.10	15.40	16.44	15.82	13.44	9.74	6.67	4.03	2.50	2.77	4.44	106 20	
107	7.50	10.96	14.33	16.70	17.72	16.91	14.37	10.87	8.10	6.15	5.71	6.50	8.36	11.33	14.12	15.97	16.50	15.10	12.22	8.67	5.24	3.17	2.56	4.11	107 19	
108	3.47	5.74	8.64	12.02	15.12	16.94	17.54	16.24	13.40	10.32	7.62	6.17	6.07	7.04	9.13	12.00	14.47	15.69	15.54	13.66	10.74	7.44	4.88	3.28	108 19	
109	3.04	4.36	6.67	9.40	12.47	15.00	16.74	16.94	15.60	13.03	10.01	7.87	6.76	6.80	7.71	9.70	12.14	14.15	15.02	14.50	12.53	9.92	7.24	5.36	109 19	



FORMS FOR SHORT-PERIOD TIDES.  
SERIES R.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
149	6.00	8.33	10.94	13.60	15.42	16.13	15.62	13.90	11.47	9.28	7.84	7.40	7.74	8.92	10.62	12.60	14.02	14.27	13.22	10.78	8.10	5.76	4.27	4.17	149 18	
150	5.26	7.20	9.70	12.28	14.66	15.94	16.04	14.86	12.64	10.27	8.44	7.54	7.34	8.10	9.52	11.55	13.36	14.27	13.92	12.06	9.48	6.90	5.12	4.32	150 18	
151	4.97	6.54	8.70	11.00	13.46	15.32	16.07	15.67	14.17	11.77	9.56	8.16	7.68	7.83	8.74	10.50	12.26	13.66	14.02	12.96	10.86	8.34	6.24	5.04	151 18	
152	4.82	5.84	7.60	9.46	11.87	14.10	15.30	15.60	14.66	12.78	10.74	9.03	7.96	7.73	8.24	9.44	11.07	12.62	13.44	13.16	11.96	9.94	7.67	6.16	152 18	
153	5.18	5.56	6.86	8.64	10.66	12.74	14.30	15.12	15.06	13.65	11.84	10.00	8.46	7.75	7.78	8.46	9.92	10.24	12.37	12.84	12.22	10.98	9.18	7.32	153 18	
154	6.03	5.94	6.87	8.17	9.67	11.58	13.28	14.64	14.97	14.22	12.62	11.08	9.47	8.38	8.08	8.30	9.20	10.24	11.40	12.12	12.46	11.72	10.38	8.77	154 18	
155	7.37	6.70	6.91	7.78	8.83	10.30	11.90	13.54	14.68	14.80	13.77	12.16	10.50	9.20	8.47	8.28	8.60	9.36	10.36	11.26	11.83	12.05	11.56	10.60	155 18	
156	9.20	8.14	7.72	7.83	8.62	9.82	11.10	12.64	13.94	14.46	14.16	13.26	11.74	10.42	9.26	8.54	8.34	8.46	9.23	10.10	10.93	11.70	11.97	11.72	156 18	
157	11.06	9.98	8.86	8.32	8.36	9.00	10.04	11.54	12.92	13.86	14.25	13.85	12.88	11.48	10.08	8.98	8.20	8.20	8.37	9.12	10.03	11.29	12.14	12.58	157 18	
158	12.36	11.84	11.02	10.06	9.23	8.78	9.20	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	10.03	8.74	7.92	7.54	7.76	8.67	9.96	11.54	12.84	158 18	
159	13.87	13.86	13.28	12.03	10.56	9.66	9.64	10.17	11.38	12.77	13.98	14.67	15.14	14.88	13.86	12.46	10.48	8.82	7.82	7.50	8.19	9.46	11.28	13.22	159 18	
160	14.76	15.82	15.76	14.97	13.34	11.70	10.67	10.27	10.56	11.52	12.90	14.12	15.30	15.65	15.48	14.17	12.02	9.86	8.00	7.09	6.85	7.72	9.34	11.40	160 18	
161	13.77	15.84	16.86	16.85	15.70	13.60	11.52	9.95	9.55	9.80	10.84	12.57	14.21	15.47	16.06	15.22	13.50	10.84	8.22	6.16	4.95	5.15	6.50	8.61	161 18	
162	11.37	14.18	16.48	17.54	17.17	15.60	12.50	10.07	8.34	8.17	8.96	10.27	12.23	14.24	15.74	16.29	15.33	12.77	9.46	6.32	4.44	3.62	4.30	6.30	162 18	
163	8.54	11.95	15.02	17.28	17.95	17.20	15.02	11.76	9.04	7.44	7.22	7.81	9.55	12.08	14.54	16.07	16.21	14.76	11.87	8.16	5.07	3.07	2.74	3.80	163 18	
164	5.94	9.24	12.80	15.92	18.07	18.53	17.65	14.65	10.90	8.00	6.62	6.55	7.50	9.65	12.45	14.89	16.40	16.14	14.28	10.90	7.10	4.31	2.62	2.37	164 18	
165	3.68	6.30	9.76	13.48	16.44	18.12	18.40	17.00	13.80	10.17	7.55	6.20	6.18	7.30	9.60	12.79	15.16	16.42	15.96	13.80	10.33	6.77	4.00	2.33	165 18	
166	2.54	4.18	7.11	10.40	13.95	16.74	17.85	17.95	16.07	12.81	9.60	7.05	5.72	5.77	7.00	9.56	12.80	15.12	16.05	15.26	12.76	9.20	6.14	3.95	166 18	
167	2.88	3.47	5.52	7.93	11.04	14.21	16.44	17.72	17.40	15.44	12.07	9.02	6.70	5.67	5.93	7.41	10.07	13.02	14.92	15.57	14.68	12.28	9.20	6.14	167 18	
168	4.77	4.20	4.94	6.52	8.80	11.67	14.34	16.42	17.20	16.60	14.54	11.30	8.66	6.74	—	6.05	6.16	6.65	10.05	12.50	14.32	14.85	14.05	11.96	168 17	
169	9.47	7.26	6.06	5.80	6.39	7.66	9.64	11.92	14.25	15.90	16.46	15.74	13.76	10.84	8.61	6.86	6.32	6.58	7.80	9.82	12.04	13.55	14.17	13.54	169 17	
170	12.03	10.34	8.60	7.57	7.26	7.62	8.44	9.92	12.12	14.20	15.46	15.74	14.58	12.66	10.40	8.31	7.04	6.60	6.77	7.78	9.32	11.22	12.80	13.58	170 17	
171	13.46	12.40	10.90	9.62	8.66	8.31	8.49	9.93	10.30	12.04	13.70	14.74	14.75	13.73	12.02	10.10	8.46	7.12	6.53	6.70	7.50	9.03	10.90	12.32	171 17	
172	13.20	13.66	14.10	13.63	12.46	11.06	10.60	9.30	9.05	10.33	11.90	13.24	14.06	14.10	13.34	11.84	10.05	8.26	6.94	6.44	6.67	7.49	9.06	10.86	172 17	
173	12.50	13.66	14.10	13.63	12.46	11.06	10.60	9.30	9.05	10.33	11.90	13.24	14.06	14.10	13.34	11.84	10.05	8.26	6.94	6.44	6.67	7.49	9.06	10.86	173 17	
174	10.94	12.77	14.05	14.63	14.17	12.86	11.33	10.04	9.14	8.86	9.20	10.08	11.26	12.44	13.30	13.52	12.80	11.00	8.85	7.06	5.67	5.05	6.60	7.15	174 17	
175	9.26	11.30	13.28	14.45	14.84	13.95	12.40	10.90	9.46	8.62	8.24	8.56	9.64	11.12	12.55	13.40	13.37	12.07	10.07	8.20	6.17	4.94	4.74	5.62	175 17	
176	7.74	9.76	12.14	14.01	15.00	14.86	13.77	12.06	10.27	8.84	8.10	7.94	8.52	9.68	11.18	12.64	13.37	13.05	11.52	9.17	6.76	5.11	4.16	4.64	176 17	
177	6.10	8.00	10.50	12.90	14.56	15.33	14.70	13.32	11.14	9.44	8.17	7.54	7.57	8.34	9.81	11.65	13.20	13.60	12.56	10.40	7.97	5.83	4.38	4.04	177 17	
178	4.96	6.82	9.02	11.57	13.86	15.24	15.44	14.56	12.56	10.36	8.63	7.62	7.30	7.74	8.86	10.67	12.47	13.67	13.60	12.02	9.66	6.93	4.96	3.94	178 17	
179	4.22	5.70	7.84	10.40	12.82	14.74	15.56	15.33	13.80	11.44	9.35	7.79	7.04	7.03	7.90	9.44	11.66	13.22	13.92	13.00	10.74	8.00	5.64	4.04	179 17	
180	3.83	4.76	6.70	9.02	11.37	13.67	15.12	15.46	14.48	12.44	9.96	8.16	6.86	6.42	6.94	8.42	10.44	12.57	13.67	13.68	12.22	9.64	6.86	4.96	180 17	
181	3.98	4.36	5.65	7.72	10.02	12.26	14.31	15.28	15.12	13.77	11.30	9.01	7.37	6.64	6.56	7.46	9.06	11.01	12.70	13.51	13.01	11.07	8.44	6.12	181 17	
182	4.72	4.42	5.32	6.94	8.97	11.17	13.22	14.74	15.17	14.22	12.16	9.74	7.86	6.74	6.51	7.07	8.16	9.92	11.66	12.82	13.10	11.86	9.72	7.36	182 17	
183	5.70	5.02	5.24	6.42	8.07	10.12	11.98	13.73	14.86	14.72	13.40	11.17	9.22	7.55	6.51	6.57	7.34	8.72	10.61	12.04	12.77	12.64	11.27	9.34	183 17	



FORMS FOR SHORT-PERIOD TIDES.

SERIES R.—(Continued).

Day	0 <sup>h</sup>		1 <sup>h</sup>		2 <sup>h</sup>		3 <sup>h</sup>		4 <sup>h</sup>		5 <sup>h</sup>		6 <sup>h</sup>		7 <sup>h</sup>		8 <sup>h</sup>		9 <sup>h</sup>		10 <sup>h</sup>		11 <sup>h</sup>		12 <sup>h</sup>		13 <sup>h</sup>		14 <sup>h</sup>		15 <sup>h</sup>		16 <sup>h</sup>		17 <sup>h</sup>		18 <sup>h</sup>		19 <sup>h</sup>		20 <sup>h</sup>		21 <sup>h</sup>		22 <sup>h</sup>		23 <sup>h</sup>		Solar Hour
	feet	d	feet	h	feet	h	feet	h	feet	h	feet	h	feet	h	feet	h	feet	h	feet	h	feet	h	feet	h	feet	h	feet	h	feet	h	feet	h	feet	h	feet	h	feet	h	feet	h	feet	h	feet	h	feet	h			
223	2.56	3.20	5.12	8.18	11.74	15.30	17.66	18.50	17.76	14.76	10.60	7.27	5.06	4.48	5.07	7.18	10.36	13.94	16.34	17.16	16.04	13.12	9.20	5.80	223 16																								
224	3.36	2.56	3.60	5.73	9.03	12.78	15.94	17.78	18.04	16.74	13.32	9.36	6.95	4.18	3.80	4.90	7.56	11.10	14.46	16.66	16.88	15.39	12.15	8.23	224 16																								
225	5.44	3.52	3.32	4.58	7.04	10.14	13.35	16.16	17.52	17.26	15.28	11.80	8.22	5.32	3.80	4.02	5.58	8.40	11.50	14.52	16.18	16.06	14.38	11.26	225 16																								
226	7.08	5.62	4.54	4.80	6.25	8.27	11.00	13.96	16.32	17.26	16.42	14.32	10.85	7.62	5.16	4.10	4.64	6.45	8.92	12.05	14.70	15.80	15.18	13.36	226 16																								
227	10.62	7.94	6.38	5.74	6.44	7.77	9.72	12.07	14.12	15.66	15.72	14.46	12.06	9.36	6.96	5.40	5.07	5.84	7.33	9.54	11.87	13.60	14.46	13.96	227 16																								
228	13.48	10.40	8.95	7.45	7.28	8.00	9.26	10.72	12.27	13.74	14.47	14.18	12.78	10.82	8.78	6.78	5.83	5.86	6.74	8.34	10.14	12.02	13.26	13.57	228 16																								
229	13.85	11.76	10.70	9.74	9.12	8.90	9.34	10.06	10.94	12.10	12.88	13.72	13.38	11.88	10.06	8.17	7.02	6.68	7.00	7.70	8.77	10.10	11.44	11.44	229 15																								
230	12.33	12.66	12.46	12.00	11.36	10.62	10.07	9.67	9.77	10.12	10.82	11.54	12.43	12.12	11.23	9.96	8.64	7.77	7.46	7.69	8.30	9.04	10.10	10.10	230 15																								
231	11.17	13.34	12.90	12.90	12.34	11.72	11.15	10.62	10.30	10.00	10.14	10.50	11.34	11.96	12.26	11.97	11.38	10.53	9.44	8.35	7.66	7.57	8.12	9.06	231 15																								
232	10.48	11.57	12.72	13.42	13.56	13.18	12.30	11.45	10.72	10.26	9.92	9.63	10.00	10.71	11.62	12.32	12.18	11.42	10.36	9.08	8.15	7.53	7.24	7.70	232 15																								
233	8.54	9.82	11.43	13.72	13.64	13.66	13.26	12.36	11.22	10.18	9.34	8.97	9.08	9.88	10.76	11.64	12.26	12.35	11.85	10.40	8.78	7.36	6.44	6.28	233 15																								
234	7.14	8.57	10.20	11.94	13.38	14.40	14.54	13.58	12.17	10.70	9.34	8.82	8.84	9.26	10.00	11.16	12.50	13.30	13.42	12.06	10.16	8.40	6.86	6.06	234 15																								
235	6.14	7.20	8.95	10.80	12.76	13.96	14.91	14.84	13.64	11.84	9.97	8.77	8.36	8.48	8.96	10.06	11.56	13.12	13.97	13.64	12.06	9.70	7.27	5.96	235 15																								
236	5.46	6.35	7.80	9.76	11.70	13.66	15.10	15.46	14.62	12.86	10.57	8.64	7.46	7.31	7.76	8.84	10.72	12.64	14.21	14.62	13.44	11.00	8.24	6.24	236 15																								
237	5.17	5.36	6.54	8.54	10.66	13.00	15.02	15.96	15.30	14.08	11.60	8.97	7.34	6.70	6.84	7.80	9.62	11.70	13.76	14.95	14.67	12.76	10.00	7.37	237 15																								
238	5.56	4.97	5.74	7.38	9.36	11.94	14.36	16.04	16.27	15.32	13.08	10.11	7.72	6.36	6.10	6.94	8.63	10.83	13.20	15.21	15.71	14.43	11.89	8.54	238 15																								
239	6.26	4.97	5.06	6.36	8.22	10.64	13.40	15.80	16.62	16.16	14.21	11.38	8.34	6.35	5.46	5.74	7.13	9.22	11.84	14.36	15.71	15.48	13.64	10.66	239 15																								
240	7.60	5.70	4.96	5.70	7.34	9.54	12.02	14.56	16.74	16.56	15.34	12.80	9.66	7.06	5.50	5.18	5.94	7.72	10.28	13.04	15.14	15.90	14.88	12.52	240 15																								
241	9.63	7.07	5.74	5.64	6.67	8.36	10.62	13.17	15.30	16.38	15.97	14.06	11.04	8.16	6.11	5.05	5.41	6.72	8.83	11.26	13.77	15.36	15.38	14.00	241 15																								
242	11.50	8.72	6.86	5.97	6.34	7.52	9.30	11.47	13.80	15.46	15.84	14.77	12.44	9.37	7.06	5.37	4.85	5.64	7.12	9.24	11.64	13.96	15.06	14.75	242 15																								
243	13.17	10.76	8.64	7.30	6.86	7.44	8.64	10.38	12.36	14.06	15.24	15.10	13.64	11.26	8.61	6.50	5.32	5.38	6.34	7.85	9.86	11.96	13.64	14.58	243 15																								
244	14.07	13.68	10.68	8.97	8.02	7.81	8.36	9.26	10.60	12.24	13.73	14.44	13.86	12.25	10.02	8.06	6.46	5.62	5.78	6.47	7.80	9.63	11.38	12.97	244 15																								
245	13.74	13.44	12.44	11.04	9.83	8.84	8.57	8.87	9.67	10.67	11.96	13.06	13.46	13.08	11.68	9.86	8.26	6.46	6.17	6.44	6.21	6.66	7.76	9.20	245 15																								
246	12.55	13.37	13.57	12.94	11.92	10.73	9.67	9.16	9.18	9.63	10.54	11.48	12.46	12.92	12.66	11.74	10.42	8.87	7.44	6.44	6.21	6.66	7.76	9.20	246 15																								
247	10.76	12.36	13.54	14.05	13.67	12.68	11.26	10.02	9.22	8.90	9.14	9.86	10.86	12.02	12.84	12.98	12.36	11.16	9.57	7.60	6.24	5.63	5.97	7.17	247 15																								
248	8.80	10.66	12.80	14.28	14.96	14.74	13.66	11.85	10.04	8.66	8.02	8.14	9.04	10.38	12.00	13.14	13.74	13.40	12.04	10.04	7.64	5.76	5.02	5.02	248 15																								
249	6.24	8.16	10.78	13.20	15.04	15.98	15.74	14.33	11.96	9.30	7.37	6.55	6.70	8.06	9.98	12.06	13.93	14.86	14.44	12.80	10.18	7.37	5.17	3.90	249 15																								
250	4.03	5.50	7.96	10.88	13.80	16.04	17.04	16.46	14.44	11.04	8.24	6.27	5.15	5.63	7.24	9.64	12.52	14.74	15.98	15.46	13.29	9.94	6.63	4.34	250 15																								
251	3.17	2.53	5.38	8.20	11.40	14.56	16.82	17.44	16.36	13.83	9.98	6.70	4.46	3.84	4.58	6.80	10.06	13.28	15.76	16.64	15.75	12.94	9.26	6.06	251 15																								
252	3.66	2.67	3.72	5.66	8.70	12.20	15.53	17.33	17.53	15.87	12.42	8.56	5.32	3.44	3.17	4.55	7.26	10.87	14.22	16.50	17.05	15.47	12.37	8.44	252 15																								
253	5.52	3.48	3.10	4.46	6.74	9.94	13.47	16.22	17.47	17.02	14.77	10.84	7.23	4.52	3.00	3.30	5.07	8.06	11.72	14.94	16.86	16.90	14.94	11.54	253 15																								
254	8.00	5.38	3.90	4.20	5.52	7.95	11.06	14.30	16.51	17.04	15.88	12.99	9.17	5.97	3.70	2.94	3.94	6.16	9.14	12.45	15.42	16.68	16.10	13.81	254 15																								
255	10.56	7.46	5.47	4.87	5.60	7.04	9.54	12.25	14.81	16.16	16.06	14.44	11.97	7.87	5.34	3.84	3.92	5.16	7.43	10.36	13.44	15.47	16.04	14.92	255 15																								
256	12.66	9.98	7.74	6.47	6.36	7.02	8.54	10.58	12.80	14.58	15.36	14.73	12.52	9.86	7.17	5.31	4.44	5.02	6.44	8.50	11.04	13.56	14.79	14.77	256 15																								
257	13.46	11.46	9.44	8.00	7.36	7.56	8.36	9.51	11.10	12.60	13.73	13.94	12.90	11.02	8.75	6.90	5.70	5.63	6.34	7.60	9.36	11.36	13.14	13.88	257 15																								



FORMS FOR SHORT-PERIOD TIDES.

SERIES R.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
297	11.00	8.32	6.36	5.84	6.47	8.16	10.16	12.84	15.02	16.10	15.46	13.28	9.87	6.84	4.45	3.04	3.57	5.44	8.15	11.37	14.60	16.81	17.35	16.28	297 13	
298	13.64	10.44	7.71	6.07	5.84	6.88	8.97	11.47	14.12	15.94	16.22	14.81	11.87	8.55	5.46	3.46	2.87	4.17	6.35	9.32	13.00	15.95	17.47	17.44	298 13	
299	15.72	12.68	9.66	7.28	5.94	6.04	7.36	9.64	12.45	14.84	16.04	15.60	13.70	10.52	7.15	4.66	2.92	3.10	4.72	7.47	10.55	13.92	16.35	17.36	299 13	
300	16.74	14.57	11.67	8.85	6.76	5.94	6.28	7.70	9.92	12.68	14.78	15.58	14.78	12.36	9.26	6.36	4.20	3.07	3.72	5.55	8.04	11.05	14.10	16.17	300 13	
301	16.96	16.12	14.06	11.35	8.92	7.14	6.57	7.02	8.46	10.56	13.14	14.64	15.04	13.76	11.47	8.74	6.42	4.70	4.22	5.00	6.80	9.02	11.88	14.60	301 13	
302	16.14	16.23	15.16	13.26	10.86	8.86	7.58	7.14	7.44	8.84	10.92	12.84	13.84	13.86	12.57	10.68	8.54	6.84	5.56	5.27	5.98	7.33	9.36	11.72	302 13	
303	14.00	15.22	15.38	14.58	12.58	11.01	9.42	8.12	7.64	7.92	8.94	10.40	11.85	12.91	13.12	12.26	10.75	9.22	7.66	6.68	6.30	6.72	7.86	9.44	303 13	
304	11.50	13.34	14.46	14.66	13.96	12.74	11.30	9.76	8.54	7.93	7.84	8.40	9.60	10.88	12.06	12.64	12.40	11.47	10.10	8.76	7.68	7.01	7.06	7.90	304 13	
305	9.22	10.97	12.56	13.72	14.38	14.04	13.04	11.45	9.76	8.15	7.22	7.02	7.48	8.84	10.32	11.48	12.55	12.87	12.46	11.36	9.70	8.28	7.14	6.80	305 13	
306	7.40	8.84	10.74	12.56	13.87	14.54	14.38	13.40	11.67	9.60	7.53	6.30	5.88	6.50	8.20	10.07	11.93	13.36	14.04	13.66	12.30	10.26	8.61	7.37	306 13	
307	6.86	7.24	8.35	10.36	12.50	14.13	15.08	14.96	13.80	11.64	9.03	6.96	5.44	5.04	5.86	7.79	10.12	12.66	14.54	15.37	14.86	13.04	10.66	8.56	307 13	
308	7.12	6.44	6.77	8.02	10.14	12.62	14.56	15.55	15.25	13.56	10.92	8.12	5.82	4.22	4.10	5.32	7.70	10.85	13.60	15.51	16.05	15.06	12.86	10.40	308 13	
309	8.16	6.53	5.96	6.51	8.24	10.85	13.27	15.16	15.84	15.03	12.98	9.78	7.04	4.71	3.46	3.86	5.60	8.44	11.74	14.64	16.50	16.72	15.38	12.86	309 13	
310	9.98	7.70	6.25	5.93	6.71	8.67	11.25	13.84	15.52	15.84	14.55	11.68	8.46	5.64	3.63	3.01	4.08	6.50	9.62	13.08	15.81	17.12	16.72	14.87	310 13	
311	12.03	9.20	7.26	6.32	6.37	7.46	9.60	12.20	14.35	15.67	15.28	13.15	10.15	7.00	4.47	3.03	3.22	5.93	7.60	10.76	14.05	16.38	17.05	16.14	311 13	
312	13.92	11.10	8.66	6.87	6.16	6.46	8.00	10.44	13.10	14.76	15.16	13.92	11.40	8.36	5.66	3.69	2.94	3.94	6.18	9.01	12.24	14.92	16.53	16.56	312 13	
313	15.16	12.66	10.06	7.96	6.74	6.60	7.35	9.00	11.24	13.43	14.50	14.36	12.66	9.94	7.20	4.97	3.56	3.77	5.34	7.72	10.56	13.46	15.64	16.34	313 13	
314	15.71	13.92	11.46	9.28	7.66	6.86	6.98	7.98	9.96	12.00	13.52	14.02	13.37	11.18	8.81	6.52	4.86	4.33	5.20	6.90	9.14	11.80	14.20	15.72	314 13	
315	15.81	14.66	12.72	10.71	8.96	7.82	7.56	7.92	9.16	10.68	12.24	13.26	13.26	12.06	10.17	8.00	6.25	5.31	5.50	6.66	8.34	10.52	12.80	14.44	315 13	
316	15.16	14.68	13.32	11.56	10.02	8.76	8.10	8.00	8.60	9.65	10.96	12.18	12.58	12.23	11.04	9.16	7.62	6.54	6.20	6.84	7.96	9.38	11.14	12.91	316 13	
317	14.18	14.40	13.64	12.37	10.90	9.58	8.78	8.46	8.68	9.30	10.00	10.94	11.57	11.80	11.36	10.28	8.94	7.84	7.18	7.20	7.86	8.80	9.98	11.46	317 13	
318	12.86	13.86	13.83	12.96	11.72	10.53	9.66	9.14	8.92	8.96	9.17	9.66	10.40	11.10	11.37	11.01	10.20	9.26	8.46	8.10	8.14	8.66	9.44	10.56	318 13	
319	11.74	12.76	13.34	13.26	12.61	11.72	10.86	9.76	9.04	8.80	8.85	9.16	9.64	10.14	10.74	11.18	11.32	11.06	10.38	9.58	8.94	8.71	8.90	9.50	319 13	
320	10.42	11.46	12.48	13.10	13.15	12.64	11.84	10.76	9.71	8.88	8.35	8.19	8.42	9.04	9.96	10.86	11.50	11.80	11.55	10.96	9.98	9.08	8.64	8.20	320 12	
321	8.75	9.38	10.38	11.46	12.41	13.07	13.16	12.84	11.84	10.56	9.24	8.13	7.50	7.43	7.86	8.83	10.03	11.16	12.23	12.80	12.64	11.66	10.25	9.04	321 12	
322	8.36	8.34	8.96	10.02	11.20	12.46	13.23	13.47	13.00	11.72	10.14	8.38	7.03	6.27	6.31	7.08	8.52	10.23	11.92	13.17	13.63	13.10	11.86	10.18	322 12	
323	8.76	7.98	7.96	8.75	10.13	11.64	13.14	13.94	13.94	13.04	11.34	9.30	7.45	5.86	5.13	5.46	6.76	8.80	11.15	13.20	14.66	14.98	13.97	11.76	323 12	
324	9.58	8.10	7.37	7.36	8.22	9.82	11.76	13.33	14.28	14.14	12.87	10.56	7.98	5.77	4.14	3.74	4.67	6.71	9.27	12.02	14.40	15.66	15.44	13.71	324 12	
325	11.16	8.74	7.02	6.40	6.78	8.22	10.37	12.25	13.88	14.74	14.20	12.36	9.36	6.51	4.12	2.75	2.94	4.56	7.03	10.05	13.27	15.65	15.90	15.90	325 12	
326	13.76	10.86	8.17	6.45	5.84	6.36	8.12	10.44	12.84	14.46	15.08	13.97	11.41	8.97	4.96	2.57	1.63	2.58	4.74	7.64	11.12	14.22	16.47	17.07	326 12	
327	15.75	12.96	9.86	7.26	5.65	5.46	6.44	8.40	11.20	13.57	15.11	15.17	13.27	9.96	6.40	3.62	1.76	1.54	3.26	6.02	9.25	12.97	15.66	17.40	327 12	
328	17.25	15.37	12.23	9.00	6.75	5.63	5.63	6.88	9.32	12.22	14.44	15.50	14.80	12.31	8.84	5.06	3.00	1.66	2.20	4.15	6.95	10.46	13.81	16.44	328 12	
329	17.54	16.82	14.56	11.38	8.50	6.32	5.44	5.74	7.26	10.06	12.76	14.67	15.26	14.06	11.32	8.05	5.16	2.94	2.16	3.11	5.16	7.96	11.23	14.30	329 12	
330	16.57	17.22	16.23	13.81	10.68	8.07	6.16	5.50	5.88	7.64	10.25	12.77	14.29	14.72	13.35	10.74	7.81	5.32	3.66	3.26	4.42	6.34	8.86	11.67	330 12	
331	14.58	16.33	16.57	15.28	12.84	9.93	7.47	6.23	5.72	6.26	7.94	10.30	12.38	13.76	13.96	12.68	10.56	8.18	6.28	4.97	4.83	5.73	7.34	9.38	331 12	



332	12·05	14·37	15·76	15·80	14·56	12·28	9·94	8·13	6·64	6·14	6·54	8·04	10·04	11·78	12·86	13·16	12·24	10·73	8·96	7·30	6·24	5·96	6·50	7·80	832 12
333	9·84	12·15	13·88	14·87	14·84	13·77	11·77	10·06	8·23	6·86	6·34	6·56	7·70	9·30	10·84	12·16	12·76	12·53	11·48	10·14	8·60	7·52	7·06	7·44	833 12
334	8·47	10·17	11·91	13·34	14·21	14·40	13·72	12·30	10·42	8·41	6·88	6·14	6·37	7·32	8·81	10·45	11·84	12·86	13·08	12·42	11·25	9·75	8·54	7·84	834 12
335	7·88	8·64	10·02	11·65	13·16	14·14	14·30	13·64	12·17	10·31	8·37	6·68	5·72	5·86	6·88	8·64	10·40	12·07	13·31	13·88	13·62	12·36	10·67	9·06	835 12
336	8·12	7·90	8·54	9·72	11·26	12·78	13·82	14·20	13·74	12·14	10·05	7·76	6·00	5·04	5·23	6·52	8·50	10·56	12·60	14·12	14·40	13·86	12·58	10·80	836 12
337	8·97	7·94	7·68	8·24	9·50	11·14	12·75	13·98	14·44	13·73	11·85	9·10	6·84	5·06	4·41	5·04	6·57	8·66	11·20	13·52	15·24	15·84	15·08	13·13	837 12
338	10·86	9·00	7·82	7·54	8·05	9·36	11·14	12·94	14·20	14·46	13·36	11·28	8·58	5·98	4·22	3·96	5·07	6·97	9·54	12·26	14·54	16·11	16·34	15·17	838 12
339	12·88	10·26	8·38	7·53	7·40	8·14	9·77	11·52	13·36	14·60	14·56	12·94	10·26	7·33	5·11	3·87	4·05	5·64	7·81	10·61	13·20	15·47	16·54	16·21	839 12
340	14·70	12·20	9·81	8·08	7·33	7·37	8·31	10·05	12·02	13·86	14·76	14·17	12·16	8·93	6·32	4·31	3·72	4·64	6·56	9·06	11·87	14·55	16·23	16·72	840 12
341	15·97	13·94	11·34	8·98	7·71	7·36	7·70	9·02	10·97	12·94	14·40	14·70	13·44	10·64	7·77	5·58	4·12	4·16	5·63	7·85	10·36	13·16	15·34	16·56	841 12
342	16·48	15·11	12·72	10·27	8·26	7·37	7·26	8·12	9·82	11·91	13·58	14·48	14·07	12·12	9·32	6·72	4·74	3·96	4·91	6·70	9·02	11·70	14·07	15·87	842 12
343	16·56	15·80	13·96	11·44	9·32	7·80	7·24	7·44	8·72	10·57	12·55	14·00	14·24	13·24	10·72	8·06	5·93	4·58	4·74	6·03	8·20	10·34	12·88	15·05	843 12
344	16·23	16·28	14·89	12·63	10·30	8·54	7·57	7·44	8·17	9·64	11·50	13·03	13·80	13·45	11·78	9·47	7·26	5·64	5·07	5·86	7·43	9·20	11·48	13·56	844 12
345	15·17	15·82	15·18	13·58	11·42	9·46	7·98	7·36	7·62	8·50	10·02	11·60	12·67	13·00	12·14	10·36	8·34	6·54	5·59	5·67	6·77	8·43	10·27	12·17	845 12
346	13·90	14·96	14·86	13·76	12·00	10·22	8·66	7·73	7·38	7·80	8·82	10·22	11·48	12·26	12·24	11·15	9·47	8·01	6·87	6·45	6·75	7·83	9·14	10·75	846 12
347	12·56	13·86	14·46	14·06	12·87	11·31	9·72	8·40	7·76	7·73	8·27	9·36	10·54	11·48	12·02	11·81	10·84	9·56	8·46	7·76	7·56	8·00	8·95	10·05	847 12
348	11·60	12·04	14·20	14·42	13·83	12·50	10·98	9·76	8·76	8·24	8·24	8·80	9·62	10·53	11·27	11·70	11·62	11·14	10·38	9·49	8·78	8·48	8·71	9·47	848 12
349	10·70	12·04	13·16	13·78	13·79	13·14	11·94	10·54	9·17	8·30	7·83	8·04	8·58	9·36	10·22	11·00	11·54	11·74	11·57	10·96	10·14	9·44	9·04	9·10	849 12
350	9·74	10·90	12·24	13·16	13·57	13·38	12·64	11·55	10·26	8·86	7·83	7·22	7·36	7·86	8·85	10·11	11·13	11·95	12·42	12·30	11·78	10·77	9·72	9·06	350 12
351	9·01	9·55	10·76	11·97	12·94	13·38	13·14	12·44	11·22	9·78		8·36	7·04	6·26	6·15	6·82	8·20	9·97	11·56	12·90	13·50	13·36	12·36	10·92	351 11
352	9·68	8·84	8·68	9·14	10·18	11·57	12·76	13·30	13·22	12·46	11·00	9·17	7·18	5·75	4·90	4·92	6·07	7·94	10·07	12·03	13·66	14·48	14·16	12·76	352 11
353	10·77	9·04	7·98	7·73	8·23	9·70	11·40	12·74	13·42	13·45	12·54	10·80	8·50	6·30	4·47	3·64	4·12	5·82	8·20	10·84	13·27	14·95	15·70	14·97	353 11
354	13·05	10·60	8·64	7·50	7·36	8·16	9·80	11·80	13·38	14·33	14·26	13·00	10·50	7·72	5·17	3·42	2·93	4·16	6·37	9·00	12·12	14·97	16·74	16·96	354 11
355	15·68	13·11	10·34	8·06	6·98	7·04	8·06	10·00	12·15	14·04	15·14	15·03	13·10	10·20	7·00	4·27	2·40	2·20	3·93	6·57	9·77	13·27	16·13	17·72	355 11
356	17·51	15·78	12·57	9·74	7·27	6·14	6·36	7·56	9·86	12·72	14·77	15·81	15·20	12·64	9·26	5·91	3·10	1·55	1·93	4·00	7·06	10·68	14·30	17·04	356 11
357	18·34	17·72	15·47	12·00	8·88	6·58	5·67	6·00	7·50	10·14	13·10	15·24	16·17	14·94	12·16	8·55	5·06	2·64	1·50	2·57	5·14	8·44	11·93	15·00	357 11
358	17·66	18·34	17·37	14·51	10·92	7·77	5·66	5·14	5·64	7·65	10·63	13·44	15·46	15·86	14·14	10·98	7·68	4·48	2·36	1·77	3·30	5·83	8·90	12·30	358 11
359	15·56	17·50	17·88	16·62	13·58	9·97	6·94	5·14	4·70	5·52	7·63	10·73	13·70	15·36	15·32	13·24	9·92	6·64	4·73	3·07	3·08	4·74	6·97	9·86	359 11
360	13·01	15·80	17·38	17·48	15·95	12·86	9·53	6·72	5·22	4·90	5·87	8·03	10·96	13·30	14·68	14·83	13·24	10·55	7·68	5·43	4·33	4·63	5·97	8·02	360 11
361	10·57	13·25	15·58	16·60	16·14	14·11	11·13	8·76	6·38	5·17	5·13	6·30	8·60	10·76	12·74	13·74	13·62	12·37	10·30	8·14	6·53	5·84	6·14	7·14	361 11
362	8·74	10·77	13·13	14·96	15·71	15·12	13·32	10·86	8·44	6·53	5·48	5·27	6·00	7·78	9·85	11·62	12·84	13·10	12·28	10·74	9·22	7·96	7·33	7·28	362 11
363	7·93	9·16	10·97	13·12	14·54	14·68	13·66	12·28	10·12	8·24	6·78	5·82	5·70	6·37	7·72	9·40	11·06	12·32	12·86	12·50	11·47	10·24	9·12	8·42	363 11
364	8·24	8·54	9·54	11·12	12·64	13·57	13·57	12·88	11·44	9·87	8·24	6·74	5·77	5·52	6·12	7·27	8·94	10·64	12·10	13·01	13·12	12·46	11·26	10·02	364 11
365	9·06	8·58	8·66	9·44	10·68	11·96	12·92	13·14	12·66	11·54	10·06	8·36	6·86	5·72	5·37	5·87	7·17	9·14	11·00	12·70	13·68	13·81	12·94	11·57	365 11
366	10·28	9·14	8·62	8·63	9·20	10·44	11·66	12·53	12·92	12·58	11·04	9·77	7·86	6·12	5·05	4·78	5·62	7·06	9·15	11·26	13·23	14·30	14·32	13·36	366 11
367	11·78	10·34	9·17	8·44	8·24	8·62	9·76	11·04	12·36	13·08	12·90	11·65	9·64	7·34	5·52	4·45	4·52	5·76	7·66	9·97	12·43	14·27	15·18	14·97	367 11
368	13·73	11·82	10·16	8·86	8·24	8·26	8·96	10·32	11·70	12·96	13·58	13·16	11·26	8·91	6·66	4·96	4·33	4·86	6·36	8·55	11·00	13·44	15·21	15·84	368 11
369	15·17	13·56	11·44	9·66	8·38	7·80	7·97	9·00	10·56	12·24	13·46	13·82	12·72	10·52	7·90	5·74	4·34	4·11	5·34	7·23	9·78	12·44	14·65	15·93	369 11
370	15·94	14·74	12·37	10·23	8·53	7·47	7·31	7·97	9·38	11·36	13·14	14·17	14·00	12·18	9·43	...	...	...	...	...	...	...	...	...	370 2
Sum	927·90	896·08	848·59	799·21	758·63	736·69	735·56	754·53	783·47	812·73	818·07	814·05	770·54	702·29	628·88	561·53	532·20	542·50	589·53	661·82	747·15	827·61	878·34	916·78	No. of Days. 73 <sup>d</sup> 13 <sup>h</sup> 18 <sup>m</sup> 44 <sup>s</sup> ·68
No.	74	74	74	74	74	74	74	74	74	74	73	74	74	74	74	73	73	73	73	73	73	73	72	73	

## FORMS FOR SHORT-PERIOD TIDES.

BOMBAY—Commencing 0 hours, Astronomical Time, 1st January, 1885.

Argument ( $\gamma - \frac{3}{2}n$ ). SERIES T. Motion per mean Solar hour = 14°9794657.

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour
1	15.54	12.96	9.13	5.76	3.03	1.68	2.28	4.80	7.90	11.70	15.50	18.00	18.85	18.08	15.14	11.54	8.50	6.21	5.53	6.08	8.20	11.31	14.16	16.06	1 23
2	16.66	15.40	12.16	8.40	4.86	2.56	1.71	2.90	5.56	8.82	12.94	16.44	18.58	18.97	17.07	14.24	10.56	7.53	5.57	5.16	6.10	8.63	11.84	14.68	2 23
3	16.63	16.96	15.24	11.92	8.00	4.87	2.80	2.57	4.24	6.84	10.20	14.07	17.26	18.86	18.84	17.06	13.20	9.77	6.90	5.23	4.96	6.16	8.86	12.14	3 23
4	14.87	16.40	16.40	14.28	11.00	7.63	4.88	3.55	3.86	5.53	8.01	11.36	14.83	17.16	18.38	17.93	15.80	12.16	8.68	6.10	5.03	5.25	6.68	9.24	4 23
5	12.28	14.51	15.96	15.58	13.48	10.47	7.54	5.76	5.07	6.84	7.54	8.67	10.60	12.84	15.06	16.36	16.35	15.24	10.96	8.16	6.22	5.47	5.84	7.18	5 23
6	9.67	12.11	14.04	15.00	14.45	13.64	12.22	10.47	9.05	8.44	8.46	9.03	9.97	11.20	13.03	14.64	15.46	15.18	13.87	11.68	9.76	8.10	7.16	6.55	6 23
7	7.86	9.76	11.80	13.27	14.00	13.24	13.07	12.20	11.16	10.27	9.64	9.60	9.90	10.60	11.70	12.96	14.02	14.44	13.75	12.27	10.82	9.20	7.93	7.24	7 23
8	7.46	8.29	9.82	11.16	12.55	13.24	12.48	12.66	12.27	11.60	10.93	10.34	9.98	9.86	10.17	11.07	12.14	13.06	13.36	12.72	11.71	10.43	9.14	7.97	8 23
9	7.06	7.34	8.07	9.14	10.55	11.74	12.48	12.67	13.14	12.97	12.20	11.24	10.48	10.12	10.05	10.23	10.84	11.64	12.27	12.68	12.37	11.53	10.42	8.97	9 23
10	7.14	6.75	6.94	7.74	8.96	10.26	11.64	12.67	13.23	13.84	13.63	12.58	11.38	10.27	9.77	9.62	9.89	10.44	11.24	11.97	12.52	12.50	11.87	10.54	10 23
11	7.86	6.96	6.38	6.44	7.28	8.73	10.47	12.14	13.23	13.84	13.63	12.58	11.38	10.27	9.77	9.62	9.89	10.44	11.24	11.97	12.52	12.50	11.87	10.54	11 23
12	8.76	7.34	6.16	5.74	6.34	7.62	9.54	11.46	13.22	14.24	14.58	13.94	12.72	11.24	10.02	9.32	9.14	9.46	10.37	11.48	12.46	13.04	12.84	11.88	12 23
13	10.23	8.20	6.52	5.62	5.56	6.50	8.14	10.17	12.34	14.10	15.20	15.17	13.97	12.27	10.58	9.35	8.75	8.76	9.26	10.34	11.68	12.96	13.64	13.36	13 23
14	11.00	9.66	7.32	5.82	5.14	5.44	6.74	8.86	11.26	13.66	15.38	15.87	15.24	13.66	11.54	9.82	8.71	8.16	8.36	9.30	10.74	12.46	13.64	13.98	14 23
15	13.00	10.84	8.24	6.20	4.76	4.46	5.40	7.36	9.78	12.57	14.82	16.13	15.97	14.56	12.25	10.05	8.46	7.82	7.74	8.41	9.71	11.76	13.30	14.26	15 23
16	14.09	12.44	9.76	7.00	5.12	4.20	6.12	8.44	11.24	14.04	15.74	16.36	15.71	13.82	11.22	8.94	7.54	6.94	7.15	8.40	10.27	12.44	14.06	14.68	17 0
17	13.84	11.50	8.60	5.94	4.37	4.02	5.06	7.26	9.66	12.72	15.20	16.55	16.63	15.27	12.77	9.97	7.86	6.84	6.68	7.56	9.32	11.40	13.55	14.80	18 0
18	14.78	13.22	10.43	7.48	5.34	4.30	4.66	6.25	8.54	11.38	14.15	16.15	16.88	16.08	14.04	11.02	8.54	6.76	6.12	6.34	7.60	9.84	12.14	14.06	19 0
19	14.84	14.14	12.06	9.06	6.46	4.67	4.24	5.16	7.15	9.68	12.56	14.87	16.44	16.45	15.00	12.42	9.50	7.22	5.80	5.43	6.26	8.16	10.65	12.88	20 0
20	14.28	14.56	13.33	10.92	8.30	6.04	4.87	5.06	6.54	8.66	11.04	13.64	15.62	16.36	15.76	13.82	11.00	8.37	6.37	5.54	5.64	6.83	8.93	11.40	21 0
21	13.32	14.42	14.25	12.47	10.10	7.91	6.34	5.70	6.30	7.70	9.76	8.97	12.17	14.36	15.74	15.96	14.86	12.76	10.13	7.78	6.17	5.70	6.11	7.62	22 0
22	11.76	13.36	14.14	13.72	12.06	9.94	8.32	7.22	7.01	7.74	8.68	9.86	11.56	14.62	15.50	15.17	13.80	11.46	9.14	7.34	6.17	6.00	6.68	8.02	23 0
23	9.76	11.65	13.04	13.76	13.34	12.14	10.65	9.07	8.15	8.14	8.88	9.28	10.22	11.70	13.06	14.14	14.41	13.60	12.06	10.26	8.46	7.10	6.25	6.08	24 0
24	7.86	9.46	11.24	12.66	13.36	13.34	12.38	11.08	9.94	9.11	8.88	9.28	10.22	11.70	13.06	14.14	14.41	13.60	12.06	10.26	8.46	7.10	6.25	6.08	25 0
25	6.56	7.64	9.14	10.84	12.34	13.44	13.81	13.33	12.18	10.75	9.76	9.24	9.34	10.07	11.16	12.40	13.38	13.66	13.03	11.87	10.24	8.47	7.00	5.83	26 0
26	5.38	5.68	6.78	8.55	10.33	12.22	13.56	14.30	14.16	13.05	11.56	10.06	9.11	8.87	9.40	10.46	11.87	12.94	13.44	13.33	12.40	10.74	8.86	6.83	27 0
27	5.22	4.41	4.77	6.10	8.10	10.50	12.63	14.53	15.56	15.33	13.76	11.64	9.52	8.28	7.92	8.25	9.53	11.24	12.70	13.80	14.14	13.30	11.34	8.72	28 0
28	6.20	4.24	3.38	3.76	5.30	7.76	10.55	13.50	15.72	16.74	16.12	14.36	11.40	8.83	7.24	6.86	7.53	9.20	11.11	12.97	14.55	15.08	14.17	11.84	29 0
29	8.82	5.70	3.60	2.56	3.06	5.04	7.88	11.48	14.56	17.04	17.86	17.00	14.36	10.96	8.07	6.27	5.77	6.57	8.62	11.25	13.92	15.74	16.28	14.96	30 0
30	12.18	8.44	5.42	3.22	2.16	3.07	5.52	8.75	12.46	16.01	18.10	18.47	17.26	13.80	10.14	7.09	5.27	5.02	6.02	8.40	11.85	14.65	16.52	16.84	31 0
31	15.28	11.68	7.88	4.80	2.74	2.38	4.00	6.66	10.10	13.98	17.01	18.64	18.38	16.30	12.42	8.97	6.01	4.46	4.57	6.12	9.14	12.50	15.46	17.00	32 0
32	16.86	14.76	11.06	7.36	4.34	2.72	2.99	4.86	7.74	11.40	14.94	17.54	18.47	17.66	14.97	11.08	7.54	5.01	3.93	4.32	6.55	9.62	13.04	15.80	33 0
33	16.84	16.08	13.73	10.16	6.82	4.54	3.58	4.44	6.36	9.36	12.84	15.86	17.74	17.94	16.48	13.27	9.84	6.84	4.96	4.33	5.26	7.44	10.66	13.70	34 0
34	15.74	16.43	15.42	12.82	9.66	6.90	5.42	5.14	6.20	8.06	10.66	13.66	16.02	17.12	16.74	14.88	11.68	8.76	6.34	4.92	4.74	5.86	8.26	11.07	35 0
35	13.60	15.16	15.34	14.06	11.68	9.04	7.34	6.56	6.94	8.04	9.56	11.76	14.24	15.60	16.04	15.34	13.02	10.16	7.80	6.27	5.54	5.86	7.18	9.07	36 0

36	11·36	13·26	14·34	14·26	12·88	11·00	9·39	8·26	7·92	8·30	9·05	10·36	12·08	13·76	14·66	14·44	13·11	11·12	9·30	7·54	6·26	6·13	6·68	7·86	37 0
37	9·28	10·86	12·27	13·10	12·94	11·93	10·66	9·72	9·12	9·06	9·26	9·66	10·60	11·82	12·86	13·34	12·82	11·45	10·03	8·74	7·48	6·86	6·78	7·17	38 0
38	7·94	9·05	10·30	11·34	11·97	11·92	11·42	10·84	10·34	10·07	9·97	9·77	9·94	10·44	11·32	12·06	12·26	11·78	10·88	9·87	8·84	7·86	7·24	6·94	39 0
39	7·18	8·03	9·07	10·14	11·00	11·56	11·85	11·77	11·46	11·12	10·57	10·07	9·70	9·70	10·13	10·80	11·27	11·45	11·25	10·76	9·97	9·00	8·00	7·11	40 0
40	6·58	6·74	7·44	8·51	9·84	10·90	11·76	12·34	12·55	12·30	11·60	10·57	9·76	9·34	9·17	9·56	10·24	10·94	11·36	11·44	10·97	10·10	9·07	7·87	41 0
41	6·85	6·30	6·50	7·26	8·50	10·16	11·44	12·65	13·26	13·32	12·56	11·36	10·08	9·16	8·67	8·64	9·01	9·76	10·58	11·25	11·66	11·34	10·36	8·82	42 0
42	7·36	6·12	5·54	5·82	6·94	8·54	10·36	12·06	13·46	13·97	13·64	12·30	10·76	9·26	8·14	7·84	8·12	8·96	10·24	11·52	12·40	12·66	12·07	10·47	43 0
43	8·56	6·64	5·46	5·20	5·93	7·55	9·56	11·72	13·53	14·67	14·84	13·98	12·14	10·00	8·54	7·66	7·53	8·16	9·56	11·03	12·66	13·62	13·60	12·30	44 0
44	10·24	7·77	5·88	4·84	4·96	6·33	8·27	10·66	13·07	14·85	15·64	15·23	13·64	11·13	9·02	7·54	6·79	7·00	8·13	9·87	11·85	13·60	14·38	13·88	45 0
45	11·93	9·10	6·54	4·66	4·00	4·90	6·86	9·20	11·97	14·34	15·82	15·96	14·78	12·26	9·64	7·46	6·24	5·96	6·74	8·48	10·85	13·07	14·56	14·85	46 0
46	13·63	10·90	7·86	5·57	4·07	4·04	5·46	7·84	10·63	13·64	15·83	16·64	16·01	13·87	10·90	8·00	6·17	5·46	5·74	7·26	9·70	12·25	14·42	15·50	47 1
47	13·08	9·90	6·94	4·75	3·92	4·66	6·62	9·46	12·60	15·08	16·60	16·64	15·00	11·93	8·96	6·76	5·63	5·06	5·54	7·84	10·54	13·30	15·12	15·66	48 1
48	14·46	11·76	8·44	5·86	4·26	4·25	5·52	7·84	10·68	13·68	15·84	16·68	15·86	13·15	10·22	7·36	5·65	4·23	4·46	6·07	8·56	11·57	14·06	15·54	49 1
49	15·51	13·57	10·53	7·47	5·38	4·52	5·04	6·70	9·14	12·18	14·74	16·26	16·26	14·64	11·74	8·68	6·28	4·54	4·14	5·07	7·06	9·74	12·44	14·55	50 1
50	15·46	14·76	12·57	9·68	7·24	5·84	5·60	6·54	8·40	10·77	13·32	15·42	16·26	15·47	13·18	10·24	7·54	5·62	4·54	4·69	5·80	7·87	10·40	12·80	51 1
51	14·50	15·06	14·03	11·86	9·36	7·58	6·64	6·76	7·86	9·60	11·66	13·73	15·08	15·32	14·12	11·86	9·24	6·90	5·18	4·58	5·06	6·46	8·24	10·33	52 1
52	12·41	13·86	14·34	13·44	11·46	9·53	8·05	7·40	7·66	8·58	9·92	11·68	13·36	14·16	14·12	12·82	10·83	8·73	6·87	5·45	4·92	5·44	6·63	8·23	53 1
53	10·14	11·77	12·96	13·40	12·76	11·56	10·24	9·04	8·45	8·28	8·67	9·76	11·20	12·50	13·18	13·06	11·88	10·25	8·57	6·98	5·77	5·38	5·64	6·37	54 1
54	7·82	9·54	11·17	12·38	13·02	12·96	12·16	11·07	10·02	8·94	8·44	8·48	9·27	10·44	11·57	12·34	12·34	11·70	10·50	8·90	7·32	5·96	5·24	5·12	55 1
55	5·86	7·17	8·90	10·63	12·10	13·16	13·56	13·13	11·86	10·27	8·88	8·08	7·87	8·42	9·56	10·87	11·93	12·44	12·26	11·27	9·76	7·96	6·27	5·06	56 1
56	4·55	5·02	6·47	8·52	10·67	12·72	14·14	14·86	14·44	12·70	10·66	8·80	7·60	7·21	7·64	9·18	11·00	12·40	13·36	13·52	12·60	10·86	8·63	6·40	57 1
57	4·63	4·06	4·70	6·46	8·84	11·30	13·80	15·56	16·25	15·33	12·96	10·26	7·95	6·54	6·18	7·03	8·83	11·00	12·96	14·40	14·74	13·76	11·70	8·84	58 1
58	6·08	4·05	3·42	4·14	6·18	8·80	12·06	14·93	16·76	17·15	15·84	12·87	9·66	7·00	5·18	5·12	6·26	8·52	11·16	13·67	15·38	15·86	14·57	11·93	59 1
59	8·26	5·48	3·42	2·92	4·14	6·52	9·58	13·16	16·04	17·62	17·34	15·27	11·66	8·27	5·56	4·16	4·32	5·84	8·66	11·92	14·74	16·46	16·54	14·66	60 1
60	11·26	7·66	4·94	3·20	3·27	4·70	7·52	10·86	14·63	17·06	17·98	16·96	13·90	10·20	6·96	4·47	3·56	4·02	6·04	9·40	12·86	15·55	16·86	16·36	61 1
61	13·86	10·44	6·92	4·54	3·37	3·90	5·80	8·56	12·33	15·44	17·27	17·40	15·46	12·03	8·50	5·70	3·74	3·27	4·33	7·10	10·34	13·76	15·97	16·76	62 1
62	15·76	12·96	9·44	6·74	4·67	4·23	5·26	7·43	10·37	13·82	16·13	17·08	16·40	13·86	10·50	7·26	4·84	3·56	3·86	5·60	8·27	11·55	14·34	16·02	63 1
63	16·28	14·66	11·66	8·60	6·46	5·26	5·46	6·56	8·86	11·44	14·36	15·97	16·18	14·88	12·00	8·86	6·28	4·57	4·06	4·86	6·67	9·40	12·24	14·39	64 1
64	15·64	15·33	13·25	10·46	8·22	6·76	6·34	7·00	8·36	10·22	12·44	14·42	15·27	14·71	12·72	10·14	7·72	5·93	4·86	5·00	6·10	8·03	10·30	12·47	65 1
65	13·97	14·58	13·92	12·03	10·14	8·54	7·56	7·56	8·42	9·82	11·34	12·96	14·04	14·24	13·22	11·36	9·36	7·56	6·27	5·84	6·34	7·46	9·00	10·76	66 1
66	12·44	13·56	13·74	12·74	11·40	10·07	9·16	8·96	9·27	9·77	10·46	11·36	12·44	13·07	13·03	12·12	10·46	8·86	7·68	7·02	7·02	7·66	8·54	9·66	67 1
67	10·96	12·24	12·88	12·88	12·24	11·43	10·66	10·24	10·16	10·24	10·47	10·86	11·44	12·02	12·40	12·24	11·36	10·18	8·87	7·97	7·67	7·94	8·50	9·00	68 1
68	9·78	10·74	11·76	12·46	12·67	12·27	11·74	11·26	10·87	10·56	10·36	10·22	10·36	10·76	11·26	11·56	11·38	10·86	9·96	9·14	8·40	7·98	7·80	7·86	69 1
69	8·34	9·30	10·46	11·44	12·08	12·36	12·27	12·03	11·50	10·78	10·20	9·73	9·58	9·87	10·35	10·89	11·10	11·10	10·78	10·32	9·72	8·86	7·97	7·28	70 1
70	7·26	7·87	8·97	10·32	11·56	12·46	13·04	13·10	12·54	11·68	10·56	9·64	9·08	8·82	9·16	9·88	10·74	11·40	11·75	11·70	11·14	10·07	8·84	7·56	71 1
71	6·74	6·70	7·63	8·94	10·62	12·06	13·26	13·78	13·68	12·86	11·34	9·88	8·86	8·16	8·03	8·46	9·64	10·86	12·06	12·78	12·56	11·57	9·92	8·17	72 1
72	6·67	5·98	6·16	7·20	8·87	10·76	12·70	14·08	14·61	14·06	12·53	10·68	8·96	7·55	6·88	7·05	8·07	9·84	11·76	12·97	13·54	13·03	11·46	9·42	73 1
73	7·27	5·74	5·30	5·90	7·44	9·66	11·92	14·02	15·17	15·16	13·87	11·66	9·44	7·56	6·34	6·07	6·86	8·68	10·80	12·96	14·26	14·55	13·37	11·16	74 1
74	8·45	6·26	5·16	5·12	6·24	8·10	10·63	13·22	15·15	15·86	15·17	13·22	10·40	7·86	6·06	5·25	5·54	6·90	9·24	11·72	13·95	15·20	15·12	13·39	75 1
Sum	802·24	763·25	708·83	654·09	616·55	615·05	642·43	706·60	789·02	870·63	931·53	961·39	956·40	914·92	859·06	778·27	714·90	669·06	650·91	663·96	701·29	750·76	792·18	809·21	No. of Days. 74 <sup>d</sup> 2 <sup>h</sup> .
No.	74	74	74	74	74	75	74	74	74	74	74	74	74	74	75	74	74	74	74	74	74	74	74	74	18 <sup>d</sup> 22 <sup>h</sup> 53 <sup>m</sup>

FORMS FOR SHORT-PERIOD TIDES.  
SERIES T.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
75	10.64	7.57	5.44	4.44	4.96	6.46	8.94	11.85	14.34	16.00	16.06	14.53	11.64	8.54	5.76	4.22	3.97	5.24	7.30	10.10	13.02	15.04	16.00	15.20	76 1	
76	12.86	9.54	6.67	4.92	4.38	5.52	7.55	10.33	13.50	15.75	16.73	16.07	13.66	10.42	7.22	4.92	3.64	4.00	5.66	8.33	11.52	14.30	16.06	15.06	77 2	
77	12.13	8.73	6.13	4.66	4.99	6.52	8.92	11.86	14.66	16.40	16.56	15.07	11.90	8.47	5.62	3.74	3.22	4.26	6.60	9.60	12.85	15.23	16.56	16.35	78 2	
78	14.16	10.83	8.00	5.75	5.11	5.88	7.84	10.46	13.38	15.68	16.60	15.80	13.36	10.12	7.06	4.83	3.54	3.76	5.34	7.86	11.00	13.93	15.92	16.74	79 2	
79	15.74	13.36	10.24	7.64	6.12	6.08	7.14	9.00	11.56	13.90	15.66	15.98	14.76	12.06	8.90	6.13	4.34	3.62	4.36	6.06	8.47	11.31	13.87	15.62	80 2	
80	16.12	14.97	12.74	10.02	8.05	6.96	7.06	7.93	9.67	12.07	14.08	15.23	15.08	13.57	11.16	8.26	6.08	4.70	4.47	5.46	7.26	9.48	11.88	13.90	81 2	
81	15.36	15.50	14.66	13.67	10.54	8.74	7.94	8.14	9.06	10.61	12.40	13.77	14.52	14.20	12.80	10.64	8.47	6.76	5.86	5.82	6.49	7.75	9.52	11.71	82 2	
82	13.54	14.73	14.90	14.06	12.63	11.05	9.70	8.86	8.72	9.12	10.24	11.76	13.06	13.34	12.06	10.56	10.56	8.92	7.40	6.43	6.30	6.68	7.68	9.46	83 2	
83	11.24	13.02	14.08	14.52	14.22	13.04	11.70	10.34	9.24	8.84	9.04	9.84	10.96	12.05	12.86	12.96	12.44	11.22	9.67	8.30	7.06	6.48	7.64	9.48	84 2	
84	8.86	10.64	12.34	13.74	14.48	14.44	13.62	12.12	10.36	8.96	8.00	9.04	9.76	10.66	11.26	11.16	12.56	13.57	14.06	13.37	11.72	9.38	7.17	5.72	85 2	
85	6.72	8.34	10.26	12.20	13.86	15.00	15.14	14.16	12.20	9.88	8.00	6.90	6.56	7.46	9.22	11.16	12.56	13.57	14.06	13.37	11.72	9.38	7.17	5.72	86 2	
86	5.38	6.17	7.82	10.00	12.50	14.54	15.84	15.94	14.64	12.14	9.36	6.97	5.74	5.63	6.67	8.88	11.24	13.46	14.86	15.36	14.34	12.05	9.44	6.93	87 2	
87	5.38	5.00	5.82	7.83	10.50	13.30	15.60	16.72	16.28	14.37	11.37	8.36	6.00	4.67	4.80	6.40	9.20	12.06	14.62	16.12	16.16	14.90	12.22	9.12	88 2	
88	6.60	5.05	4.86	5.87	8.10	11.14	14.15	16.35	17.15	16.24	13.58	10.14	7.06	4.83	3.96	4.70	6.72	9.92	13.20	15.64	17.04	16.75	14.92	11.81	89 2	
89	8.56	6.27	5.14	5.64	6.94	9.43	12.61	15.44	17.03	17.08	15.36	11.92	8.64	6.18	4.48	4.25	5.24	7.57	11.00	14.10	16.43	17.34	16.56	14.28	90 2	
90	10.82	7.84	5.95	5.43	6.12	7.87	10.62	13.66	16.10	17.14	16.46	13.96	10.41	7.12	4.80	3.83	4.41	6.43	8.78	12.04	14.74	16.66	17.13	15.64	91 2	
91	12.86	9.53	7.16	5.81	5.93	7.22	9.26	12.02	14.66	16.44	16.67	15.06	12.02	8.56	5.84	4.04	3.84	4.93	7.24	10.09	13.22	15.56	16.90	16.56	92 2	
92	14.74	11.68	8.84	7.02	6.48	7.04	8.26	10.50	13.00	14.94	15.83	15.12	12.94	9.87	7.14	5.16	4.22	4.76	6.40	8.73	11.37	14.00	15.82	16.34	93 2	
93	15.46	13.10	10.40	8.36	7.32	7.28	8.03	9.50	11.53	13.48	14.74	14.92	13.67	11.34	8.76	6.67	5.40	5.22	6.16	7.85	9.97	12.30	14.30	15.48	94 2	
94	15.67	14.27	12.24	10.20	8.78	8.26	8.47	9.24	10.52	12.04	13.48	14.16	13.84	12.27	10.16	8.14	6.47	5.74	6.22	7.44	9.20	10.85	12.64	14.05	95 2	
95	14.67	14.27	12.97	11.44	10.04	9.16	8.84	9.16	9.84	10.95	11.96	12.80	12.96	12.28	10.94	9.24	7.80	6.78	6.70	7.30	8.37	9.54	10.90	12.34	96 2	
96	13.52	13.80	13.26	12.13	10.96	10.04	9.60	9.33	9.54	9.90	10.56	11.44	11.92	12.05	11.54	10.36	9.16	8.12	7.47	7.44	7.87	8.52	9.46	10.73	97 2	
97	11.93	12.74	12.98	12.60	11.86	11.07	10.34	9.94	9.77	9.87	10.02	10.36	10.81	11.14	11.27	10.92	10.30	9.34	8.36	7.74	7.58	7.98	8.76	9.87	98 2	
98	11.04	11.96	12.50	12.66	12.42	11.96	11.34	10.55	9.91	9.47	9.34	9.52	9.94	10.53	10.94	11.12	11.02	10.62	10.00	9.22	8.40	8.01	8.13	8.63	99 2	
99	9.70	10.66	11.77	12.66	13.06	12.94	12.40	11.47	10.50	9.62	8.94	8.54	8.74	9.48	10.45	11.36	11.88	11.89	11.44	10.50	9.40	8.46	7.84	7.76	100 2	
100	8.43	9.46	10.86	12.30	13.36	13.82	13.66	12.66	11.42	10.02	8.72	7.96	7.82	8.36	9.47	10.86	11.90	12.70	12.87	12.44	11.06	9.52	8.12	7.40	101 2	
101	7.47	8.26	9.54	11.08	12.70	14.06	14.56	14.22	12.80	10.96	8.88	7.46	6.81	6.84	7.92	9.62	11.52	13.00	13.97	14.12	13.00	11.02	9.05	7.48	102 2	
102	6.74	6.92	7.97	9.72	11.72	13.58	14.86	15.12	14.21	12.35	9.67	7.47	5.98	5.88	6.14	7.76	9.84	12.16	14.02	15.18	15.06	13.40	10.95	8.28	103 2	
103	6.66	6.02	6.46	7.88	10.06	12.53	14.55	15.72	15.49	13.80	11.08	8.22	5.93	4.52	4.32	5.47	7.72	10.54	13.27	15.36	16.20	15.32	13.00	9.88	104 2	
104	7.34	5.76	5.40	6.24	8.22	10.70	13.40	15.52	16.25	15.36	12.80	9.46	6.56	4.47	3.42	3.91	5.74	8.31	11.40	14.40	16.28	16.72	15.47	12.68	105 2	
105	9.44	6.81	5.47	5.38	6.52	8.91	11.80	14.40	15.97	16.08	14.35	11.30	7.80	4.97	2.93	2.46	3.76	6.21	9.51	12.97	15.58	17.14	17.04	14.94	106 2	
106	11.68	8.36	6.14	5.06	5.37	7.24	10.07	13.10	15.40	16.44	15.82	13.44	9.74	6.67	4.03	2.50	2.77	4.44	7.64	10.96	14.33	16.70	17.52	16.91	107 2	
107	14.37	10.87	8.10	6.15	5.71	6.50	8.36	11.33	14.12	16.50	15.10	12.22	8.67	5.24	3.17	2.58	3.47	5.74	8.64	12.02	15.12	16.94	17.54	16.24	108 3	
108	13.40	10.32	7.62	6.17	6.07	7.04	9.13	12.00	14.47	15.69	15.54	13.66	10.74	7.44	4.88	3.38	3.04	4.36	6.67	9.40	12.47	15.00	16.74	16.94	109 3	
109	15.60	13.03	10.01	7.87	6.76	6.80	7.71	9.70	12.14	14.15	15.02	14.50	12.53	9.24	7.24	5.36	4.17	4.16	5.20	7.26	9.89	12.40	14.57	15.77	110 3	



FORMS FOR SHORT-PERIOD TIDES.

SERIES T.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
149	7'84	7'40	7'74	8'92	10'62	12'60	14'02	14'27	13'22	10'78	8'10	5'76	4'27	4'17	5'26	7'20	9'70	12'28	14'66	15'94	16'04	14'86	12'64	10'27	150 4	
150	8'44	7'54	7'34	8'10	9'52	11'55	13'36	14'27	13'92	12'06	9'48	6'90	5'12	4'32	4'97	6'54	8'70	11'00	13'46	15'32	16'07	15'67	14'17	11'77	151 4	
151	9'56	8'16	7'68	7'83	8'74	10'50	12'26	13'66	14'02	12'96	10'86	8'34	6'24	5'04	4'82	5'84	7'60	9'46	11'87	14'10	15'30	15'60	14'66	12'78	152 4	
152	10'74	9'03	7'96	7'73	8'24	9'44	11'07	12'62	13'44	13'16	11'96	9'94	7'67	6'16	5'18	5'56	6'86	8'64	10'66	12'74	14'30	15'12	15'06	13'65	153 4	
153	11'84	10'00	8'46	7'75	7'78	8'46	9'92	11'36	12'37	12'84	12'22	10'98	9'18	7'32	6'03	5'94	6'87	8'17	9'67	11'58	13'28	14'64	14'97	14'22	154 4	
154	12'62	11'08	9'47	8'38	8'08	8'30	9'20	10'24	11'40	12'12	12'46	11'72	10'38	8'77	7'37	6'70	6'93	7'78	8'83	10'30	11'90	13'54	14'68	14'80	155 4	
155	13'77	12'16	10'50	9'20	8'47	8'28	8'60	9'36	10'36	11'26	11'83	12'05	11'56	10'60	9'20	8'14	7'72	7'83	8'62	9'82	11'10	12'64	13'94	14'46	156 4	
156	14'16	13'26	11'74	10'42	9'26	8'54	8'34	8'46	9'23	10'10	10'93	11'70	11'97	11'72	11'06	9'98	8'86	8'32	8'36	9'00	10'04	11'54	12'92	13'86	157 4	
157	14'25	13'85	12'88	11'48	10'08	8'98	8'20	8'20	8'37	9'12	10'03	11'29	12'14	12'58	12'36	11'84	11'02	10'06	9'23	8'78	9'20	10'37	11'98	13'44	158 4	
158	14'23	14'34	13'94	12'86	11'59	10'03	8'74	7'92	7'54	7'76	8'67	9'96	11'54	12'84	13'87	13'86	13'28	12'03	10'56	9'66	9'64	10'17	11'38	12'77	159 4	
159	13'98	14'67	15'14	14'88	13'86	12'46	10'48	8'82	7'82	7'50	8'19	9'46	11'28	13'22	14'76	15'82	15'76	14'97	13'34	11'70	10'67	10'27	10'56	11'52	160 4	
160	12'90	14'12	15'30	15'65	15'48	14'17	12'02	9'86	8'00	7'09	6'85	7'72	9'34	11'40	13'77	15'84	16'86	16'85	15'70	13'60	11'52	9'95	9'55	9'80	161 4	
161	10'84	12'57	14'21	15'47	16'06	15'22	13'50	10'84	8'22	6'16	4'95	5'15	6'50	8'61	11'37	14'18	16'48	17'54	17'17	15'60	12'50	10'07	8'34	8'17	162 4	
162	8'96	10'27	12'23	14'24	15'74	16'29	15'33	12'77	9'46	6'32	4'44	3'62	4'30	6'30	8'54	11'95	15'02	17'28	17'95	17'20	15'02	11'76	9'04	7'44	163 4	
163	7'22	7'81	9'55	12'08	14'54	16'07	16'21	14'76	11'87	8'16	5'07	3'07	2'74	3'80	5'94	9'24	12'80	15'92	18'07	18'53	17'65	14'65	10'90	8'00	164 4	
164	6'62	6'55	7'50	9'65	12'45	14'89	16'40	16'14	14'28	10'90	7'10	4'31	2'62	2'37	3'68	6'30	9'76	13'48	16'44	18'12	18'40	17'00	13'80	10'17	165 4	
165	7'55	6'20	6'18	7'30	9'60	12'79	15'16	16'42	15'96	13'80	10'33	6'77	4'00	2'33	2'54	4'18	7'11	10'40	13'95	16'74	17'85	17'95	16'07	12'81	166 4	
166	9'60	7'05	5'72	5'77	7'00	9'56	12'80	15'12	16'05	15'26	12'76	9'20	6'14	3'95	2'88	3'47	5'52	7'93	11'04	14'21	16'44	17'72	17'40	15'44	167 4	
167	12'07	9'02	6'70	5'67	5'93	7'41	10'07	13'02	14'92	15'57	14'68	12'28	9'20	6'52	4'77	4'20	4'94	6'52	8'80	11'67	14'34	16'42	17'20	16'60	168 4	
168	14'54	11'30	8'66	6'74 6'05	6'16	7'65	10'05	12'50	14'32	14'85	14'05	11'96	9'47	7'26	6'06	5'80	6'39	7'66	9'64	11'92	14'25	15'90	16'46	15'74	169 5	
169	13'76	10'84	8'61	6'86	6'32	6'58	7'80	9'82	12'04	13'55	14'17	13'54	12'03	10'34	8'60	7'57	7'26	7'62	8'44	9'92	12'12	14'20	15'46	15'54	170 5	
170	14'58	12'66	10'40	8'31	7'04	6'60	6'77	7'78	9'32	11'22	12'80	13'58	13'46	12'40	10'90	9'62	8'66	8'31	8'49	9'05	10'30	12'04	13'70	14'74	171 5	
171	14'75	13'73	12'02	10'10	8'46	7'12	6'53	6'70	7'50	9'03	10'90	12'32	13'20	13'38	12'92	11'94	10'67	9'60	8'94	8'82	9'24	10'33	11'90	13'24	172 5	
172	14'06	14'10	13'34	11'84	10'05	8'26	6'94	6'44	6'67	7'49	9'06	10'86	12'50	13'66	14'10	13'63	12'46	11'06	10'06	9'30	9'05	9'33	10'22	11'60	173 5	
173	12'90	13'82	13'85	13'08	11'64	9'76	8'00	6'70	6'08	6'22	7'28	9'00	10'94	12'77	14'05	14'63	14'17	12'86	11'33	10'04	9'14	8'86	9'20	10'08	174 5	
174	11'26	12'44	13'30	13'52	12'80	11'00	8'85	7'06	5'67	5'05	5'60	7'15	9'26	11'30	13'28	14'45	14'84	13'95	12'40	10'90	9'46	8'62	8'24	8'56	175 5	
175	9'64	11'12	12'55	13'40	13'37	12'07	10'07	8'20	6'17	4'94	4'74	5'62	7'74	9'76	12'14	14'01	15'00	14'86	13'77	12'06	10'27	8'84	8'10	7'94	176 5	
176	8'52	9'68	11'18	12'64	13'37	13'05	11'52	9'17	6'76	5'11	4'16	4'64	6'10	8'00	10'50	12'90	14'56	15'33	14'70	13'32	11'14	9'44	8'17	7'54	177 5	
177	7'57	8'34	9'81	11'65	13'20	13'60	12'56	10'40	7'97	5'83	4'38	4'04	4'96	6'82	9'02	11'57	13'86	15'24	15'44	14'56	12'56	10'36	8'63	7'62	178 5	
178	7'30	7'74	8'86	10'67	12'47	13'67	13'60	12'02	9'66	6'93	4'96	3'94	4'22	5'70	7'84	10'40	12'82	14'74	15'56	15'33	13'80	11'44	9'35	7'79	179 5	
179	7'04	7'03	7'90	9'44	11'66	13'22	13'92	13'00	10'74	8'00	5'64	4'04	3'83	4'76	6'70	9'02	11'37	13'67	15'12	15'46	14'48	12'44	9'96	8'16	180 5	
180	6'86	6'43	6'94	8'42	10'44	12'57	13'67	13'68	12'22	9'64	6'86	4'96	3'98	4'36	5'65	7'72	10'02	12'26	14'31	15'28	15'12	13'77	11'30	9'01	181 5	
181	7'37	6'64	6'56	7'46	9'06	11'01	12'70	13'51	13'01	11'07	8'44	6'12	4'72	4'42	5'32	6'94	8'97	11'17	13'22	14'74	15'17	14'22	12'16	9'74	182 5	
182	7'86	6'74	6'51	7'07	8'16	9'92	11'66	12'82	13'10	11'86	9'72	7'36	5'70	5'02	5'24	6'42	8'07	10'12	11'98	13'73	14'86	14'72	13'40	11'17	183 5	
183	9'22	7'55	6'51	6'57	7'34	8'72	10'61	12'04	12'77	12'64	11'27	9'34	7'48	6'30	5'87	6'54	7'66	9'24	10'97	12'94	14'38	14'88	14'20	12'50	184 5	



FORMS FOR SHORT-PERIOD TIDES.  
 SERIES T.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d
228	5.07	7.18	10.36	13.94	16.34	17.16	16.04	13.12	9.20	5.80	3.36	2.56	3.60	5.73	9.03	12.78	15.94	17.78	18.04	16.74	13.32	9.36	6.05	4.18	224 6	
229	3.80	4.90	7.56	11.10	14.46	16.66	16.88	15.39	12.15	8.23	5.44	3.52	3.32	4.58	7.04	10.14	13.35	16.16	17.52	17.26	15.28	11.80	8.22	5.32	225 6	
230	3.80	4.02	5.58	8.40	11.50	14.52	16.18	16.06	14.38	11.26	7.98	5.62	4.54	4.80	6.25	8.27	11.00	13.96	16.32	17.26	16.42	14.32	10.85	7.62	226 6	
231	5.16	4.10	4.64	6.45	8.92	12.05	14.70	15.80	15.18	13.36	10.62	7.94	6.32	5.74	6.44	7.77	9.72	12.07	14.12	15.66	15.72	14.46	12.06	9.36	227 6	
232	6.96	5.40	5.07	5.84	7.33	9.54	11.87	13.60	14.46	13.96	12.48	10.40	8.65	7.45	7.28	8.00	9.26	10.72	12.27	13.74	14.47	14.18	12.78	10.82	228 6	
233	8.78	6.78	5.83	5.86	6.74	8.34	10.14	12.02	13.26	13.57	12.85	11.76	10.70	9.74	9.12	8.90	9.34	10.06	10.94	12.10	12.88	13.72	13.38	11.88	10.06	229 7
234	8.17	7.02	6.68	7.00	7.70	8.77	10.10	11.44	12.33	12.66	12.46	12.00	11.36	10.62	10.07	9.67	9.77	10.12	10.82	11.54	12.43	12.67	12.12	11.23	280 7	
235	9.96	8.64	7.77	7.46	7.69	8.30	9.04	10.10	11.17	12.34	12.90	12.90	12.34	11.72	11.15	10.62	10.30	10.00	10.14	10.50	11.34	11.96	12.26	11.97	231 7	
236	11.38	10.53	9.44	8.35	7.66	7.57	8.12	9.06	10.48	11.57	12.72	13.42	13.56	13.18	12.30	11.45	10.72	10.26	9.92	9.63	9.08	9.88	10.76	11.62	12.32	282 7
237	12.18	11.42	10.36	9.08	8.15	7.53	7.24	7.70	8.54	9.82	11.43	12.72	13.64	13.66	13.26	12.36	11.22	10.18	9.34	8.97	9.08	9.88	10.76	11.64	283 7	
238	12.16	12.35	11.85	10.40	8.78	7.36	6.44	6.28	7.14	8.37	10.20	11.94	13.38	14.40	14.54	13.58	12.17	10.70	9.34	8.82	8.84	9.26	10.00	11.16	284 7	
239	12.50	13.30	13.42	12.06	10.16	8.40	6.86	6.06	6.14	7.20	8.95	10.80	12.76	13.96	14.91	14.84	13.64	11.84	9.97	8.77	8.36	8.48	8.96	10.06	285 7	
240	11.56	13.12	13.97	13.64	12.06	9.70	7.27	5.96	5.56	6.35	7.80	9.76	11.70	13.66	15.10	15.46	14.62	12.86	10.57	8.64	7.46	7.31	7.76	8.84	286 7	
241	10.72	12.64	14.21	14.62	13.44	11.00	8.24	6.24	5.17	5.36	6.54	8.54	10.66	13.00	15.02	15.96	15.30	14.08	11.60	8.97	7.34	6.70	6.84	7.80	287 7	
242	9.62	11.70	13.76	14.95	14.97	12.76	10.00	7.37	5.56	4.97	5.74	7.38	9.36	11.94	14.36	16.04	16.27	15.32	13.08	10.11	7.72	6.36	6.10	6.94	288 7	
243	8.63	10.82	13.20	15.21	15.71	14.43	11.89	8.54	6.26	4.97	5.06	6.36	8.22	10.64	13.40	15.80	16.62	16.16	14.21	11.38	8.34	6.35	5.46	5.74	289 7	
244	7.13	9.22	11.84	14.36	15.71	15.48	13.64	10.66	7.60	5.70	4.96	5.70	7.24	9.54	12.02	14.56	16.24	16.56	15.34	12.80	9.60	7.06	5.50	5.18	240 7	
245	5.94	7.72	10.28	13.04	15.14	15.90	14.88	12.52	9.63	7.07	5.74	5.64	6.67	8.36	10.62	13.17	15.30	16.38	15.97	14.06	11.04	8.16	6.11	5.05	241 7	
246	4.85	5.64	7.12	9.24	11.64	13.96	15.06	14.75	13.17	10.76	8.64	7.30	6.86	7.52	9.30	11.47	13.80	15.46	15.84	14.77	12.44	9.37	7.06	5.37	242 7	
247	5.32	5.38	6.34	7.85	9.86	11.96	13.64	14.58	14.07	12.68	10.68	8.97	8.02	7.81	8.36	9.26	10.60	12.24	13.73	14.41	13.86	12.25	10.02	8.06	243 7	
248	6.46	5.62	5.78	6.47	7.80	9.63	11.38	12.97	13.74	13.44	12.44	11.04	9.83	8.84	8.57	8.87	9.67	10.67	11.96	13.06	13.46	13.08	11.68	9.86	244 7	
249	8.26	6.87	6.17	6.26	7.02	8.17	9.66	11.26	12.55	13.37	13.57	12.94	11.92	10.73	9.67	9.16	9.18	9.63	10.54	11.48	13.46	12.92	12.66	11.74	245 7	
250	10.42	8.87	7.44	6.44	6.21	6.66	7.76	9.20	10.76	12.36	13.54	14.05	13.67	12.68	11.26	10.02	9.22	8.90	9.14	9.86	10.86	12.02	12.84	12.98	246 7	
251	12.36	11.16	9.57	7.60	6.44	5.63	5.97	7.17	8.80	10.66	12.80	14.28	14.96	14.74	13.66	11.82	10.04	8.66	8.02	8.14	9.04	10.38	12.00	13.14	247 7	
252	13.74	13.40	12.04	10.04	7.64	5.76	4.78	5.02	6.24	8.16	10.78	13.20	15.04	15.98	15.74	14.33	11.96	9.30	7.37	6.55	5.70	8.06	9.98	12.06	248 7	
253	13.93	14.86	14.44	12.80	10.18	7.37	5.17	3.90	4.03	5.50	7.96	10.88	13.80	16.04	17.04	16.46	14.44	11.04	8.24	6.27	5.15	5.63	7.24	9.64	249 7	
254	12.54	14.74	15.98	15.46	13.29	9.94	6.63	4.34	3.17	2.53	5.38	8.20	11.40	14.56	16.82	17.44	16.36	13.83	9.98	6.70	4.46	3.84	4.58	6.80	250 7	
255	10.06	13.28	15.76	16.64	15.75	12.94	9.26	6.06	3.66	2.97	3.72	5.66	8.70	12.20	15.53	17.33	17.53	15.87	12.42	8.56	5.32	3.44	3.17	4.55	251 7	
256	7.26	10.87	14.22	16.50	17.05	15.47	12.37	8.41	5.52	3.48	3.10	4.46	6.74	9.94	13.47	16.22	17.47	17.02	14.77	10.84	7.23	4.52	3.00	3.30	252 7	
257	5.07	8.06	11.72	14.94	16.86	16.90	14.94	11.54	8.00	5.38	3.90	4.20	5.52	7.95	11.06	14.30	16.51	17.04	15.88	12.99	9.17	5.97	3.70	2.94	253 7	
258	3.94	6.16	9.14	12.45	15.42	16.68	16.10	13.81	10.56	7.46	5.47	4.87	5.60	7.04	9.54	12.25	14.81	16.16	16.06	14.44	11.07	7.87	5.34	3.84	254 7	
259	3.92	5.16	7.43	10.36	13.44	15.47	16.04	14.92	12.66	9.98	7.74	6.47	6.36	7.02	8.54	10.58	12.80	14.58	15.36	14.73	12.52	9.86	7.17	5.31	255 7	
260	4.44	5.02	6.44	8.50	11.04	13.56	14.79	14.77	13.46	11.46	9.44	8.00	7.36	7.56	8.36	9.51	11.10	12.60	13.73	13.94	12.90	11.02	8.73	6.90	256 7	
261	5.70	5.63	6.34	7.60	9.36	11.36	13.14	13.88	13.60	12.43	10.94	9.64	8.76	8.44	8.70	9.18	9.95	10.88	12.06	12.76	12.71	11.64	9.87	8.26	257 7	





FORMS FOR SHORT-PERIOD TIDES.

SERIES T.--(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
207	14.60	16.81	17.35	16.28	13.64	10.44	7.71	6.07	5.84	6.88	8.97	11.47	14.12	15.94	16.22	14.81	11.87	8.55	5.46	3.46	2.87	4.17	6.35	9.32	208 9	
208	13.00	15.95	17.47	17.44	15.72	12.68	9.66	7.28	5.94	6.04	7.36	9.64	12.45	14.81	16.04	15.60	13.70	10.52	7.15	4.66	2.92	3.10	4.72	7.47	209 9	
209	10.55	13.92	16.35	17.36	16.74	14.57	11.67	8.85	6.76	5.94	6.28	7.70	9.92	12.68	14.78	15.58	14.78	12.36	9.26	6.36	4.20	3.07	3.72	5.55	300 9	
300	8.04	11.05	14.10	16.17	16.96	16.12	14.06	11.35	8.82	7.14	6.57	7.02	8.46	10.56	13.14	14.64	15.04	13.76	11.47	8.74	6.42	4.70	4.22	5.00	301 9	
301	6.86	9.02	11.88	14.60	16.11	16.22	15.16	13.26	10.86	8.86	7.58	7.14	7.44	8.84	10.92	12.84	13.84	13.86	12.57	10.68	8.54	6.84	5.56	5.27	302 9	
302	5.98	7.33	9.36	11.72	14.00	15.22	15.38	14.58	12.88	11.01	9.42	8.12	7.64	7.92	8.94	10.40	11.82	12.91	13.12	12.26	10.75	9.22	7.66	6.68	303 9	
303	6.30	6.72	7.86	9.44	11.50	13.34	14.46	14.66	13.96	13.74	11.30	9.76	8.54	7.93	7.84	8.40	9.60	10.88	12.06	12.64	12.40	11.47	10.10	8.76	304 9	
304	7.68	7.01	7.14	6.80	7.40	8.84	10.74	12.56	13.87	14.54	13.04	11.45	9.76	8.15	7.22	7.02	7.48	8.84	10.32	11.48	12.55	12.87	12.46	11.36	305 9	
305	9.70	8.28	7.14	6.80	7.40	8.84	10.74	12.56	13.87	14.54	13.04	11.45	9.76	8.15	7.22	7.02	7.48	8.84	10.32	11.48	12.55	12.87	12.46	11.36	306 9	
306	12.30	10.26	8.61	7.37	6.86	7.24	8.35	10.36	12.50	14.13	15.08	14.96	13.80	11.64	9.03	6.30	5.88	6.50	8.20	10.07	11.93	13.36	14.04	13.66	307 9	
307	14.86	13.04	10.66	8.56	7.12	6.44	6.77	8.02	10.14	12.62	14.56	15.55	15.25	13.56	10.92	8.12	5.82	4.22	4.10	5.32	7.70	10.12	12.66	14.54	15.37	307 9
308	16.05	15.06	12.86	10.40	8.16	6.53	5.96	6.51	8.24	10.85	13.27	15.16	15.84	15.03	14.55	11.68	8.46	5.64	3.63	3.86	5.60	8.44	11.74	14.64	15.31	308 9
309	16.50	16.72	15.38	12.86	9.98	7.70	6.95	5.93	6.71	8.67	11.55	13.84	15.52	15.84	14.55	11.68	8.46	5.64	3.63	3.86	5.60	8.44	11.74	14.64	15.31	309 9
310	15.81	17.12	16.72	14.87	12.03	9.20	7.26	6.32	6.37	7.46	9.60	12.20	14.35	15.67	15.28	13.15	10.15	7.00	4.47	3.03	3.22	5.03	9.62	13.08	310 9	
311	14.05	16.38	17.05	16.14	13.92	11.10	8.66	6.87	6.16	6.46	8.00	10.44	13.10	14.76	15.16	13.92	11.40	8.36	5.66	3.69	2.94	3.94	6.18	9.01	312 9	
312	12.24	14.92	16.53	16.56	15.16	12.66	10.06	7.96	6.74	6.60	7.35	9.00	11.24	13.43	14.50	14.36	12.66	9.94	7.20	4.97	3.56	3.77	5.34	7.72	313 9	
313	10.56	13.46	15.64	16.34	15.71	13.92	11.46	9.28	7.66	6.80	6.98	7.98	9.96	12.00	13.52	14.02	13.37	11.18	8.81	6.52	4.86	4.33	5.20	6.90	314 9	
314	9.14	11.80	14.20	15.72	15.81	14.66	12.72	10.71	8.96	7.82	7.56	7.92	9.16	10.68	12.24	13.26	13.26	12.06	10.17	8.00	6.25	5.31	5.50	6.66	315 9	
315	8.34	10.52	12.80	14.44	15.18	14.68	13.32	11.56	10.02	8.76	8.10	8.00	8.60	9.65	10.96	12.18	12.58	12.23	11.04	9.16	7.62	6.54	6.20	6.84	316 9	
316	7.96	9.38	11.14	12.91	14.18	14.40	13.64	12.37	10.90	9.38	8.78	8.46	8.68	9.30	10.00	10.94	11.57	11.80	11.36	10.28	8.94	7.84	7.18	7.20	317 9	
317	7.86	8.86	9.98	11.46	12.86	13.86	13.83	12.96	11.72	10.53	9.66	9.14	8.92	8.96	9.17	9.66	10.40	11.10	11.37	11.01	10.20	9.26	8.46	8.10	318 9	
318	8.14	8.66	9.44	10.56	11.74	12.76	13.34	13.26	12.61	11.72	10.86	9.76	9.04	8.80	8.85	9.16	9.64	10.14	10.74	11.18	11.32	11.06	10.36	9.58	319 9	
319	8.94	8.71	8.90	9.50	10.42	11.46	12.48	13.10	13.15	12.64	11.84	10.76	9.24	8.13	7.50	7.43	7.86	8.83	10.03	11.16	12.23	12.80	12.64	11.66	320 9	
320	9.98	8.64	8.75	9.38	10.38	11.46	12.41	13.07	13.16	12.84	11.84	10.56	9.24	8.13	7.50	7.03	6.31	7.08	8.52	10.23	11.92	13.17	13.63	13.10	321 9	
321	10.25	9.04	8.36	8.34	8.96	10.02	11.20	12.46	13.23	13.47	13.00	11.72	10.14	8.38	7.03	6.27	6.31	7.08	8.52	10.23	11.92	13.17	13.63	13.10	322 9	
322	11.86	10.18	8.76	7.98	7.96	8.75	10.13	11.64	13.14	13.94	13.94	13.04	11.34	9.36	7.45	5.86	5.13	5.46	6.76	8.80	11.15	13.20	14.66	14.98	323 9	
323	13.97	11.76	9.58	8.10	7.27	7.36	8.22	9.83	11.76	13.33	14.28	14.14	12.87	10.56	7.98	5.77	4.14	3.74	4.67	6.71	9.27	12.01	14.40	15.66	324 9	
324	15.44	13.71	11.16	8.74	7.02	6.40	6.78	8.22	10.37	12.25	13.88	14.74	14.20	12.26	9.36	6.51	4.12	2.75	2.94	4.56	7.03	10.05	13.37	15.65	325 9	
325	16.62	15.90	13.76	10.86	8.17	6.45	5.84	6.36	8.12	10.44	12.84	14.46	15.08	13.97	11.41	8.07	4.96	2.57	1.63	2.58	4.74	7.64	11.12	14.22	326 9	
326	16.47	17.07	15.75	12.96	9.86	7.36	5.65	5.46	6.44	8.40	11.20	13.57	15.11	15.17	13.27	9.96	6.40	3.62	1.76	1.54	3.26	6.02	9.35	12.97	327 9	
327	15.66	17.40	17.25	15.37	12.23	9.00	6.75	5.63	5.63	6.88	9.32	12.22	14.44	15.50	14.80	12.31	8.84	5.46	3.00	1.66	2.20	4.15	6.95	10.46	328 9	
328	13.81	16.44	17.54	16.82	14.56	11.38	8.50	6.32	5.44	5.74	7.26	10.06	12.76	14.67	15.26	14.06	11.32	8.05	5.16	2.94	2.16	3.11	5.16	7.96	329 9	
329	11.25	14.30	16.57	17.22	16.23	13.81	10.68	8.07	6.16	5.50	5.88	7.64	10.25	12.77	14.29	14.72	13.33	10.74	7.81	5.32	3.66	3.26	4.42	6.34	330 9	
330	8.86	11.67	14.58	16.33	16.57	15.28	12.84	9.93	7.47	6.23	5.72	6.26	7.94	10.30	12.38	13.76	13.96	12.68	10.56	8.18	6.28	4.97	4.83	5.73	331 9	
331	7.34	9.38	12.05	14.37	15.76	15.80	14.56	12.28	9.94	8.13	6.64	6.14	6.54	8.04	10.04	11.78	12.86	13.16	12.24	10.73	8.96	7.30	6.24	5.96	332 9	

332	6.50	7.80	9.84	12.15	13.88	14.87	14.84	13.77	11.77	10.66	8.23	6.86	6.34	6.56	7.79	9.30	10.84	12.16	12.76	13.53	11.48	10.14	8.60	7.52	333 10	
333	7.06	7.44	8.47	10.17	11.91	13.34	14.21	14.40	13.72	12.30	10.42	8.41	6.88	6.14	6.37	7.32	8.81	10.45	11.84	12.86	13.08	12.42	11.25	9.75	334 10	
334	8.54	7.84	7.88	8.64	10.02	11.65	13.16	14.14	14.30	13.64	12.17	10.31	8.37	6.68	5.72	5.86	6.88	8.64	10.40	12.07	13.31	13.88	13.62	12.36	335 10	
335	10.67	9.06	8.12	7.90	8.54	9.72	11.26	12.78	13.82	14.20	13.74	12.14	10.05	7.76	6.00	5.04	5.23	6.52	8.50	10.56	12.60	14.12	14.40	13.86	336 10	
336	12.58	10.80	8.97	7.94	7.68	8.24	9.30	11.14	12.75	13.98	14.44	13.73	11.85	9.10	6.84	5.06	4.41	5.04	6.57	8.66	11.20	13.52	15.24	15.84	337 10	
337	15.08	13.13	10.86	9.00	7.82	7.54	8.05	9.36	11.14	12.94	14.20	14.46	14.56	12.94	10.26	7.33	5.11	3.87	4.05	5.64	7.81	10.61	13.20	15.47	338 10	
338	16.34	15.17	12.88	10.26	8.38	7.53	7.40	8.14	9.77	11.52	13.36	14.60	14.76	14.17	12.16	8.93	6.32	4.31	3.72	4.64	6.56	9.06	11.87	14.55	340 10	
339	16.54	16.22	14.70	12.20	9.81	8.08	7.33	7.37	8.31	10.05	12.02	13.86	14.58	14.48	13.44	10.64	7.77	5.58	4.12	4.16	5.63	7.85	10.36	13.16	341 10	
340	16.23	16.72	15.37	13.94	11.34	8.98	7.71	7.36	7.70	9.02	10.97	12.94	14.40	14.70	13.44	10.64	7.77	5.58	4.12	4.16	5.63	7.85	10.36	13.16	341 10	
341	15.34	16.56	16.48	15.11	12.72	10.27	8.26	7.37	7.26	8.12	9.82	11.91	13.58	14.48	14.07	12.12	9.32	6.72	4.74	3.96	4.91	6.70	9.02	11.70	342 10	
342	14.07	15.87	16.56	15.80	13.96	11.44	9.32	7.8c	7.24	7.44	8.72	10.57	12.55	14.00	14.24	13.24	10.72	8.06	5.93	4.58	4.74	6.03	8.20	10.34	343 10	
343	12.88	15.05	16.23	16.28	14.89	12.65	10.30	8.54	7.58	7.44	8.17	9.64	11.50	13.03	13.80	13.45	11.78	9.47	7.26	5.64	5.07	5.86	7.43	9.20	344 10	
344	11.48	13.56	15.17	15.82	15.18	13.58	11.42	9.46	7.98	7.36	7.62	8.50	10.02	11.60	12.67	13.00	12.14	10.36	8.34	6.54	5.59	5.67	6.77	8.43	345 10	
345	10.27	12.57	13.90	14.96	14.86	13.76	12.00	10.22	8.66	7.73	7.38	7.80	8.82	10.22	11.48	12.26	12.24	11.15	9.47	8.01	6.87	6.45	6.75	8.83	346 10	
346	9.14	10.75	12.56	13.86	14.46	14.06	12.87	11.31	9.72	8.40	7.76	7.73	8.27	9.36	10.54	11.48	12.02	11.81	10.84	9.56	8.46	7.76	7.56	8.00	347 10	
347	8.95	10.95	11.60	13.13	14.20	14.42	13.83	12.50	10.98	9.76	8.76	8.24	8.24	8.80	9.62	10.53	11.27	11.70	11.62	11.14	10.38	9.49	8.78	8.48	348 10	
348	8.71	9.47	10.70	12.04	13.16	13.78	13.79	13.14	11.94	10.54	9.17	8.30	7.83	8.04	8.58	9.36	10.22	11.00	11.54	11.74	11.57	10.96	10.14	9.44	349 10	
349	9.04	9.10	9.74	10.90	12.24	13.16	13.57	13.38	12.64	11.55	10.26	8.86	7.83	7.22	7.36	7.86	8.85	10.11	11.13	11.95	12.42	12.30	11.74	10.77	350 10	
350	9.72	9.66	9.01	9.55	10.76	11.97	12.94	13.38	13.14	12.44	11.22	9.78	7.04	6.26	6.15	6.82	8.20	9.97	11.56	12.90	13.50	13.36	12.36	10.92	351 11	
351	9.68	8.84	8.68	9.14	10.18	11.57	12.70	13.30	13.22	12.46	11.00	9.17	7.18	5.75	4.90	4.92	6.07	7.94	10.07	12.03	13.66	14.48	14.16	12.76	352 11	
352	10.77	9.04	7.98	7.73	8.23	9.70	11.40	12.74	13.42	13.45	12.54	10.80	8.50	6.30	4.47	3.64	4.12	5.82	8.20	10.84	13.27	14.95	15.70	14.97	353 11	
353	13.05	10.60	8.64	7.50	7.36	8.16	9.80	11.80	13.38	14.33	14.26	13.00	10.50	7.72	5.17	3.42	2.93	4.16	6.37	9.00	12.12	14.97	16.74	16.96	354 11	
354	15.68	13.11	10.34	8.06	6.98	7.04	8.06	10.00	12.15	14.04	15.14	15.03	13.10	10.20	7.00	4.27	2.40	2.20	3.93	6.57	9.77	13.27	16.13	17.72	355 11	
355	17.51	15.78	12.57	9.74	7.27	6.14	6.36	7.56	9.86	12.72	14.77	15.81	15.20	12.64	9.26	5.91	3.10	1.55	1.93	4.00	7.06	10.68	14.30	17.04	356 11	
356	18.34	17.24	15.47	12.00	8.88	6.58	5.67	6.00	7.50	10.14	13.10	15.24	16.17	14.94	12.16	8.55	5.06	2.64	1.50	2.57	5.14	8.44	11.93	15.00	357 11	
357	17.66	18.34	17.37	14.51	10.92	7.77	5.66	5.14	5.64	7.65	10.63	13.44	15.46	15.86	14.14	10.98	7.68	4.48	2.36	1.77	3.30	5.83	8.90	12.30	358 11	
358	15.56	17.50	17.88	16.62	13.58	9.97	6.94	5.14	4.70	5.52	7.63	10.73	13.70	15.36	15.32	13.24	9.92	6.64	4.73	3.07	3.08	4.74	6.97	9.86	359 11	
359	13.01	15.80	17.38	17.48	15.95	12.86	9.53	6.72	5.22	4.90	5.97	8.93	10.96	13.30	14.68	14.83	13.24	10.55	7.68	5.43	4.33	4.63	5.97	8.02	360 11	
360	10.57	13.25	15.58	16.60	16.14	14.11	11.13	8.76	6.38	5.17	5.13	6.30	8.60	10.76	12.74	13.74	13.62	12.37	10.30	8.14	6.53	5.84	6.14	7.14	361 11	
361	8.74	10.77	13.13	14.96	15.71	15.12	13.32	10.86	8.44	6.53	5.48	5.27	6.00	7.78	9.85	11.62	12.84	13.10	12.28	10.74	9.22	7.96	7.33	7.28	362 11	
362	7.93	9.16	10.97	13.12	14.54	14.68	13.66	12.28	10.12	8.24	6.78	5.82	5.70	6.37	7.72	9.40	11.06	12.32	12.86	12.50	11.47	10.24	9.12	8.42	363 11	
363	8.24	8.54	9.54	11.12	12.64	13.57	13.57	12.88	11.44	9.87	8.24	6.74	5.77	5.52	6.12	7.27	8.94	10.64	12.10	13.01	13.12	12.46	11.26	10.02	364 11	
364	9.06	8.38	8.66	9.44	10.68	11.96	12.92	13.14	12.66	11.54	10.06	8.36	6.86	5.72	5.37	5.87	7.17	9.14	11.00	12.70	13.68	13.81	12.94	11.57	365 11	
365	10.28	9.14	8.62	8.63	9.20	10.44	11.66	12.53	12.92	12.58	11.64	9.77	7.86	6.12	5.05	4.78	5.62	7.06	9.15	11.26	13.23	14.30	14.32	13.36	366 11	
366	11.78	10.34	9.17	8.44	8.24	8.62	9.76	11.04	12.36	13.08	12.90	11.65	9.64	7.34	5.52	4.45	4.52	5.76	7.66	9.97	12.43	14.27	15.18	14.97	367 11	
367	13.73	11.82	10.16	8.86	8.24	8.26	8.96	10.32	11.70	12.96	13.58	13.16	11.26	8.91	6.66	4.96	4.33	4.86	6.36	8.55	11.00	13.44	15.21	15.84	368 11	
368	15.17	13.56	11.44	9.66	8.38	7.80	7.97	9.00	10.56	12.24	13.46	13.82	12.72	10.52	7.90	5.74	4.34	4.11	5.34	7.23	9.78	12.44	14.65	15.93	369 11	
369	15.94	14.74	12.37	10.23	8.53	7.47	7.31	7.97	9.38	11.36	13.14	14.17	14.00	12.18	9.43	...	...	...	...	...	...	...	...	...	...	370 2
Sum	858.6389703	898.1888536	832.8880882	767.2673954	727.5173631	757.2778673	788.5177934	747.9569064	636.7959100	565.8056693	600.2665901	727.3179398	72	72	72	72	72	72	72	72	72	72	72	72	72	No. of Days. 729 178 17862.94
No.	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	

FORMS FOR SHORT-PERIOD TIDES.

BOMBAY—Commencing 0 hours, Astronomical Time, 1st January, 1885.

Argument ( $\gamma - \frac{1}{2}\sigma - \frac{1}{2}\eta$ ).

SERIES MS.

Motion per mean Solar hour = 14°.7460261.

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
1	15.52	12.96	9.13	5.76	3.03	1.68	2.28	4.80	7.90	11.70	15.50	18.00	18.85	18.08	15.14	11.54	8.50	6.21	5.53	6.08	8.20	11.31	14.16	16.06	1 23	
2	16.66	15.40	12.16	8.40	4.86	2.56	2.90	5.56	8.82	12.94	16.44	18.58	18.97	17.67	14.24	10.56	7.53	5.57	5.16	6.10	8.63	11.84	14.68	16.63	3 0	
3	16.96	15.24	11.92	8.00	4.87	2.80	2.57	4.24	6.84	10.20	14.07	17.26	18.86	18.84	17.06	13.20	9.77	6.90	5.23	4.96	6.16	8.86	12.14	14.87	4 0	
4	16.40	16.40	14.28	11.00	7.63	4.88	3.55	3.86	5.55	8.01	11.36	14.83	17.16	18.38	17.93	15.80	8.68	6.10	5.05	5.25	6.68	9.24	12.28	14.51	5 1	
5	15.96	15.58	13.48	10.47	7.54	5.76	5.07	5.67	7.22	9.17	12.11	15.02	17.02	17.55	16.63	14.11	10.96	8.16	6.22	5.47	5.84	7.18	9.67	12.12	6 1	
6	14.04	15.00	14.45	12.62	10.24	8.07	7.04	6.84	7.54	8.67	10.60	12.84	15.06	16.36	16.35	15.24	12.76	10.11	8.00	6.64	6.17	6.55	7.86	9.76	7 1	
7	11.80	13.27	13.64	12.22	10.47	9.05	8.44	8.46	9.03	9.97	11.20	13.05	14.64	15.46	15.18	13.87	11.68	9.76	8.10	7.16	7.03	7.40	8.29	9.82	8 2	
8	11.16	12.55	13.24	13.07	12.20	11.16	10.27	9.64	9.60	9.90	10.60	11.70	12.96	14.02	14.44	13.75	12.27	10.82	9.20	7.93	7.24	7.06	7.34	8.07	9 2	
9	9.14	10.55	11.74	12.48	12.66	12.27	11.60	10.93	10.34	9.98	9.86	10.17	12.14	13.06	13.36	12.72	11.71	10.43	9.14	7.97	7.14	6.75	6.94	7.74	10 3	
10	8.96	10.26	11.64	12.67	13.14	12.97	12.20	11.24	10.48	10.12	10.05	10.23	10.84	11.64	12.27	12.68	12.37	11.53	10.42	8.97	7.80	6.96	6.38	6.44	11 3	
11	7.28	8.73	10.47	12.14	13.23	13.84	13.63	12.58	11.38	10.27	9.77	9.62	9.89	10.44	11.24	11.97	12.52	12.50	11.87	10.54	8.76	7.34	6.16	5.74	6.34	12 4
12	7.62	9.54	11.46	13.22	14.24	14.58	13.94	12.72	11.24	10.02	9.32	9.14	9.46	10.37	11.48	12.46	13.04	12.84	11.88	10.23	8.20	6.52	5.62	5.56	13 4	
13	6.50	8.14	10.17	12.34	14.10	15.20	15.17	13.97	12.27	10.58	9.35	8.75	8.76	9.26	10.34	11.68	12.96	13.64	13.36	11.80	9.66	7.32	5.82	5.14	14 4	
14	5.44	6.74	8.86	11.26	13.66	15.38	15.87	15.24	13.66	11.54	9.82	8.71	8.16	8.36	9.30	10.74	12.46	13.64	13.98	13.00	10.84	8.24	6.20	4.76	4.46	15 5
15	5.40	7.36	9.78	12.57	14.82	16.13	15.97	14.56	12.25	10.05	8.46	7.82	7.74	8.41	9.71	11.76	13.30	14.26	14.09	12.44	9.76	7.00	5.12	4.20	16 5	
16	4.63	6.12	8.44	11.24	14.04	15.74	16.36	15.71	13.82	11.22	8.94	7.54	6.94	7.15	8.40	10.27	12.44	14.06	14.68	13.84	11.50	8.60	5.94	4.37	4.02	17 6
17	5.06	7.26	9.66	12.72	15.20	16.55	16.63	15.27	12.77	9.97	7.86	6.84	6.68	7.56	9.32	11.40	13.55	14.80	14.78	13.22	10.43	7.48	5.34	4.30	18 6	
18	4.66	6.25	8.54	11.38	14.15	16.15	16.88	16.08	14.04	11.02	8.54	6.76	6.12	6.34	7.60	9.84	12.14	14.06	14.84	14.14	12.06	9.06	6.46	4.67	19 6	
19	4.24	5.16	7.15	9.68	14.87	16.44	16.45	15.00	12.42	9.50	7.22	5.80	5.43	6.26	8.16	10.65	12.88	14.28	14.56	13.33	10.92	8.30	6.04	4.87	20 7	
20	5.06	6.54	8.66	11.04	13.64	15.62	16.36	15.76	13.82	11.00	8.37	6.37	5.54	5.64	6.83	8.93	11.40	13.32	14.42	14.25	12.47	10.10	7.91	6.34	21 7	
21	5.70	6.30	7.70	9.76	12.17	14.36	15.74	15.96	14.86	12.76	10.13	7.78	6.17	5.70	6.11	7.62	9.70	11.76	13.36	14.14	13.72	12.06	9.94	8.32	7.22	22 8
22	7.01	7.74	8.97	10.80	12.97	14.62	15.50	15.17	13.80	11.46	9.14	7.34	6.17	6.00	6.68	8.02	9.76	11.65	13.04	13.76	13.34	12.14	10.65	9.07	23 8	
23	8.15	8.14	8.68	9.86	11.56	13.36	14.56	15.02	14.37	12.76	10.76	8.71	6.96	6.23	6.09	6.68	7.86	9.46	11.24	12.66	13.36	13.34	12.38	11.08	24 8	
24	9.94	8.88	9.28	10.22	11.70	13.06	14.14	14.41	13.60	12.06	10.26	8.46	7.10	6.25	6.08	6.56	7.64	9.14	10.84	12.34	13.44	13.81	13.33	12.18	25 9	
25	10.75	9.76	9.24	9.34	10.07	11.16	12.40	13.38	13.66	13.03	11.87	10.24	8.47	7.00	5.83	5.38	5.68	6.78	8.55	10.33	12.22	13.56	14.30	14.16	26 9	
26	13.05	11.56	10.06	9.11	8.87	9.40	10.46	11.87	12.94	13.44	13.33	12.40	10.74	8.86	6.83	5.22	4.41	4.77	6.10	8.10	10.50	12.63	14.53	15.56	15.33	27 10
27	13.76	11.64	9.52	8.28	7.92	8.25	9.53	11.24	12.70	13.80	14.14	13.30	11.34	8.72	6.20	4.24	3.38	3.76	5.30	7.76	10.55	13.50	15.72	16.74	28 10	
28	16.12	14.36	11.40	8.83	7.24	6.86	7.53	9.20	11.11	12.97	14.55	15.08	14.17	11.84	8.82	5.70	3.60	2.56	3.06	5.04	7.88	11.48	14.56	17.04	17.86	29 11
29	17.00	14.36	10.96	8.07	6.27	5.77	6.57	8.62	11.25	13.92	15.74	16.28	14.96	12.18	8.44	5.42	3.22	2.16	3.07	5.52	8.75	12.46	16.01	18.10	30 11	
30	18.47	17.26	13.80	10.14	7.09	5.27	5.02	6.02	8.40	11.85	14.65	16.52	16.84	15.28	11.68	7.88	4.80	2.74	2.38	4.00	6.66	10.10	13.98	17.01	31 11	
31	18.64	18.38	16.30	12.42	8.97	6.01	4.46	4.57	6.12	9.14	12.56	15.46	17.00	16.86	14.76	11.06	7.36	4.34	2.72	2.99	4.86	7.74	11.40	14.94	17.54	32 12
32	18.47	17.66	14.67	11.08	7.54	5.01	3.93	4.32	6.55	9.62	13.04	15.80	16.84	16.08	13.73	10.16	6.82	4.54	3.58	4.44	6.36	9.36	12.84	15.86	33 12	
33	17.74	17.94	16.48	13.27	9.84	6.84	4.96	4.33	5.26	7.44	10.66	13.70	15.74	16.43	15.42	12.82	9.66	5.42	5.14	6.20	8.06	10.66	13.66	16.02	34 13	
34	17.12	16.74	14.88	11.68	8.76	6.34	4.92	4.74	5.86	8.26	11.07	13.60	15.16	15.34	14.06	11.68	9.04	7.34	6.56	6.94	8.04	9.56	11.76	14.24	35 13	
35	15.60	16.04	15.34	13.02	10.16	7.86	6.27	5.54	5.86	7.18	9.07	11.36	13.26	14.34	14.26	12.88	11.00	9.39	8.26	7.92	8.30	9.05	10.36	12.08	36 13	

TIDAL OBSERVATIONS.

[CAP. VII.]

36	13.76	14.66	14.44	11.12	9.30	7.54	6.26	6.13	6.88	7.86	9.28	10.86	12.27	13.10	12.54	11.93	10.66	9.72	9.12	9.06	9.26	9.66	10.60	11.82	37 14	
37	12.86	13.34	12.82	11.45	10.03	8.74	7.48	6.86	6.78	7.17	7.94	9.02	10.30	11.34	11.07	11.92	11.42	10.84	10.34	10.07	9.97	9.77	9.94	10.44	38 14	
38	11.32	12.06	12.26	11.78	10.88	9.87	8.84	7.86	7.24	6.94	7.18	8.03	10.14	11.00	11.56	11.85	11.77	11.46	11.12	10.57	10.07	9.70	9.70	10.13	39 15	
39	10.80	11.27	11.45	11.23	10.76	9.97	9.00	8.00	7.11	6.58	6.74	7.44	8.31	9.84	10.90	11.76	12.34	12.55	12.30	11.66	10.37	9.76	9.34	9.17	40 15	
40	9.56	10.24	10.94	11.36	11.44	10.97	10.10	9.07	7.87	6.85	6.30	6.30	7.26	8.50	10.16	11.44	12.65	13.26	13.32	12.56	11.36	10.08	9.16	8.64	41 16	
41	9.01	9.76	10.58	11.23	12.40	12.66	12.07	10.47	8.56	6.12	5.54	5.82	6.94	8.54	10.36	12.06	13.46	13.97	13.64	12.30	10.76	9.26	8.14	7.84	42 16	
42	8.12	8.96	10.24	11.32	12.40	12.66	13.60	12.30	7.77	5.88	4.84	4.96	6.33	8.27	10.66	13.07	14.53	14.67	14.84	13.98	12.14	10.00	8.54	7.66	43 16	
43	7.53	8.16	9.56	11.03	12.66	13.62	13.88	11.93	9.10	6.54	4.66	4.00	4.90	6.86	9.20	11.97	14.34	15.82	15.64	14.78	12.26	9.64	7.54	6.79	44 17	
44	7.00	8.13	9.67	11.85	13.60	14.38	13.88	11.93	9.10	6.54	4.66	4.00	4.90	6.86	9.20	11.97	14.34	15.82	15.64	14.78	12.26	9.64	7.54	6.79	45 17	
45	5.96	6.74	8.48	10.85	13.07	14.56	14.85	13.63	10.90	7.86	5.57	4.07	4.04	5.46	7.84	10.63	13.64	15.83	16.01	13.87	10.90	8.00	6.17	5.46	46 18	
46	5.74	7.26	9.70	12.35	14.42	15.30	15.15	13.08	9.90	6.94	4.75	3.92	4.66	6.62	9.46	12.60	15.08	16.60	16.64	15.00	11.93	8.96	6.76	5.63	47 18	
47	5.06	5.54	7.84	10.54	13.30	15.12	15.66	14.46	11.76	8.44	5.86	4.26	4.25	5.52	7.84	10.68	13.68	15.94	16.68	15.86	13.15	10.22	7.36	5.65	48 18	
48	4.23	4.46	6.07	8.36	11.57	15.34	15.51	13.57	10.53	7.47	5.38	4.52	5.04	6.70	9.14	12.18	14.74	16.26	16.26	14.64	11.74	8.68	6.28	4.54	49 19	
49	4.14	5.07	7.06	9.74	12.44	14.55	15.46	14.76	12.37	9.68	7.24	5.84	5.00	6.54	8.40	10.77	13.32	15.42	16.26	15.47	13.18	10.24	7.54	5.62	50 19	
50	4.34	4.69	5.80	7.87	10.40	12.80	14.50	15.06	14.93	11.86	9.36	7.58	6.64	6.76	7.86	11.66	13.73	15.08	15.32	14.12	11.86	9.24	6.90	5.18	51 20	
51	4.38	5.06	6.46	8.24	10.33	12.41	13.86	14.34	13.41	11.46	9.53	8.05	7.40	7.66	8.38	9.92	11.68	13.36	14.16	14.12	12.82	10.83	8.73	6.87	52 20	
52	5.45	4.92	5.44	6.63	8.23	10.14	11.77	12.96	13.40	12.76	11.56	10.24	9.04	8.45	8.28	8.67	9.76	11.20	12.50	13.18	13.06	11.88	10.25	8.57	53 20	
53	6.98	5.38	5.64	6.37	7.82	9.54	11.17	12.38	13.02	12.96	12.16	11.07	10.02	8.94	8.44	8.48	9.27	10.44	11.57	12.34	12.34	11.70	10.50	8.90	54 21	
54	7.32	5.96	5.24	5.12	5.86	7.17	8.90	10.63	12.10	13.16	13.56	13.13	11.86	10.27	8.88	8.08	7.87	8.42	9.56	10.87	11.93	12.44	12.26	11.27	55 21	
55	9.76	7.96	6.27	5.06	4.55	5.02	6.47	8.52	10.07	12.72	14.86	14.41	12.70	10.66	8.80	7.60	7.21	7.64	9.18	11.00	12.36	13.52	12.60	11.27	56 22	
56	10.86	8.63	6.84	4.63	4.06	4.70	6.46	8.84	11.30	13.80	15.56	16.25	15.33	12.96	10.26	7.95	6.54	6.18	7.03	8.83	11.40	12.96	14.40	14.74	57 22	
57	13.76	11.70	8.84	6.08	4.05	3.42	4.14	6.18	8.80	13.06	14.93	16.76	17.15	15.84	12.87	9.66	7.00	5.18	5.12	6.26	11.16	13.67	15.38	15.86	58 23	
58	14.57	11.26	5.48	3.42	2.92	4.14	6.52	9.58	13.16	16.04	17.62	17.34	17.34	15.27	11.66	8.27	5.56	4.16	4.32	5.81	8.66	11.92	14.74	16.46	59 23	
59	16.54	14.66	11.26	7.66	4.94	3.20	3.27	4.70	7.52	10.86	14.63	17.06	17.98	16.96	13.90	10.20	6.96	4.47	3.56	4.02	6.04	9.40	12.86	15.55	60 23	
60	16.86	16.36	13.86	10.44	6.92	4.34	3.37	3.90	8.56	12.33	15.44	17.27	17.40	15.46	12.93	8.50	5.70	3.74	3.27	4.33	7.10	10.34	13.76	15.97	62 0	
61	16.76	15.76	12.96	9.44	6.74	4.67	4.23	5.26	7.43	10.37	13.82	16.13	17.08	16.40	13.86	10.50	7.26	4.84	3.56	3.86	5.60	8.27	11.55	14.34	63 0	
62	16.02	16.28	14.66	11.66	8.60	6.46	5.26	5.46	6.56	8.86	11.44	14.36	15.97	16.18	14.88	12.00	8.86	4.57	4.06	4.86	6.67	9.40	12.24	14.39	64 1	
63	15.64	15.33	13.25	10.46	8.22	6.76	6.34	7.00	8.36	10.22	12.44	14.42	15.27	14.71	12.72	10.14	7.72	5.93	4.86	5.00	6.10	8.03	10.30	12.47	65 1	
64	13.97	14.58	13.92	12.03	10.14	8.54	7.56	8.42	9.82	11.34	12.96	14.42	14.94	14.24	13.22	11.36	9.36	7.56	6.27	5.84	6.34	7.46	9.00	10.76	66 1	
65	12.44	13.56	13.74	11.40	10.07	9.16	8.96	9.27	9.77	10.46	11.36	12.44	13.97	13.03	12.12	10.40	8.86	7.68	7.02	7.02	7.66	8.54	9.66	10.96	67 2	
66	12.24	12.88	12.88	12.24	11.43	10.66	10.24	10.16	10.24	10.47	10.86	11.44	12.02	12.40	12.24	11.36	10.18	8.87	7.97	7.67	7.94	8.50	9.00	9.78	68 2	
67	10.74	11.76	12.46	12.67	12.27	11.74	11.26	10.87	10.56	10.36	9.58	9.87	10.35	10.89	11.10	11.10	10.78	10.32	9.72	8.86	7.97	7.28	7.26	7.87	69 3	
68	10.46	11.44	12.08	12.36	12.27	12.03	11.50	10.78	10.20	9.73	9.58	9.87	10.16	9.88	10.74	11.40	11.75	11.70	11.14	10.07	8.84	7.56	6.74	7.63	70 3	
69	8.97	10.32	11.56	12.46	13.04	13.10	12.54	11.68	10.56	9.64	9.08	8.82	9.16	9.88	10.74	11.40	11.75	11.70	11.14	10.07	8.84	7.56	6.74	7.63	71 4	
70	8.94	10.62	12.06	13.26	13.78	13.68	12.86	11.34	9.88	8.86	8.16	8.03	8.46	9.64	10.86	12.06	12.78	12.56	11.57	9.92	8.17	6.67	5.98	6.16	72 4	
71	7.20	8.87	10.76	12.70	14.06	14.61	14.06	12.53	10.68	8.96	7.55	6.88	7.05	8.07	9.84	11.76	12.97	13.54	13.03	11.46	9.42	7.27	5.74	5.30	73 4	
72	5.90	7.44	9.66	11.92	14.02	15.17	15.16	13.87	11.66	7.56	6.34	6.07	6.86	8.68	10.80	12.96	14.26	14.55	13.37	11.16	8.45	6.26	5.16	5.12	74 5	
Sum	780.48	791.55	84.03	776.19	756.55	739.51	739.98	754.28	739.34	740.07	775.30	781.18	798.51	806.78	798.63	775.47	745.83	740.42	725.86	696.83	707.13	696.37	715.24	738.79	No. of Days, 73 <sup>d</sup> 18104.31	
No.	74	73	73	74	73	73	73	74	73	73	74	73	73	73	74	73	73	74	73	74	73	74	73	73	73	18104.31

## FORMS FOR SHORT-PERIOD TIDES.

## SERIES MS.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
73	6.24	8.10	10.61	13.22	15.15	15.86	15.17	13.22	10.40	7.86	6.06	5.25	5.54	6.90	9.24	11.72	13.95	15.20	15.12	13.39	10.64	7.57	5.44	4.44	4.44	75 5
74	4.96	6.46	8.94	11.85	14.34	16.00	16.06	14.53	11.64	8.54	5.76	4.22	3.97	5.24	7.30	10.10	13.02	15.04	16.00	12.86	9.54	6.67	4.92	4.38	4.38	76 6
75	5.52	7.55	10.33	13.50	15.75	16.73	16.07	13.66	10.42	7.22	4.92	3.64	4.00	5.66	8.33	11.52	14.30	16.06	16.52	15.06	12.13	8.73	6.13	4.66	4.66	77 6
76	4.99	6.52	8.92	11.86	14.66	16.40	16.50	15.07	11.90	8.47	5.62	3.74	3.22	4.26	6.60	9.60	12.85	15.23	16.56	16.25	14.26	10.83	8.00	5.75	5.75	78 6
77	5.11	5.88	7.84	10.46	13.38	15.68	15.80	13.36	10.12	7.06	4.83	3.54	3.76	5.34	7.86	11.00	13.93	15.92	16.74	15.74	13.36	10.24	7.64	6.12	6.12	79 7
78	6.08	7.14	9.00	11.56	13.90	15.66	15.98	14.76	12.06	8.90	6.13	4.34	3.62	4.36	6.06	8.47	11.31	13.87	15.62	16.12	14.97	12.74	10.02	8.05	8.05	80 7
79	6.96	7.06	7.93	9.67	12.07	14.08	15.23	15.08	13.57	11.16	8.26	6.08	4.76	4.47	5.46	7.26	11.88	13.90	15.36	15.50	14.66	12.67	10.54	8.74	8.74	81 8
80	7.94	8.14	9.06	10.62	12.40	13.77	14.52	14.20	12.80	10.64	8.47	6.76	5.86	5.82	6.49	7.75	9.52	11.71	13.54	14.73	14.90	14.06	12.63	11.05	11.05	82 8
81	9.70	8.86	8.72	9.12	10.24	11.76	13.06	13.60	13.34	12.06	10.56	8.92	7.40	6.43	6.30	6.68	7.68	9.46	11.24	13.02	14.08	14.52	14.22	13.04	13.04	83 8
82	11.70	10.34	8.84	9.04	9.84	10.96	12.02	12.86	12.96	12.44	11.22	9.67	8.30	7.06	6.48	6.64	7.48	8.86	10.64	12.34	13.74	14.48	14.44	13.62	13.62	84 9
83	12.12	10.36	8.96	8.11	7.96	8.44	9.76	7.46	9.22	11.16	12.56	13.57	14.06	11.72	9.38	7.17	5.72	5.38	6.17	7.82	10.00	12.50	14.54	15.84	15.84	86 10
84	14.16	13.20	9.88	8.00	6.90	6.56	6.67	8.88	11.24	13.46	14.86	15.36	14.34	12.05	9.44	6.93	5.38	5.00	5.82	7.83	10.50	13.30	15.60	16.72	16.72	87 10
85	14.64	13.14	9.36	6.97	5.74	5.63	6.67	4.80	6.40	9.20	12.06	16.12	16.16	14.90	12.22	9.12	6.60	5.05	4.86	5.87	8.10	14.15	16.35	17.15	17.15	88 11
86	16.48	14.37	11.37	8.36	6.00	4.67	4.70	6.72	9.92	13.20	15.64	17.04	16.43	16.75	14.92	11.81	8.56	6.27	5.14	5.64	6.94	9.43	12.61	15.44	17.03	89 11
87	16.24	13.58	10.14	7.06	4.83	3.96	4.70	6.72	9.92	13.20	15.64	16.43	17.34	16.56	14.28	10.82	7.84	5.95	5.42	6.12	7.87	10.62	13.66	16.10	16.10	90 11
88	17.08	15.36	11.92	8.64	6.18	4.48	4.35	5.24	7.57	11.00	14.10	16.43	17.13	15.64	12.86	9.53	7.16	5.81	5.93	7.22	9.26	12.02	14.66	16.44	16.44	91 12
89	17.14	16.46	13.96	10.44	7.12	4.80	3.83	6.43	4.41	8.78	12.04	14.74	16.66	16.90	16.50	14.74	11.68	8.84	7.02	6.48	7.04	8.26	10.50	14.94	14.94	92 12
90	16.67	15.06	12.02	8.56	5.84	4.04	3.84	4.93	7.24	10.09	13.22	15.56	16.90	15.82	16.34	15.34	13.10	10.40	7.32	7.28	8.03	9.50	11.53	13.48	14.74	93 13
91	15.83	15.12	12.94	9.87	7.14	5.16	4.22	4.76	6.40	8.73	11.37	14.00	15.48	15.46	14.27	12.24	10.20	8.78	8.26	8.47	9.24	10.52	12.04	13.48	14.74	94 13
92	14.92	13.67	11.34	8.76	6.67	5.40	5.22	6.16	7.85	9.97	12.30	14.30	15.48	15.46	14.27	12.24	10.20	8.78	8.26	8.47	9.24	10.52	12.04	13.48	14.74	95 13
93	14.16	13.84	12.27	10.16	8.14	6.47	5.74	6.22	7.44	9.20	10.85	12.64	14.05	14.67	14.27	12.97	11.44	10.04	9.16	8.84	9.16	9.84	10.95	11.96	11.96	96 14
94	12.80	12.96	12.28	9.24	7.80	6.78	6.70	7.30	8.37	9.54	10.90	12.31	13.52	13.80	13.26	12.13	10.90	10.04	9.60	9.33	9.54	9.90	10.56	11.44	11.44	98 14
95	11.92	12.05	11.54	11.27	10.92	10.30	9.34	8.36	7.74	7.58	7.98	8.76	9.87	11.04	12.50	12.66	12.42	11.96	11.34	10.55	9.91	9.47	9.34	9.52	9.52	98 15
96	10.81	11.14	11.27	11.02	10.62	10.00	9.22	8.40	8.01	8.13	8.63	9.70	10.66	11.77	12.66	13.06	12.94	12.40	11.47	10.59	9.62	8.94	8.54	8.74	8.74	99 15
97	10.53	10.94	11.12	11.02	10.30	9.34	8.36	7.74	7.58	7.98	8.76	9.87	10.66	11.77	12.66	13.06	12.94	12.40	11.47	10.59	9.62	8.94	8.54	8.74	8.74	100 16
98	9.48	10.45	11.36	11.88	11.89	11.44	10.50	9.40	8.46	7.84	7.76	8.43	9.46	10.86	12.30	13.36	13.82	13.66	12.66	11.42	10.02	8.72	7.96	8.36	8.36	101 16
99	9.47	10.86	11.90	12.70	12.87	12.44	11.06	9.52	8.12	7.40	7.47	8.26	9.54	10.86	12.30	13.36	14.06	14.56	14.22	12.80	10.96	8.88	7.46	6.84	6.84	102 16
100	7.92	9.62	11.52	13.00	13.97	14.12	13.00	11.02	9.05	7.48	6.74	6.92	7.97	9.72	11.72	13.58	14.86	15.12	14.21	12.35	9.67	7.47	5.98	5.58	5.58	102 16
101	6.14	7.76	9.84	12.16	14.02	15.18	15.06	13.40	10.95	8.28	6.66	6.40	7.88	10.06	12.53	14.55	15.72	15.49	13.80	11.08	8.22	5.93	4.52	4.32	4.32	103 17
102	5.47	7.72	10.54	13.27	15.36	16.20	15.32	13.00	9.88	7.34	5.76	5.40	6.24	8.22	10.70	13.40	15.52	16.25	15.36	12.80	9.46	6.56	4.47	3.42	3.42	104 17
103	3.91	5.74	8.31	11.40	14.40	16.28	16.72	15.47	12.68	9.44	6.81	5.47	5.38	6.52	8.91	11.80	14.40	15.97	16.08	14.35	7.80	4.97	2.93	2.46	2.46	105 18
104	3.76	6.21	9.51	12.97	15.58	17.14	17.04	14.94	11.68	8.36	6.14	5.06	5.57	7.24	10.07	13.10	15.40	16.44	15.82	13.44	9.74	6.67	4.03	2.50	2.50	106 18
105	2.77	4.44	7.50	10.96	14.33	16.70	17.72	16.91	14.37	10.87	8.10	6.15	5.71	6.50	8.36	11.33	14.12	15.97	16.50	15.10	12.22	8.67	5.24	3.17	3.17	107 18
106	2.56	3.47	5.74	8.64	12.02	15.12	17.54	16.94	16.24	13.40	10.32	7.62	6.07	7.04	9.13	12.00	14.47	15.69	15.54	13.66	10.74	7.44	4.88	3.28	3.28	108 19
107	3.04	4.36	6.67	9.40	12.47	15.00	16.74	16.94	15.60	13.03	10.01	7.87	6.76	6.80	7.71	9.70	12.14	14.15	15.02	14.50	12.53	9.92	7.24	5.36	5.36	109 19



FORMS FOR SHORT-PERIOD TIDES.  
SERIES MS.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
146	14.16	13.22	9.68	6.84	4.84	3.94	4.50	6.00	8.33	10.94	13.60	15.42	16.13	15.62	13.90	11.47	9.28	7.84	7.40	7.74	8.92	10.62	12.60	14.02	148 11	
147	14.27	13.22	10.78	8.10	5.76	4.27	4.17	5.26	7.20	9.70	12.28	14.66	16.04	14.86	12.64	10.27	8.44	7.54	7.34	8.10	9.52	11.55	13.36	14.27	150 12	
148	13.92	12.06	9.48	6.90	5.12	4.32	4.97	6.54	8.70	11.00	13.46	15.32	16.07	15.67	14.17	11.77	9.56	8.16	7.68	7.83	8.74	10.50	12.26	13.66	151 12	
149	14.02	12.96	10.86	8.34	6.24	5.04	4.82	5.84	7.60	9.46	11.87	14.10	15.30	15.60	14.66	12.78	10.74	9.03	7.96	7.73	8.44	11.07	12.62	13.44	152 13	
150	13.16	11.96	9.94	7.67	6.16	5.18	5.56	6.86	8.64	10.66	12.74	14.30	15.12	15.06	13.65	11.84	10.00	8.46	7.75	7.78	8.46	9.92	11.36	12.37	153 13	
151	12.84	12.22	10.98	9.18	7.32	6.03	5.94	6.87	8.17	9.67	11.38	13.28	14.64	14.97	14.22	12.62	11.08	9.47	8.38	8.08	8.30	9.20	10.24	11.40	154 13	
152	12.12	12.46	11.72	10.38	8.77	7.37	6.93	7.78	8.83	10.30	11.90	13.54	14.68	14.80	13.77	12.16	10.50	9.20	8.47	8.28	8.60	9.36	10.36	11.26	155 14	
153	11.83	12.05	11.56	10.60	9.20	8.14	7.72	7.83	8.62	9.82	11.10	12.64	13.94	14.46	14.16	13.26	11.74	10.42	9.26	8.54	8.34	8.46	9.23	10.10	156 14	
154	10.93	11.70	11.97	11.72	11.06	9.98	8.86	8.32	8.36	9.00	10.04	11.54	12.92	13.86	14.25	13.85	11.48	10.08	8.98	8.20	8.20	8.37	9.12	10.03	157 15	
155	11.20	12.14	12.58	12.36	11.84	11.02	10.66	9.23	8.78	9.20	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	10.03	8.74	7.92	7.54	7.76	8.67	158 15	
156	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	9.64	10.17	11.38	12.77	13.98	14.67	15.14	14.88	13.86	12.46	10.48	8.82	7.82	7.50	8.19	159 15	
157	9.46	13.22	14.76	15.82	15.76	14.97	13.34	11.70	10.67	10.27	10.56	11.52	12.90	14.12	15.30	15.65	15.48	14.17	12.02	9.86	8.00	7.09	6.85	7.72	160 16	
158	9.34	11.40	13.77	15.84	16.86	16.85	15.70	13.60	11.52	9.95	9.55	9.80	10.84	12.57	14.24	15.74	16.29	15.33	13.50	10.84	8.22	6.16	4.95	5.15	161 16	
159	6.50	8.61	11.37	14.18	16.48	17.54	17.17	15.60	13.50	10.07	8.34	8.96	10.27	12.33	14.24	15.74	16.29	15.33	12.77	9.40	6.32	4.44	3.62	4.30	162 17	
160	6.30	8.54	11.95	15.02	17.28	17.95	17.20	15.02	11.76	9.04	7.44	7.22	7.81	9.55	12.08	14.54	16.07	16.21	14.76	11.87	8.16	5.07	3.07	2.74	163 17	
161	3.80	5.94	9.24	12.80	15.92	18.07	18.53	17.65	14.65	10.90	8.00	6.22	6.55	7.50	9.65	12.45	14.89	16.40	16.14	14.28	10.90	7.10	2.62	2.37	164 18	
162	3.68	6.30	9.76	13.48	16.44	18.12	18.40	17.00	13.80	10.17	7.55	6.20	6.18	7.30	9.60	12.79	15.16	16.42	15.96	13.80	10.33	6.77	4.00	2.33	165 18	
163	2.54	4.18	7.11	10.40	13.95	16.74	17.85	17.95	16.07	12.81	9.60	7.05	5.72	5.77	7.00	9.56	12.80	15.12	16.05	15.26	12.76	9.20	6.14	3.95	166 18	
164	2.88	4.94	5.52	7.93	11.04	14.21	16.44	17.72	15.44	12.97	9.02	6.70	5.67	5.93	7.41	10.07	13.02	14.92	15.57	14.68	12.28	9.20	6.52	4.77	167 19	
165	4.20	4.94	6.52	8.80	11.67	14.34	16.42	17.20	16.60	14.54	11.30	8.66	6.74	6.05	6.16	7.65	10.05	12.50	14.32	14.85	14.05	11.96	9.47	7.26	168 19	
166	6.06	5.80	6.39	7.66	9.64	11.92	14.25	15.90	16.46	15.74	13.76	10.84	8.61	6.86	6.32	6.58	7.80	9.82	13.55	14.17	13.54	12.03	10.34	8.60	169 20	
167	7.57	7.26	7.62	8.44	9.92	12.12	14.20	15.46	15.54	14.58	12.66	10.40	8.31	7.04	6.60	6.77	7.78	9.32	11.22	12.80	13.58	13.46	12.40	10.90	170 20	
168	9.62	8.66	8.31	8.49	9.03	10.30	12.04	13.70	14.74	14.75	13.73	12.02	10.10	8.46	7.12	6.53	6.70	7.50	9.03	10.90	12.32	13.20	13.38	12.92	171 20	
169	11.94	10.67	9.60	8.04	9.24	10.33	11.90	13.24	14.06	14.10	13.34	11.84	10.05	8.26	6.94	6.44	6.67	7.49	9.06	10.86	12.50	13.66	14.10	13.63	172 21	
170	12.46	11.06	10.06	9.30	9.05	9.33	10.22	11.60	12.90	13.82	13.85	13.08	11.64	9.76	8.00	6.70	6.08	6.22	7.28	9.00	10.94	12.77	14.05	14.63	173 21	
171	14.17	12.86	11.33	10.04	9.14	8.86	9.20	10.68	11.26	12.44	13.30	13.52	12.80	11.00	7.06	5.67	5.95	5.60	7.15	9.26	11.30	13.28	14.45	14.84	174 22	
172	13.95	12.40	10.90	9.46	8.62	8.24	8.56	9.64	11.12	12.55	13.40	13.37	12.07	10.07	8.20	6.17	4.94	4.74	5.62	7.74	9.76	12.14	14.01	15.00	175 22	
173	14.86	13.77	12.06	10.27	8.84	8.10	7.94	8.57	9.68	11.18	12.64	13.37	13.05	11.52	9.17	6.76	5.11	4.16	4.64	6.10	8.00	10.50	12.90	14.56	176 23	
174	14.70	13.32	11.14	9.44	8.17	7.54	7.57	8.34	9.81	11.65	13.20	13.60	12.56	10.40	7.97	5.83	4.38	4.04	4.96	6.82	9.02	11.57	13.86	15.24	177 23	
175	15.44	14.56	12.56	10.36	8.63	7.62	7.30	7.74	8.86	10.67	12.47	13.67	13.60	12.02	9.66	6.93	4.96	3.94	4.22	5.70	7.84	10.40	12.82	14.74	178 23	
176	15.56	15.33	13.80	11.44	9.35	7.79	7.04	7.03	7.90	9.44	13.22	13.92	13.00	10.74	8.00	5.64	4.04	3.83	4.76	6.70	9.02	11.37	13.67	15.12	180 0	
177	15.46	14.48	12.44	9.96	8.16	6.86	6.42	6.94	8.42	10.44	12.57	13.67	13.68	12.22	9.64	6.86	4.96	3.98	4.36	5.65	7.72	10.07	13.26	14.31	181 0	
178	15.28	15.12	13.77	11.30	9.01	7.37	6.64	6.56	7.46	9.06	11.01	12.70	13.51	13.01	11.07	8.44	6.12	4.72	4.43	5.32	8.97	11.17	13.22	14.74	182. 1	
179	15.17	14.22	12.16	9.74	7.86	6.74	6.51	7.07	8.16	9.92	11.66	12.82	13.10	11.86	9.72	7.36	5.70	5.02	5.24	6.42	8.07	10.12	11.98	13.75	183 1	
180	14.86	14.72	13.40	11.17	9.22	7.55	6.51	6.57	7.34	8.72	10.61	12.04	12.77	12.64	11.27	9.34	7.48	6.30	5.87	6.54	7.66	9.24	10.97	12.94	184 1	





FORMS FOR SHORT-PERIOD TIDES.

SERIES MS.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
219	3.20	5.12	8.18	11.74	15.30	17.66	18.50	17.76	14.76	10.60	7.27	5.06	4.48	5.07	7.18	10.36	13.94	16.34	17.16	16.04	13.12	9.20	5.80	3.36	223 18	
220	3.60	5.73	9.03	12.78	15.94	17.78	18.04	16.74	13.32	9.36	6.05	4.18	3.80	4.90	7.56	11.10	14.46	16.66	16.88	15.39	12.15	8.23	5.44	3.52	224 18	
221	3.32	4.58	7.04	10.14	13.35	16.16	17.52	17.26	15.28	11.80	8.22	5.32	3.80	4.02	5.58	8.40	11.50	14.52	16.18	16.06	14.38	11.26	7.98	5.62	225 18	
222	4.54	4.80	6.25	8.27	11.00	13.96	16.32	17.26	16.42	14.32	10.85	7.62	5.16	4.10	4.64	6.45	8.92	12.05	14.70	15.80	15.18	13.36	10.62	7.94	6.32	226 19
223	5.74	6.44	7.77	9.72	12.07	14.12	15.66	15.72	14.46	12.06	9.36	6.96	5.40	5.07	5.84	7.33	9.54	11.87	13.60	14.46	13.96	12.48	10.40	8.65	227 19	
224	7.45	7.28	8.00	9.26	10.72	12.27	13.74	14.47	14.18	12.78	10.82	8.78	6.78	5.83	5.86	6.74	8.34	10.14	12.02	13.26	12.85	11.76	10.70	9.74	228 20	
225	9.12	8.90	9.34	10.06	10.94	12.10	12.88	13.72	13.38	11.88	10.06	8.17	7.02	6.68	7.00	7.70	8.77	10.10	11.44	12.33	12.66	12.46	12.00	11.36	229 20	
226	10.62	10.07	9.67	9.77	10.12	10.82	11.54	12.43	12.67	12.12	11.23	9.96	8.64	7.77	7.46	7.69	8.30	9.04	10.10	11.17	12.34	12.90	12.90	12.34	230 20	
227	11.72	11.15	10.62	10.30	10.00	10.14	10.50	11.34	11.96	12.26	11.97	11.38	10.53	9.44	8.35	7.66	7.57	8.12	9.06	10.48	11.57	12.72	13.42	13.56	13.18	231 21
228	12.30	11.45	10.72	10.26	9.92	9.63	10.00	10.71	11.62	12.32	12.18	11.42	10.36	9.08	8.15	7.53	7.24	7.70	8.54	9.82	11.43	12.72	13.64	13.66	13.66	232 21
229	13.26	12.36	11.22	10.18	9.34	8.97	9.08	9.88	10.76	11.64	12.26	12.35	11.85	10.40	8.78	7.36	6.28	7.14	8.37	10.20	11.94	13.38	14.40	14.54	14.54	233 22
230	13.58	12.17	10.70	9.34	8.82	8.84	9.26	10.00	11.16	12.50	13.30	13.42	12.06	10.16	8.40	6.86	6.06	6.14	7.20	8.95	10.80	12.76	13.96	14.91	14.91	234 22
231	14.84	13.64	11.84	9.97	8.77	8.36	8.48	8.96	10.06	11.36	13.12	13.97	13.64	12.06	9.70	7.27	5.96	5.56	6.35	7.80	9.76	11.70	13.66	15.10	15.10	235 22
232	15.46	14.62	12.86	10.57	8.64	7.46	7.31	7.76	8.84	10.72	12.64	14.21	14.62	13.44	11.00	8.24	6.24	5.17	5.36	6.54	8.54	10.66	13.00	15.02	15.96	236 23
233	15.50	14.08	11.60	8.97	7.34	6.70	6.84	7.80	9.62	11.70	13.76	14.95	14.67	12.76	10.00	7.37	5.56	4.97	5.74	7.38	9.36	11.94	14.36	16.04	16.04	237 23
234	16.27	15.32	13.08	10.11	7.72	6.36	6.10	6.94	8.63	10.83	13.20	15.21	14.43	11.89	8.54	6.26	4.97	5.06	6.36	8.22	10.64	13.40	15.80	16.62	16.62	239 0
235	16.16	14.21	11.38	8.34	6.35	5.46	5.74	7.13	9.22	11.84	14.36	15.71	15.48	13.64	10.66	7.60	5.70	4.96	5.70	7.24	9.54	12.02	14.56	16.24	16.24	240 0
236	16.56	15.34	12.80	9.60	7.06	5.50	5.18	5.94	7.72	10.28	13.04	15.14	15.90	14.88	12.52	9.63	7.07	5.74	5.64	6.67	8.36	10.62	13.17	15.30	16.38	241 1
237	15.97	14.06	11.04	8.16	6.11	5.05	5.41	6.72	8.83	11.26	13.77	15.36	15.38	14.00	11.50	8.72	6.86	5.97	6.34	7.52	9.30	11.47	13.80	15.46	15.46	242 1
238	15.84	14.77	12.44	9.37	7.06	5.37	4.85	5.64	7.12	9.24	11.64	13.96	15.06	14.75	13.17	10.76	8.64	7.30	6.86	7.44	8.64	10.38	12.36	14.06	14.06	243 1
239	15.24	15.10	13.64	11.26	8.61	6.50	5.32	5.38	6.34	7.85	9.86	11.96	13.64	14.58	14.07	12.68	10.68	8.97	8.02	7.81	8.36	9.26	10.60	12.24	13.73	244 2
240	14.44	13.86	12.25	10.02	8.06	6.46	5.62	5.78	6.47	7.80	9.63	11.38	12.97	13.74	13.44	12.44	11.04	9.83	8.84	8.57	8.87	9.67	10.67	11.96	245 2	
241	13.06	13.46	13.08	11.68	9.86	8.26	6.87	6.17	6.26	7.02	8.17	9.66	11.26	12.55	13.37	13.57	12.94	11.92	10.73	9.67	9.16	9.18	9.63	10.54	11.48	246 3
242	12.46	12.92	12.66	11.74	10.42	8.87	7.44	6.44	6.21	6.66	7.76	9.20	10.76	12.36	13.54	14.05	13.67	12.68	11.26	10.02	9.22	8.90	9.14	9.86	247 3	
243	10.86	12.02	12.34	12.98	12.36	11.16	9.37	7.60	6.24	5.63	5.97	7.17	8.80	10.66	12.80	14.28	14.96	14.74	13.66	11.85	10.04	8.66	8.02	8.14	248 3	
244	9.04	10.38	12.00	13.14	13.74	13.40	12.04	10.04	7.64	5.76	4.78	5.02	6.24	8.16	10.78	13.20	15.04	15.98	15.74	14.33	11.96	9.30	7.37	6.55	6.70	249 4
245	8.06	9.98	12.06	13.93	14.86	14.44	12.80	10.18	7.37	5.17	3.90	4.03	5.50	7.96	10.88	13.80	16.04	17.04	16.46	14.44	11.04	8.24	6.27	5.15	250 4	
246	5.63	7.24	9.64	12.52	14.74	15.98	15.46	13.29	9.94	6.63	4.34	3.17	2.53	5.38	8.20	11.40	14.56	16.82	17.44	16.36	13.83	9.98	6.70	4.46	3.84	251 5
247	4.58	6.80	10.06	13.28	15.76	16.64	15.73	12.94	9.26	6.06	3.66	2.67	3.72	5.66	8.70	12.20	15.53	17.33	17.53	15.87	12.42	8.56	5.32	3.44	252 5	
248	3.17	4.55	7.26	10.87	14.22	16.50	17.05	15.47	12.37	8.44	5.52	3.48	3.10	4.46	6.74	9.94	13.47	16.22	17.47	17.02	14.77	10.84	7.23	4.52	3.00	253 6
249	3.30	5.07	8.06	11.72	14.94	16.86	16.90	14.94	11.54	8.00	5.38	3.90	4.20	5.52	7.95	11.06	14.30	16.51	17.04	15.88	12.99	9.17	5.97	3.70	254 6	
250	2.94	3.94	6.16	9.14	12.45	15.42	16.68	16.10	13.81	10.56	7.46	5.47	4.87	5.60	7.04	9.54	12.25	14.81	16.16	16.06	14.44	11.07	7.87	5.34	255 6	
251	3.84	3.92	5.16	7.43	10.36	13.44	15.47	16.04	14.92	12.66	9.98	7.74	6.47	6.36	7.02	8.54	10.58	12.80	14.58	15.36	14.73	12.52	9.86	7.17	5.31	256 7
252	4.44	5.02	6.44	8.50	11.04	13.56	14.79	14.77	13.46	11.46	9.44	8.00	7.36	7.56	8.36	9.51	11.10	12.60	13.73	13.94	12.90	11.02	8.73	6.90	257 7	
253	5.70	5.63	6.34	7.60	9.36	11.36	13.14	13.88	13.60	12.43	10.94	9.64	8.76	8.44	8.70	9.18	9.95	10.88	12.06	12.76	12.71	11.64	9.87	8.26	7.04	258 8

TIDAL OBSERVATIONS.

[CONT. VII.]

254	6.44	6.67	7.34	8.36	9.74	11.16	12.23	12.70	12.20	11.38	10.60	9.88	9.34	9.16	9.13	9.34	9.87	10.66	11.30	11.64	11.37	10.56	9.48	8.44	289 8
255	7.52	7.14	7.33	7.86	8.66	9.84	10.90	11.62	11.97	11.87	11.54	11.08	9.54	9.92	9.60	9.42	9.54	9.86	10.24	10.70	10.91	10.80	10.34	9.74	260 8
256	9.06	8.35	7.72	7.46	7.67	8.44	10.73	11.52	11.88	12.06	11.88	11.53	10.97	10.23	9.48	9.04	9.01	9.38	10.01	10.64	11.05	11.18	10.94	10.46	261 9
257	9.52	8.56	7.74	7.42	7.64	8.34	9.42	10.67	11.65	12.46	12.82	12.62	12.04	10.96	9.85	8.96	8.54	8.42	8.86	9.64	10.44	11.23	11.67	11.60	262 9
258	10.92	9.74	8.36	7.26	6.68	6.86	7.74	9.24	10.86	12.34	13.24	13.55	13.17	12.08	10.64	9.21	7.54	7.74	8.74	9.92	11.30	12.38	12.82	12.42	263 10
259	11.17	9.62	7.86	6.55	6.10	6.54	7.88	9.68	11.56	13.16	14.03	14.06	13.18	11.60	9.86	8.07	6.97	6.64	7.14	8.38	10.20	11.92	13.16	13.44	264 10
260	12.50	10.70	8.70	6.90	5.75	5.90	6.36	8.04	10.20	12.32	13.87	14.64	14.36	12.87	10.73	8.45	6.71	5.90	6.17	7.29	9.02	11.07	13.02	14.14	265 10
261	14.04	12.68	10.30	6.07	5.14	5.48	6.87	9.06	11.46	13.68	15.18	15.37	14.28	12.24	9.67	7.34	5.74	5.30	6.12	7.84	9.97	12.54	14.50	15.33	266 11
262	14.46	12.23	9.34	6.94	5.36	4.94	5.94	8.06	10.08	12.62	14.76	15.76	15.26	13.46	10.67	7.88	5.74	4.48	4.66	6.00	8.44	11.24	13.97	15.67	267 11
263	15.66	14.20	11.46	8.47	6.20	4.97	5.22	6.65	8.86	11.54	14.06	15.76	16.97	12.14	9.06	6.37	4.56	3.93	4.93	6.93	9.67	12.77	15.34	16.35	268 12
264	15.80	13.61	10.52	7.73	5.58	4.88	5.77	7.56	10.04	12.74	14.90	15.94	15.62	13.71	10.64	7.47	5.10	3.54	3.83	5.50	7.97	11.14	14.16	16.01	269 12
265	16.37	15.04	12.33	9.34	6.97	5.54	5.42	6.51	8.50	11.14	13.77	15.60	15.98	14.86	12.14	8.87	6.16	4.30	3.67	4.60	6.44	9.03	12.27	16.21	270 13
266	15.96	14.09	11.42	8.56	6.75	5.80	6.17	7.42	9.65	12.22	14.26	15.46	15.24	13.48	10.57	7.65	5.42	3.96	4.06	5.34	7.30	9.97	12.69	14.83	271 13
267	15.87	15.16	13.24	10.76	8.47	7.04	6.68	7.20	8.44	10.38	12.56	14.16	14.83	14.05	12.07	9.24	7.02	5.32	4.44	4.61	5.87	7.97	10.37	13.07	272 13
268	14.81	15.06	14.13	12.37	10.44	8.86	7.87	7.56	7.92	10.67	12.44	13.74	13.97	12.81	10.83	8.83	7.10	5.78	5.25	5.76	6.66	8.34	10.76	12.86	273 14
269	14.16	14.44	13.68	12.40	10.86	9.52	8.53	8.21	8.56	9.40	10.68	12.08	13.04	13.08	11.93	10.54	9.05	7.64	6.61	6.06	6.30	7.07	8.81	10.63	274 14
270	12.30	13.68	14.16	13.66	12.66	11.46	10.12	9.18	8.77	8.56	9.10	10.17	11.30	12.30	12.61	12.14	11.16	9.92	8.44	6.37	6.38	7.34	8.76	10.57	275 15
271	12.10	13.44	13.92	13.88	13.56	12.37	11.18	9.72	8.32	7.60	7.94	9.26	10.84	12.04	12.52	12.48	11.98	11.16	9.77	7.94	6.58	6.06	6.50	7.97	276 15
272	9.84	11.56	13.26	14.17	14.66	14.52	13.27	11.34	9.06	7.37	6.82	7.46	8.74	10.60	12.11	13.20	14.04	13.84	12.76	10.92	8.58	6.74	5.94	6.30	277 15
273	7.68	9.72	11.97	13.90	15.26	15.54	13.97	11.26	8.63	6.70	5.98	6.37	7.97	10.25	12.66	14.44	15.38	15.04	13.48	11.07	8.36	6.38	5.47	5.87	278 16
274	7.36	9.62	12.14	14.54	16.28	16.98	16.37	13.80	10.49	7.50	5.61	5.14	5.74	7.77	10.54	13.45	15.71	16.85	16.30	14.16	10.84	7.77	5.85	5.07	279 16
275	5.66	7.50	9.87	12.74	15.25	16.92	17.15	15.62	12.54	8.66	5.94	4.14	3.96	5.28	7.85	14.38	16.70	17.32	16.33	13.48	9.84	7.20	5.47	4.98	280 17
276	5.96	7.74	10.58	13.66	16.26	17.40	16.86	14.56	10.89	7.40	4.72	3.37	3.98	5.86	8.86	12.43	15.47	17.34	17.64	16.26	9.26	6.56	5.24	281 17	
277	5.38	6.54	8.77	11.76	14.62	16.82	17.12	15.72	12.71	9.14	6.06	3.77	3.17	4.42	6.67	9.72	13.44	16.35	17.55	17.22	15.06	11.70	8.40	6.26	282 17
278	5.44	7.47	10.01	12.74	15.12	16.37	16.06	14.21	11.94	7.42	4.80	3.12	3.62	5.50	8.04	11.13	14.40	16.50	17.22	16.16	13.58	10.36	6.24	283 18	
279	6.04	6.91	8.53	10.52	13.06	15.02	15.64	14.36	11.93	8.64	6.01	4.31	3.47	4.52	6.20	8.94	11.94	14.56	16.24	16.32	14.74	12.13	9.47	7.47	284 18
280	6.58	6.90	7.84	9.30	11.26	13.26	14.41	14.26	13.74	10.35	7.88	4.44	4.38	5.92	7.85	10.30	12.70	14.67	15.54	15.01	13.36	11.14	7.80	285 19	
281	7.42	7.74	8.64	10.04	11.80	13.04	13.64	13.06	11.30	9.07	7.14	5.84	5.47	6.20	7.44	9.04	10.97	13.06	14.36	14.30	13.40	11.82	9.16	286 19	
282	8.44	8.24	8.54	9.26	10.30	11.46	12.12	12.22	11.46	10.00	8.37	7.08	6.36	6.44	7.32	8.34	9.60	11.24	12.72	13.46	13.28	11.06	10.10	9.27	287 20
283	8.97	8.94	9.08	9.61	10.14	11.01	11.52	11.46	10.73	9.52	8.47	7.66	7.41	7.56	8.04	8.76	9.91	11.17	12.30	12.88	12.66	11.92	11.04	10.37	288 20
284	9.76	9.36	9.12	9.08	9.27	9.86	10.44	10.68	10.66	10.30	9.78	9.22	8.56	8.06	7.74	8.02	8.86	10.06	11.16	12.02	12.40	12.34	12.06	11.48	289 20
285	10.82	9.97	9.24	8.77	8.68	8.96	9.55	10.70	10.88	10.82	10.57	10.03	9.26	8.44	7.90	8.07	8.80	9.84	10.90	11.78	12.36	12.58	12.54	12.97	290 21
286	11.12	9.97	8.90	8.23	8.12	8.56	9.27	10.10	10.90	11.50	11.78	11.53	10.67	9.30	8.14	7.56	7.77	8.55	9.74	11.07	12.15	12.94	13.28	13.04	291 21
287	12.24	10.77	9.14	7.88	7.18	7.36	8.12	9.26	10.62	11.94	12.78	12.88	12.06	10.48	8.86	7.70	7.28	8.65	10.02	11.54	12.81	13.77	14.04	13.50	292 22
288	12.16	10.00	8.34	6.96	6.50	6.88	7.96	9.76	11.52	13.07	13.96	13.77	12.48	10.52	8.76	7.36	6.77	7.36	8.52	10.36	12.17	13.66	14.56	14.48	293 22
289	13.40	11.12	8.84	6.87	5.64	5.46	6.30	8.06	10.30	12.80	14.34	15.00	14.16	12.26	9.96	7.92	6.50	6.22	7.10	8.82	10.86	13.12	14.54	15.07	294 22
290	14.56	12.60	9.98	5.46	4.56	4.96	6.60	9.03	11.80	14.15	15.84	15.96	14.52	12.00	9.24	7.24	6.16	6.40	7.67	9.66	11.93	14.14	15.62	15.76	295 28
291	14.36	11.76	8.61	6.02	4.24	3.86	5.14	7.32	10.15	13.10	15.67	16.78	16.26	14.16	11.00	8.32	6.36	5.84	6.47	8.16	10.16	12.84	15.02	16.10	296 28
Sum	759.72	757.68	747.32	738.03	754.23	781.97	793.89	796.22	787.52	782.28	749.60	748.59	735.87	713.44	705.92	705.90	736.03	763.99	790.44	825.82	806.03	794.53	793.70	781.00	No. of Days.
No.	74	74	75	74	74	74	74	74	74	74	74	74	74	74	74	74	75	74	74	74	74	74	74	75	18349.83

FORMS FOR SHORT-PERIOD TIDES.

SERIES MS.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
202	15.46	13.28	9.87	6.84	4.45	3.04	3.57	5.44	8.15	11.37	14.60	16.81	17.35	13.64	10.44	7.71	6.97	5.84	6.88	8.87	11.47	14.12	15.94	16.22	298 0	
203	14.81	11.87	8.35	5.46	3.46	2.87	4.17	6.35	9.32	13.00	15.95	17.47	17.44	15.72	12.68	9.66	7.28	5.94	6.04	7.36	9.64	12.45	14.84	16.04	299 0	
204	15.60	13.70	10.52	7.15	4.66	2.92	3.10	4.72	7.47	10.55	13.92	16.35	17.36	16.74	14.57	11.67	8.85	6.76	5.94	6.28	7.70	9.92	12.68	15.38	300 1	
205	14.78	13.36	9.16	6.36	4.20	3.97	3.72	5.55	8.04	11.05	14.10	16.17	16.96	16.12	14.06	11.35	8.82	7.14	6.57	7.02	8.46	10.56	13.14	14.64	301 1	
206	15.04	13.76	11.47	8.74	6.43	4.70	4.22	5.00	6.80	9.02	11.88	14.60	16.14	15.22	15.16	13.26	10.86	8.86	7.58	7.14	7.44	8.84	10.92	12.84	302 1	
207	13.84	13.86	12.57	10.08	8.54	6.84	5.56	5.27	5.98	7.33	11.72	14.00	15.22	15.38	14.58	12.88	11.01	9.42	8.12	7.64	7.92	8.94	10.40	11.85	303 2	
208	13.91	13.12	12.26	10.75	9.22	7.66	6.68	6.30	6.72	7.86	9.44	11.50	13.34	14.46	14.66	13.96	12.74	11.30	9.76	8.54	7.93	7.84	8.40	9.60	304 2	
209	10.88	12.06	12.64	12.40	11.47	10.10	8.76	7.68	7.01	7.06	7.90	9.22	10.97	12.56	13.72	14.38	14.04	13.04	11.45	9.76	7.22	7.02	7.48	8.84	305 3	
200	10.32	11.48	12.55	13.87	12.46	11.36	9.70	8.28	7.14	6.80	7.40	8.84	10.74	12.56	13.87	14.54	14.38	13.40	11.67	9.60	7.53	6.30	5.88	6.50	306 3	
301	8.20	10.07	11.93	13.36	14.04	13.66	12.30	10.26	8.61	7.37	6.86	7.24	8.35	10.36	12.50	14.13	15.08	14.96	13.80	11.64	9.03	6.96	5.44	5.04	307 3	
302	5.86	7.79	10.12	12.66	14.54	15.37	13.04	10.66	8.56	7.12	6.44	6.77	8.02	10.14	12.62	14.56	15.55	15.25	13.56	10.92	8.12	5.82	4.22	4.10	308 4	
303	5.32	7.70	10.85	13.69	15.51	16.05	13.06	12.86	10.40	8.16	6.53	5.96	6.51	8.24	10.85	13.27	15.16	15.84	15.03	12.98	9.78	7.04	4.71	3.46	309 4	
304	3.86	5.60	8.44	11.74	14.64	16.50	16.73	15.38	12.86	9.98	7.70	6.25	5.93	6.71	8.67	11.25	15.32	15.84	14.55	11.68	8.46	5.64	3.63	3.01	310 5	
305	4.08	6.50	9.62	13.08	15.81	17.12	16.72	14.87	12.03	9.20	7.26	6.32	6.37	7.46	9.60	12.20	14.35	15.67	15.28	13.15	10.15	7.00	4.47	3.03	311 5	
306	3.22	5.93	7.60	10.76	14.05	16.38	17.05	16.14	13.92	11.10	8.66	6.87	6.16	6.46	8.00	10.44	13.10	14.76	15.16	13.92	11.40	8.36	5.66	3.69	312 5	
307	2.94	3.94	9.01	12.24	14.92	16.53	16.56	15.16	12.66	10.06	7.96	6.74	6.60	7.35	9.00	11.24	13.43	14.50	14.36	12.66	9.94	7.20	4.97	3.56	313 6	
308	3.77	5.34	7.72	10.56	13.46	15.64	16.34	15.71	13.92	11.46	9.28	7.66	6.86	6.98	7.98	9.96	12.00	13.52	14.02	13.37	11.18	8.81	6.52	4.86	314 6	
300	4.33	5.20	6.90	9.14	11.80	14.20	15.72	15.81	14.66	12.72	10.71	8.96	7.56	7.92	9.16	10.68	12.24	13.26	13.26	12.06	10.17	8.00	6.25	5.31	315 7	
310	5.50	6.66	8.34	10.52	12.80	14.44	15.18	14.68	13.32	11.56	10.02	8.76	8.10	8.00	8.60	9.65	10.96	12.18	12.58	12.23	11.04	9.16	7.62	6.54	316 7	
311	6.20	6.84	7.96	9.38	11.14	12.91	14.18	14.40	13.64	12.37	10.90	9.58	8.78	8.46	8.68	9.30	10.00	10.94	11.57	11.80	11.36	8.94	7.84	7.18	317 8	
312	7.20	7.86	8.80	9.98	11.46	12.86	13.86	13.83	12.96	11.72	10.53	9.66	9.14	8.92	8.96	9.17	9.66	10.40	11.10	11.37	11.01	10.20	9.26	8.46	318 8	
313	8.10	8.14	8.66	9.44	10.56	11.74	12.76	13.34	13.26	12.61	11.72	10.86	9.76	9.04	8.80	8.85	9.16	9.64	10.14	10.74	11.18	11.32	11.06	10.38	319 8	
314	9.38	8.94	8.71	8.90	9.50	10.42	11.46	13.10	13.15	12.64	11.84	10.76	9.71	8.88	8.35	8.19	8.42	9.04	9.96	10.86	11.50	11.80	11.55	10.90	320 9	
315	9.98	9.08	8.64	8.75	9.38	10.38	11.46	12.41	13.07	13.16	12.84	11.84	10.56	9.24	8.13	7.50	7.43	7.86	8.83	10.03	11.16	12.23	12.80	12.64	321 9	
316	11.66	10.25	9.04	8.36	8.34	8.96	10.02	11.20	12.46	13.23	13.47	13.00	11.72	10.14	8.38	7.03	6.27	7.08	8.52	10.23	11.92	13.17	13.63	13.10	322 10	
317	11.86	10.18	8.76	7.98	7.96	8.75	10.13	11.64	13.14	13.94	13.94	13.04	11.34	9.30	7.45	5.86	5.13	5.46	6.76	8.80	11.15	13.20	14.66	14.98	323 10	
318	13.97	11.76	9.58	8.10	7.27	7.36	8.22	9.82	11.76	13.33	14.28	14.14	12.87	10.56	7.98	5.77	4.14	3.74	4.67	6.71	9.27	12.02	14.40	15.66	324 10	
319	15.44	13.71	11.16	7.02	6.40	6.78	8.22	10.37	12.25	13.88	14.74	14.20	12.26	9.36	6.51	4.12	2.75	2.94	4.56	7.03	10.05	13.27	15.65	16.62	325 11	
320	15.90	13.76	10.86	8.17	6.45	5.84	6.36	8.12	10.44	12.84	14.46	15.08	13.97	11.41	8.07	4.96	2.87	1.63	2.58	4.74	7.64	11.12	14.22	16.47	326 11	
321	17.97	15.75	12.96	9.86	7.26	5.65	5.46	6.44	8.40	11.20	13.57	15.11	15.17	13.27	6.40	3.62	1.76	1.54	3.26	6.02	9.25	12.97	15.66	17.40	327 12	
322	17.25	15.37	12.23	9.00	6.75	5.63	5.63	6.88	9.32	12.22	14.44	15.50	14.80	12.31	8.84	5.46	3.00	1.66	2.20	4.15	6.95	10.46	13.81	16.44	328 12	
323	17.54	16.82	13.51	11.38	8.50	6.32	5.44	5.74	7.26	10.06	12.76	14.67	15.26	14.06	11.32	8.05	5.16	2.94	2.16	3.11	5.16	7.96	11.23	14.30	329 13	
324	17.22	16.23	13.81	10.68	8.07	6.16	5.50	5.88	7.64	10.25	12.77	14.29	14.72	13.35	10.74	7.81	5.32	3.66	3.26	4.42	6.34	8.66	11.67	14.58	330 13	
325	16.33	16.37	15.28	12.84	9.93	7.47	6.23	5.72	6.26	7.94	10.30	12.38	13.76	13.96	12.68	10.56	8.18	6.28	4.97	4.83	5.73	7.34	9.38	12.05	331 13	
326	14.37	15.76	15.80	14.56	12.28	9.94	8.13	6.64	6.14	8.54	10.04	11.78	12.86	13.16	12.24	10.73	8.96	7.30	6.44	5.96	6.50	7.80	9.84	12.15	332 14	



FORMS FOR SHORT-PERIOD TIDES.

BOMBAY—Commencing 0 hours, Astronomical Time, 1st January, 1885.

Motion per mean Solar hour = 15°-50'79"479.

SERIES 2SM.

Argument ( $\gamma - 2\eta + \sigma$ ).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
1	15.52	12.96	9.13	5.76	3.03	1.68	2.28	4.80	7.90	11.70	15.50	18.00	18.85	18.08	15.14	11.54	8.50	6.21	5.53	6.08	8.20	11.31	14.16	1 22	
2	16.06	16.66	15.40	12.16	8.40	4.86	2.56	1.71	2.90	5.56	8.82	12.94	16.44	18.58	18.97	17.67	14.24	10.56	7.53	5.57	5.16	6.10	8.63	2 21	
3	11.84	14.68	16.63	16.96	15.24	11.92	8.00	4.87	2.80	2.57	4.24	6.84	10.20	14.07	17.36	18.86	18.84	17.06	13.20	9.77	6.90	5.23	4.96	8 21	
4	8.86	12.14	14.87	16.40	16.40	16.40	14.28	11.00	7.63	4.88	3.55	3.86	5.55	8.01	11.36	14.83	17.16	18.38	17.93	15.80	12.16	8.68	6.10	4 20	
5	5.25	6.68	9.24	12.28	14.51	15.96	15.58	13.48	10.47	7.54	5.76	8.07	7.04	5.67	7.22	9.17	12.11	15.02	17.02	17.55	16.63	14.11	10.96	5 19	
6	6.22	5.47	5.84	7.18	9.67	12.12	14.04	15.00	14.45	12.62	10.24	8.07	7.04	6.84	7.54	8.67	10.60	12.84	15.06	16.36	16.35	15.24	12.76	6 18	
7	10.11	8.00	6.64	6.17	6.55	7.86	9.76	11.80	13.27	14.00	13.64	12.22	10.47	9.05	8.44	8.46	9.03	9.97	11.20	13.05	14.64	15.46	15.18	7 18	
8	11.68	9.76	8.10	7.16	7.03	7.40	8.29	9.82	11.16	11.88	12.55	13.24	13.07	12.20	11.16	10.27	9.64	9.60	9.90	10.60	11.70	12.96	14.02	14.44	8 17
9	13.75	12.27	10.82	9.20	7.93	7.24	7.06	7.34	8.07	9.14	9.14	10.55	11.74	12.48	12.66	12.27	11.60	10.93	10.34	9.98	9.86	10.17	11.07	12.14	9 16
10	13.06	13.36	12.72	11.71	10.43	9.14	7.97	7.14	6.75	6.94	7.74	8.96	10.26	11.64	12.67	13.14	13.14	12.97	12.20	11.24	10.48	10.12	10.05	10.23	10 15
11	10.84	11.64	12.27	12.68	12.37	11.53	10.42	8.97	7.80	6.96	6.38	6.44	7.28	8.73	10.47	12.14	13.23	13.84	13.63	12.58	11.38	10.27	9.77	11 14	
12	9.62	9.89	10.44	11.24	11.97	12.52	12.50	11.87	10.54	8.76	7.34	6.16	5.74	6.34	7.62	9.54	11.40	13.22	14.24	14.58	13.94	12.72	11.24	12 14	
13	9.32	9.14	9.46	10.37	11.48	12.46	13.04	13.04	12.84	11.88	10.23	8.20	6.52	5.62	5.56	6.50	8.14	10.17	12.34	14.10	15.20	15.17	13.97	10.27	13 13
14	10.58	9.35	8.75	8.76	9.26	10.34	11.68	12.96	13.64	13.64	13.36	11.80	9.66	7.32	5.82	5.14	5.44	6.74	8.86	11.26	13.66	15.38	15.87	15.24	14 12
15	13.66	11.54	9.82	8.71	8.16	8.36	9.30	10.74	12.46	13.64	13.98	13.00	10.84	8.24	6.20	4.76	4.16	4.46	5.40	7.36	9.78	12.57	14.82	16.13	15 11
16	15.97	14.56	13.25	10.05	8.46	7.82	7.74	8.41	9.71	11.76	13.30	14.26	14.06	14.68	13.84	11.50	8.60	5.94	4.37	4.02	5.06	7.26	9.66	12.72	17 10
17	15.74	16.36	15.71	13.82	11.22	8.94	7.54	6.94	7.15	8.40	10.27	12.44	14.06	13.55	14.80	14.78	13.22	10.43	7.48	5.34	4.30	4.66	6.25	8.54	18 9
18	15.20	16.55	16.53	16.88	16.08	14.77	9.97	7.86	6.84	6.68	7.56	9.32	11.40	13.55	14.14	14.06	14.84	14.14	12.06	9.06	6.46	4.67	4.24	5.16	19 8
19	11.38	14.15	16.15	16.88	16.08	14.04	11.02	8.54	6.76	6.12	6.34	5.43	7.60	9.84	12.14	14.06	14.84	14.14	12.06	9.06	6.46	4.67	4.24	5.16	19 8
20	7.15	9.68	12.56	14.87	16.44	16.45	15.00	12.42	9.50	7.22	5.80	5.43	6.26	8.16	10.65	12.88	14.28	14.56	13.33	13.33	10.92	8.30	6.04	4.87	20 7
21	5.06	6.54	8.66	11.04	13.64	15.62	16.36	15.74	15.96	14.86	12.76	10.13	7.78	6.17	5.70	6.11	7.62	9.70	11.76	13.36	14.14	13.72	12.06	9.94	21 7
22	8.32	7.22	7.01	7.74	8.97	10.80	12.97	14.62	15.50	15.50	15.17	13.80	11.46	9.14	7.34	6.17	6.00	6.68	8.02	9.76	11.65	13.04	13.76	13.34	22 6
23	12.14	10.65	9.07	8.15	8.14	8.68	9.86	11.56	13.36	14.56	15.02	14.37	12.76	10.76	8.71	6.96	6.23	6.09	6.08	6.08	7.86	9.46	11.24	12.66	23 5
24	13.36	13.34	13.38	11.08	9.94	9.11	8.88	9.28	10.22	11.70	13.06	14.14	14.41	13.60	12.06	10.26	8.40	7.10	6.23	6.08	6.56	7.64	9.14	25 3	
25	10.84	12.34	13.44	13.81	13.33	12.18	10.75	9.76	9.24	9.34	10.07	11.16	12.40	13.38	13.66	13.03	11.87	10.24	8.47	7.00	5.83	5.38	5.68	6.78	26 3
26	8.55	10.33	12.22	13.56	14.30	14.16	13.05	11.56	10.06	9.11	8.87	9.40	10.46	11.87	12.94	13.44	13.33	12.40	10.74	8.86	6.83	5.22	4.41	27 2	
27	4.77	6.10	8.10	10.50	12.63	14.53	15.56	15.33	13.76	11.64	9.52	8.28	7.92	8.25	9.53	11.24	12.70	13.80	14.14	13.30	11.34	8.72	6.20	28 1	
28	4.24	3.38	3.76	5.30	7.76	10.55	13.50	15.72	16.74	16.12	14.36	11.40	8.83	7.24	6.86	7.33	9.20	11.11	12.97	14.55	15.08	14.17	11.84	29 0	
29	8.82	5.70	3.60	2.56	3.06	5.04	7.88	11.48	14.56	17.04	17.86	17.00	14.36	10.96	8.97	6.27	5.77	6.57	8.62	11.25	13.92	15.74	16.28	29 23	
30	14.96	12.18	8.44	5.42	3.22	2.16	3.07	5.52	8.75	12.46	16.01	18.10	18.47	17.26	13.80	10.14	7.99	5.27	5.02	6.02	8.40	11.85	14.65	16.52	30 23
31	16.84	15.28	11.68	7.88	4.80	2.74	2.38	4.00	6.66	10.10	13.98	17.01	17.01	18.64	18.38	16.30	12.42	8.97	6.01	4.46	4.57	6.12	9.14	12.56	31 22
32	15.46	17.00	16.86	14.76	11.06	7.36	4.34	2.72	2.99	4.86	7.74	6.36	9.36	12.84	15.86	17.74	17.94	16.48	13.27	9.84	4.32	4.36	6.55	32 21	
33	9.62	13.04	15.80	16.84	16.08	13.73	10.16	6.82	4.54	3.58	4.44	6.36	9.36	12.84	15.86	17.74	17.94	16.48	13.27	9.84	4.32	4.36	6.55	32 21	
34	5.26	7.44	10.66	13.70	15.74	16.43	15.42	12.82	9.66	6.90	5.44	5.14	6.20	8.06	10.66	13.66	16.02	17.12	16.74	14.88	11.68	8.76	6.34	4.92	34 20
35	4.74	5.86	8.26	11.07	13.60	15.16	15.34	14.06	11.97	13.60	9.04	7.34	6.56	6.94	8.04	9.56	11.76	14.24	15.64	16.04	15.34	13.02	10.16	7.86	36 19
36	6.21	5.54	5.86	7.18	9.07	11.36	13.26	14.34	14.26	12.88	11.00	9.39	8.26	7.92	8.30	9.05	10.36	12.08	13.76	14.66	14.44	13.11	11.12	8.61	38 16

38	9.39	7.54	6.36	6.13	6.68	7.86	9.28	10.86	12.27	13.10	13.94	11.03	10.66	9.73	9.12	9.06	9.36	10.60	11.82	13.80	13.32	12.83	57.17	
39	11.45	10.03	8.74	7.48	6.86	6.78	7.17	7.94	9.05	10.30	11.34	11.07	11.03	11.42	10.84	10.34	10.07	9.77	9.94	10.44	11.32	12.06	12.06	39.16
40	12.26	11.78	10.88	9.87	8.84	7.86	7.24	6.94	7.18	8.03	9.07	10.14	11.00	11.56	11.85	11.77	11.46	11.12	10.97	10.70	10.13	10.80	39.16	
41	11.27	11.45	11.25	10.76	9.97	9.00	8.08	7.11	6.58	6.74	7.44	7.44	8.31	9.84	10.90	11.76	12.34	12.55	12.30	11.60	9.34	9.17	40.15	
42	9.51	10.24	10.94	11.36	11.44	10.97	10.10	9.07	7.87	6.85	6.30	6.30	6.58	7.26	8.50	10.16	11.44	12.05	13.26	13.32	12.56	11.36	41.14	
43	8.61	8.64	9.01	9.76	10.58	11.25	11.66	11.34	10.36	8.82	7.36	6.12	5.54	5.82	6.94	8.54	10.36	12.06	13.46	13.97	13.64	12.30	42.13	
44	9.26	8.14	7.84	8.12	8.96	10.24	11.52	12.40	12.66	12.07	10.47	8.56	6.64	5.46	5.20	5.93	7.55	9.16	11.72	13.53	14.67	14.84	43.12	
45	12.14	10.00	8.54	7.66	7.53	8.16	9.56	11.03	12.66	13.62	13.60	12.30	10.24	7.77	5.88	4.84	4.96	6.33	8.27	10.66	13.07	15.23	44.12	
46	13.64	11.13	9.02	7.54	7.00	6.79	7.00	8.13	9.87	11.85	13.60	14.38	13.88	11.93	9.10	6.54	4.66	4.00	4.90	6.86	9.20	11.97	45.11	
47	15.96	14.78	12.26	9.64	7.46	6.24	5.96	6.74	8.48	10.85	7.84	13.97	14.56	14.85	13.63	10.90	7.86	5.57	4.07	4.04	5.46	7.84	46.10	
48	15.83	16.64	16.01	13.87	10.90	8.00	6.17	5.46	5.74	7.26	4.46	12.35	14.42	15.50	15.15	13.68	12.44	11.76	10.53	10.53	7.47	5.38	47.9	
49	12.60	15.08	16.60	16.64	15.00	11.93	8.96	6.76	5.63	5.65	4.23	4.54	4.14	5.07	7.06	9.74	12.44	14.55	15.46	14.76	12.57	9.68	50.7	
50	7.84	10.68	13.68	15.84	16.68	15.80	13.15	10.22	7.36	6.28	6.28	4.54	4.14	5.07	7.06	9.74	12.44	14.55	15.46	14.76	12.57	9.68	50.7	
51	6.70	9.14	12.18	14.74	16.26	16.26	14.64	11.74	8.68	7.54	5.61	9.24	6.90	4.54	4.69	5.84	7.87	10.40	12.80	14.50	15.06	14.03	51.6	
52	5.60	6.54	8.40	10.77	13.32	15.42	16.26	15.47	13.18	11.86	9.24	7.84	10.54	13.30	15.12	15.66	14.46	11.76	10.53	10.53	7.47	5.38	47.9	
53	7.58	6.64	6.76	7.86	9.60	11.66	13.73	15.08	13.32	14.12	11.86	9.24	10.83	8.73	6.87	5.45	4.92	5.44	6.63	8.23	10.14	11.77	53.5	
54	11.46	9.33	8.05	7.40	7.66	8.58	9.92	11.68	13.36	14.16	14.12	13.18	13.06	11.88	10.25	8.37	6.98	5.77	5.38	5.64	6.37	7.82	54.4	
55	12.76	11.56	10.24	9.04	8.45	8.28	8.67	9.76	11.20	12.50	12.50	10.44	11.57	12.34	12.34	11.70	10.50	8.90	7.32	5.96	5.24	5.12	55.3	
56	12.38	13.02	12.96	12.16	11.07	10.02	8.94	8.44	8.48	9.27	10.44	10.44	11.57	12.34	12.34	11.70	10.50	8.90	7.32	5.96	5.24	5.12	55.3	
57	8.90	10.63	12.10	13.16	13.56	13.13	11.86	10.27	8.88	8.08	7.87	8.42	9.56	10.87	11.93	12.44	12.26	11.27	9.76	7.96	6.27	5.06	56.2	
58	5.02	6.47	8.52	10.67	12.72	14.14	14.86	14.44	12.70	10.66	8.80	7.60	7.95	6.54	6.18	7.03	8.83	11.00	12.40	13.36	13.52	12.60	57.1	
59	4.63	4.06	4.70	6.46	8.84	11.30	13.80	15.56	16.25	15.33	12.96	10.26	12.87	9.66	7.00	5.18	5.12	6.26	8.52	11.16	13.67	15.38	58.1	
60	6.08	4.05	3.42	4.14	4.14	6.18	8.86	12.06	14.93	16.76	17.15	15.84	12.87	9.66	7.00	5.18	5.12	6.26	8.52	11.16	13.67	15.38	59.0	
61	11.93	8.26	5.48	3.42	2.92	4.14	6.52	9.58	13.16	16.04	17.62	17.62	17.34	15.27	11.66	8.27	5.56	4.16	4.32	5.84	8.66	11.92	59.23	
62	16.54	14.66	11.26	7.66	4.94	3.20	3.27	4.70	7.53	10.86	14.63	17.06	17.98	16.96	13.90	10.20	6.96	4.47	3.56	4.02	6.04	9.40	60.22	
63	15.55	16.86	16.36	13.80	10.44	6.92	4.54	3.37	3.90	5.80	8.56	12.33	15.44	17.27	17.40	15.46	12.03	8.50	5.70	3.74	3.27	4.33	61.21	
64	10.34	13.76	15.97	16.76	15.76	12.96	9.44	6.74	4.67	4.23	5.26	7.43	10.37	13.82	16.13	17.08	16.40	13.86	10.50	7.26	4.84	3.56	62.21	
65	8.27	11.55	14.34	16.02	16.28	14.66	11.66	8.60	6.46	5.26	6.76	5.46	6.56	8.86	11.44	14.36	15.97	16.18	14.88	12.00	8.86	6.28	63.20	
66	4.86	6.67	9.40	12.24	14.39	15.64	15.33	13.25	10.46	8.22	6.76	6.34	7.00	8.36	10.22	12.44	14.42	15.27	14.71	12.72	10.14	7.72	64.19	
67	4.86	5.00	6.10	8.03	10.30	12.47	13.97	14.58	13.92	12.03	10.14	8.54	7.56	7.56	8.42	9.82	11.34	12.96	14.04	14.24	13.22	11.36	65.18	
68	7.56	6.27	5.84	6.34	7.46	9.00	10.76	12.44	13.56	13.74	12.74	11.40	10.07	9.16	8.96	9.27	9.77	10.46	11.36	12.44	13.07	13.03	66.18	
69	8.86	7.68	7.02	7.02	7.02	7.66	8.54	9.66	10.96	12.24	12.88	12.88	12.24	11.43	10.66	10.24	10.16	10.24	10.47	10.86	11.44	12.02	67.17	
70	11.36	10.18	8.87	7.97	7.67	7.94	8.50	9.00	9.78	9.78	10.74	11.76	12.46	12.67	12.27	11.74	11.26	10.87	10.56	10.36	10.22	10.36	68.16	
71	11.56	11.38	10.86	9.96	9.14	8.40	7.98	7.80	7.86	8.34	9.30	10.40	11.44	12.08	12.27	12.36	12.27	12.03	11.50	10.78	10.20	9.73	69.15	
72	10.35	10.89	11.10	11.10	10.78	10.32	9.72	8.86	7.97	7.28	7.26	7.97	8.97	10.32	11.56	12.46	13.04	13.10	12.54	11.68	10.36	9.64	70.14	
73	8.82	9.16	9.88	10.74	11.40	11.75	11.70	11.14	10.97	8.84	7.56	6.74	6.70	7.63	8.94	10.62	12.06	13.26	13.78	13.68	12.86	11.34	71.14	
74	8.16	8.03	8.46	9.64	10.80	12.06	12.78	12.56	11.57	9.92	8.17	6.67	6.67	5.98	6.16	7.20	8.87	10.76	12.70	14.08	14.61	14.06	72.13	
75	8.96	7.55	6.88	7.95	8.07	9.84	11.76	12.97	13.54	13.03	11.46	8.17	9.42	7.27	5.74	5.30	5.90	7.44	9.66	11.92	14.02	15.17	73.12	
76	11.66	9.44	7.56	6.34	6.07	6.86	8.68	10.80	12.96	14.26	14.55	13.37	11.16	8.45	6.26	5.16	5.12	6.24	8.10	10.63	13.22	15.15	74.11	
Sum	755.17	779.71	736.02	778.71	720.68	780.55	717.69	776.94	735.19	762.29	734.14	754.02	764.70	748.80	774.19	745.98	794.17	734.89	707.60	751.32	775.74	736.02	763.71	No. of Days, 73 <sup>rd</sup> 12 <sup>th</sup> , 1873.51
No.	73	75	72	76	70	76	71	70	72	75	73	73	74	73	75	71	76	70	76	72	75	72	74	74

FORMS FOR SHORT-PERIOD TIDES.

SERIES 2SM.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
77	15.17	13.32	10.40	7.86	6.06	5.25	5.54	6.90	9.24	11.72	13.95	15.20	15.12	13.39	10.64	7.57	5.44	4.44	4.96	6.46	8.94	11.85	14.34	13.50	75 10	
78	16.00	16.06	14.53	11.64	8.54	5.76	4.22	3.97	5.24	7.30	10.10	13.02	15.04	16.00	15.20	12.86	9.54	6.07	4.92	4.38	5.52	7.55	10.33	13.50	76 10	
79	15.75	16.73	16.07	13.66	10.42	7.32	—	4.92	3.64	4.00	5.66	8.33	11.52	14.30	16.06	16.52	15.06	12.13	8.73	6.13	4.66	4.99	6.52	8.92	77 9	
80	11.86	14.66	16.40	16.56	15.07	11.90	8.47	5.63	3.74	3.22	4.26	6.60	—	9.60	12.85	15.23	16.56	16.25	14.26	10.83	8.00	5.75	5.11	5.88	78 8	
81	7.84	10.46	13.38	15.68	16.60	15.80	13.36	10.12	7.00	4.83	3.54	3.76	5.34	7.86	11.00	13.93	15.92	16.74	15.74	—	13.36	10.24	7.64	6.12	79 7	
82	6.08	7.14	9.00	11.56	13.90	15.66	15.98	14.76	12.06	8.90	6.13	4.34	3.62	4.36	6.06	8.47	11.31	13.87	15.62	16.12	14.97	12.74	10.02	8.03	80 7	
83	6.96	—	7.06	7.93	9.67	12.07	14.08	15.23	15.08	13.57	11.16	8.26	6.08	4.76	4.47	5.46	7.26	9.48	11.88	13.90	15.36	15.50	14.66	12.67	81 6	
84	10.54	8.74	7.94	8.14	9.06	10.62	12.40	13.77	—	14.53	14.20	12.80	10.64	8.47	6.76	5.86	5.82	6.49	7.75	9.52	11.71	13.54	14.73	14.90	82 5	
85	14.06	13.63	11.05	9.70	8.86	8.72	9.12	10.24	11.76	13.06	13.60	13.34	12.06	10.56	—	8.92	7.40	6.43	6.30	6.68	7.68	9.46	11.24	13.02	83 4	
86	14.08	14.52	14.22	13.04	11.70	10.34	9.24	8.84	9.04	9.84	10.96	12.05	12.86	12.96	12.44	11.22	9.67	8.30	7.06	6.48	6.64	—	7.48	8.86	84 3	
87	10.64	12.34	13.74	14.48	14.44	13.62	12.12	10.36	8.96	8.11	7.96	8.44	9.76	11.26	12.36	12.92	12.78	11.94	10.50	8.78	7.20	6.06	5.92	6.72	85 3	
88	8.34	10.26	12.20	—	13.86	15.00	15.14	14.16	12.20	9.88	8.00	6.90	6.56	7.46	9.22	11.16	12.56	13.57	14.06	13.37	11.72	9.38	7.17	5.72	80 2	
89	5.38	6.17	7.82	10.00	12.50	14.54	15.84	15.94	14.64	12.14	—	9.36	6.97	5.74	5.63	6.67	8.88	11.24	13.46	14.86	15.36	14.34	12.05	9.44	87 1	
90	6.93	5.38	5.00	5.82	7.83	10.50	13.30	15.60	16.72	16.38	14.37	11.37	8.36	6.00	4.67	4.80	—	6.40	9.20	12.06	14.62	16.12	16.16	14.90	88 0	
91	12.22	9.12	6.60	5.05	4.86	5.87	8.10	11.14	14.15	16.35	17.15	16.24	13.58	10.14	7.06	4.83	3.96	4.70	6.72	9.92	13.20	15.64	17.04	—	88 23	
92	16.75	14.92	11.81	8.56	6.27	5.14	5.64	6.94	9.43	12.61	15.44	17.03	17.08	15.36	11.92	8.64	6.18	4.48	4.25	5.24	7.57	11.00	14.10	16.43	89 23	
93	17.34	16.56	14.28	10.82	7.84	—	5.95	5.42	6.12	7.87	10.62	13.66	16.10	17.14	16.46	13.96	10.44	7.12	4.80	3.83	4.41	6.43	8.78	12.04	90 22	
94	14.74	16.66	17.13	15.64	12.86	9.53	7.16	5.81	5.93	7.22	9.26	12.02	—	14.66	16.44	16.67	15.06	12.02	8.56	5.84	4.04	3.84	4.93	7.24	91 21	
95	10.99	13.22	15.56	16.90	16.56	14.74	11.68	8.84	7.02	6.48	7.04	8.26	10.50	13.00	14.94	15.83	15.12	12.94	9.87	—	7.14	5.16	4.22	4.76	92 20	
96	6.40	8.73	11.37	14.00	15.82	16.34	15.34	13.10	10.40	8.36	7.32	7.28	8.03	9.50	11.53	13.48	14.74	14.92	13.67	11.34	8.76	6.67	5.40	5.22	93 20	
97	6.16	—	7.85	9.97	12.30	14.30	15.48	15.46	14.27	12.24	10.20	8.78	8.16	8.47	9.24	10.52	12.04	13.48	14.16	13.84	12.27	10.16	8.14	6.47	94 19	
98	5.74	6.22	7.44	9.20	10.85	12.64	14.05	14.67	—	14.27	12.97	11.44	10.04	9.16	8.84	9.16	9.84	10.95	11.96	12.80	12.96	12.28	10.94	9.24	95 18	
99	7.80	6.78	6.70	7.30	8.37	9.54	10.90	12.34	13.52	13.80	13.26	12.98	12.60	11.86	11.07	10.34	9.94	9.77	9.87	10.56	11.44	11.92	12.05	11.54	96 17	
100	10.36	9.16	8.12	7.47	7.44	7.87	8.52	9.46	10.73	11.93	12.74	12.98	12.50	12.66	12.42	11.96	11.34	10.55	9.91	9.47	9.34	9.52	9.94	8.74	98 16	
101	11.27	10.92	10.30	9.34	8.36	7.74	7.58	7.98	8.76	9.87	11.04	11.96	12.50	12.77	12.66	13.06	12.94	12.40	11.47	10.50	9.62	8.94	8.54	8.74	99 15	
102	10.94	11.12	11.02	—	10.62	10.00	9.22	8.40	8.01	8.13	8.63	9.70	10.66	11.77	12.66	13.06	12.94	13.82	13.66	12.66	11.42	10.02	8.72	7.96	100 14	
103	9.48	10.45	11.36	11.88	11.89	11.44	10.50	9.40	8.46	7.84	—	7.76	8.43	9.46	10.86	12.30	13.36	13.70	13.66	12.66	11.42	10.02	8.72	7.96	100 14	
104	7.82	8.36	9.47	10.86	11.90	12.70	12.87	12.44	11.06	9.52	8.12	7.40	7.47	8.26	9.34	11.08	—	12.70	14.06	14.56	14.22	12.80	10.96	8.88	101 13	
105	7.46	6.81	6.84	7.92	9.62	11.52	13.00	13.97	14.12	13.00	11.02	9.05	7.48	6.74	6.92	7.97	9.72	11.72	13.58	14.86	15.12	14.21	12.35	—	102 12	
106	9.67	7.47	5.98	5.58	6.14	7.16	9.84	12.16	14.02	15.18	15.06	13.40	10.95	8.28	6.66	6.02	6.46	7.88	10.06	12.53	14.55	15.72	15.49	13.80	103 12	
107	11.08	8.22	5.93	4.52	4.32	—	5.47	7.72	10.34	13.27	15.36	16.20	15.32	13.00	9.88	7.34	5.76	5.40	6.24	8.22	10.70	13.40	15.32	16.25	104 11	
108	15.36	12.80	9.46	6.56	4.47	3.42	3.91	5.74	8.31	11.40	14.40	16.28	—	16.72	15.47	12.68	9.44	6.81	5.47	5.38	6.52	8.91	11.80	14.40	105 10	
109	15.97	16.08	14.35	11.30	7.80	4.97	2.93	2.46	3.76	6.21	9.51	12.97	15.58	17.14	17.04	14.94	11.68	8.36	—	6.14	5.06	5.57	7.24	10.07	106 9	
110	13.10	15.40	16.44	15.82	13.44	9.74	6.67	4.03	2.50	2.77	4.44	7.50	10.96	14.33	16.70	17.72	16.91	14.37	10.87	8.10	6.15	5.71	6.50	8.36	107 9	
111	11.33	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	108 8
112	7.04	9.13	12.00	14.47	15.69	15.54	13.66	—	10.74	7.44	4.88	3.28	3.04	4.36	6.67	9.40	12.47	15.00	16.74	16.94	15.60	13.03	10.07	7.87	109 7	
113	6.76	6.80	7.71	9.70	12.14	14.15	15.04	14.50	13.53	9.92	7.24	5.36	4.17	4.16	—	5.20	7.26	9.89	12.40	14.57	15.77	15.74	14.47	12.12	110 6	



CHAP. VII.]

114	9.90	8.07	7.14	7.11	7.83	9.54	11.38	13.16	13.74	13.28	11.76	9.56	7.60	5.96	4.93	5.02	5.86	7.52	9.74	12.00	13.87	14.87	14.77	111.8		
115	13.76	12.06	10.26	8.74	7.82	7.54	8.00	9.34	11.00	12.36	12.96	12.72	11.38	10.14	8.48	6.94	5.06	5.96	7.97	10.20	11.87	13.34	14.34	112.5		
116	14.44	13.66	12.26		10.62	9.10	8.03	7.66	7.76	8.68	10.20	11.03	12.43	12.66	12.10	10.96	9.47	8.14	7.03	6.54	6.88	7.94	11.42	113.4		
117	13.00	14.07	14.44	13.93	12.76	11.00	9.18	7.74	6.96	6.96		7.85	9.40	10.96	12.36	13.66	13.12	12.22	10.65	8.87	7.52	6.74	7.66	114.3		
118	9.26	11.04	12.88	14.12	14.66	14.30	12.64	10.64	8.66	6.78	5.94	5.93	7.08	9.00	11.04	12.64		13.72	13.87	12.97	11.36	9.32	7.66	115.2		
119	6.47	7.28	8.88	10.96	12.96	14.54	15.17	14.54	12.77	10.22	7.74	5.76	4.88	5.14	6.58	8.88	11.33	13.36	14.66	14.94	13.86	11.70	9.34	116.1		
120	7.26	6.22	6.20	7.24	9.00	11.22	13.36	14.86	15.37	14.44	12.10	9.16	6.48	4.70	4.20	4.74	6.70	9.17	11.77	14.02	15.57	15.54	117.1			
121	8.80	6.96	6.07	6.34	7.48		9.44	11.96	14.10	15.48	15.44	13.84	10.92	7.66	5.31	3.77	3.70	5.12	7.30	10.10	12.94	15.14	16.26	118.0		
122	13.86	11.00	8.24	6.47	5.97	6.54	7.98	10.16	12.70	14.64	15.66	14.96		12.70	9.46	6.57	4.32	3.42	4.04	5.86	8.48	11.42	14.32	118.23		
123	16.57	15.46	16.28	14.70	11.93	9.06	7.20	6.40	6.70	7.74	9.37	11.47	13.86	15.04	15.06	12.96	9.73	7.17	4.24	3.42	4.04	5.68	8.27	10.68	120.22	
124	14.92	16.36	16.28	14.70	11.93	9.06	7.20	6.40	6.70	7.74	9.37	11.47	13.86	15.04	15.06	12.96	9.73	7.17	4.24	3.42	4.04	5.68	8.27	10.68	120.22	
125	13.46				15.48	16.25	15.62	13.50	10.52	8.22	6.72	6.40	7.02	8.34	10.44	12.60	14.08	14.45	13.26	10.82	7.87	5.57	3.94	8.88	121.21	
126	9.18	11.76	14.24	15.36	15.54	14.30	11.86		9.46	7.76	6.94	7.06	7.86	9.36	11.24	13.06	13.96	13.66	11.90	9.20	6.72	5.07	4.36	4.90	122.20	
127	6.32	8.22	10.36	12.80	14.56	15.43	14.76	13.04	10.84	8.96	7.76	7.44	7.76	8.80		10.26	11.94	13.06	13.30	12.28	10.40	8.28	6.46	5.35	123.19	
128	5.20	6.00	7.54	9.26	11.42	13.34	14.60	14.86	13.86	12.06	10.14	8.84	8.15	8.06	8.46	8.56	9.00	9.74	10.53	11.36	11.86	11.68	7.94	124.18		
129	6.74	6.04	6.20	7.12	8.46	10.24	12.10	13.38	14.58	13.92	12.90	11.41	10.00	8.90	8.46	8.56	9.00	9.74	10.53	11.36	11.86	11.68	7.94	124.18		
130	7.86	6.96	6.92		7.44	8.22	9.26	10.47	12.10	13.34	13.78	13.40	12.16	10.87	9.94	9.24	8.96	8.94	9.17	9.58	10.34	10.96	11.44	11.34	125.17	
131	10.58	9.56	8.46	7.16	7.66	7.97	8.66	9.74	10.97		12.22	13.24	13.54	13.24	12.12	10.96	9.98	9.27	8.94	8.74	8.80	9.24	10.03	10.86	127.16	
132	11.26	11.29	10.79	10.06	9.26	8.46	8.06	8.06	8.06	8.10	8.66	9.60	9.60	10.93	12.94	12.14		11.17	9.96	8.96	8.28	7.92	8.00	8.61	128.15	
133	9.56	10.46	11.34	11.77	11.44	10.76	9.74	8.78	8.17	8.10	8.06	7.83	8.24	9.37	10.96	12.50	13.57	14.02	13.54	12.37	10.74	8.97	7.34	6.90	129.14	
134	7.45	8.52	10.00	11.40	12.36	12.92	12.66	11.62	10.20	8.85	8.06	8.55	7.53	7.27	7.93	9.36	11.30	13.16	13.16	12.36	11.16	9.68	8.30	7.26	6.90	130.14
135	5.98	6.71	8.26	10.20	12.12		13.30	14.22	13.67	12.20	10.16	8.55	7.53	7.27	7.93	9.36	11.30	13.16	13.16	12.36	11.16	9.68	8.30	7.26	6.90	130.14
136	5.85	4.92	5.06	6.42	8.60	10.95	13.28	14.84	15.34	14.46	12.38		10.01	8.14	6.95	6.90	8.01	9.74	11.84	13.66	14.84	15.16	14.10	11.76	132.12	
137	8.83	6.14	4.18	3.66	4.53	6.46	9.08	11.92	14.30	15.96	16.28	14.95	12.41	9.36	7.14	6.17	6.50	7.92		10.02	12.41	14.46	15.64	15.47	133.11	
138	13.76	10.66	7.20	4.46	2.86	2.74	4.17	6.63	9.77	13.00	15.72	17.16	16.96	15.18	11.90	8.78	6.57	5.95	6.52	7.94	10.30	12.84	15.02	15.97	134.11	
139	15.24		12.56	8.86	5.70	3.17	1.97	2.43	4.23	7.22	10.62	13.96	16.50	17.69	17.06	14.58	10.90	8.02	5.94	5.46	6.30	8.25	10.90	13.74	136.10	
140	15.64	16.06	14.62	11.54	7.86	4.52	2.14		1.42	2.56	5.03	8.20	11.45	14.68	16.97	17.83	16.77	14.06	10.36	7.66	5.84	5.52	6.20	8.20	136.9	
141	11.20	14.02	15.72	15.74	13.76	10.48	6.92	4.07	2.74	1.86	3.24	5.60	8.58	12.24		15.14	17.16	17.74	16.33	13.21	10.00	7.30	5.76	5.60	137.8	
142	6.58	8.80	11.97	14.34	15.47	15.07	12.82	9.66	6.56	4.08	2.67	2.88	4.46	6.78	9.71	12.92	15.50	17.10	17.16	15.40		12.67	9.57	7.36	138.7	
143	6.16	6.11	7.20	9.40	12.06	14.14	14.98	14.36	12.18	9.28	6.58	4.76	3.86	4.30	5.66	7.78	10.44	13.15	15.36	16.54	16.23	14.86	11.94	9.36	139.7	
144	7.54	6.48	6.38		7.36	9.30	11.76	13.38	13.98	13.42	11.66	9.36	7.30	5.74	4.98	5.46	6.33	8.08	10.42	12.87	14.66	15.72	15.46	14.00	140.6	
145	11.78	9.46	7.72	6.96	6.82	7.44	8.91	10.74	12.30		13.13	12.92	11.76	10.08	8.18	6.84	6.28	6.46	7.26	8.54	10.38	12.48	14.22	14.94	141.5	
146	14.74	13.52	11.62	9.40	7.84	6.86	6.52	6.83	8.02	9.54	11.12	12.28	12.53	12.07	10.86	9.35		7.86	6.87	6.74	7.36	8.54	10.16	11.86	142.4	
147	13.27	14.14	13.98	12.92	11.14	9.14	7.48	6.36	5.86	5.93	7.12	8.94	10.74	12.22	12.86	12.65	11.60	10.66	8.56	7.47	7.24	7.70		8.44	143.3	
148	10.00	11.62	13.06	13.93	13.82	12.68	10.82	9.01	7.20	5.72	5.17	5.56	6.97	8.92	10.90	12.46	13.44	13.42	12.46	10.73	9.12	8.02	7.47	7.63	144.3	
149	8.26	9.76	11.56	13.14	14.05		13.96	12.62	10.76	8.52	6.66	5.12	4.84	5.46	7.38	9.67	11.66	13.40	14.34	14.36	13.24	11.36	9.64	8.16	145.2	
150	7.52	7.50	8.44	10.16	11.93	13.46	14.20	13.97	12.62	10.50	7.84		5.72	4.46	4.54	5.90	7.82	10.17	12.67	14.36	15.22	14.76	13.34	11.12	146.1	
151	9.16	7.84	7.36	7.72	8.72	10.32	12.06	13.66	14.36	13.76	11.92	9.27	6.82	4.82	3.97	4.57	6.16	8.40		11.03	13.46	15.10	15.52	14.67	147.0	
152	12.94	10.67	8.77	7.60	7.38	7.93	9.10	10.86	12.73	14.28	14.53	13.00	10.66	7.86	5.58	4.22	4.13	5.24	7.24	9.70	12.30	14.40	15.74	15.70	148.0	
153			14.12	12.14	9.74	8.36	7.64	7.54	8.20	9.70	11.80	13.62	14.16	12.22	9.68	6.84	4.84	3.94	4.50	6.00	8.33	10.94	13.60	15.42	148.23	
Sum	794.81	753.76	805.37	752.80	707.38	743.69	776.69	756.27	749.30	730.90	730.64	762.48	728.56	781.55	735.85	783.90	734.45	788.40	759.96	766.66	757.82	784.66	788.37	754.70	No. of Days, 7 <sup>h</sup> 12 <sup>m</sup>	
No.	76	72	77	72	77	72	76	74	75	75	74	75	73	77	72	77	72	77	73	75	74	75	75	73	73	1837.84

FORMS FOR SHORT-PERIOD TIDES.  
SERIES 2 SM.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	
154	16.11	15.63	13.90	11.47	9.28	7.84	7.40		7.74	8.92	10.62	12.60	14.02	14.27	13.22	10.78	8.10	5.76	4.27	4.17	5.26	7.20	9.70	12.28	149 22	
155	14.66	15.94	16.04	14.86	12.64	10.27	8.44	7.54	7.34	8.10	9.52	11.55	13.36	14.27	13.92	12.06	9.48	6.90	5.12	4.32	4.97	6.54	8.70	150 21		
156	11.00	13.46	15.33	16.07	15.67	14.17	11.77	9.56	8.16	7.68	7.83	8.74	10.50	12.26	13.66	14.02	12.96	10.86	8.34	6.24		5.04	4.82	5.84	151 20	
157	7.60	9.46	11.87	14.10	15.30	15.60	14.66	12.78	10.74	9.03	7.96	7.73	8.24	9.44	11.07	12.62	13.44	13.16	11.96	9.94	7.67	6.16	5.18	5.56	152 20	
158	6.86	8.64	10.66		12.74	14.30	15.12	15.06	13.65	11.84	10.00	8.46	7.75	7.78	8.46	9.92	11.36	12.37	12.84	12.22	10.98	9.18	7.32	6.03	153 19	
159	5.94	6.87	8.17	9.67	11.58	13.28	14.64	14.97	14.22		12.62	11.08	9.47	8.38	8.08	8.30	9.20	10.24	11.40	12.12	12.46	11.72	10.38	8.77	154 18	
160	7.37	6.70	6.93	7.78	8.83	10.30	11.90	13.54	14.68	14.80	13.77	12.16	10.50	9.20	8.47	8.28		8.60	9.36	10.36	11.26	11.83	12.05	11.56	155 17	
161	10.60	9.20	8.14	7.72	7.83	8.62	9.82	11.10	12.64	13.94	14.46	14.16	13.26	11.74	10.42	9.26	8.54	8.34	8.40	9.23	10.10	10.93		11.70	156 16	
162	11.97	11.72	11.06	9.98	8.86	8.32	8.36	9.00	10.04	11.54	12.92	13.86	14.25	13.85	12.88	11.48	10.08	8.98	8.20	8.20	8.37	9.12	10.03	11.29	157 16	
163	12.14	12.58	12.36	11.84	11.02		10.06	9.23	8.78	9.20	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	10.93	8.74	7.92	7.54	7.76	8.67	158 15	
164	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	9.64	10.17	11.38	12.77	13.98	14.97	15.14	14.88	13.86	12.46	10.48	8.82	7.82	7.50	8.72	159 14	
165	8.10	9.46	11.28	13.22	14.76	15.82	15.76	14.97	13.34	11.70	10.67	10.27	10.56	11.52	12.90	14.12	15.30	15.65		15.48	14.17	12.02	9.86	8.00	160 13	
166	7.09	6.85	7.72	9.34	11.40	13.77	15.84	16.86	16.85	15.70	13.60	11.52	9.95	9.55	9.80	10.84	12.57	14.21	15.47	16.06	15.22	13.50	10.84	8.22	161 13	
167		6.16	4.95	5.15	6.50	8.61	11.37	14.18	16.48	17.54	17.17	15.60	12.50	10.07	8.34	8.17	8.96	10.27	12.23	14.24	15.74	16.29	15.33	12.77	162 12	
168	9.46	6.32	4.44	3.62	4.30	6.30	8.54		11.95	15.02	17.28	17.95	17.20	15.02	11.76	9.04	7.44	7.22	7.81	9.55	12.08	14.54	16.07	16.21	163 11	
169	14.76	11.87	8.16	5.97	3.07	2.74	3.80	5.94	9.24	12.80	15.92	18.07	18.53	18.40	17.65	14.65	10.90	8.00	6.62	6.55	7.50	9.95	12.45	14.89	164 10	
170	16.40	16.14	14.28	10.90	7.10	4.31	2.62	2.37	3.68	6.30	9.76	13.48	16.44	18.12	18.40	17.00	13.80	10.17	7.55	6.20		6.18	7.30	9.60	165 9	
171	13.79	15.16	16.42	15.96	13.80	10.33	6.77	4.00	2.33	2.54	4.18	7.11	10.40	13.95	16.74	17.85	17.95	16.07	12.81	9.60	7.05	5.72	5.77	7.00	166 9	
172	9.56	12.80			15.12	16.03	15.26	12.76	9.20	6.14	3.95	2.88	3.47	5.52	7.93	11.04	14.21	16.44	17.72	17.40	15.44	12.07	6.70	5.67	167 8	
173	5.93	7.41	10.07	13.02	14.92	15.57	14.68	12.28	9.20		6.52	4.77	4.20	4.94	6.52	8.80	11.67	14.34	16.43	17.20	16.60	14.54	11.30	8.66	168 7	
174	6.74	6.03	6.16	7.65	10.05	12.50	14.32	14.85	14.05	11.96	9.47	7.26	6.06	5.80	6.39		7.66	9.64	11.92	14.25	15.90	16.46	15.74	13.76	169 6	
175	10.84	8.61	6.86	6.32	6.58	7.80	9.82	12.04	13.55	14.17	13.54	12.03	10.34	8.60	7.57	7.26	7.62	8.44	9.92	12.12	14.20	15.46		15.54	170 5	
176	14.58	13.66	10.40	8.31	7.04	6.60	6.77	7.78	9.32	11.22	12.80	13.58	13.46	12.40	10.90	9.62	8.66	8.31	8.49	9.03	10.30	12.04	13.70	14.74	171 5	
177	14.75	13.73	12.02	10.10		8.46	7.12	6.53	6.70	7.50	9.03	10.90	12.32	13.20	13.38	12.92	11.94	10.67	9.60	8.94	8.82	9.24	10.33	11.90	172 4	
178	13.34	14.06	14.10	13.34	11.84	10.05	8.26	6.94	6.44	6.67	7.49		9.06	10.86	12.50	13.66	14.10	13.63	12.46	11.06	10.06	9.30	9.05	9.33	173 3	
179	10.22	11.60	12.90	13.82	13.85	13.08	11.64	9.76	8.00	6.70	6.08	6.22	7.28	9.00	10.94	12.77	14.05	14.63		14.17	12.86	11.33	10.04	9.14	174 2	
180	8.86	9.20	10.08	11.26	12.44	13.30	13.52	12.80	11.00	8.85	7.06	5.67	5.05	5.60	7.15	9.26	11.30	13.28	14.45	14.84	13.95	12.40	10.90	9.46	175 2	
181		8.62	8.24	8.56	9.64	11.12	12.55	13.40	13.37	12.07	10.07	8.20	6.17	4.94	4.74	5.62	7.74	9.76	12.14	14.01	15.00	14.86	13.77	12.06	176 1	
182	10.27	8.84	8.10	7.94	8.52	9.68	11.18		12.64	13.37	13.05	11.52	9.17	6.76	5.11	4.16	4.64	6.10	8.00	10.50	12.90	14.56	15.33	14.70	177 0	
183	13.32	11.14	9.44	8.17	7.54	7.57	8.34	9.81	11.65	13.20	13.60	12.56	10.40		7.97	5.83	4.38	4.04	4.96	6.82	9.02	11.57	13.86	15.24	177 23	
184	15.44	14.56	12.56	10.36	8.63	7.62	7.30	7.74	8.86	10.67	12.47	13.67	13.60	12.02	9.66	6.93	4.96	3.94	4.22	5.70		7.84	10.40	12.82	178 22	
185	14.74	15.56	15.33	13.80	11.44	9.35	7.79	7.04	7.03	7.90	9.44	11.66	13.22	13.92	13.00	10.74	8.00	5.64	4.04	3.83	4.76	6.70	9.02	11.37	179 22	
186	13.61	15.12			15.46	14.48	12.44	9.96	6.86	6.42	6.94	8.42	10.44	12.57	13.67	13.68	12.22	9.64	6.86	4.96	3.98	4.36	5.65	7.72	180 21	
187	10.02	12.26	14.31	13.28	15.12	13.77	11.30	9.01	7.37		6.64	6.56	7.46	9.06	11.01	12.70	13.51	13.01	11.07	8.44	6.12	4.72	4.42	5.32	181 20	
188	6.94	8.97	11.17	13.22	14.74	15.17	14.22	12.16	9.74	7.86	6.74	6.51	7.07	8.16	9.92		11.66	12.82	13.10	11.86	9.72	7.36	5.70	5.01	182 19	
189	5.24	6.42	8.07	10.12	11.98	13.73	14.86	14.72	13.40	11.17	9.22	7.55	6.51	6.57	7.34	8.72	10.61	12.04	12.77	12.64	11.27	9.34	7.48	6.82	183 18	
190	6.30	5.81	6.54	7.66	9.24	10.97	13.94	14.38	14.88	14.20	12.50	10.34	8.44	7.22	6.77	6.97	7.87	9.34	10.94	12.19	13.66	12.22	10.84	9.25	184 18	

191	7.99	6.96	6.94	7.56	8.50	10.00	11.48	13.24	14.34	13.34	11.44	9.00	8.01	6.94	6.51	6.91	7.47	6.91	6.48	6.84	7.86	9.16	10.51	11.71	136.10		
192	11.12	9.70	8.48	7.63	7.56	8.14	9.04	10.41	11.98	13.30	13.08	12.51	10.84	8.96	8.96	7.47	6.70	6.51	6.48	6.84	7.86	9.16	10.51	11.71	186.10		
193	12.36	12.28	11.46	10.38	9.16	8.34	8.14	8.38	9.04	10.37	11.82	13.66	13.27	11.87	10.24	8.57	7.05	6.14	5.87	6.14	5.87	6.26	7.22	8.72	187.15		
194	10.36	11.70	12.36	12.86	12.14	11.14	9.86	8.86	8.32	8.34	9.02	10.46	11.88	13.12	13.48	12.96	11.86	10.30	8.58	7.00	5.74	5.32	5.74	6.86	188.15		
195		8.67	10.62	12.30	13.47	13.96	13.31	12.10	10.48	9.04	8.28	8.37	8.98	10.28	11.72	13.02	13.62	13.24	12.02	10.14	8.20	6.16	4.76	4.31	189.14		
196	4.90	6.40	8.62	10.94	13.04	14.57	15.22	14.64	12.87	10.58	8.66	7.68	7.68	7.62	8.40	10.00	11.70	13.12	13.97	13.69	12.32	10.27	7.76	5.44	190.13		
197	3.88	3.19	3.88	5.80	8.60	11.46	13.00	15.54	16.06	15.08	12.92	10.40	8.23		7.07	6.90	7.82	9.54	11.60	13.35	14.34	12.76	10.16	191.12			
198	7.15	4.46	2.56	2.27	3.49	5.92	8.80	12.36	15.04	16.76	17.06	15.00	13.27	10.08	7.42	6.33	6.04	7.17	9.30	11.84		13.92	15.05	14.90	192.11		
199	13.08	9.91	6.43	3.53	1.84	1.84	3.38	6.20	9.54	13.00	15.92	17.60	17.55	15.88	12.54	9.04	6.46	5.24	5.54	6.76	9.24	12.48	14.76	16.12	193.11		
200	15.46	13.17		9.32	5.65	2.96	1.56	1.90	3.97	6.70	10.13	13.94	16.86	18.22	17.87	15.72	12.00	8.47	5.86	4.66	4.98	6.66	9.72	13.12	194.10		
201	15.46	16.44	15.54	12.76	8.60	5.17	2.76	1.62	2.37		4.50	7.60	11.14	14.80	17.30	18.38	17.46	14.77	11.14	7.30	5.12	4.24	4.66	6.66	195.9		
202	9.96	13.24	15.56	16.37	15.10	12.10	8.47	5.36	3.22	2.47	3.46	5.71	8.66	12.13	15.36		17.38	17.97	16.76	13.80	10.38	7.04	4.79	4.26	196.8		
203	5.04	7.14	10.42	13.83	15.77	16.14	14.53	11.60	8.45	5.84	4.20	3.82	5.12	6.97	9.80	13.00	15.56	17.04	17.17	15.44	12.60	9.26		6.86	197.7		
204	5.22	4.84	5.76	8.06	10.85	13.97	15.36	15.40	13.86	11.04	8.20	6.43	5.40	5.54	6.64	7.95	10.24	12.80	15.30	16.34	15.86	14.11		8.50	198.7		
205	6.30	5.34	5.40	6.24		8.00	10.50	12.97	14.30	14.44	12.94	10.91	9.08	7.74	7.24	7.56	8.14	9.16	11.11	13.10	14.71	15.40		12.96	199.6		
206	10.60	8.38	6.86	5.92	6.05	6.82	8.26	10.28	12.30	13.38	13.40	12.62	11.34	10.16	8.58	8.59	8.86	8.59	8.86	9.62	10.96	12.55	13.78	14.97	200.5		
207	13.40	11.92	10.10	8.37	6.87	6.38	6.51	7.24	8.41	9.82	11.28	12.52	12.90	12.68	11.87	10.93	10.01		9.34	9.14	9.27	9.97	10.90	12.12	201.4		
208	13.14	13.41	12.71	11.34	9.77	8.47	7.34	6.76	6.86	7.36	8.56	10.06	11.46	12.50	13.02	12.96	12.57	11.86	10.96	10.04	9.53	9.52	9.76	10.73	202.4		
209		11.74	12.78	13.04	12.50	11.42	10.20	8.76	7.52	6.90	6.76	7.25	8.50	10.20	11.86	13.24	13.87	13.87	13.28	12.22	11.04	10.07	9.54	9.50	203.8		
210	9.87	10.64	11.70	12.60	12.94	12.66		11.70	10.10	8.56	7.16	6.24	6.28	7.14	8.62	10.44	12.07	13.40	14.20	14.14	13.28	12.08	10.74	9.52	204.2		
211	8.94	8.91	9.48	10.50	11.72	12.63	13.06	12.60	11.28	9.36	7.66	6.38	5.86		6.06	7.07	8.94	10.96	13.07	14.58	15.07	14.54	13.34	11.84	205.1		
212	10.26	9.14	8.46	8.46	9.16	10.36	11.74	13.14	13.52	12.81	11.24	9.13	7.31	5.74	5.33	6.10	7.65	9.76	12.02		14.00	15.20	15.33	14.58	206.0		
213	12.97	11.01	9.35	8.37	8.18	8.73	9.62	10.95	12.64	13.76	13.92	12.56	10.36	8.02	6.14	5.26	5.24	6.52	8.36	10.60	12.96	14.83	16.05	15.98	207.0		
214	14.35	12.14		9.94	8.56	8.04	8.20	8.78	9.90	11.82	13.73	14.66	14.04	11.84	8.90	6.50	5.04	4.74	5.78	7.22	9.33	11.77	14.22	15.86	207.23		
215	16.07	15.15	13.18	10.77	8.67	7.57	7.18	7.78		8.96	10.77	12.83	14.27	14.50	13.28	10.70	7.76	5.53	4.56	4.86	6.26	8.20	10.44	13.14	208.22		
216	15.37	16.51	16.11	14.47	11.94	9.36	7.58	6.88	7.16	8.00	9.72	11.80	13.84	14.90	14.32		12.37	9.57	6.78	5.10	4.56	5.42	7.13	9.26	209.21		
217	11.96	14.36	15.96	16.14	15.17	12.96	10.25	8.01	6.67	6.34	6.89	8.16	10.14	12.46	14.24	14.84	13.50	10.90	8.02	5.86	4.76		5.04	6.52	210.20		
218	8.34	10.66	13.15	15.27	16.14	15.82	14.14	11.47	8.96	7.02	6.16	6.33	7.34	9.23	11.44	13.54	14.58	14.24	12.41	9.84	7.44	5.64	5.14	5.97	211.20		
219	7.54	9.60	11.76	13.95		15.50	15.83	14.93	12.72	10.10	7.72	6.16	5.77	6.54	7.96	9.86	12.04	13.74	14.37	13.56	11.51	8.97	7.02	5.96	212.19		
220	5.96	7.12	8.61	10.53	12.64	14.44	15.55	15.26	13.84	11.46	8.86		6.95	5.97	6.05	7.05	8.56	10.54	12.48	13.67	13.96	12.84	10.98	9.00	213.18		
221	7.60	6.88	7.24	8.26	9.61	11.37	13.15	14.57	15.10	14.32	12.72	10.34	8.27	6.67	6.12	6.40	7.34		8.74	10.52	12.26	13.26	13.32	12.36	214.17		
222	10.84	9.38	8.24	7.77	8.12	8.86	10.16	11.76	13.33	14.29	14.38	13.46	11.64	9.64	7.76	6.48	6.10	6.50	7.54	9.00	10.63	12.05	12.96	13.18	215.17		
223		12.64	11.47	10.24	9.16	8.76	9.04	9.66	10.72	12.02	13.24	14.10	14.04	13.02	11.29	9.63	7.96	6.84	6.50	6.73	7.66	9.04	10.52	12.10	216.10		
224	13.14	13.55	13.28	12.50	11.34	10.26		9.52	9.35	9.67	10.59	11.83	12.88	13.62	13.44	12.54	11.15	9.50	7.86	6.50	5.94	6.16	7.10	8.50	217.15		
225	10.20	11.94	13.44	14.14	14.16	13.42	12.16	10.76	9.56	9.05	9.15	9.96	11.33		12.62	13.38	13.55	12.96	11.68	9.90	7.96	6.26	5.30	5.46	218.14		
226	6.46	8.25	10.24	12.44	14.18	15.26	15.50	14.64	12.94	10.78	9.16	8.56	8.76	9.78	11.16	12.57	13.70	14.26	14.02		12.80	10.52	8.01	5.84	219.13		
227	4.76	4.81	5.98	7.77	10.32	13.02	15.24	16.66	16.76	15.58	13.24	10.54	8.38	7.60	7.78	8.76	10.54	12.56	14.24	15.18	14.86	13.21	10.40	7.41	220.13		
228	4.97	3.62		3.84	5.16	7.44	10.44	13.54	16.14	17.54	17.44	15.94	12.90	9.72	7.44	6.60	6.85	8.10	10.22	12.92	15.15	16.26	15.72	13.66	221.13		
229	10.33	6.96	4.40	3.04	3.33	5.32	7.86	11.08		14.56	17.20	18.37	18.04	16.16	12.38	8.82	6.46	5.54	5.95	7.72	10.60	13.60	16.07	17.04	222.11		
Sum	728.84	779.36	759.60	779.67	753.65	788.98	767.05	776.39	782.09	771.24	802.76	750.64	803.99	738.72	804.83	755.32	787.00	765.76	757.79	759.06	750.82	772.23	730.95	775.81	No. of Days.		
No.	71	76	71	75	72	75	73	73	74	72	76	71	76	70	76	72	75	73	74	74	72	75	72	76	76	76	18409.55

FORMS FOR SHORT-PERIOD TIDES.  
SERIES 2SM.--(Continued).

Table with columns for Day, Solar Hour, and tide measurements in feet for hours 0h to 25h. The table lists tidal data for days 230 through 265, including values for 1h intervals and 23h, 22h, 21h, 20h, 19h, 18h, 17h, 16h, 15h, 14h, 13h, 12h, 11h, 10h, 9h, 8h, 7h, 6h, 5h, 4h, 3h, 2h, 1h, and 23h.

267	8.28	7.04	6.44	6.07	7.34	8.36	9.74	11.16	12.22	12.70	12.20	11.39	10.60	9.88	9.34	9.16	9.13	9.34	9.87	10.66	11.30	11.62	11.37	259	5	
268	10.56	9.48	8.44	7.52	7.14	7.33	7.86	8.66	9.84	10.90	11.62	11.97	11.87	11.54	11.08	10.42	9.92	9.60	9.42	9.54	9.86	10.24	10.70	260	4	
269	10.91	10.86	10.34	9.74	9.06	8.35	7.72	7.46	7.67	8.44	9.64	10.73	11.52	11.88	12.06	11.88	11.53	10.97	10.23	9.48	9.04	9.01	9.38	261	4	
270	10.64	10.40	11.18	10.94	10.46	9.52	8.56	7.74	7.42	7.64	8.34	9.42	10.67	11.65	12.46	12.82	12.62	12.04	10.96	9.85	8.96	8.54	8.42	262	3	
271	8.81	9.64	10.44	11.23	11.67	11.66	10.92	9.74	8.36	7.26	6.68	6.68	6.86	7.74	9.24	10.86	12.34	13.24	13.55	13.17	12.08	10.64	8.06	263	2	
272	7.54	7.74	8.74	9.92	11.30	12.38	12.85	12.42	11.17	9.62	7.86	6.55	6.10	6.54	7.88	9.68	11.56	13.16	14.03	14.06	13.18	11.60	9.86	264	1	
273	8.07	6.97	6.64	7.14	8.38	10.20	11.92	13.16	13.44	12.50	10.70	8.70	6.90	5.75	5.50	6.36	8.04	10.20	12.32	13.87	14.61	14.36	12.87	265	0	
274	10.73	8.45	6.71	5.90	6.17	7.29	9.02	11.07	13.02	14.14	14.04	12.68	10.30	7.96	6.07	5.14	5.48	6.87	9.06	11.46	13.68	15.18	14.28	266	0	
275	12.24	9.07	7.34	6.34	5.74	5.30	6.12	7.84	9.97	12.54	14.50	15.33	14.46	12.33	9.34	6.94	5.36	4.94	5.94	8.06	10.08	12.62	15.76	266	23	
276	15.26	13.46	10.67	7.88	5.74	4.48	4.66	6.00	8.44	11.24	13.97	15.67	15.67	15.66	14.20	11.46	8.47	6.20	4.97	5.22	6.65	8.86	14.06	267	22	
277	15.76	16.07	14.86	12.14	9.06	6.37	4.56	3.93	4.93	6.93	9.67	12.77	15.34	16.35	15.80	13.61	10.52	7.73	5.58	4.88	5.77	7.56	10.04	268	21	
278	12.74	14.90	15.94	15.62	13.71	10.64	7.47	5.10	3.54	3.83	5.50	7.97	11.14	14.16	16.01	16.37	15.04	12.33	9.34	6.97	5.54	6.51	8.61	269	20	
279	8.50	11.14	13.77	15.60	15.98	14.86	12.14	8.87	6.16	4.30	3.67	4.60	6.44	9.03	12.27	14.84	16.21	15.96	14.09	11.42	8.56	6.75	6.17	270	20	
280	7.42	9.65	12.22	14.26	15.46	15.24	13.48	10.57	7.65	5.42	3.96	4.06	5.44	7.30	9.97	12.69	14.83	15.87	15.16	13.24	10.76	8.47	7.04	271	19	
281	6.68	7.20	8.44	10.38	12.56	14.16	14.83	14.05	12.07	9.24	7.02	5.32	4.44	6.11	8.77	11.97	14.77	16.06	14.81	13.07	10.76	14.44	13.68	272	18	
282	8.86	7.87	7.56	7.92	8.91	10.67	12.44	13.74	13.97	12.81	10.83	8.83	7.10	5.78	5.25	5.76	6.66	8.34	10.76	12.86	14.16	14.44	14.16	273	17	
283	12.40	10.86	9.52	8.53	8.21	8.51	9.40	10.68	12.08	13.04	13.08	11.93	10.54	9.05	7.64	6.61	6.06	6.30	7.07	8.81	10.63	13.68	14.16	274	17	
284	13.66	12.66	11.46	10.12	9.18	8.77	8.56	9.10	10.17	11.30	12.30	12.61	12.14	12.14	12.32	12.48	11.98	11.16	9.77	7.94	6.58	6.50	7.97	276	15	
285	13.44	13.92	13.88	13.56	12.37	11.18	9.72	8.32	7.60	7.94	9.26	10.84	12.04	12.52	12.48	11.98	11.16	9.77	7.94	6.58	6.06	6.50	7.97	278	15	
286	9.84	11.56	13.26	14.17	14.66	14.52	13.27	11.31	9.06	7.37	6.82	7.46	8.74	10.60	12.11	13.20	14.04	13.84	12.76	10.92	8.58	6.74	5.94	277	14	
287	6.30	7.68	9.72	11.97	13.90	15.26	15.99	15.54	13.97	11.26	8.63	6.70	5.98	6.37	7.97	10.25	12.66	14.44	15.38	15.04	13.48	11.07	8.36	278	13	
288	6.38	5.47	5.87	7.36	9.62	12.14	14.54	16.28	16.38	16.37	13.80	10.40	7.50	5.61	5.14	5.74	7.77	10.54	13.45	15.71	16.85	16.30	10.84	279	13	
289	7.77	5.85	5.07	6.24	8.24	10.67	12.74	15.25	16.92	17.15	15.62	12.54	8.66	5.94	4.14	3.96	5.28	7.85	11.15	14.38	16.70	17.32	16.33	280	12	
290	13.48	9.84	7.20	5.47	4.98	5.96	7.74	10.58	13.66	16.26	17.40	16.86	14.56	10.89	7.40	4.72	3.37	3.98	5.86	8.86	12.43	15.47	17.34	281	11	
291	17.64	10.26	12.76	9.26	6.56	5.24	5.38	6.54	8.77	11.76	14.62	17.12	17.12	15.72	12.71	9.14	6.06	3.77	3.17	4.42	6.67	9.72	13.44	282	10	
292	16.25	17.55	17.22	15.06	11.70	8.40	6.26	5.44	6.06	7.47	10.01	12.74	15.12	16.37	16.06	14.21	11.04	7.42	4.80	3.12	3.62	5.50	8.04	283	9	
293	11.13	14.40	16.50	17.22	16.16	13.58	10.36	7.77	6.24	6.04	6.91	8.53	10.52	13.06	15.02	15.64	14.36	11.93	8.64	6.01	4.31	4.52	6.20	284	9	
294	8.94	11.94	14.56	16.24	16.32	14.74	12.13	9.47	7.47	6.58	6.90	7.84	9.30	11.26	13.26	14.41	14.26	12.74	10.35	7.88	5.80	4.44	4.38	285	8	
295	5.92	7.85	10.30	12.70	16.24	16.32	14.74	12.13	9.47	7.47	6.58	6.90	7.84	9.30	11.26	13.26	14.41	14.26	12.74	10.35	7.88	5.80	4.44	4.38	285	8
296	5.47	6.20	7.44	9.04	10.97	13.06	14.36	14.36	13.40	11.82	10.44	9.16	8.41	8.24	8.54	9.26	10.30	11.46	13.06	11.36	9.07	7.14	5.84	286	7	
297	7.08	6.36	6.44	7.32	8.34	9.60	11.24	12.72	13.46	13.28	12.32	11.06	10.10	9.27	8.97	8.94	9.08	9.61	10.14	13.06	11.36	9.07	7.14	5.84	286	7
298	8.47	7.66	7.41	7.56	8.04	8.76	9.91	11.17	12.30	12.88	12.66	12.66	11.92	11.04	10.37	9.76	9.36	9.12	9.08	9.27	9.86	10.44	8.37	287	6	
299	10.30	9.78	9.22	8.56	8.06	7.74	8.02	8.86	10.06	11.16	12.02	12.40	12.34	12.06	11.48	10.82	9.97	9.24	8.77	8.68	8.96	9.55	10.22	290	4	
300	10.70	10.88	10.82	10.57	10.03	9.26	8.44	7.90	8.07	8.80	10.90	11.78	12.40	12.34	12.06	11.48	10.82	9.97	9.24	8.77	8.68	8.96	9.55	10.22	290	4
301	9.27	10.10	10.90	11.50	11.78	11.53	10.67	9.30	8.14	7.56	7.77	8.55	9.74	11.07	12.15	12.94	13.28	13.04	12.24	10.77	9.14	7.88	7.18	292	2	
302	7.36	8.12	9.26	10.62	11.94	12.78	12.88	12.06	10.48	8.86	7.70	7.28	7.65	8.65	10.02	11.54	12.81	13.77	14.04	13.50	12.16	10.00	8.34	6.96	293	2
303	6.50	6.88	7.96	9.76	11.52	13.07	13.96	13.77	12.48	10.52	8.76	7.36	6.77	7.26	8.52	10.36	12.17	13.66	14.56	14.48	13.40	11.12	8.84	294	1	
304	6.87	5.64	5.46	6.30	8.06	10.30	12.80	14.34	15.00	14.16	12.26	9.96	7.92	6.50	6.22	7.10	8.82	10.86	13.12	14.54	15.07	14.56	12.60	295	0	
305	9.98	7.47	5.46	4.56	4.96	6.06	9.03	11.80	14.15	15.84	15.96	14.52	12.00	9.24	7.24	6.16	6.40	7.67	9.66	11.93	14.14	15.62	15.76	295	23	
306	14.36	11.76	8.61	6.02	4.24	3.86	5.14	7.32	10.15	13.10	15.67	16.78	16.26	14.16	11.00	8.32	6.36	5.84	6.47	8.16	10.16	12.84	15.02	296	22	
Sum	788.17	747.44	781.64	762.08	763.36	764.37	762.95	782.60	746.24	704.36	732.62	794.82	750.16	797.48	759.05	777.70	772.73	754.30	782.03	750.70	778.21	729.88	785.84	748.36	No.	
No.	77	73	76	73	75	74	74	76	73	77	71	77	72	77	73	75	74	74	76	73	76	72	77	71	18387.09	

TIDAL OBSERVATIONS.

FORMS FOR SHORT-PERIOD TIDES.

SERIES 2 SM.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
307	16.10	15.46	13.28	9.87	6.84	4.45	3.04	3.57	5.44	8.15	11.37	14.60	16.81	17.35	16.38	13.64	10.44	7.71	6.07	5.84	6.88	8.87	11.47	14.12	297 22	
308	15.94	16.22	14.81	11.87	8.55	5.46	3.46	2.87	4.17	6.35	9.32	13.00	15.95	17.47	17.44	15.72	12.68	9.66	7.28	7.28	5.94	6.04	7.36	9.64	298 21	
309	13.45	14.81	16.04	15.60	13.70	10.52	7.15	4.66	2.92	3.10	4.72	7.47	10.55	13.92	16.35	17.36	16.74	14.57	11.67	8.85	6.76	5.94	6.76	9.48	299 20	
310	7.70	9.2	12.68	14.78	15.58	14.78	12.36	9.26	6.36	4.20	3.07	3.72	5.55	8.04	11.03	14.10	16.17	16.96	16.12	14.06	11.35	8.82	7.14	7.14	300 19	
311	6.57	7.02	8.46	10.56	13.14	14.64	15.04	13.76	11.47	8.74	6.42	4.70	4.22	5.00	6.86	9.02	11.88	14.60	16.14	16.22	15.16	13.26	10.86	8.86	301 19	
312	7.58	7.14	7.44	8.84	10.92	12.84	13.84	13.86	12.57	10.68	8.54	6.84	5.66	5.27	5.98	7.33	9.36	11.72	14.00	15.22	15.38	14.58	12.88	12.88	302 18	
313	11.01	9.42	8.12	7.64	7.92	8.94	10.40	11.85	12.91	13.12	12.26	10.75	9.22	7.66	6.68	6.30	6.72	7.86	9.44	11.50	13.34	14.46	14.46	14.66	303 17	
314	13.96	13.74	11.30	9.76	8.54	7.93	7.84	8.40	9.60	10.88	12.06	12.64	12.40	11.47	10.10	8.76	7.68	7.01	7.06	7.90	9.22	10.97	12.56	13.56	304 16	
315	13.72	14.38	14.04	13.04	11.45	9.76	8.15	7.22	7.02	7.48	8.84	10.32	11.48	12.55	12.97	12.46	11.36	9.70	8.28	7.14	6.80	7.40	8.84	8.84	305 15	
316	10.74	12.56	13.87	14.54	14.38	13.40	11.67	9.60	7.53	6.30	5.88	6.50	8.20	10.07	11.93	13.36	14.04	13.66	12.30	10.26	8.61	7.37	6.86	7.24	306 15	
317	8.35	10.36	12.50	14.11	15.08	14.96	13.80	11.64	9.03	6.96	5.44	5.44	5.82	4.22	4.10	5.32	7.70	10.85	13.60	15.51	16.95	15.06	12.86	10.40	308 13	
318	6.44	6.77	8.02	10.14	12.62	14.56	15.55	15.25	13.56	10.92	8.12	5.82	4.22	4.71	3.46	3.86	3.01	4.08	5.50	6.62	8.62	10.66	12.86	15.38	309 12	
319	8.16	6.53	5.96	6.51	8.24	10.85	13.27	15.16	15.84	15.03	12.98	9.78	7.04	4.71	3.46	3.63	3.01	4.08	5.50	6.62	8.62	10.66	12.86	15.38	310 11	
320	12.86	9.98	7.70	6.25	5.93	6.71	8.67	11.25	13.84	15.52	15.84	14.55	15.28	13.15	10.15	7.00	4.47	3.03	3.22	5.03	7.60	10.76	14.05	16.38	311 11	
321	16.72	14.87	12.92	9.20	7.26	6.32	6.37	7.46	9.60	12.20	14.35	15.67	15.16	13.92	11.40	8.36	5.66	3.69	2.94	3.94	6.18	9.01	12.24	15.38	312 10	
322	17.05	16.14	13.92	11.10	8.66	7.96	6.87	6.16	6.46	8.00	10.44	13.10	14.76	15.16	13.92	11.40	8.36	5.66	3.69	2.94	3.94	6.18	9.01	12.24	313 9	
323	14.91	16.53	16.56	15.16	12.66	10.06	7.96	6.74	6.60	7.35	9.00	11.24	13.43	14.50	14.36	12.66	12.66	11.18	9.94	7.20	4.97	3.56	3.77	5.34	314 8	
324	10.56	13.46	15.64	16.34	15.71	13.92	11.46	9.28	7.66	6.86	6.98	7.98	9.96	12.00	13.52	14.02	13.37	11.18	8.81	6.52	4.86	4.33	5.20	5.20	315 8	
325	6.90	9.14	11.80	14.20	15.72	15.81	14.66	12.72	10.71	8.96	7.82	7.56	7.92	9.16	10.68	12.24	13.26	13.26	12.06	10.17	8.00	6.25	5.31	5.30	316 7	
326	6.66	8.34	10.52	12.80	14.44	15.18	14.68	13.32	11.56	10.02	8.76	8.10	8.10	8.00	8.60	9.65	10.96	12.18	12.58	12.23	11.04	9.16	7.62	6.54	317 6	
327	6.20	6.84	7.96	9.38	11.14	12.91	14.18	14.40	13.64	12.37	10.90	9.38	8.78	8.46	8.68	9.30	10.00	10.94	11.57	11.80	11.36	10.28	8.94	8.94	318 5	
328	7.84	7.18	7.20	7.86	8.80	9.98	11.46	12.86	13.86	13.83	12.96	11.72	10.53	9.66	9.14	8.92	8.92	8.96	9.17	9.66	10.40	11.10	11.37	11.01	319 4	
329	10.20	9.16	8.46	8.10	8.14	8.66	9.44	10.56	11.74	12.76	13.34	13.26	12.61	11.72	10.86	9.76	9.04	8.80	8.85	9.16	9.64	10.14	10.74	10.74	320 4	
330	11.18	11.32	11.06	10.38	9.58	8.94	8.71	8.90	9.50	10.42	11.46	12.48	13.10	13.15	12.64	11.84	10.76	9.71	8.88	8.35	8.19	8.42	9.04	9.96	321 3	
331	10.86	11.50	11.80	11.06	10.38	9.58	8.94	8.71	8.90	9.50	10.42	11.46	12.48	13.10	13.15	12.64	11.84	10.76	9.71	8.88	8.35	8.19	8.42	9.04	322 2	
332	8.13	10.03	11.16	12.23	12.80	12.64	11.66	10.25	9.04	8.36	8.34	8.36	8.34	8.96	10.02	12.46	13.23	13.47	13.00	11.72	10.14	8.58	7.03	6.27	323 1	
333	6.31	7.08	8.52	10.23	11.92	13.17	13.63	13.10	11.86	10.18	8.76	7.98	7.96	8.75	10.13	11.64	11.64	13.14	13.94	13.94	13.04	11.34	9.30	7.45	324 0	
334	5.86	5.13	5.46	6.76	8.80	11.15	13.20	14.66	14.98	13.87	11.76	9.58	8.10	7.27	7.36	8.22	9.82	11.76	13.33	14.28	14.14	12.87	10.56	8.56	325 0	
335	7.98	5.77	4.14	3.74	4.67	6.71	9.27	12.02	14.40	15.66	15.44	13.71	11.16	8.74	7.02	6.40	6.78	8.22	10.37	12.25	13.88	14.74	14.20	12.26	326 0	
336	9.36	6.51	4.12	2.75	2.94	4.56	7.03	10.05	13.37	15.65	16.62	16.47	17.07	15.75	12.96	9.66	7.26	5.65	4.46	6.44	8.40	11.20	13.57	15.08	327 21	
337	13.97	11.41	8.07	4.96	3.62	3.62	2.58	4.74	7.64	11.12	14.22	15.66	17.40	17.25	15.37	12.33	9.00	7.26	5.65	6.75	5.63	6.88	9.32	328 21		
338	15.11	15.17	13.27	9.06	6.40	3.62	1.76	1.54	3.26	6.02	9.25	12.97	15.66	17.40	17.25	15.37	12.33	9.00	7.26	5.65	6.75	5.63	6.88	9.32	329 21	
339	12.22	14.44	15.50	14.80	12.31	8.84	5.46	3.00	1.66	2.20	4.15	6.95	10.46	13.81	16.44	17.54	16.82	14.56	11.38	8.50	6.32	5.44	5.74	7.26	330 20	
340	10.06	12.76	14.97	15.26	14.66	11.32	8.05	5.16	2.94	2.16	3.11	5.16	7.96	11.23	14.30	16.57	17.22	16.33	13.81	10.68	8.07	6.16	5.59	5.59	331 19	
341	5.88	7.64	10.25	13.77	14.20	14.72	13.35	10.74	7.81	5.32	3.66	3.26	4.42	6.34	8.86	11.67	14.58	16.33	16.57	15.28	12.84	9.93	7.47	7.47	332 19	
342	6.23	5.72	6.26	7.94	10.30	12.38	13.76	13.96	12.68	10.56	8.18	6.28	4.97	4.83	5.72	7.34	9.38	12.05	14.37	15.76	15.80	14.56	14.56	14.56	333 17	
	9.94	8.13	6.64	6.14	6.34	8.04	10.04	11.78	12.88	13.16	12.24	10.73	8.96	7.30	6.24	5.96	6.20	7.80	9.84	12.15	13.88	14.67	14.67	14.67	334 17	

844	13.77	11.77	10.06	8.23	6.86	6.34	6.56	7.70	9.30	10.84	12.16	13.76	12.53	11.48	10.14	8.60	7.52	7.06	7.44	8.47	10.17	11.91	13.34	14.21	838 17			
845	14.40	13.72	12.30		10.42	8.41	6.88	6.14	6.37	7.32	8.81	10.45	11.84	12.86	13.08	12.42	11.25	9.75	8.54	7.84	7.88	8.64	10.02	11.65	334 16			
846	13.16	14.14	14.30	13.64	12.17	10.31	8.37	6.68	5.72		5.86	6.88	8.64	10.40	12.07	13.31	13.88	13.62	12.36	10.67	9.06	8.12	7.90	8.54	335 15			
847	9.72	11.26	12.78	13.82	14.20	13.74	12.14	10.05	7.76	6.00	5.04	5.23	6.52	8.50	10.56	12.60		14.12	14.40	13.86	12.58	10.80	8.97	7.94	336 14			
848	7.68	8.24	9.50	11.14	12.75	13.98	14.44	13.73	11.85	9.10	6.84	5.06	4.41	5.04	6.57	8.66	11.20	13.52	15.24	15.84	15.08	13.13		10.86	337 13			
849	9.00	7.82	7.54	8.05	9.36	11.14	12.94	14.20	14.46	13.36	11.28	8.58	5.98	4.22	3.96	5.07	6.97	9.54	12.26	14.54	16.11	16.34	15.17	12.88	338 12			
850	10.26	8.38	7.53	7.40	8.14		9.77	11.52	13.36	14.60	14.56	12.94	10.26	7.33	5.11	3.87	4.05	5.64	7.81	10.61	13.20	15.47	16.54	16.21	339 11			
851	14.70	13.20	9.81	8.08	7.33	7.37	7.36	7.70	7.37	7.26	7.44	8.72	10.57	12.55	14.00	14.24	13.20	10.72	8.06	6.56	9.06	11.87	14.55	16.23	340 11			
852	16.72	15.97	13.94	11.34	8.98	7.71	8.26	7.37	7.80	7.24	7.44	8.72	10.57	12.55	14.00	14.24	13.20	10.72	8.06	4.74	5.63	7.85	10.36	13.16	341 10			
853	15.34	16.56	16.48	15.11	12.72	10.27	8.26	7.37	7.80	7.24	7.44	8.72	10.57	12.55	14.00	14.24	13.20	10.72	8.06	3.96	4.91	6.70	9.02	11.70	342 10			
854	14.07	15.87	16.56	15.80	13.96	11.44	9.32	7.80	8.54	7.57	7.44	8.72	10.57	12.55	14.00	14.24	13.20	10.72	8.06	5.93	4.58	4.74	6.03	8.20	343 9			
855	10.34	12.88	15.05	16.23	16.28	14.89	12.65		10.30	8.54	7.57	7.44	8.72	10.57	12.55	14.00	14.24	13.20	10.72	9.47	7.26	5.64	5.07	5.86	344 8			
856	7.43	9.20	11.48	13.56	15.17	15.82	15.18	13.58	11.42	9.46	7.98	7.36	7.62	7.62	8.50	10.02	11.60	12.67	13.00	12.14	10.36	8.34	6.54	5.59	345 7			
857	5.67	6.77	8.43	10.27	12.17	13.90	14.96	14.86	13.76	12.00	10.22	8.66	7.73	7.38	7.80	8.82	10.22	11.48	12.26	12.24		11.15	9.47	8.01	346 6			
858	6.87	6.45	6.75	7.83	9.14	10.75	12.56	13.86	14.46	14.06	12.87	11.31	9.72	8.40	7.76	7.73	8.27	9.36	10.54	11.48	12.02	11.81	10.84	9.56	347 6			
859	8.46	7.76		7.56	8.00	8.95	10.05	11.60	13.13	14.20	14.42	13.83	12.50	10.98	9.76	8.76	8.24	8.24	8.80	9.62	10.53	11.27	11.70	11.62	348 5			
860	11.14	10.38	9.49	8.78	8.48	8.71	9.47	10.70	12.04		13.16	13.78	13.79	13.14	11.94	10.54	9.17	8.30	7.83	8.04	8.58	9.36	10.22	11.00	349 4			
861	11.54	11.74	11.57	10.96	10.14	9.44	9.04	9.10	9.74	10.90	12.24	13.16	13.57	13.38	12.64		11.55	10.26	8.86	7.83	7.22	7.36	7.86	8.85	350 3			
862	10.11	11.13	11.95	12.42	12.30	11.78	10.77	9.72	9.06	9.01	9.55	10.76	11.97	12.94	13.38	13.14	12.44	11.22	9.78	8.36	7.04	6.26		6.15	351 2			
863	6.82	8.20	9.97	11.56	12.90	13.50	13.36	12.36	10.92	9.68	8.84	8.68	9.14	10.18	11.57	12.76	13.30	13.22	12.46	11.00	9.17	7.18	5.75	4.90	352 2			
864	4.92	6.07	7.94	10.07		12.03	13.66	14.48	14.16	12.76	10.77	9.04	7.98	7.73	8.23	9.70	11.40	12.74	13.42	13.45	12.54	10.80	8.50	6.30	353 1			
865	4.47	3.64	4.12	5.82	8.20	10.84	13.27	14.95	15.70	14.97	13.05		10.50	8.64	7.50	7.36	8.16	9.80	11.80	13.38	14.33	14.26	13.00	10.50	354 0			
866	7.72	5.17	3.42	2.93	4.16	6.37	9.00	12.12	14.97	16.74	16.96	15.68	13.11	10.34	8.06	6.98	7.04	8.06		10.00	12.15	14.04	15.14	15.03	355 23			
867	13.10	10.20	7.00	4.27	2.40	2.30	3.93	6.57	9.77	13.27	17.72	17.51	17.51	15.78	12.57	9.74	7.27	6.14	6.36	7.56	9.86	12.72	14.77	15.81	355 23			
868		15.20	12.64	9.26	5.91	3.10	1.55	1.93	4.00	7.06	14.30	17.04	17.04	18.34	17.72	15.47	12.00	8.88	6.58	5.67	6.00	7.50	10.14	13.10	356 22			
869	15.24	16.17	14.94	15.46	15.86	14.14	10.98	7.68	4.48	2.36	1.77	3.30	8.90		12.30	15.56	17.50	17.88	16.62	13.58	9.97	6.94	5.14	4.70	358 20			
870	10.63	13.44	15.46	15.86	14.14	10.98	7.68	4.48	2.36	1.77	3.30	5.83	8.90		12.30	15.56	17.50	17.88	16.62	13.58	9.97	6.94	5.14	4.70	358 20			
871	5.52	7.63	10.73	13.70	15.36	15.32	13.24	9.92	6.64	4.73	3.07	3.08	4.74	6.97	9.86	13.01	15.80	17.38	17.48	15.95		12.86	9.53	6.72	359 19			
872	5.22	4.90	5.87	8.03	10.96	13.30	14.68	14.83	13.24	10.55	7.68	5.43	4.33	4.63	5.97	8.02	10.57	13.35	15.58	16.60	16.14	14.11	11.13	8.76	360 19			
873	6.38	5.17		5.13	6.30	8.60	10.76	12.74	13.74	13.62	12.37	10.30	8.14	6.53	5.84	6.14	7.14	8.74	10.77	13.13	14.96	15.71	15.12	13.32	361 18			
874	10.86	8.44	6.53	5.48	5.27	6.00	7.78	9.85	11.62		12.84	13.10	12.58	10.74	9.22	7.96	7.33	7.28	7.93	9.16	10.97	13.12	14.54	14.68	362 17			
875	13.66	12.28	10.12	8.24	6.78	5.82	5.70	6.37	7.72	9.40	11.06	12.32	12.86	12.50	11.47		10.24	9.12	8.42	8.24	8.54	9.54	11.12	13.64	363 16			
876	13.57	13.57	12.88	11.44	9.87	8.24	6.74	5.77	5.52	6.12	7.27	8.94	10.64	12.10	13.01	13.12	12.46	11.26	10.02	9.06	8.58	8.66		9.44	364 15			
877	10.68	11.96	12.92	13.14	12.66	11.54	10.06	8.36	6.86	5.72	5.37	5.87	7.17	9.14	11.00	12.70	13.68	13.81	12.94	11.57	10.28	9.14	8.62	8.63	365 16			
878	9.20	10.44	11.66	12.53		12.92	12.58	11.64	9.77	7.86	6.12	5.05	4.78	5.62	7.06	9.15	11.26	13.23	14.30	14.32	13.36	11.78	10.34	9.17	366 14			
879	8.44	8.24	8.62	9.76	11.04	12.36	13.08	12.90	11.65	9.64	7.34		5.52	4.45	4.52	5.76	7.66	9.07	12.43	14.27	15.18	14.97	13.73	11.82	367 13			
880	10.16	8.86	8.24	8.26	8.96	10.32	11.70	12.96	13.58	13.16	11.26	8.91	6.66	4.96	4.33	4.86	6.36		8.55	11.00	13.44	15.21	15.84	15.17	368 12			
881	13.56	11.44	9.66	8.38	7.80	7.97	9.00	10.56	12.24	13.46	13.82	12.72	10.52	7.90	5.74	4.34	4.11	5.34	7.23	9.78	12.44	14.65	15.93	15.94	369 12			
882		14.74	12.37	10.23	8.53	7.47	7.31	7.97	9.38	11.36	13.14	14.17	14.00	12.18	9.43										870 2			
Sum	738.82	775.73	774.76	744.42	50.88	742.91	762.09	706.44	754.79	703.22	756.55	713.75	745.27	744.18	750.67	748.91	747.20	771.79	735.10	83.93	736.70	787.74	722.69	778.69	No. of Days, 731 4, 17960.51			
No.	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100

FORMS FOR SHORT-PERIOD TIDES.

BOMBAY—Commencing 0 hours, Astronomical Time, 1st January, 1885.

Argument ( $\gamma - 2\sigma + \omega$ ).

SERIES 2N.

Motion per mean Solar hour = 13°-94'76"774.

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	d	h
1	15.52	12.96	9.31	5.76	3.03	1.08	2.22	7.90	11.70	15.50	18.00	18.85	18.08	15.14	11.54	8.50	6.21	5.53	6.08	8.20	14.16	16.06	16.66	15.40	2	1	
2	12.16	8.40	4.86	2.56	1.71	2.90	5.56	8.82	12.94	16.44	18.97	17.67	14.74	10.56	7.53	5.57	5.16	6.10	8.63	11.31	14.68	16.63	16.96	11.92	3	3	
3	8.00	4.87	2.80	2.57	4.24	6.84	10.20	14.07	17.20	18.86	18.84	17.06	9.77	6.90	5.23	4.96	6.16	8.86	12.14	14.97	16.40	16.40	14.28	11.00	4	4	
4	7.61	3.55	3.86	5.35	8.01	11.36	14.83	17.16	18.38	17.93	15.80	12.16	8.68	6.10	5.05	6.68	9.24	12.28	14.51	15.96	15.58	13.48	10.47	7.54	5	6	
5	4.88	3.07	5.07	9.17	7.22	13.11	15.02	17.02	16.63	14.11	8.00	6.64	6.22	5.47	5.84	7.18	12.12	14.04	15.00	14.85	12.62	10.24	8.07	7.04	6	8	
6	5.76	7.54	8.07	10.60	12.84	15.06	16.36	15.18	13.87	9.76	8.10	6.16	6.17	6.55	7.86	9.76	11.80	13.27	14.00	13.64	10.47	8.44	9.60	8.46	7	10	
7	9.03	9.97	11.20	13.05	14.44	13.75	12.27	10.82	9.20	7.93	7.24	7.03	7.40	8.29	9.82	11.16	12.55	13.24	13.07	12.20	11.16	9.64	9.60	9.90	8	12	
8	10.60	11.70	13.96	14.02	14.44	13.75	12.27	10.82	9.20	7.93	7.24	7.03	7.40	8.29	9.82	11.16	12.55	13.24	13.07	12.20	11.16	9.64	9.60	9.90	9	13	
9	11.07	12.14	13.06	13.56	12.72	11.71	10.43	9.14	7.97	7.14	6.75	6.94	7.74	8.96	11.64	12.67	13.14	12.97	12.20	11.74	10.48	10.12	10.05	10.23	10	15	
10	10.84	11.64	13.68	13.37	11.53	10.44	8.97	7.80	6.96	6.38	6.44	7.28	8.73	10.47	12.14	13.23	13.63	12.58	11.38	10.27	9.77	9.62	9.89	10.44	11	17	
11	11.34	11.97	12.52	12.50	10.87	8.70	7.34	6.16	5.74	6.34	7.62	9.54	11.46	13.22	14.14	14.58	13.94	12.72	11.24	9.32	9.14	9.46	10.37	11.48	12	19	
12	12.46	13.04	12.84	11.88	10.23	8.20	6.52	5.62	6.50	8.14	10.17	12.34	14.10	15.20	15.17	13.97	12.27	10.58	9.35	8.75	9.26	10.34	11.68	12.96	13	21	
13	13.64	13.36	11.80	9.66	7.32	5.82	5.14	5.44	6.74	8.86	11.26	15.38	15.87	15.24	13.66	11.54	9.82	8.71	8.16	8.36	9.30	10.74	12.46	13.61	14	23	
14	13.00	10.84	8.24	6.20	4.76	4.46	5.40	7.36	9.78	12.57	14.82	16.13	15.97	12.25	10.05	8.46	7.82	7.74	8.41	9.71	11.76	13.30	14.26	14.09	15	0	
15	13.44	7.00	5.12	4.20	4.63	6.12	8.44	11.24	14.94	15.74	16.36	15.71	13.82	11.22	8.94	7.54	7.15	8.40	10.27	12.44	14.06	14.68	13.84	11.50	16	2	
16	8.60	5.94	4.37	4.02	5.06	7.26	9.66	12.72	15.20	16.55	16.63	15.27	12.77	9.97	7.86	6.84	6.66	7.56	9.32	11.55	14.80	14.78	13.22	10.43	17	4	
17	5.34	4.30	4.66	6.25	8.54	11.38	16.15	16.88	16.08	14.04	11.02	8.34	6.76	6.12	6.34	7.60	9.84	12.14	14.06	14.84	14.14	13.22	10.43	7.48	18	2	
18	4.24	5.16	7.15	9.68	12.56	14.87	16.44	16.45	15.00	12.42	7.22	5.80	5.43	6.26	8.16	10.65	12.88	14.28	14.56	13.33	10.92	8.30	6.46	6.16	19	6	
19	6.54	8.66	11.04	13.64	15.62	16.36	15.76	13.82	11.00	8.37	6.37	5.54	6.83	8.93	11.40	13.32	14.42	14.25	12.47	10.10	7.91	6.34	5.70	6.30	20	8	
20	7.70	9.76	14.36	15.74	15.96	14.86	12.76	10.13	7.78	6.17	5.70	6.11	9.76	11.65	13.04	13.76	13.34	12.14	10.65	9.07	8.15	8.14	8.68	9.86	21	9	
21	10.80	13.97	14.62	15.17	13.80	11.46	9.14	7.34	6.17	6.00	6.68	8.02	9.76	11.65	13.04	13.76	13.34	12.14	10.65	9.07	8.15	8.14	8.68	9.86	22	13	
22	13.36	14.56	15.02	14.37	12.76	10.76	8.71	6.96	6.06	6.68	7.86	9.46	11.24	12.66	13.36	13.34	12.38	11.08	9.94	9.94	8.88	9.28	10.22	11.70	23	15	
23	14.14	14.41	13.60	12.06	10.26	8.46	7.10	6.25	6.06	6.68	8.06	9.46	11.24	12.66	13.36	13.34	12.38	11.08	9.94	9.94	8.88	9.28	10.22	11.70	24	17	
24	13.66	13.03	11.87	10.24	8.47	7.00	5.83	5.38	5.68	6.78	8.55	10.33	13.56	14.30	14.16	13.05	11.56	10.06	9.11	8.87	9.40	10.46	11.87	12.94	25	17	
25	13.44	12.40	10.74	8.86	6.83	5.22	4.41	4.77	6.10	8.10	10.50	12.63	14.53	15.33	13.76	11.64	9.52	8.28	7.92	7.92	8.25	9.53	11.24	12.70	26	18	
26	14.14	13.30	11.34	8.72	4.24	3.38	3.76	5.30	7.76	10.55	13.50	15.72	16.74	16.12	14.36	11.40	7.24	6.57	6.57	6.57	6.57	6.57	6.57	6.57	27	20	
27	14.17	11.84	8.82	5.70	3.60	2.56	3.06	7.88	11.48	14.56	17.04	17.86	17.00	14.36	10.96	8.07	6.27	5.77	5.77	5.77	5.77	5.77	5.77	5.77	28	22	
28	12.18	8.44	5.42	3.22	2.16	3.07	5.52	8.75	12.46	18.10	18.47	17.26	13.80	10.14	7.09	5.27	5.02	6.02	8.40	11.85	14.65	16.84	15.28	11.68	30	0	
29	7.88	4.80	2.74	2.38	4.00	6.66	10.10	13.98	17.01	18.64	16.30	12.42	8.97	6.01	4.46	4.57	6.12	9.14	12.56	15.46	17.00	10.86	14.76	11.68	31	2	
30	4.34	3.72	2.99	4.86	7.74	11.40	14.94	17.54	18.47	17.06	14.67	11.08	7.54	5.01	4.32	6.55	9.62	13.04	15.80	16.84	16.08	13.73	10.16	6.82	32	4	
31	4.54	3.58	6.36	4.44	9.36	12.84	15.86	17.74	17.94	16.48	13.27	9.84	4.96	4.33	5.26	10.60	13.70	15.74	16.43	15.42	12.82	9.66	6.90	5.42	33	7	
32	5.14	6.20	8.06	10.66	16.02	17.12	16.74	14.88	11.68	8.76	6.34	4.92	4.74	5.86	8.26	11.07	13.60	15.16	15.24	11.68	9.04	7.34	6.56	6.94	34	9	
33	8.04	9.56	11.76	14.24	15.60	16.04	15.34	13.02	7.86	6.27	5.54	5.86	7.18	9.07	11.36	13.26	14.34	14.26	12.88	11.00	9.30	7.92	8.30	9.05	35	11	
34	10.36	12.08	13.76	14.66	14.44	13.11	11.12	9.30	7.54	6.13	5.86	7.86	9.28	10.86	12.27	13.10	12.94	11.93	10.66	9.72	9.12	9.06	9.26	10.60	36	13	
35	11.82	13.86	13.34	11.84	11.45	10.03	8.74	7.48	6.86	6.78	7.17	7.94	10.25	11.34	11.92	11.92	11.34	10.84	10.34	10.07	9.97	9.77	9.04	10.44	37	14	



36	11.37	12.26	11.78	10.88	9.87	8.84	7.84	6.94	7.18	8.03	9.07	10.14	11.00	11.56	11.77	11.46	11.12	10.57	10.07	9.70	9.70	10.13	10.80	39.16	
37	11.27	11.45	11.25	10.76	9.07	8.00	7.11	6.58	6.74	7.44	8.51	9.84	10.90	11.76	12.34	12.55	12.30	11.60	9.76	9.34	9.17	9.56	10.24	10.94	40.18
38	11.36	11.44	10.97	10.10	9.07	7.87	6.30	6.50	7.26	8.50	10.16	11.44	12.65	13.26	13.32	12.56	11.36	10.08	9.16	8.64	9.01	9.76	10.58	41.20	
39	11.66	11.34	10.36	8.82	7.36	6.12	5.54	5.82	6.94	8.54	12.06	13.46	13.97	13.64	12.30	10.76	9.26	8.14	7.84	8.12	8.96	10.24	11.52	42.22	
40	12.07	10.47	8.56	6.64	5.46	5.20	5.93	7.55	9.56	11.72	13.53	14.84	13.98	12.14	10.00	8.54	7.66	7.53	8.16	9.56	11.03	12.66	13.60	43.23	
41	12.30	7.77	5.88	4.84	4.96	6.33	8.27	10.66	13.07	14.85	15.64	15.23	13.64	11.13	9.02	6.79	7.00	8.13	9.67	11.85	13.60	14.38	13.88	45.1	
42	9.10	6.54	4.66	4.00	6.86	9.20	11.97	14.34	15.82	15.96	14.78	12.26	9.64	7.46	6.24	5.96	6.48	6.74	8.05	13.07	14.56	14.85	13.63	46.3	
43	5.57	4.07	4.04	5.40	7.84	10.63	15.83	16.64	16.01	13.87	10.90	8.00	6.17	5.46	5.74	7.26	9.70	12.25	14.42	15.95	13.08	9.90	6.94	47.5	
44	3.92	4.66	6.62	9.46	12.60	15.08	16.60	16.64	11.93	8.96	6.76	5.63	5.06	5.54	7.84	10.54	13.30	15.12	15.66	14.46	11.76	5.86	4.26	48.7	
45	5.52	7.84	10.68	13.68	15.84	16.68	15.86	13.15	10.22	7.36	4.23	4.46	6.07	8.56	11.57	14.06	15.54	15.51	13.57	10.53	7.47	5.38	4.52	49.8	
46	6.70	12.18	14.74	16.26	16.26	14.64	11.74	8.68	6.28	4.54	4.14	5.07	7.06	9.74	14.55	15.46	14.76	12.51	9.68	7.24	5.84	5.60	8.40	50.10	
47	10.77	13.32	16.26	15.47	13.18	10.24	7.54	5.62	4.44	4.69	5.80	7.87	10.40	12.80	14.59	14.05	11.86	9.36	7.58	6.64	6.76	7.86	9.60	51.12	
48	13.73	15.08	15.32	14.12	11.86	9.24	5.18	4.58	5.06	6.46	8.24	10.33	12.41	13.86	14.34	13.41	11.46	9.53	8.05	7.66	8.58	9.92	11.68	52.14	
49	14.16	14.12	12.82	10.83	8.73	6.87	5.45	5.44	6.63	8.23	10.14	11.77	12.96	13.40	12.76	11.56	10.24	9.04	8.45	8.28	9.76	11.20	12.50	53.16	
50	13.06	11.88	10.25	8.57	6.98	5.77	5.38	5.64	6.37	7.82	9.54	12.38	13.02	12.96	12.16	11.07	10.02	8.94	8.44	8.48	9.27	10.44	11.57	54.18	
51	11.70	10.50	8.90	7.32	5.96	5.24	5.12	5.86	7.17	8.90	10.63	12.10	13.16	13.13	11.86	10.27	8.88	8.08	7.87	8.42	9.56	10.87	12.44	55.19	
52	12.26	11.27	9.76	6.27	5.06	4.55	5.02	6.47	8.52	10.67	12.72	14.14	14.86	14.44	12.76	8.80	7.60	7.21	7.64	9.18	11.00	12.40	13.52	56.21	
53	12.60	10.86	8.63	6.40	4.06	4.70	6.46	8.84	11.30	13.80	15.56	16.25	15.33	12.96	10.26	7.95	6.54	7.03	8.83	11.00	12.96	14.40	14.74	57.23	
54	11.70	8.84	6.08	4.05	3.42	4.14	6.18	8.80	14.93	16.76	17.15	15.84	12.97	9.66	7.00	5.18	5.12	6.20	8.52	11.16	13.67	15.86	14.57	59.1	
55	8.26	5.48	3.42	2.92	4.14	6.52	9.58	13.16	16.04	17.34	15.27	11.66	8.27	5.56	4.16	4.32	5.84	8.66	11.92	14.74	16.46	16.54	11.26	60.3	
56	4.94	3.20	4.70	7.52	10.86	14.63	17.06	17.96	16.96	13.90	13.90	10.20	4.47	3.56	4.02	6.04	9.40	12.86	15.55	16.86	16.36	13.86	10.44	61.4	
57	4.54	3.37	5.80	8.56	12.33	15.44	17.27	17.40	15.46	12.03	8.50	5.70	3.74	3.27	7.10	10.34	13.76	15.97	16.76	15.76	12.96	9.44	6.74	62.6	
58	4.23	5.26	7.43	10.37	13.82	16.13	17.08	16.40	13.86	10.59	7.26	4.84	3.56	3.86	5.60	8.27	11.55	14.34	16.38	14.66	11.66	8.60	6.46	63.8	
59	6.50	8.86	11.44	14.36	15.97	16.18	12.00	8.86	6.28	4.57	4.06	4.86	6.67	9.40	12.24	14.39	15.64	15.33	13.25	10.46	6.76	6.34	7.00	64.10	
60	10.22	12.44	14.42	15.27	14.71	12.72	10.14	7.72	5.93	4.86	5.00	6.10	8.03	10.30	12.47	13.97	14.58	13.92	12.03	10.14	8.54	7.56	8.42	65.12	
61	12.06	14.04	14.24	13.22	11.36	9.36	7.56	6.27	5.84	6.34	7.46	10.76	12.44	13.56	13.74	12.74	11.40	10.66	10.24	10.16	10.24	10.47	10.86	66.13	
62	12.44	13.03	12.12	10.46	8.86	7.68	7.02	7.66	8.54	9.66	10.74	11.76	12.46	12.67	12.27	11.74	10.87	10.78	10.20	9.75	9.87	10.35	11.10	68.17	
63	13.07	12.24	11.36	8.87	7.97	7.07	7.94	8.50	9.00	9.78	10.74	12.08	12.36	12.27	12.03	11.50	10.78	10.20	9.58	9.75	9.87	10.35	11.10	69.19	
64	11.38	10.86	9.96	9.14	8.40	7.86	7.86	7.86	8.34	9.30	10.46	11.44	13.10	12.54	11.68	10.56	9.64	9.08	8.82	9.16	9.88	10.74	11.70	70.21	
65	10.78	10.32	9.72	8.86	7.97	7.28	7.26	7.87	8.97	11.56	12.46	13.04	12.86	12.54	11.68	10.56	9.64	9.08	8.82	9.16	9.88	10.74	11.70	71.23	
66	11.14	10.07	8.84	7.56	6.74	6.70	7.63	8.94	10.62	12.06	13.78	13.68	12.86	11.34	9.88	8.86	8.16	8.03	8.46	9.64	10.86	12.06	12.78	71.23	
67	9.92	8.17	6.67	5.98	6.16	7.20	8.87	10.76	12.70	14.06	14.61	14.06	12.53	10.68	7.55	6.88	7.05	8.07	9.84	11.76	12.97	13.54	13.03	73.0	
68	9.42	7.27	5.74	5.30	7.44	9.66	11.92	14.02	15.17	15.16	13.87	11.66	9.44	7.56	6.34	6.07	8.68	10.80	12.96	14.26	14.55	13.37	11.16	8.45	74.2
69	6.26	5.16	5.12	6.24	8.10	10.63	13.22	15.15	15.86	15.17	13.22	10.40	7.86	6.06	5.25	5.54	6.90	9.24	11.72	13.95	15.12	13.39	10.64	5.44	75.4
Sum	747.71	694.17	689.93	694.26	690.35	720.01	732.20	740.10	786.83	800.63	807.04	784.97	769.73	769.60	745.63	768.17	759.58	795.97	821.34	832.74	823.49	803.67	804.80	763.37	No. of Days.
No.	75	73	74	75	74	75	74	73	75	74	75	73	74	75	74	75	74	73	74	75	74	73	75	74	18346.18
																									74 <sup>d</sup> 8 <sup>h</sup> .

FORMS FOR SHORT-PERIOD TIDES.  
SERIES 2N.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour d h	
70	4.44	4.96	6.46	8.94	11.85	14.34	16.00	16.06	11.64	8.54	5.76	4.22	3.97	5.24	7.30	10.10	13.02	15.04	16.00	15.20	12.86	10.54	8.67	4.92	4.38	76 6
71	5.53	7.55	10.33	13.50	15.75	16.73	16.07	13.60	10.42	7.22	3.64	4.00	5.66	8.33	11.52	14.30	16.06	16.52	15.06	12.13	8.73	6.13	4.66	6.52	4.99	77 8
72	8.92	11.86	14.66	16.40	16.56	15.07	11.90	8.47	5.62	3.74	3.22	4.26	9.60	12.85	15.23	16.56	16.25	14.26	10.83	8.00	5.75	5.11	5.88	7.84	78 9	
73	10.46	13.38	15.08	16.00	15.80	13.36	12.06	4.83	3.54	3.76	5.34	7.86	11.00	13.93	15.92	15.74	13.36	10.24	7.64	6.12	6.08	7.14	9.00	11.56	79 11	
74	13.90	15.06	15.98	14.76	12.06	6.13	4.34	3.62	4.36	6.06	8.47	11.31	13.87	15.62	16.12	14.97	12.74	10.02	6.96	7.06	7.93	9.67	12.07	14.08	80 13	
75	15.23	15.08	13.57	11.16	8.50	6.08	4.76	5.46	7.26	9.48	11.88	13.90	15.36	15.50	14.66	12.67	10.54	8.74	7.94	9.06	10.62	12.40	13.77	14.52	81 15	
76	14.20	13.80	10.64	8.47	6.76	5.86	5.82	6.49	7.75	11.71	13.54	14.73	14.98	14.06	12.63	11.05	9.70	8.86	8.72	9.12	10.24	11.76	13.06	13.60	82 17	
77	12.06	10.56	8.92	7.40	6.43	6.30	6.68	7.68	9.46	11.24	13.74	14.48	14.22	13.04	11.70	10.34	9.24	8.84	9.04	9.84	10.96	13.05	12.86	12.96	83 18	
78	11.22	9.67	8.30	7.06	6.48	6.64	7.48	8.86	10.64	12.34	13.74	14.48	14.44	13.62	12.12	10.36	8.96	7.46	8.44	9.76	11.26	12.36	12.92	12.78	84 20	
79	11.94	10.50	8.78	7.20	6.06	6.72	8.34	10.26	12.20	13.86	15.00	15.14	14.16	12.20	9.88	8.00	6.90	7.46	9.22	11.16	12.56	13.57	14.06	13.37	85 22	
80	11.72	9.38	7.17	5.72	5.38	6.17	10.00	12.50	14.54	15.84	15.94	14.64	12.14	9.36	6.97	5.63	6.90	7.46	9.22	11.16	12.56	13.57	14.06	13.37	86 22	
81	9.44	6.93	5.38	5.00	5.82	7.83	10.50	13.30	16.72	16.24	10.14	13.58	12.14	8.36	6.00	4.67	4.80	6.40	9.20	12.06	14.62	16.12	14.90	12.22	87 0	
82	6.60	5.05	4.86	5.87	8.10	11.14	14.15	16.35	17.15	16.24	10.14	13.58	12.14	8.36	6.00	4.67	4.80	6.40	9.20	12.06	14.62	16.12	14.90	12.22	88 2	
83	6.27	5.64	6.94	9.43	12.61	15.44	17.03	17.08	15.36	11.92	8.64	6.18	4.48	3.96	4.70	6.72	9.92	13.20	15.64	17.04	16.75	14.92	11.81	8.56	89 3	
84	5.42	6.12	7.87	13.66	16.10	17.14	16.46	13.96	10.44	7.12	4.04	3.84	4.41	3.96	4.70	6.72	9.92	13.20	15.64	17.04	16.75	14.92	11.81	8.56	90 5	
85	7.22	9.26	12.02	14.66	16.44	15.06	12.02	7.14	4.22	4.76	6.40	8.73	11.37	14.00	13.22	15.56	16.90	16.56	14.74	15.64	16.56	14.28	8.84	7.84	91 7	
86	10.50	13.00	14.94	15.83	15.12	12.94	9.87	5.16	5.22	6.16	9.97	12.30	14.30	15.48	15.46	14.27	13.24	13.10	10.40	8.36	7.32	8.03	9.50	11.53	93 11	
87	13.48	14.74	14.92	13.67	8.14	6.47	5.74	6.40	5.22	6.16	9.97	12.64	14.67	13.80	13.26	12.13	10.04	9.47	9.34	14.02	13.36	11.88	11.44	10.52	94 13	
88	14.16	13.84	12.97	10.16	8.14	6.47	5.74	6.40	5.22	6.16	9.97	12.64	14.67	13.80	13.26	12.13	10.04	9.47	9.34	14.02	13.36	11.88	11.44	10.52	95 14	
89	13.96	12.28	10.94	9.24	6.78	6.70	7.30	8.37	9.54	10.90	12.34	13.52	12.60	11.86	11.07	10.34	9.94	9.77	10.02	10.36	10.81	11.44	11.92	12.80	98 16	
90	11.54	10.36	9.16	8.12	7.47	7.87	8.52	9.46	10.73	11.93	12.98	12.40	11.96	11.34	10.55	9.91	9.47	9.34	9.52	9.94	10.53	11.14	11.27	10.92	97 18	
91	10.30	9.34	8.36	7.74	7.58	7.98	8.76	9.87	11.06	12.66	12.66	12.40	11.47	10.50	9.62	8.94	8.54	8.74	9.48	10.45	11.36	11.88	11.44	10.50	99 22	
92	10.00	9.22	8.40	8.01	8.13	8.63	9.70	10.66	11.77	13.06	12.94	12.40	11.47	10.50	9.62	8.94	8.54	8.74	9.48	10.45	11.36	11.88	11.44	10.50	99 22	
93	9.40	8.46	7.84	7.76	8.43	9.46	10.86	12.30	13.36	13.82	13.66	12.66	11.42	8.72	7.96	7.82	8.36	9.47	10.86	11.90	12.70	12.87	12.44	11.06	100 23	
94	9.52	7.40	7.47	8.26	9.54	11.08	12.70	14.06	14.56	14.22	12.80	12.66	10.82	8.88	7.46	6.84	6.81	7.92	11.52	13.00	13.97	14.12	13.00	11.02	9.05	102 1
95	7.48	6.74	6.92	7.92	11.72	13.58	14.86	15.12	14.21	12.35	9.67	7.47	5.98	5.58	6.14	7.76	9.84	12.16	15.18	15.06	13.40	10.95	8.28	6.66	103 3	
96	6.02	6.46	7.88	10.66	12.53	14.55	15.49	13.80	11.08	8.22	5.93	4.52	4.32	5.47	7.72	10.54	13.27	15.36	16.20	13.00	10.95	7.34	5.76	5.40	104 5	
97	6.24	8.22	10.70	13.40	15.52	16.25	15.36	12.80	9.16	6.56	4.47	3.42	3.91	5.74	8.31	11.40	14.40	16.28	16.72	15.47	12.68	9.44	6.81	5.47	105 7	
98	8.91	11.80	14.40	15.97	16.08	14.35	11.30	7.80	4.97	2.93	2.46	3.66	5.74	8.31	11.40	14.40	16.28	16.72	15.47	12.68	9.44	6.81	5.47	5.38	106 8	
99	10.07	15.40	16.44	15.82	13.44	9.74	6.67	4.03	2.50	2.77	4.44	7.50	10.96	16.70	17.72	16.91	14.37	10.87	8.10	6.15	5.71	6.50	8.36	11.33	107 10	
100	14.12	15.97	16.50	13.22	8.67	5.24	3.17	2.56	3.47	5.74	8.64	12.02	15.12	16.94	17.54	16.24	13.40	7.62	6.17	6.07	7.04	9.13	12.00	14.47	108 12	
101	15.69	15.54	13.66	10.74	7.44	4.88	3.04	4.36	6.67	9.40	12.47	15.00	16.74	16.94	15.60	13.03	10.01	7.87	6.76	6.80	7.71	9.70	13.14	14.15	109 14	
102	14.50	12.53	9.92	7.24	5.36	4.17	4.16	5.20	7.26	12.40	14.57	15.77	15.74	14.47	12.12	9.90	8.07	7.14	7.11	7.83	9.54	11.58	13.74	15.02	110 16	
103	11.76	9.56	7.60	5.96	4.93	5.02	5.86	7.52	9.74	12.00	14.87	14.77	13.76	12.56	10.26	8.74	7.82	7.54	8.00	9.34	11.00	12.36	12.96	11.56	111 18	
104	10.14	8.48	6.94	6.06	5.96	6.60	7.81	9.74	11.62	13.34	14.34	14.44	13.66	12.56	9.10	8.02	7.66	7.76	8.68	10.20	11.63	12.43	12.66	11.56	112 19	



FORMS FOR SHORT-PERIOD TIDES.  
SERIES 2 N.--(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour
139	13.60	14.03	14.27	13.22	10.78	8.10	5.76	4.37	4.17	7.20	9.70	12.28	14.46	15.94	16.04	14.86	12.64	10.27	8.44	7.54	7.34	8.10	11.55	13.36	150 11
140	14.27	13.92	13.06	9.48	6.90	5.12	4.32	4.97	6.54	8.70	11.00	15.32	16.07	15.67	14.17	11.77	9.56	8.16	7.68	7.83	8.74	10.50	12.26	14.02	151 13
141	13.96	10.86	8.34	6.24	5.04	4.82	5.84	7.60	9.46	11.87	14.10	15.30	15.60	12.78	10.74	9.03	7.96	7.73	8.24	9.44	11.07	12.62	13.44	13.16	152 14
142	11.96	9.94	7.67	5.18	5.16	6.86	8.64	10.66	12.74	14.30	15.12	15.06	11.08	11.84	10.00	8.46	7.78	8.46	9.92	11.36	12.37	12.84	12.22	10.98	153 10
143	9.18	7.32	6.03	5.94	6.87	9.67	11.58	13.28	14.64	14.97	14.22	12.62	9.20	8.47	8.38	8.08	8.30	9.20	10.24	12.12	12.46	11.72	10.38	8.77	154 18
144	7.37	6.70	6.91	7.78	8.83	10.30	11.90	13.54	14.80	13.77	12.16	10.50	8.20	8.37	9.12	9.23	10.10	10.93	11.70	11.97	11.72	11.06	9.20	8.14	155 20
145	7.72	7.83	8.62	9.82	11.10	12.64	13.94	14.46	14.16	11.74	10.42	9.26	8.54	8.34	8.46	8.60	9.36	10.36	11.26	11.83	11.56	10.60	9.98	8.86	156 22
146	8.36	9.00	10.04	11.54	12.92	13.86	14.25	13.85	12.88	11.48	10.08	8.98	8.20	8.37	9.12	10.03	11.29	12.14	12.58	12.36	11.84	11.02	10.06	9.23	157 23
147	8.78	9.20	11.08	13.44	14.22	14.34	13.94	12.86	11.59	10.03	8.74	7.92	8.20	8.37	9.12	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	9.64	159 1
148	10.17	11.38	12.77	13.98	14.67	14.88	13.86	12.46	10.48	8.82	7.82	7.50	8.19	9.46	11.28	13.22	14.76	15.82	14.97	13.34	11.70	10.27	10.56	10.56	160 3
149	11.52	12.90	14.12	15.30	15.65	15.48	14.17	9.86	8.00	7.09	6.85	7.72	9.34	11.40	13.77	15.84	16.86	16.85	15.70	13.66	9.95	9.55	9.80	10.84	161 5
150	12.57	14.21	15.47	16.06	15.22	13.50	10.84	8.22	6.16	5.15	6.50	8.61	11.37	14.18	16.48	17.54	17.17	15.60	12.50	10.07	8.34	8.17	10.27	12.23	162 7
151	14.14	15.74	16.29	15.33	12.77	9.46	6.32	4.44	3.62	4.30	6.30	11.95	15.02	17.28	17.95	17.20	15.02	11.76	9.04	7.44	7.22	7.81	9.55	12.08	163 8
152	14.54	16.21	14.76	11.87	8.16	5.07	3.07	2.74	3.80	5.94	9.24	12.80	15.92	18.07	17.65	14.65	10.17	8.00	6.62	6.55	7.50	9.65	12.45	14.89	164 10
153	16.40	16.14	14.28	7.10	4.31	2.62	2.37	3.68	6.30	9.76	13.48	16.44	18.12	18.40	17.00	13.80	10.17	6.20	6.18	7.30	9.60	12.79	15.16	16.42	165 12
154	15.96	13.80	10.33	6.77	4.00	2.33	4.18	7.11	10.40	13.95	16.74	17.85	17.95	16.07	12.81	9.60	7.05	5.72	5.77	7.00	9.56	15.12	16.05	15.26	166 14
155	12.76	9.20	6.14	3.95	2.88	3.47	5.52	7.93	14.21	16.44	17.72	17.40	15.44	12.07	9.02	6.70	5.67	5.93	7.41	10.07	13.02	15.57	14.68	12.28	167 16
156	9.20	6.52	4.77	4.20	4.94	6.52	8.80	11.67	14.34	16.42	17.20	16.60	11.30	8.66	6.74	6.05	6.16	7.65	10.05	12.50	14.32	14.85	14.05	11.96	168 17
157	9.47	6.06	5.80	6.39	7.66	9.64	11.92	14.25	15.90	16.46	15.74	14.54	10.84	8.66	6.32	6.58	7.80	9.81	12.04	13.55	14.17	13.54	12.03	10.34	169 19
158	8.60	7.57	7.63	8.44	9.92	12.12	14.20	15.46	15.54	14.58	12.66	10.40	8.31	7.04	6.60	6.77	7.78	11.22	12.80	13.58	13.46	12.40	10.67	9.60	171 23
159	8.66	8.31	8.49	9.03	10.30	12.04	14.74	14.75	13.73	12.02	10.10	8.46	7.12	6.53	6.70	7.50	9.06	10.86	12.50	13.66	14.10	13.63	11.06	10.67	173 1
160	8.94	8.82	9.24	10.33	11.90	13.24	14.06	14.10	13.34	11.84	10.05	8.26	6.44	6.67	7.40	9.06	10.86	12.50	13.22	13.58	12.92	11.94	10.67	9.30	173 1
161	9.05	9.31	10.22	11.60	12.90	13.82	13.85	13.08	11.64	9.76	8.00	6.08	6.22	7.28	8.00	10.39	13.25	14.45	14.84	13.99	12.40	10.90	10.67	9.14	174 3
162	9.05	10.08	11.26	12.44	13.30	13.52	12.80	11.00	8.85	7.06	5.67	5.05	5.60	7.15	8.00	10.50	12.77	14.05	14.65	14.17	12.86	11.33	10.04	8.80	174 3
163	8.56	9.64	11.12	13.40	13.37	13.03	9.17	6.76	5.11	4.64	4.74	5.62	6.44	7.67	8.40	10.40	12.77	14.05	13.99	12.40	10.90	9.46	8.62	8.24	175 4
164	9.68	11.18	12.64	13.37	13.52	11.52	9.17	6.76	5.11	4.64	4.74	5.62	6.44	7.67	8.40	10.40	12.77	14.05	13.99	12.40	10.90	9.46	8.62	8.24	175 4
165	11.65	13.20	13.60	12.56	10.40	7.97	5.83	4.04	4.96	6.82	9.02	11.57	13.86	15.24	15.44	14.56	12.56	10.36	8.63	7.62	7.74	7.90	10.67	9.30	178 10
166	13.67	13.60	12.02	9.66	6.93	4.96	3.94	4.22	5.70	7.84	12.82	14.74	15.46	12.44	9.96	8.16	6.86	6.42	6.94	8.42	10.44	12.57	13.67	13.68	180 13
167	13.00	10.74	8.00	5.64	4.04	3.83	4.76	6.70	9.02	11.37	13.67	15.12	15.46	12.44	9.96	8.16	6.86	6.42	6.94	8.42	10.44	12.57	13.67	13.68	180 13
168	12.22	8.64	6.64	4.96	3.98	4.36	5.65	7.72	10.02	12.26	14.31	15.28	15.12	13.77	11.30	9.01	6.64	6.56	7.46	9.06	11.01	12.70	13.01	11.07	181 15
169	8.44	6.12	4.72	4.42	6.94	8.97	11.17	13.22	14.74	15.17	14.22	12.16	13.77	11.30	9.01	6.64	6.56	7.46	9.06	11.01	12.70	13.01	11.07	11.07	181 15
170	5.70	5.02	5.24	6.42	8.07	10.12	13.75	14.86	14.72	13.40	11.17	9.22	7.55	6.51	6.57	7.34	8.72	10.61	11.66	12.82	13.10	11.86	9.72	7.36	182 17
171	5.97	6.54	7.66	9.24	10.97	12.94	14.38	14.88	14.20	10.34	8.44	7.22	6.77	6.97	7.87	9.34	10.94	12.10	12.66	12.32	10.84	9.35	7.48	6.30	183 19
172	7.56	8.50	10.00	11.48	13.23	14.36	14.44	13.38	11.42	9.60	8.02	6.94	6.92	7.70	9.26	10.80	11.02	12.33	12.16	11.12	9.70	8.48	7.63	7.56	185 22
173	8.14	10.41	11.98	13.30	13.98	13.72	12.51	10.84	8.96	7.47	6.70	6.48	6.84	7.86	9.16	10.52	11.71	12.36	11.46	10.38	9.16	8.34	8.14	8.38	187 0



FORMS FOR SHORT-PERIOD TIDES.

SERIES 2N.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour d A		
208	9.10	5.80	3.36	3.32	4.58	7.04	10.14	13.35	16.16	17.52	17.26	15.28	13.32	9.36	6.05	4.18	3.80	4.90	7.56	11.10	14.46	16.66	16.88	15.39	12.15	8.23	224 16
209	5.44	3.52	3.32	4.80	6.25	8.27	11.00	13.96	16.32	17.26	16.42	14.32	10.85	5.16	4.64	5.58	8.92	12.05	14.70	15.80	16.18	16.06	14.38	11.26	7.98	225 17	
210	5.62	4.80	6.25	8.27	11.00	13.96	16.32	17.26	16.42	14.32	10.85	5.16	4.64	5.58	8.92	12.05	14.70	15.80	16.18	16.06	14.38	11.26	7.94	6.32	226 19		
211	4.54	6.44	7.77	13.07	14.12	15.66	15.72	14.46	12.06	9.36	6.96	5.40	5.07	8.84	7.33	9.54	11.87	13.60	14.46	13.96	12.48	10.40	8.65	7.45	227 21		
212	8.00	9.26	10.72	12.27	13.74	14.18	12.78	10.82	8.17	6.68	5.83	5.86	6.74	8.34	10.14	12.02	13.26	13.37	12.85	10.70	9.74	9.12	8.90	9.34	228 23		
213	10.06	10.94	12.10	12.88	13.72	13.38	11.88	10.06	8.64	7.77	7.69	7.70	8.77	10.10	11.44	12.33	12.66	12.46	12.00	11.36	10.62	10.07	9.77	10.12	230 1		
214	10.82	11.54	12.43	12.67	12.12	11.23	9.96	8.35	7.66	7.57	8.12	9.04	10.10	11.17	12.34	12.90	13.18	12.30	11.45	10.72	10.26	9.92	9.63	10.00	232 4		
215	11.34	11.96	12.26	11.97	11.38	10.53	9.44	8.35	7.53	7.24	8.54	9.82	10.48	11.57	13.42	13.56	13.66	12.36	11.22	10.18	9.34	8.97	9.88	10.76	233 6		
216	10.71	11.62	12.18	11.42	10.36	9.08	8.15	7.53	7.14	8.30	10.20	11.94	13.38	14.40	14.54	13.58	12.17	10.70	9.34	8.84	8.26	10.00	11.16	12.50	234 8		
217	11.64	12.26	12.35	11.85	10.40	7.36	6.44	6.18	6.14	8.95	10.80	13.96	14.91	14.84	13.64	11.84	9.97	8.77	8.36	8.48	8.06	11.56	13.12	13.97	235 10		
218	13.30	13.42	12.06	10.16	8.40	6.86	6.06	6.06	9.76	11.70	13.66	15.46	14.62	12.86	10.57	8.64	7.46	7.31	7.76	8.84	10.72	12.64	14.21	14.62	236 12		
219	13.64	12.06	9.70	7.27	5.96	5.56	6.35	7.80	9.76	11.70	15.10	15.46	14.08	12.86	10.57	8.64	7.46	7.31	7.76	8.84	10.72	12.64	14.21	14.62	237 13		
220	11.00	8.24	6.24	5.17	5.36	6.54	8.54	10.66	13.00	15.02	15.96	15.50	14.08	12.72	10.57	8.64	7.46	7.31	7.76	8.84	10.72	12.64	14.21	14.62	238 15		
221	10.00	7.37	4.97	5.74	7.38	9.36	11.94	14.36	16.04	16.27	15.32	13.08	10.11	7.72	6.36	6.94	9.22	11.84	15.71	15.48	13.64	10.66	7.60	5.70	239 17		
222	6.16	4.97	5.06	6.36	10.64	14.56	16.24	16.56	14.06	11.04	6.11	5.05	5.64	7.12	9.24	11.64	13.77	15.36	15.38	14.00	11.50	8.72	6.86	5.74	240 19		
223	4.96	5.70	7.24	9.34	12.02	14.56	16.24	16.56	14.06	11.04	6.11	5.05	5.64	7.12	9.24	11.64	13.77	15.36	15.38	14.00	11.50	8.72	6.86	5.74	241 21		
224	6.67	8.36	10.62	13.17	15.30	16.38	15.97	14.06	11.04	6.11	5.05	5.64	7.12	9.24	11.64	13.77	15.36	15.38	14.00	11.50	8.72	6.86	5.74	7.52	242 22		
225	9.30	11.47	13.80	15.46	15.84	14.77	12.44	9.37	7.06	5.38	6.34	7.85	9.86	11.96	14.07	14.97	12.68	10.68	8.97	8.02	7.81	8.36	9.26	10.60	244 0		
226	10.38	12.36	15.24	15.10	13.64	11.26	8.61	6.50	5.32	5.78	6.47	7.80	9.63	11.38	12.97	13.74	13.44	11.04	9.83	8.84	8.57	8.87	9.67	10.67	245 2		
227	12.24	13.73	14.44	13.86	10.02	8.06	6.46	5.62	5.78	6.47	7.80	9.63	11.38	12.97	13.74	13.44	11.04	9.83	8.84	8.57	8.87	9.67	10.67	11.96	246 4		
228	13.06	13.46	13.08	11.68	9.86	8.26	6.17	6.26	7.02	8.17	9.66	11.26	12.55	13.37	13.57	12.94	11.92	10.73	9.67	9.18	9.63	10.54	11.48	12.46	248 6		
229	12.92	12.66	11.74	10.42	8.87	7.44	6.44	6.21	6.66	9.20	10.76	12.36	13.54	14.05	13.67	12.68	11.26	10.02	9.22	8.90	9.14	9.86	12.02	12.84	247 6		
230	12.98	12.36	11.16	9.57	7.60	6.24	5.63	5.97	7.17	8.80	10.66	12.80	14.96	14.74	13.66	11.85	10.04	8.66	8.02	8.14	9.04	10.38	12.00	13.14	248 7		
231	13.74	12.04	10.04	7.64	5.76	4.78	5.02	6.24	8.16	10.78	13.20	15.04	15.98	15.74	14.33	11.96	9.30	7.37	6.55	6.70	8.06	9.98	12.06	13.93	14.86	249 9	
232	14.44	12.80	7.37	5.17	3.90	4.03	5.50	7.96	10.88	13.80	16.04	17.04	16.46	14.44	11.04	8.24	5.15	5.63	7.24	9.64	12.52	14.74	15.98	15.46	250 11		
233	13.29	9.94	6.63	4.34	3.17	5.38	8.20	11.40	14.56	16.82	17.44	16.36	13.83	9.98	6.70	4.46	3.84	4.58	6.80	9.38	13.28	15.76	16.64	15.75	12.94	251 13	
234	9.26	6.06	3.66	2.67	3.72	5.66	8.70	12.20	15.33	17.53	15.87	12.42	8.56	5.32	3.44	3.17	4.55	7.26	10.87	14.22	16.50	17.05	13.37	8.44	252 15		
235	5.52	3.48	3.10	4.46	6.74	9.94	13.47	16.22	17.47	17.02	14.77	10.84	7.23	3.70	3.94	6.16	9.36	12.43	15.42	16.86	16.10	13.81	10.56	5.47	254 18		
236	3.90	4.20	5.52	7.95	11.06	14.30	16.51	17.04	15.88	12.99	9.17	5.97	3.92	5.16	7.43	10.36	12.43	15.42	16.86	16.10	13.81	10.56	7.46	6.47	256 20		
237	4.87	5.60	7.04	12.25	14.81	16.16	16.06	14.44	11.07	7.87	5.34	4.44	5.02	6.44	8.50	11.04	13.88	16.04	14.92	12.66	9.98	7.74	6.47	7.36	255 20		
238	7.02	8.34	10.55	12.80	14.58	15.36	14.73	12.52	9.86	7.17	5.31	4.44	5.02	6.44	8.50	11.04	13.88	16.04	14.92	12.66	9.98	7.74	6.47	7.36	256 22		
239	9.51	11.10	12.60	13.73	13.94	13.90	11.02	8.73	5.70	5.63	6.34	7.60	9.36	11.36	13.14	13.88	13.60	12.43	10.94	9.64	8.76	8.70	9.18	9.58	258 0		
240	10.88	12.06	12.76	12.71	11.64	9.87	8.26	7.04	6.67	8.36	9.74	11.16	12.22	12.70	12.20	11.38	10.60	9.88	9.34	9.16	9.13	9.34	9.87	10.66	259 2		
241	11.30	11.62	11.37	10.56	9.48	8.44	7.52	7.14	7.34	7.86	8.66	9.84	10.90	11.97	11.87	11.54	11.08	10.42	9.92	9.60	9.42	9.54	9.86	10.34	260 3		
242	10.70	10.91	10.34	9.74	9.06	8.35	7.72	7.46	7.67	8.44	9.64	10.73	11.52	11.88	12.06	11.53	10.97	10.23	9.48	9.04	9.01	9.38	10.01	10.64	261 5		

243	11.05	11.18	10.94	10.46	8.56	7.74	7.42	7.64	8.34	9.42	10.67	11.65	12.46	12.82	12.62	12.04	10.96	8.96	8.54	8.42	8.86	9.64	10.44	10.44	11.23	262	7
244	11.67	11.60	10.92	9.74	8.36	7.74	6.86	7.74	9.24	10.86	12.34	13.24	13.55	13.17	12.08	10.64	9.21	8.06	7.54	7.74	7.74	9.92	11.30	12.38	12.82	263	9
245	12.42	11.17	9.62	7.86	6.55	6.10	6.54	7.88	11.56	13.16	14.03	14.06	13.18	11.60	9.86	8.07	6.97	6.64	7.14	8.38	10.20	11.92	13.16	13.44	12.50	264	11
246	10.70	8.70	6.90	5.75	5.50	6.30	8.04	10.20	12.32	13.87	14.64	14.36	10.73	8.45	6.71	5.90	6.17	7.29	9.02	11.07	13.02	14.14	14.04	12.68	265	12	
247	10.35	6.07	5.14	5.48	6.87	9.06	11.46	13.68	15.18	15.37	14.28	12.24	9.67	7.34	5.30	6.12	7.84	9.97	12.54	14.50	15.33	14.46	12.23	9.34	266	13	
248	7.96	5.36	4.94	8.06	10.08	12.62	14.76	15.76	15.26	13.46	10.67	7.88	5.74	4.48	4.66	6.00	8.44	13.97	15.67	15.66	14.20	11.46	8.47	6.20	267	16	
249	4.97	5.22	6.65	8.86	11.51	15.76	16.07	14.86	12.14	9.06	6.37	4.56	3.93	4.93	6.93	9.67	12.77	15.34	16.35	15.80	10.52	7.73	5.58	4.88	268	18	
250	5.77	7.56	10.04	12.74	14.96	15.94	15.62	13.71	7.47	5.10	3.54	3.83	5.50	7.97	11.14	14.16	16.01	16.37	15.04	13.33	9.34	6.97	5.42	6.51	269	20	
251	8.50	11.14	13.77	15.60	15.98	14.86	12.14	8.87	6.16	4.30	3.67	6.44	9.03	12.27	14.84	16.21	15.96	14.09	11.42	8.56	6.75	5.80	6.17	7.42	270	21	
252	9.65	14.26	15.46	15.24	13.48	10.57	7.65	5.42	3.96	4.06	5.34	7.30	9.97	12.69	15.87	15.16	13.24	10.76	8.47	7.04	6.68	7.20	8.44	10.38	271	23	
253	12.22	14.16	14.85	12.07	9.24	7.02	5.32	4.44	4.61	5.87	7.97	10.37	13.07	14.81	15.06	12.37	10.44	8.86	7.87	7.56	7.92	8.94	10.67	12.44	273	1	
254	13.74	13.97	12.81	10.83	8.83	7.10	5.25	5.76	6.66	8.34	10.76	12.86	14.16	14.44	13.68	12.40	10.86	9.52	8.21	8.56	9.40	10.68	12.08	13.04	274	3	
255	13.08	11.93	10.54	9.05	7.64	6.61	6.06	6.30	8.81	10.63	12.30	13.92	13.88	13.56	12.37	11.18	9.72	8.32	7.60	7.94	9.26	10.84	12.04	13.61	275	5	
256	12.14	11.16	9.92	8.44	7.14	6.37	6.38	7.34	8.76	10.57	13.44	14.17	14.52	13.27	11.31	9.06	7.37	6.82	7.46	8.74	10.60	12.11	13.20	14.04	277	8	
257	11.98	11.16	9.77	7.94	6.58	6.06	6.50	7.97	9.84	11.56	15.26	15.99	15.54	13.97	11.26	8.63	5.98	6.37	7.97	10.25	12.66	14.44	15.38	15.04	278	10	
258	13.84	12.76	8.58	6.74	5.94	6.30	7.68	9.72	11.97	13.90	16.98	16.37	13.80	10.49	7.50	5.61	5.14	5.74	10.54	13.45	15.71	16.85	16.30	14.16	279	12	
259	13.48	11.07	8.36	6.38	5.87	7.50	9.87	12.14	14.54	16.28	15.62	12.54	8.66	5.94	4.14	3.96	5.28	7.85	11.15	14.38	16.70	16.33	13.48	9.84	280	14	
260	10.84	7.77	5.85	5.07	5.66	7.50	12.74	16.26	17.40	14.56	10.89	7.40	4.72	3.37	3.98	5.86	8.86	12.43	15.47	17.34	17.64	16.26	9.26	6.56	281	16	
261	7.20	5.47	4.98	5.96	7.74	10.58	13.66	16.26	17.40	14.56	9.14	3.77	3.12	3.62	5.50	8.04	14.40	16.24	17.22	16.16	13.58	10.36	8.40	6.36	282	17	
262	5.44	5.38	6.54	8.77	11.76	14.62	16.82	17.12	15.72	12.71	4.80	4.52	4.32	3.62	5.90	11.13	14.40	16.50	17.22	16.16	13.58	10.36	7.77	6.24	6.04	283	19
263	5.44	6.06	7.47	10.01	12.74	15.12	16.37	16.06	14.21	11.04	7.42	4.80	3.77	3.17	4.42	6.67	9.72	13.44	16.25	17.55	17.22	15.06	11.70	8.40	6.36	282	17
264	6.91	8.53	10.32	13.02	15.02	15.64	14.36	11.93	8.64	6.01	3.47	4.52	4.32	3.62	5.90	11.13	14.40	16.50	17.22	16.16	13.58	10.36	7.77	6.24	6.04	283	19
265	9.30	11.26	13.26	14.41	14.26	12.74	7.88	5.80	4.44	4.38	5.92	7.85	10.30	12.70	14.67	15.54	15.01	13.36	11.14	7.80	7.42	7.74	8.64	10.04	285	23	
266	11.80	13.04	13.64	13.06	11.36	9.07	7.14	5.84	5.47	7.44	9.04	10.97	13.06	14.36	14.36	13.40	11.82	10.44	9.16	8.44	8.24	9.36	10.30	11.46	287	1	
267	12.12	12.22	11.46	10.00	8.37	7.08	6.36	6.44	7.32	8.34	9.60	11.24	13.46	13.28	12.32	11.04	10.37	9.76	9.36	9.12	9.08	9.86	10.44	10.68	289	4	
268	11.52	10.73	9.32	8.47	7.66	7.41	7.56	8.04	8.76	9.91	11.17	12.72	12.88	12.66	11.92	11.04	10.37	9.76	9.36	9.12	9.08	9.86	10.44	10.68	289	4	
269	10.66	10.30	9.22	8.56	8.06	7.74	8.02	8.86	10.06	11.16	12.02	12.40	12.34	12.06	11.48	10.82	9.97	9.77	8.68	8.96	9.55	10.22	10.70	10.88	290	6	
270	10.82	10.57	10.03	9.26	8.44	8.07	8.80	9.84	10.90	11.78	12.36	12.58	12.54	12.07	11.12	9.97	8.90	8.23	8.12	9.27	10.10	10.90	11.50	11.78	291	8	
271	11.53	10.67	9.30	8.14	7.56	7.77	8.55	11.07	12.15	12.94	13.28	13.04	12.24	10.77	9.14	7.88	7.18	7.36	8.12	9.26	10.62	11.94	12.88	13.06	292	10	
272	10.48	8.86	7.70	7.28	7.65	8.65	10.02	11.54	12.81	13.77	13.50	12.16	10.00	8.34	6.96	6.50	6.88	7.96	9.76	11.52	13.07	13.96	13.77	12.48	293	12	
273	8.76	7.36	6.77	7.26	8.32	10.36	12.17	13.66	14.56	14.48	13.40	11.12	6.84	5.64	5.46	6.30	8.06	10.30	12.80	14.34	15.00	14.16	12.26	9.96	294	13	
274	7.92	6.50	6.22	8.82	10.86	13.12	14.54	15.07	14.56	12.60	9.98	7.47	5.46	4.56	4.96	6.03	8.06	10.30	12.80	14.34	15.00	14.16	12.26	9.96	294	13	
275	6.16	6.40	7.67	9.66	11.93	15.62	15.76	14.36	11.76	8.61	6.02	4.24	3.86	5.14	7.32	10.15	13.10	15.67	16.56	14.16	11.00	8.32	6.36	5.84	296	17	
276	6.47	8.16	10.16	12.84	15.02	16.10	15.46	13.28	9.87	3.04	3.57	3.57	5.44	8.15	11.37	14.60	16.81	17.35	16.28	13.64	7.71	6.07	5.84	6.88	297	19	
Sum	75.25	709.21	714.11	715.11	718.09	748.25	757.39	774.00	777.74	748.74	771.49	753.66	733.03	746.95	729.65	772.71	800.69	815.81	817.37	814.37	829.91	813.02	776.11	749.42	No. of Days.		
No.	74	74	75	74	73	75	74	75	75	72	75	75	74	75	72	75	75	74	74	73	75	75	74	74	74	74	18308.08

FORMS FOR SHORT-PERIOD TIDES.

SERIES 2N.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
277	8.87	11.47	14.12	15.94	16.22	14.81	11.87	8.55	5.46	3.46 2.87	4.17	6.35	9.32	13.00	15.95	17.47	17.44	15.72	12.68	9.66	7.28	5.94	6.04 7.36	9.64	298 21	
278	12.45	14.84	16.04	15.60	13.70	10.52	7.15	4.66	2.92	3.10	4.72	7.47	10.55 13.92	16.35	17.36	16.74	14.57	11.67	8.85	6.76	5.94	6.28	7.70	9.92	299 22	
279	12.68	14.78 15.58	14.78	12.36	9.26	6.36	4.20	3.07	3.72	5.55	8.04	11.05	14.10	16.17	16.96 16.12	14.06	11.35	8.82	7.14	6.57	7.02	8.46	10.56	13.14	301 0	
280	14.64	15.04	13.76	11.47 8.74	6.42	4.70	4.22	5.00	6.80	9.02	11.88	14.60	16.14	16.22	15.16	13.26	10.86	8.86 7.58	7.14	7.44	8.84	10.92	12.84	13.84	302 2	
281	13.86	12.57	10.68	8.54	6.84	5.56	5.27 5.98	7.33	9.36	11.72	14.00	15.22	15.38	14.58	12.88	11.01	9.42	8.12	7.64	7.92 8.94	10.40	11.85	12.91	13.12	303 4	
282	12.26	10.75	9.22	7.66	6.68	6.30	6.72	7.86	9.44	11.50 13.34	14.46	14.66	13.96	12.74	11.30	9.76	8.54	7.93	7.84	8.40	9.60	10.88	12.64	12.40	304 6	
283	11.47	10.10	8.76	7.68	7.01	7.06	7.90	9.22	10.97	12.56	13.72	14.04	13.04	11.45	9.76	8.15	7.22	7.02	7.48	8.84	10.32	11.48	12.55	12.87	305 7	
284	12.46 11.36	9.70	8.28	7.14	6.80	7.40	8.84	10.74	12.56	13.87	14.54	14.38	13.40	11.67	9.60	6.30	5.88	6.50	8.20	10.07	11.93	13.36	14.04	13.66	306 9	
285	12.30	10.26	8.61	7.37 6.86	7.24	8.35	10.36	12.50	14.13	15.08	14.96	13.80	11.64	9.03	6.96	5.44	5.04 5.86	7.79	10.12	12.66	14.54	15.37	14.86	13.04	307 11	
286	10.66	8.56	7.12	6.44	6.77	10.14	12.62	14.56	15.55	15.25	13.56	10.92	8.12	5.82	4.22	4.10	5.32	7.70	10.85	16.05	15.06	12.86	10.40	308 18		
287	8.16	6.53	5.96	6.51	8.24	10.85	13.27	15.16	15.84 15.03	12.98	9.78	7.04	4.71	3.46	3.86	5.60	8.44	11.74	14.64	16.50	16.72	12.86	9.98	7.70	309 15	
288	6.25	5.93	6.71	8.67	11.25	13.84	15.52	15.84	14.55	11.68	8.46	5.64	3.63	3.01	4.08	6.50	9.62	13.08	15.81	17.12	16.72	14.87	12.03	9.20	7.26	310 16
289	6.32 6.37	7.46	9.60	12.20	14.35	15.67	15.28	13.15	10.15	7.00	4.47	3.03	3.22	5.03 7.60	10.76	14.05	16.38	17.05	16.14	13.92	11.10	8.66	6.87	6.16	311 18	
290	6.46	8.00	10.44 13.10	14.76	15.16	13.92	11.40	8.36	5.66	3.69	2.94	3.94	6.18	9.01	12.24	16.53	16.56	15.16	12.66	10.06	7.96	6.74	6.60	7.35	312 20	
291	9.00	11.24	13.43	14.50	14.36	12.66 9.94	7.20	4.97	3.56	3.77	5.34	7.72	10.56	13.46	15.64	16.34	15.71	13.92	7.66	6.86	6.88	7.98	9.16	10.68	12.24	315 0
292	12.00	13.52	14.02	13.37	11.18	8.81	6.52	4.86 4.33	5.20	6.90	9.14	11.80	14.20	15.72	15.81	14.66	12.72	10.71	8.96	7.82	7.56 7.92	9.16	10.68	12.24	316 0	
293	13.26	13.26	12.06	10.17	8.00	6.25	5.31	5.50	6.66	8.34	10.52 12.80	14.44	15.18	14.68	13.32	11.56	10.02	8.76	8.10	8.00	8.60	9.65	10.96	12.18 12.58	316 2	
294	12.23	11.04	9.16	7.62	6.54	6.20	6.84	7.96	9.38	11.14	12.91	14.18	14.40 13.64	12.37	10.90	9.58	8.78	8.46	8.68	9.38	10.00	10.94	11.57	11.80	317 3	
295	11.36	10.28 8.94	7.84	7.18	7.20	7.86	8.80	9.98	11.46	12.86	13.86	13.83	12.96	11.72	10.53	9.66 9.14	8.92	8.96	9.17	9.66	10.40	11.10	11.37	11.01	318 5	
296	10.20	9.26	8.46	8.10	8.14 8.66	9.44	10.56	11.74	12.76	13.34	13.26	12.61	11.72	10.86	9.76	9.04	8.80	8.85 9.16	9.64	10.14	10.74	11.18	11.32	11.06	319 7	
297	10.38	9.58	8.94	8.71	8.90	9.50	10.42 11.46	12.48	13.10	13.15	12.64	11.84	10.76	9.71	8.88	8.35	8.19	8.42	9.04	9.96	10.86 11.50	11.80	11.55	10.96	320 9	
298	9.98	9.08	8.64	8.75	9.38	10.38	11.46	12.41	13.07	13.16 12.84	11.84	10.56	9.24	8.13	7.50	7.43	7.86	8.83	10.03	11.16	12.23	12.80	12.64 11.66	10.25	321 11	
299	9.04	8.36	8.34	8.96	10.02	11.20	12.46	13.23	13.47	13.00	11.72	10.14 8.38	7.03	6.27	6.31	7.08	8.52	10.23	11.92	13.17	13.63	13.10	11.86	10.18	322 12	
300	8.76	7.98 7.96	8.75	10.13	11.64	13.14	13.94	13.94	13.04	11.34	9.30	7.45	5.86	5.13	5.46 6.76	8.80	11.15	13.20	14.66	14.98	13.87	11.76	9.58	8.10	323 14	
301	7.27	7.36	8.22	9.82 9.76	13.33	14.28	14.14	12.87	10.56	7.98	5.77	4.14	3.74	4.67	6.71	9.27	12.02 14.40	15.66	15.44	13.71	11.16	8.74	7.02	6.40	324 16	
302	6.78	8.22	10.37	12.25	13.88	14.74	14.20 12.26	9.36	6.51	4.12	2.75	2.94	4.56	7.03	10.05	13.27	15.65	16.62	15.90	13.76 10.86	8.17	6.45	5.84	6.36	325 18	
303	8.12	10.44	12.84	14.46	15.08	13.97	11.41	8.07	4.96 2.57	1.63	2.58	4.74	7.64	11.12	14.22	16.47	17.07	15.75	12.96	9.86	7.26	5.65 5.46	6.44	8.40	326 20	
304	11.20	13.57	15.11	15.17	13.27	9.96	6.40	3.62	1.76	1.54	3.26	6.02 9.25	12.97	15.66	17.40	17.25	15.37	12.23	9.00	6.75	5.63	5.63	6.88	9.32	327 21	
305	12.22 14.44	15.50	14.80	12.31	8.84	5.46	3.00	1.66	2.20	4.15	6.95	10.46	13.81	16.44 17.54	16.82	14.56	11.38	8.50	6.32	5.44	5.74	7.26	10.06	12.76	328 23	
306	14.67	15.26	14.06 11.32	8.05	5.16	2.94	2.16	3.11	5.16	7.96	11.23	14.30	16.57	17.22	16.23	13.81	10.68 8.07	6.16	5.50	5.88	7.64	10.25	12.77	14.29	330 1	
307	14.72	13.33	10.74	7.81	5.32	3.66 3.26	4.42	6.34	8.86	11.67	14.58	16.33	16.57	15.28	12.84	9.93	7.47	6.23	5.72 6.26	7.94	10.30	12.38	13.76	13.96	331 3	
308	12.68	10.56	8.18	6.28	4.97	4.83	5.73	7.34 9.38	12.05	14.37	15.76	15.80	14.56	12.28	9.94	8.13	6.64	6.14	6.54	8.04	10.04	12.86	13.16	12.24	332 5	
309	10.73	8.96	7.30	6.24	5.96	6.50	7.80	9.84	12.15	13.88	14.87 14.84	13.77	11.77	10.06	8.23	6.86	6.34	6.56	7.70	9.30	10.84	12.16	12.76	12.53 11.48	333 7	
310	10.14	8.60	7.52	7.06	7.44	8.47	10.17	11.91	13.34	14.21	14.40	13.72	12.30 10.42	8.41	6.88	6.14	6.37	7.32	8.81	10.45	11.84	12.86	13.08	12.42	334 8	
311	11.25	9.75	8.54 7.84	7.88	8.64	10.02	11.65	13.16	14.14	14.30	13.64	12.17	10.31	8.37	6.68	5.72 5.86	6.88	8.64	10.40	12.07	13.31	13.88	13.62	12.36	335 10	

TIDAL OBSERVATIONS.

[CONT. VII.]



312	10.67	9.06	8.12	7.90	8.54	11.26	12.78	13.82	14.20	13.74	12.14	10.95	7.76	6.00	5.04	5.23	6.52	8.50	12.60	14.12	14.40	13.86	12.58	10.80	386 12	
313	8.97	7.94	7.68	8.24	9.30	11.14	12.75	13.98	13.73	11.85	9.10	6.84	5.06	4.41	5.04	6.37	8.66	10.56	13.52	15.24	15.84	13.13	10.86	9.00	387 14	
314	7.82	7.54	8.05	9.36	11.14	12.94	14.20	14.46	13.36	11.28	5.98	4.22	3.96	5.07	6.97	9.54	12.26	14.34	16.11	16.34	15.17	12.88	10.26	8.38	388 16	
315	7.40	8.14	9.77	11.52	13.36	14.60	14.56	12.94	10.26	7.33	5.11	3.87	4.95	7.81	10.61	13.20	15.47	16.84	16.21	14.70	12.20	9.81	8.08	7.33	389 17	
316	7.37	10.05	8.34	12.02	13.86	14.76	14.17	12.16	8.93	6.32	4.31	3.72	4.64	6.56	10.34	16.56	16.48	13.72	10.27	8.26	7.37	7.26	8.12	9.82	341 21	
317	9.02	10.97	12.94	14.40	14.70	13.44	6.72	3.96	4.74	6.03	10.34	15.95	16.23	16.28	14.89	12.63	10.30	8.54	7.57	7.44	8.17	9.64	11.50	13.80	344 1	
318	11.91	13.58	14.48	14.97	12.12	9.32	4.74	3.96	4.74	6.03	10.34	15.95	16.23	16.28	14.89	12.63	10.30	8.54	7.57	7.44	8.17	9.64	11.50	13.80	345 2	
319	14.00	14.24	13.24	10.72	8.06	5.93	4.58	4.74	6.03	10.34	15.95	16.23	16.28	14.89	12.63	10.30	8.54	7.57	7.44	8.17	9.64	11.50	13.80	11.15	346 4	
320	13.45	11.78	9.47	7.26	5.64	5.07	5.86	7.43	9.20	11.34	12.88	15.95	15.18	13.58	11.42	9.46	7.98	7.36	8.82	10.22	11.48	12.26	10.84	9.56	347 6	
321	12.14	8.34	6.54	5.59	5.67	6.77	8.43	10.27	12.17	13.90	14.96	15.87	13.76	12.00	8.66	7.73	7.38	7.80	8.82	10.22	11.48	12.26	10.84	9.56	348 8	
322	9.47	8.01	6.87	6.45	7.83	9.14	10.75	12.56	13.86	14.46	14.06	12.87	11.31	9.72	8.40	7.76	8.24	8.80	9.61	11.27	11.62	11.14	10.38	9.49	349 10	
323	8.46	7.76	7.56	8.00	8.95	11.00	13.13	14.20	14.42	13.83	12.50	10.98	9.76	8.76	8.24	8.24	8.80	9.61	11.27	11.62	11.14	10.38	9.49	348 8		
324	8.78	8.48	8.71	9.47	10.70	12.04	13.16	13.57	13.38	12.64	11.55	8.86	7.83	7.22	7.36	7.86	8.85	10.11	11.13	11.95	12.42	12.30	11.78	9.72	350 11	
325	9.04	9.10	9.74	10.90	12.24	13.16	13.38	13.14	12.44	11.22	9.78	8.36	7.04	6.26	6.15	8.20	9.97	11.56	12.90	13.50	13.36	12.36	10.92	9.68	8.84	351 13
326	9.06	9.55	10.76	11.97	12.94	13.38	13.14	12.44	11.22	9.78	8.36	7.04	6.26	6.15	8.20	9.97	11.56	12.90	13.50	13.36	12.36	10.92	9.68	8.84	351 13	
327	8.68	9.14	10.18	12.74	13.42	12.54	13.45	10.80	8.50	6.30	4.47	3.64	4.12	5.82	8.20	10.84	13.27	14.95	15.70	14.97	10.60	8.64	7.50	7.36	8.16	353 17
328	8.23	9.70	11.40	12.74	13.42	12.54	13.45	10.80	8.50	6.30	4.47	3.64	4.12	5.82	8.20	10.84	13.27	14.95	15.70	14.97	10.60	8.64	7.50	7.36	8.16	353 17
329	9.80	11.80	13.38	14.33	14.26	13.00	10.50	5.17	3.42	2.93	4.16	6.37	9.00	12.12	14.97	16.74	16.96	15.68	13.11	10.34	6.98	7.04	8.06	10.00	354 19	
330	12.15	14.04	15.14	15.03	13.10	10.20	7.00	4.27	2.40	2.20	3.93	9.77	13.27	16.13	17.72	17.51	15.78	12.57	9.74	7.27	6.14	6.36	7.56	12.72	8.86	355 21
331	14.77	15.81	15.20	12.64	9.26	5.91	3.10	1.55	1.93	4.00	7.06	10.68	17.04	18.34	17.72	15.47	12.00	8.88	6.58	5.67	6.00	7.50	10.14	13.10	356 22	
332	15.24	16.17	14.94	12.16	8.55	5.06	2.64	1.50	2.57	5.14	8.44	11.93	17.00	18.34	17.37	14.51	11.77	9.56	5.14	5.64	7.65	10.63	13.44	15.46	358 0	
333	15.86	14.14	10.98	7.08	4.48	3.36	4.74	3.30	5.83	8.90	12.30	15.56	17.50	17.88	16.62	13.58	9.97	6.94	5.14	5.52	7.63	10.73	13.70	15.36	359 2	
334	13.24	9.92	6.64	4.73	3.07	3.08	4.74	9.86	13.01	15.80	17.38	17.48	15.95	12.86	9.53	6.72	5.22	4.90	5.87	8.03	10.96	14.68	14.83	13.24	360 4	
335	10.55	7.68	5.43	4.33	4.63	5.97	8.02	10.57	13.25	15.58	16.14	14.11	11.13	8.76	6.38	5.17	5.13	6.30	8.60	10.76	12.74	13.74	13.62	10.30	361 6	
336	8.14	6.53	5.84	6.14	7.14	8.74	10.77	13.13	14.96	15.71	15.12	10.86	8.44	6.53	5.48	5.27	6.00	7.78	9.85	11.62	12.84	13.10	12.28	10.74	362 7	
337	9.22	7.33	8.24	9.54	11.12	12.64	13.57	13.57	13.57	13.57	13.57	10.12	8.24	6.78	5.70	6.37	7.72	9.40	11.06	12.32	12.86	12.50	11.47	10.24	363 9	
338	9.12	8.42	8.24	9.54	11.12	12.64	13.57	13.57	13.57	13.57	13.57	10.12	8.24	6.78	5.70	6.37	7.72	9.40	11.06	12.32	12.86	12.50	11.47	10.24	363 9	
339	9.06	8.58	8.66	9.44	10.68	11.96	13.14	12.66	11.34	10.06	8.36	6.86	5.72	5.37	5.87	7.17	9.14	11.00	12.70	13.68	12.94	11.57	10.38	9.14	365 13	
340	8.62	8.63	9.20	10.44	11.66	12.53	12.92	12.58	11.64	7.86	6.12	5.05	4.78	5.62	7.06	9.15	11.26	13.23	14.30	14.32	13.36	10.34	9.17	8.44	366 15	
341	8.24	8.62	9.76	11.04	12.36	13.08	12.90	11.65	9.64	7.34	5.52	4.45	5.76	7.66	9.97	12.43	14.27	15.18	14.97	13.73	11.82	10.16	8.86	8.24	367 16	
342	8.26	10.32	11.70	12.96	13.58	13.16	11.26	8.91	6.66	4.96	4.33	4.86	6.36	8.55	13.44	15.21	15.84	15.17	13.56	11.44	9.66	8.38	7.80	7.97	368 18	
343	9.00	10.56	13.46	13.82	12.72	10.52	7.90	5.74	4.34	4.11	5.34	7.23	9.78	12.44	14.65	15.93	15.94	12.37	10.23	8.53	7.47	7.31	7.97	9.38	369 20	
344	11.36	13.14	14.17	14.00	12.18	9.43	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	370 2	
Sum	772.43	769.90	752.24	727.62	704.70	702.99	694.10	670.79	681.10	706.39	705.04	734.50	745.73	745.38	775.50	772.37	766.06	759.07	739.00	773.61	760.90	761.94	764.52	751.51	No. of Days.	
No.	74	74	73	73	72	73	73	71	71	73	72	73	72	71	73	72	73	72	70	73	72	72	72	71	7747.32	
																									75 <sup>th</sup> 7 <sup>th</sup> .	

FORMS FOR SHORT-PERIOD TIDES.

BOM BAY—Commencing 0 hours, Astronomical Time, 1st January, 1885.

SERIES M<sub>2</sub>N.

Argument (4y — 5σ + ω). Motion per mean Solar hour = 57°·4238388.

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
1	15.52	12.96	9.13	5.76	3.03	1.68	2.28	4.80	7.90	11.70	15.50	18.00	18.08	15.14	11.54	8.50	6.21	5.53	6.08	8.20	11.31	14.16	16.06	16.66	2 0	
2	15.40	13.16	8.40	4.86	2.56	1.71	2.90	5.56	8.82	12.94	18.58	18.97	17.67	14.24	10.56	7.53	5.57	5.16	6.10	8.63	11.84	14.68	16.63	16.96	3 1	
3	15.24	11.92	8.00	4.87	2.80	3.57	4.24	6.84	10.20	17.26	18.86	18.84	17.06	13.20	9.77	6.90	5.23	4.96	6.16	8.86	12.14	14.87	16.40	16.40	4 2	
4	14.28	11.00	7.63	4.88	3.55	3.86	5.55	8.01	14.83	17.16	18.38	17.93	15.80	12.16	8.68	6.10	5.05	5.25	6.68	9.24	12.28	14.51	15.96	15.58	5 3	
5	13.48	10.47	7.54	5.76	5.07	7.22	9.17	12.11	15.02	17.02	17.55	16.63	14.11	10.96	8.16	6.22	5.47	5.84	7.18	9.67	12.12	14.04	15.00	14.45	6 4	
6	13.62	10.24	8.07	7.04	7.54	8.67	10.66	12.84	15.06	16.36	16.35	15.24	12.76	10.11	8.00	6.64	6.17	6.55	7.86	9.76	11.80	13.27	14.00	13.64	7 5	
7	12.22	9.95	8.44	6.84	9.03	9.97	11.20	13.05	14.64	15.46	15.18	13.87	11.68	9.76	8.10	7.16	7.03	7.40	8.29	9.82	11.16	12.55	13.24	12.20	8 7	
8	11.16	10.37	9.64	9.60	9.90	10.60	11.70	12.96	14.02	14.44	13.75	12.27	10.82	9.20	7.93	7.24	7.06	7.34	8.07	9.14	10.55	12.48	12.66	12.37	9 8	
9	11.60	10.93	10.34	9.98	9.86	10.17	11.07	12.14	13.06	13.36	12.72	11.71	10.43	9.14	7.97	7.14	6.75	6.94	7.74	8.96	10.26	12.67	13.14	12.97	10 9	
10	12.20	11.34	10.48	10.12	10.05	10.23	10.84	11.64	12.27	12.68	13.37	11.53	10.41	8.97	7.80	6.96	6.38	6.44	7.28	8.96	11.64	13.23	13.84	13.63	11 10	
11	12.58	11.38	10.27	9.77	9.61	9.89	10.44	11.24	11.97	12.52	13.50	11.87	10.54	8.76	7.34	6.16	5.74	5.74	6.38	8.96	13.22	14.24	14.58	13.94	12 11	
12	13.72	11.24	10.02	9.32	9.14	9.46	10.37	11.48	12.46	13.04	12.84	11.80	10.23	8.20	6.32	5.62	5.56	5.30	6.44	10.17	12.34	14.10	15.20	15.17	13 12	
13	13.27	10.58	9.35	8.75	8.76	9.26	10.34	11.68	12.96	13.64	13.36	11.80	9.66	7.32	5.74	5.44	5.44	5.44	6.74	8.86	11.26	13.66	15.38	15.87	14 13	
14	11.54	9.82	8.71	8.16	8.36	9.30	10.74	12.46	13.64	13.98	13.06	10.84	6.20	4.76	4.46	5.40	5.40	4.36	9.78	12.57	14.82	16.13	15.97	14.56	15 14	
15	10.05	8.46	7.82	7.74	8.41	9.71	11.76	13.30	14.26	14.09	12.44	8.24	5.12	4.20	4.63	6.12	6.12	4.46	11.24	14.04	15.74	16.36	15.71	13.82	16 15	
16	8.94	7.54	6.94	7.15	8.40	10.27	12.44	14.06	14.68	14.09	12.44	7.00	4.37	4.02	5.06	7.26	7.26	3.30	9.66	12.72	15.20	16.55	16.63	15.27	17 16	
17	7.86	6.84	6.68	7.56	9.32	11.40	13.55	14.78	13.22	10.43	7.48	5.34	4.30	4.66	6.35	8.54	8.54	11.38	14.15	16.15	16.88	16.08	14.04	11.02	18 17	
18	6.76	6.12	6.34	7.60	9.84	14.06	14.84	14.14	12.06	9.06	6.46	4.67	4.24	5.16	7.15	9.68	9.68	12.56	14.87	16.44	16.45	15.00	12.42	8.54	19 18	
19	5.80	5.43	6.34	8.16	10.65	12.88	14.28	14.56	13.33	10.92	8.30	4.87	4.06	4.67	6.54	11.04	11.04	13.64	15.62	16.36	15.76	13.82	11.00	8.37	20 19	
20	5.54	6.83	8.93	11.40	13.32	14.42	14.72	12.47	10.10	7.91	6.34	5.70	4.87	5.06	7.70	9.76	9.76	14.36	15.74	15.96	14.86	12.76	10.13	6.17	21 21	
21	6.11	7.62	9.70	11.76	13.36	14.14	13.72	12.06	9.94	8.32	7.22	7.01	6.30	6.30	8.97	10.80	10.80	14.62	15.30	15.17	13.80	11.46	9.14	6.70	22 22	
22	6.68	8.02	9.76	11.65	13.04	13.76	13.34	12.14	10.65	9.07	8.15	8.14	6.68	6.68	9.86	11.56	11.56	14.56	15.02	14.37	12.76	10.76	7.78	6.09	23 23	
23	6.68	7.86	9.46	11.24	12.66	13.36	13.34	12.38	11.08	9.94	9.11	8.88	7.28	6.68	9.86	11.56	11.56	14.14	14.41	13.60	12.06	10.26	8.46	6.08	25 0	
24	6.56	7.64	9.14	10.84	12.34	13.44	13.81	13.33	12.18	10.75	9.76	9.24	6.68	6.68	9.40	10.46	11.84	13.36	13.03	12.06	10.24	8.47	7.00	5.38	26 1	
25	5.68	6.78	8.55	10.33	12.22	13.56	14.30	14.16	13.05	11.56	10.06	9.11	6.86	6.86	8.25	11.24	12.70	13.80	14.14	13.30	11.34	8.72	6.20	4.41	27 2	
26	4.77	6.10	8.10	10.50	12.63	14.53	15.56	15.33	13.76	11.64	9.52	8.28	7.92	6.25	11.24	12.70	13.80	14.14	13.30	11.34	8.72	6.20	4.24	3.38	28 3	
27	3.76	5.30	7.76	10.55	13.50	15.72	16.74	16.12	14.36	11.40	8.83	7.24	6.86	5.93	9.20	11.11	12.97	14.55	15.08	14.17	11.84	8.82	5.70	3.60	29 4	
28	3.06	5.04	7.88	11.48	14.56	17.04	17.86	17.00	14.36	10.96	6.27	5.77	6.57	6.62	8.62	11.35	13.92	15.74	16.28	14.96	12.18	8.44	5.42	3.22	2.16	30 5
29	3.07	5.52	8.75	12.46	16.01	18.10	18.47	17.26	13.80	7.09	5.27	5.02	6.02	6.40	11.85	14.65	16.52	16.84	15.28	11.68	7.88	4.80	2.74	2.38	31 6	
30	4.00	6.66	10.10	13.98	17.01	18.64	18.38	16.30	12.42	8.97	6.01	4.46	4.57	6.12	9.14	12.56	15.46	17.00	16.86	14.76	11.06	7.36	4.34	2.72	2.99	32 7
31	4.86	7.74	11.40	14.94	17.54	17.66	16.30	14.67	11.08	7.54	5.01	3.93	4.32	6.55	9.62	13.94	15.80	16.84	16.08	13.73	10.16	6.82	4.54	3.58	4.41	33 8
32	6.36	9.36	12.84	15.86	17.94	16.48	13.27	9.84	6.94	4.96	4.33	5.26	7.44	10.66	13.70	15.74	16.43	15.42	12.82	9.66	6.90	5.42	5.14	6.20	6.20	34 9
33	8.06	10.66	16.02	17.12	16.74	14.88	11.68	8.76	6.34	4.92	4.74	5.86	8.26	11.07	13.60	15.16	15.34	14.06	11.68	9.04	7.34	6.56	8.04	9.56	8.04	35 11
34	11.76	14.24	15.60	16.04	15.34	13.02	10.16	7.86	6.27	5.54	5.86	7.18	9.07	11.36	13.26	14.34	14.26	12.88	11.00	9.39	8.26	7.92	9.30	10.36	8.30	36 12
35	12.08	13.76	14.06	14.44	13.11	11.12	9.30	7.54	6.26	6.13	6.68	7.86	9.28	10.86	12.27	13.10	12.94	11.93	10.66	9.72	9.12	9.26	10.66	10.66	9.66	37 13



FORMS FOR SHORT-PERIOD TIDES.  
SERIES M<sub>2</sub>N.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
72	5.44	4.44	4.96	8.94	11.85	14.34	16.00	16.06	14.53	11.64	8.54	5.76	4.22	3.97	5.24	7.30	10.10	13.02	15.04	16.00	15.20	12.86	9.54	6.67	76 4	
73	4.93	5.52	7.55	10.33	13.59	15.75	16.73	16.97	13.66	10.42	7.22	4.92	3.64	4.00	5.66	8.33	11.52	14.30	16.06	16.52	15.06	12.13	8.73	4.66	77 6	
74	4.99	6.52	8.92	11.86	14.66	16.40	16.56	15.97	11.90	8.47	5.62	3.74	3.22	4.26	6.66	9.00	12.88	15.23	16.56	16.25	14.26	8.00	5.75	5.11	78 7	
75	5.88	7.84	10.46	13.38	15.68	16.60	15.80	13.36	10.12	7.00	4.83	3.54	3.76	5.34	7.86	11.00	13.93	15.92	16.74	13.36	10.24	7.64	6.12	6.08	78 8	
76	7.14	9.00	11.56	13.90	15.66	15.98	14.76	12.06	8.90	6.13	4.34	3.62	4.36	6.06	8.47	11.31	13.87	15.62	16.74	12.74	10.02	8.05	7.96	7.06	80 9	
77	7.93	9.67	13.07	14.08	15.23	15.08	13.57	11.16	8.26	6.08	4.76	4.47	5.46	7.26	9.48	11.88	13.90	15.36	16.74	12.67	10.54	8.74	7.94	8.14	81 10	
78	9.06	10.62	13.40	13.77	14.52	14.20	12.80	10.64	8.47	6.76	5.86	5.82	6.49	7.75	11.71	13.54	14.73	14.90	14.06	12.63	11.05	9.70	8.86	8.72	82 11	
79	9.12	10.24	11.76	13.06	13.60	13.34	12.06	10.56	8.92	7.40	6.43	6.30	6.68	9.52	11.71	13.54	14.73	14.90	14.06	12.63	11.05	9.70	8.86	8.72	83 12	
80	9.04	9.84	10.96	12.05	13.86	12.96	12.44	11.22	9.67	8.30	7.00	6.48	7.68	9.46	11.24	13.02	13.74	14.48	14.44	13.62	12.12	10.36	9.96	8.11	84 13	
81	7.96	8.44	9.76	11.16	12.56	12.30	12.78	11.94	10.50	7.20	6.06	5.92	6.72	8.34	10.26	12.20	13.86	15.00	15.14	14.16	12.20	9.88	8.00	6.90	85 14	
82	6.56	7.46	9.22	11.16	12.56	13.57	14.06	11.72	9.38	7.17	5.72	5.38	6.17	7.82	10.00	12.50	14.54	15.84	15.94	14.64	12.14	9.36	6.97	5.74	86 15	
83	5.63	6.67	8.88	11.24	13.46	14.86	14.34	12.95	9.44	6.93	5.38	5.00	5.82	7.83	10.50	13.30	15.60	16.72	16.28	14.37	11.37	8.36	6.00	4.67	87 16	
84	4.80	6.40	9.20	12.06	16.12	16.16	14.90	12.22	9.12	6.60	5.05	4.86	5.87	8.10	11.14	14.15	16.35	17.15	16.24	13.58	10.14	7.06	4.83	3.96	88 17	
85	4.70	6.72	13.20	15.64	17.04	16.75	14.92	11.81	8.56	6.27	5.14	5.64	6.94	9.43	12.61	15.44	17.03	17.08	15.36	11.92	8.64	6.78	4.48	4.25	89 18	
86	5.24	9.92	13.40	16.43	17.34	16.56	14.28	10.82	7.84	5.95	5.42	6.12	7.87	10.62	13.66	16.10	17.14	16.46	13.96	10.44	7.12	4.80	3.83	6.43	90 20	
87	7.57	11.00	14.10	16.43	17.34	16.56	14.28	10.82	7.84	5.95	5.42	6.12	7.87	10.62	13.66	16.10	17.14	16.46	13.96	10.44	7.12	4.80	3.83	6.43	91 21	
88	8.78	12.04	14.74	16.66	17.13	15.64	12.86	9.53	7.16	5.81	5.93	7.22	9.26	12.02	14.66	16.44	16.67	15.06	12.02	8.56	4.02	3.84	4.93	7.24	92 22	
89	10.09	13.22	15.56	16.90	16.56	14.74	11.68	8.84	7.02	6.48	7.04	8.26	10.50	13.00	14.94	15.83	15.12	12.94	9.87	5.16	4.22	4.76	6.40	8.73	93 23	
90	11.37	14.00	15.82	16.34	15.34	13.10	10.40	8.36	7.32	7.28	8.03	9.50	11.53	13.48	14.74	14.92	13.67	8.70	11.34	6.67	5.40	5.22	6.16	7.85	94 0	
91	12.30	14.30	15.48	15.46	14.27	12.24	10.20	8.78	8.26	8.47	9.24	10.52	12.04	13.48	14.16	12.27	13.84	10.16	11.34	7.14	6.47	6.22	7.44	9.20	95 1	
92	13.64	14.05	14.67	14.77	12.97	11.44	10.04	9.16	8.84	9.16	9.84	10.95	11.96	12.96	12.28	10.94	9.24	7.80	6.78	6.70	7.30	8.37	9.54	10.90	96 1	
93	12.34	13.52	13.80	13.26	12.13	10.96	10.04	9.60	9.33	9.54	9.90	10.56	11.44	12.05	11.54	10.36	9.16	8.12	7.47	7.44	7.87	8.52	9.46	10.73	97 2	
94	11.93	12.74	12.98	12.66	11.86	11.07	10.34	9.94	9.77	9.87	10.02	10.81	11.14	11.27	10.92	10.30	9.34	8.56	7.74	7.58	7.98	8.76	9.87	11.04	98 3	
95	11.96	12.50	12.66	12.42	11.96	11.34	10.55	9.91	9.47	9.52	9.94	10.53	10.94	11.12	11.02	10.62	10.00	9.22	8.40	8.01	8.13	8.63	9.70	10.66	99 4	
96	11.77	12.66	13.06	12.94	12.40	11.47	10.50	9.62	8.94	8.74	9.48	10.45	11.36	11.88	11.89	11.44	10.50	9.40	8.46	7.84	7.76	8.43	9.46	10.86	100 5	
97	12.30	13.36	13.82	13.66	12.66	11.42	10.02	9.62	8.84	8.54	9.48	10.45	11.36	11.88	11.89	11.44	10.50	9.40	8.46	7.84	7.76	8.43	9.46	10.86	101 6	
98	12.70	14.06	14.56	14.22	10.96	8.88	7.46	6.81	6.84	7.92	9.62	11.52	13.00	13.97	14.12	13.00	11.02	9.05	7.48	6.74	6.92	7.97	9.72	11.72	102 7	
99	13.58	14.86	14.86	14.22	10.96	8.88	7.46	6.81	6.84	7.92	9.62	11.52	13.00	13.97	14.12	13.00	11.02	9.05	7.48	6.74	6.92	7.97	9.72	11.72	103 8	
100	14.55	15.49	13.80	11.08	8.22	5.93	4.52	4.32	5.47	7.72	10.54	13.27	15.36	16.20	15.32	13.00	9.88	7.34	5.76	5.40	6.24	8.22	10.70	15.52	104 10	
101	16.25	15.36	12.80	9.46	6.56	4.47	3.42	3.91	5.74	8.31	11.40	14.40	16.28	16.72	15.47	12.68	9.44	6.81	5.47	5.38	6.52	8.91	11.80	14.40	15.97	105 11
102	16.08	14.33	11.30	7.80	4.97	2.93	2.46	3.76	6.21	9.51	12.97	15.58	17.14	17.04	14.91	11.68	8.36	6.14	5.06	5.57	7.24	10.67	13.10	15.40	16.44	106 12
103	15.82	13.44	9.74	6.67	4.03	2.50	2.77	4.44	7.50	10.96	14.33	16.70	17.72	16.91	14.37	10.87	6.10	5.71	6.50	8.36	11.33	14.12	15.97	16.50	16.44	107 13
104	15.10	12.22	8.67	5.24	3.17	2.56	3.47	5.74	8.64	12.02	15.12	16.94	17.54	16.24	13.40	10.32	6.17	7.04	9.13	12.00	14.47	15.69	15.54	108 14		
105	13.66	10.74	7.44	4.88	3.28	3.04	4.36	6.67	9.40	12.47	15.00	16.74	16.94	15.60	10.01	7.87	6.76	6.80	7.71	9.70	12.14	14.15	15.02	14.50	109 15	
106	12.53	9.92	7.24	5.36	4.17	4.16	5.20	7.26	9.80	12.40	14.57	15.77	15.74	12.12	9.90	8.07	7.14	7.11	7.83	9.54	11.58	13.16	13.74	13.28	110 16	
105	11.76	9.56	7.60	5.96	4.93	5.02	5.86	7.52	9.74	12.00	14.87	14.77	13.76	12.06	10.26	8.74	7.82	7.54	8.00	9.34	11.00	12.36	12.96	12.96	111 17	

107	11.58	10.14	8.48	6.94	6.06	5.96	6.60	7.87	9.72	13.34	14.34	14.44	13.66	12.26	10.62	9.10	8.03	7.66	7.76	8.68	10.20	11.63	12.43	12.66	11.18		
108	13.10	10.96	9.47	8.14	7.03	6.54	6.88	9.57	11.42	13.00	14.07	14.44	13.93	12.76	11.00	9.18	7.74	6.96	6.96	7.85	9.40	10.96	12.36	13.06	11.18		
109	13.12	12.22	10.65	8.87	7.52	6.84	7.66	9.26	11.04	12.88	14.12	14.66	14.30	12.64	10.64	8.60	7.78	5.94	5.93	7.08	9.00	11.04	12.64	13.72	11.42		
110	13.87	12.97	11.36	9.32	7.66	6.62	7.28	8.88	10.96	12.96	14.54	15.17	14.54	12.77	10.22	7.74	5.76	4.88	5.14	6.58	8.88	11.33	13.36	14.66	11.52		
111	14.94	13.86	11.70	9.34	7.26	6.22	7.24	9.00	11.22	13.36	14.86	15.37	14.44	12.10	9.16	6.48	4.70	4.20	4.74	6.70	9.17	11.77	14.02	15.57	11.62		
112	15.54	11.70	8.80	6.96	6.07	6.34	7.48	9.44	11.96	14.10	15.48	15.44	13.84	10.92	7.66	5.31	3.77	3.70	5.12	7.30	10.10	12.94	15.14	16.26	11.80		
113	13.86	11.00	8.24	6.47	5.97	6.54	7.98	10.16	12.70	14.64	15.66	14.96	12.70	9.46	6.57	4.32	3.42	4.04	5.86	8.48	11.42	16.17	16.57	15.46	11.91		
114	12.94	10.06	7.04	6.36	6.16	6.82	8.40	10.90	13.45	15.07	15.35	13.81	11.00	7.70	5.15	3.44	3.36	4.67	6.96	12.56	14.92	16.36	16.28	14.70	12.02		
115	11.93	9.06	7.20	6.40	6.70	7.74	9.37	11.47	13.86	15.04	15.06	12.96	9.73	7.17	4.24	3.42	4.04	5.68	10.08	13.46	15.48	16.25	15.62	13.50	12.13		
116	10.52	8.22	6.72	6.40	7.02	8.34	10.44	12.60	14.08	14.43	13.26	10.82	7.87	5.57	3.94	3.86	6.80	9.18	11.76	14.24	15.56	15.54	14.30	11.86	12.24		
117	9.46	7.76	6.94	7.06	7.86	9.36	11.24	13.06	13.96	13.66	11.96	9.20	6.72	5.07	4.90	6.32	8.22	10.36	12.80	14.56	15.43	14.70	13.04	10.84	12.85		
118	8.96	7.76	7.44	7.76	8.80	10.26	11.94	13.06	13.30	12.28	10.40	8.28	6.46	5.20	6.00	7.54	9.26	12.10	13.34	14.60	14.86	13.86	12.06	10.14	12.46		
119	8.84	8.15	8.06	8.40	9.36	10.62	11.94	12.68	12.46	11.36	9.18	7.94	6.74	6.04	6.20	7.12	8.46	10.24	12.10	13.38	14.08	13.92	12.90	11.41	10.00	12.57	
120	8.90	8.46	8.56	9.00	9.74	10.55	11.36	11.86	10.72	9.26	7.86	6.96	6.92	7.44	8.22	9.26	10.47	12.10	13.34	13.78	13.40	12.16	10.87	9.94	12.68		
121	9.24	8.96	8.94	9.17	9.58	10.34	10.96	11.44	10.58	9.54	8.46	7.76	7.66	7.97	8.66	9.74	10.97	12.22	13.24	13.54	13.24	12.12	10.96	9.98	12.79		
122	9.27	8.94	8.74	8.80	9.24	10.80	11.34	11.77	11.44	10.76	9.74	8.78	8.17	8.10	8.66	9.60	10.93	12.30	13.21	13.50	13.18	12.36	11.16	9.68	12.91		
123	8.96	8.20	7.92	8.00	8.62	9.56	10.40	11.22	12.36	11.62	10.26	8.85	8.06	7.83	8.24	9.37	10.96	12.50	13.57	14.02	13.54	12.37	10.74	8.97	13.02		
124	8.30	6.90	7.45	8.52	9.26	10.12	13.50	14.22	13.67	12.20	10.16	8.55	7.53	7.27	7.93	9.36	11.30	13.16	14.26	14.66	13.94	12.24	9.97	5.85	13.14		
125	7.34	5.98	6.71	8.26	10.20	12.12	13.50	14.22	13.67	12.20	10.16	8.55	7.53	7.27	7.93	9.36	11.30	13.16	14.26	14.66	13.94	12.24	7.60	5.85	13.14		
126	4.92	5.06	6.42	8.60	10.95	13.28	14.84	15.34	14.46	12.38	10.01	8.14	6.95	6.90	8.01	9.74	11.84	13.66	14.84	15.16	11.76	8.83	6.14	4.18	132.15		
127	3.66	4.53	6.40	9.08	11.92	14.30	15.96	16.28	14.95	12.41	9.36	7.14	6.17	6.50	7.92	10.02	12.44	14.66	15.64	15.47	10.66	7.20	4.46	2.86	132.15		
128	2.74	4.17	6.63	9.77	13.00	15.72	17.16	16.96	15.18	11.90	8.78	6.57	5.95	6.52	7.94	10.30	12.84	15.02	15.24	12.56	8.86	5.70	3.17	1.97	134.17		
129	2.43	4.23	7.22	10.62	13.96	16.50	17.69	17.06	14.58	10.90	8.02	5.94	5.46	6.30	8.25	10.90	13.74	15.64	15.06	14.62	11.54	4.52	2.14	1.42	135.18		
130	2.56	5.03	8.20	11.45	14.68	16.97	17.83	16.77	14.06	10.36	7.66	5.84	5.52	6.20	8.20	11.20	14.02	15.72	15.74	13.76	10.48	6.92	4.07	2.24	1.86	136.19	
131	3.24	5.60	8.58	12.24	15.14	17.16	17.74	16.33	13.21	10.00	7.30	5.76	6.11	7.20	9.40	12.06	14.14	15.47	15.07	12.82	9.66	6.56	4.07	2.88	137.20		
132	4.46	6.78	9.71	12.92	15.90	17.10	17.16	15.40	12.67	9.57	7.30	6.48	6.38	7.36	9.30	11.76	13.38	14.98	14.32	12.18	9.28	6.58	4.76	4.30	138.21		
133	5.66	7.78	10.44	12.87	14.66	15.72	15.46	14.00	9.56	7.72	6.96	6.82	7.44	8.91	10.74	12.30	13.13	12.92	11.76	10.08	8.18	6.84	6.38	6.46	140.23		
134	6.33	8.08	10.42	12.48	14.22	14.94	13.52	11.62	9.46	7.84	6.86	6.52	7.44	8.91	10.74	12.30	13.13	12.92	11.76	10.08	8.18	6.84	6.38	6.46	140.23		
135	7.26	8.54	10.38	12.48	14.22	14.94	13.52	11.62	9.46	7.84	6.86	6.52	7.44	8.91	10.74	12.30	13.13	12.92	11.76	10.08	8.18	6.84	6.38	6.46	140.23		
136	7.36	8.54	10.16	11.86	13.27	14.14	13.98	12.92	11.14	9.14	7.48	6.36	5.86	5.93	7.12	8.94	10.74	12.22	12.86	12.65	11.60	10.06	8.56	7.47	143.1		
137	7.70	8.44	10.00	13.27	14.05	13.96	13.82	12.68	10.82	9.01	7.20	5.72	5.17	5.56	6.97	8.92	10.90	12.46	13.44	13.42	12.46	10.72	9.12	8.02	144.2		
138	8.26	9.76	11.56	13.14	14.05	13.96	12.62	10.76	8.52	6.66	5.32	4.84	4.84	5.46	7.38	9.67	11.66	13.40	14.34	14.36	13.24	11.30	9.64	8.16	145.4		
139	8.44	10.16	11.93	13.46	14.20	13.97	12.62	10.50	7.84	5.72	4.46	4.54	5.90	7.82	10.17	12.67	14.36	15.22	14.76	13.34	11.12	7.84	7.36	7.72	146.5		
140	8.72	10.32	12.06	13.66	14.36	13.76	11.92	9.27	6.82	4.82	3.97	4.57	6.16	8.40	11.03	13.46	15.10	15.52	14.67	12.94	9.16	7.60	7.38	7.92	147.6		
141	9.10	10.86	12.73	14.28	14.53	13.00	10.66	7.86	5.58	4.22	4.13	5.24	7.24	9.70	12.30	14.40	15.74	15.70	14.67	10.67	8.77	7.60	7.38	7.92	147.6		
142	9.70	11.80	13.62	14.54	14.16	12.22	9.68	6.84	4.84	3.94	4.50	6.00	8.33	10.94	13.60	15.42	15.62	13.90	11.47	9.28	7.84	7.40	7.74	8.20	148.7		
																									8.92	149.8	
Sum	723.70	742.55	743.25	828.93	869.38	821.74	798.11	771.06	676.94	696.88	642.33	700.96	725.46	736.65	837.64	800.17	881.37	821.07	808.08	786.27	690.16	721.72	661.34	71	18288.91		
No.	77	76	72	76	71	76	73	74	76	71	76	71	76	75	72	77	77	73	75	77	77	71	77	71	77	74	88

FORMS FOR SHORT-PERIOD TIDES.

SERIES M<sub>2</sub>N.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour
143	10.62	12.60	14.03	14.27	13.22	10.78	8.10	5.76	4.27	4.17	5.26	7.20	9.70	12.28	14.66	16.04	14.86	12.64	10.27	8.44	7.34	7.34	8.10	9.32	150 9
144	11.55	13.36	14.37	13.92	12.06	9.48	6.90	5.12	4.32	4.97	6.54	8.70	11.00	13.40	15.67	15.67	14.17	11.77	9.56	8.16	7.68	7.83	8.74	10.50	151 10
145	13.26	13.66	14.02	12.96	10.86	8.34	6.24	5.04	4.82	5.84	7.60	11.87	14.10	15.30	15.60	14.66	12.78	10.74	9.03	7.96	7.73	8.24	9.44	11.07	152 11
146	12.62	13.44	13.16	11.96	9.94	7.65	6.16	5.18	5.68	6.84	10.66	12.74	14.30	15.12	15.06	13.65	11.84	10.00	8.46	7.75	7.78	8.46	9.92	11.36	153 12
147	13.32	12.84	12.32	10.98	9.18	7.32	6.03	5.94	6.87	8.17	11.58	13.28	14.64	14.97	14.22	12.62	11.08	9.47	8.38	8.08	8.30	9.20	10.24	11.40	154 13
148	11.12	12.46	11.72	10.38	8.77	7.37	6.70	6.93	7.78	8.83	10.30	13.54	14.68	14.80	13.77	12.16	10.50	9.20	8.47	8.28	8.60	9.36	10.36	11.26	155 14
149	11.83	12.05	11.56	10.60	8.14	7.22	7.83	8.62	9.82	11.10	12.64	13.94	14.46	14.16	13.26	11.74	10.42	9.26	8.54	8.34	8.46	9.23	10.10	10.93	156 15
150	11.70	11.97	11.72	9.98	8.86	8.32	8.36	9.00	10.04	11.54	12.92	13.86	14.23	13.85	12.88	11.48	10.08	8.98	8.20	8.20	8.20	9.12	10.03	11.29	157 16
151	12.58	12.36	11.84	11.02	9.01	7.66	7.88	9.20	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	10.03	8.74	7.92	7.54	7.76	8.67	9.56	12.84	158 18
152	13.87	13.86	13.28	11.02	11.02	10.56	9.64	10.17	11.38	12.77	13.98	14.67	15.14	14.88	13.86	12.46	10.48	8.82	7.82	7.82	8.19	11.28	13.22	14.76	159 19
153	15.82	15.76	14.97	13.34	11.70	10.67	10.27	10.56	11.52	12.90	14.12	15.30	15.65	15.48	14.17	12.02	9.86	8.00	7.09	7.72	8.54	11.40	13.77	15.84	160 20
154	16.86	16.85	15.70	13.60	11.52	9.95	9.55	9.80	10.84	12.57	14.23	15.47	16.06	15.22	13.50	10.84	8.22	6.16	5.15	5.55	6.50	11.37	14.18	16.48	161 21
155	17.54	17.17	15.60	12.50	10.07	8.34	8.17	8.96	10.27	12.23	14.24	15.74	16.29	15.33	12.77	9.46	6.44	4.30	3.62	4.30	6.30	11.95	15.02	17.28	162 22
156	17.95	17.20	15.02	11.76	9.04	7.44	7.22	7.81	9.55	12.08	14.54	16.07	16.21	14.76	11.87	8.16	5.07	2.74	2.74	3.80	5.94	12.80	15.92	18.07	163 23
157	18.53	17.65	14.65	10.90	8.00	6.62	6.55	7.50	9.65	12.45	14.89	16.40	16.14	14.28	10.90	7.10	4.31	2.62	2.37	3.68	6.30	13.48	16.44	18.12	165 0
158	18.40	17.00	13.80	10.17	7.55	6.20	6.18	7.30	9.60	12.79	15.16	16.42	15.96	13.80	10.33	6.77	4.00	2.33	2.54	4.18	7.11	14.20	16.74	17.85	166 1
159	17.95	16.07	12.81	9.60	7.05	5.72	5.77	7.00	9.56	15.12	16.05	15.26	12.76	9.20	6.14	3.95	2.88	3.47	5.52	7.93	11.04	14.21	16.44	17.72	167 2
160	17.40	15.44	12.07	9.02	6.70	5.67	5.93	7.41	13.02	14.92	15.57	14.68	12.28	9.20	6.52	4.77	4.20	4.91	6.52	8.80	11.92	14.25	16.42	17.20	168 8
161	16.60	14.54	11.30	8.66	6.74	6.16	6.16	7.65	10.05	12.50	14.82	14.95	11.96	9.47	7.26	6.06	5.80	6.30	7.66	9.64	11.92	14.25	15.90	16.46	169 4
162	15.74	13.76	10.84	8.61	6.32	6.58	7.80	9.82	12.04	13.55	14.17	13.54	12.03	10.34	8.60	7.57	7.26	7.61	8.41	9.92	12.12	14.20	15.46	15.54	170 5
163	14.38	12.66	8.31	7.04	6.60	6.77	7.78	9.32	11.22	12.80	13.58	13.46	12.40	10.90	9.62	8.66	8.31	8.49	9.03	10.30	12.04	13.70	14.74	14.75	171 6
164	12.92	10.10	8.46	7.12	6.53	6.70	7.50	9.03	10.90	12.32	13.20	13.38	12.92	11.94	10.67	9.60	8.94	8.82	9.24	10.33	11.90	13.24	14.06	13.34	172 8
165	11.84	10.05	8.26	6.94	6.44	6.67	7.40	9.06	10.86	12.50	13.66	14.10	13.63	12.46	11.06	10.06	9.30	9.05	9.31	10.22	11.60	13.82	13.82	13.08	173 9
166	11.64	9.76	8.00	6.70	6.08	6.22	7.28	9.00	10.94	12.77	14.05	14.63	14.17	12.86	11.33	10.04	9.14	8.86	9.20	10.08	12.44	13.30	13.52	12.80	174 10
167	11.00	8.85	7.06	5.67	5.05	5.60	7.15	9.26	11.30	13.28	14.45	14.84	13.95	12.40	10.90	9.46	8.62	8.56	9.64	11.12	12.55	13.40	13.37	12.07	175 11
168	10.97	8.20	6.17	4.94	4.74	5.62	7.74	9.76	12.14	14.01	15.00	14.86	13.77	12.06	10.27	8.10	7.54	8.52	9.68	11.18	12.64	13.37	13.05	11.52	176 12
169	9.17	6.76	5.11	4.16	4.64	6.10	8.00	10.50	12.90	14.56	15.33	14.70	13.32	11.14	9.44	7.30	7.57	8.31	9.81	11.65	13.20	13.60	12.56	10.40	177 13
170	7.97	5.83	4.38	4.04	4.96	6.82	9.02	11.57	13.86	15.24	15.44	14.56	12.56	10.36	8.63	7.62	7.30	7.74	8.86	10.67	12.47	13.67	13.56	9.66	178 14
171	6.93	4.96	3.94	4.22	5.70	7.84	10.40	12.82	14.74	15.56	15.33	14.70	12.56	10.36	8.63	7.62	7.03	7.74	8.86	10.67	12.47	13.67	13.56	9.06	179 15
172	5.64	4.04	3.83	4.76	6.70	9.02	12.26	14.31	15.12	14.48	12.44	9.96	8.16	6.86	6.42	6.91	8.42	10.44	12.57	13.42	13.92	13.00	10.74	8.00	180 16
173	4.96	3.98	4.36	5.65	7.72	10.02	12.26	14.74	15.12	13.77	11.30	9.01	7.37	6.64	6.56	7.46	9.06	11.01	12.70	13.51	13.01	11.07	8.44	6.12	181 17
174	4.72	4.42	5.31	6.94	8.97	11.17	14.74	15.17	14.22	12.16	9.74	7.86	6.74	6.51	7.07	8.16	9.92	11.66	12.82	13.10	11.86	9.72	7.36	5.70	182 18
175	5.02	5.24	6.42	8.07	11.08	13.73	14.86	14.72	13.40	11.17	9.22	7.55	6.51	6.57	7.34	8.72	10.61	12.04	13.77	12.64	11.27	9.34	7.48	6.30	183 19
176	5.87	6.54	7.66	10.12	12.94	14.38	14.88	14.70	13.50	10.34	8.44	7.22	6.77	6.97	7.87	9.34	10.94	12.19	13.66	12.22	10.84	9.25	7.90	6.96	184 20
177	6.93	8.50	10.00	11.48	13.33	14.36	14.44	13.38	11.42	9.60	8.02	6.94	6.56	6.92	7.79	9.26	10.80	11.92	12.43	13.16	11.12	9.70	7.56	7.56	185 22

178	8.14	9.04	10.41	11.98	13.30	13.98	13.72	12.51	10.84	8.96	7.47	6.70	6.48	6.84	7.86	9.16	10.52	11.71	12.36	13.28	11.46	10.38	8.34	8.14	186 23	
179	8.38	9.04	10.37	11.82	13.16	13.66	13.27	11.87	10.24	8.57	7.05	6.14	5.87	6.26	7.22	8.72	10.36	11.70	12.56	13.86	11.14	9.86	8.86	8.31	188 0	
180	8.34	9.02	10.46	11.88	13.12	13.48	12.96	11.86	10.30	8.58	7.00	5.74	5.32	5.74	6.86	8.67	10.62	12.30	13.96	13.31	12.10	10.48	9.04	8.28	189 1	
181	8.37	8.98	10.28	11.72	13.02	13.62	13.24	12.02	10.14	8.20	6.16	4.76	4.31	4.90	6.40	8.62	13.04	14.57	15.22	14.64	12.87	10.58	8.66	7.68	190 2	
182	7.62	8.40	10.00	11.70	13.12	13.97	13.69	12.32	10.27	7.76	5.44	3.88	3.19	3.88	5.80	8.60	11.46	13.90	15.54	16.06	15.08	12.92	10.40	8.23	7.07	191 3
183	6.90	7.82	9.34	11.60	13.35	14.38	14.34	12.76	10.16	7.15	4.46	2.56	2.27	5.02	8.80	11.46	13.90	15.54	17.06	17.55	15.88	12.54	9.04	6.46	5.24	192 4
184	6.04	7.17	9.30	11.84	13.92	15.05	14.90	13.08	9.91	6.43	3.53	1.84	3.58	6.20	9.54	13.00	15.92	17.60	17.55	15.88	12.54	9.04	6.46	5.24	193 5	
185	5.54	6.76	9.24	12.48	14.76	16.12	15.46	13.17	9.32	5.65	1.84	1.84	3.58	6.20	9.54	13.00	15.92	17.60	17.55	15.88	12.54	9.04	6.46	5.24	194 6	
186	4.98	6.66	9.72	13.12	15.46	16.44	15.54	13.76	9.17	5.65	1.62	1.90	3.97	6.70	10.13	13.94	16.80	18.22	17.87	15.72	12.00	8.47	5.86	4.66	194 6	
187	4.66	6.66	9.96	13.24	15.56	16.37	15.10	13.86	8.45	5.84	2.47	3.46	5.71	8.66	12.13	15.36	17.38	17.97	16.76	13.80	10.38	7.04	4.79	4.26	196 8	
188	5.04	7.14	10.42	13.85	15.77	16.14	14.53	11.60	8.45	5.84	3.82	5.12	6.91	9.80	13.00	15.56	17.04	17.17	15.44	12.60	9.26	6.86	5.22	4.84	197 9	
189	5.76	8.06	10.85	13.97	15.36	15.40	13.86	11.04	8.20	6.43	5.34	6.64	7.95	10.24	12.80	15.30	16.34	15.86	14.11	11.28	8.50	6.30	5.34	5.40	198 10	
190	6.24	10.50	13.97	14.30	14.44	12.94	10.92	9.08	7.74	7.24	7.56	8.14	9.16	11.11	13.10	14.71	15.40	14.72	12.96	10.60	8.38	6.86	6.05	6.82	199 12	
191	8.26	10.28	12.30	13.38	13.40	12.62	11.34	10.16	9.24	8.58	8.59	8.86	9.62	10.96	12.55	13.78	14.07	13.40	11.92	10.10	8.37	6.38	6.51	7.24	200 13	
192	8.41	9.82	11.28	12.52	12.90	12.68	11.87	10.93	10.01	9.34	9.14	9.27	9.97	10.90	12.12	13.14	13.41	12.71	11.34	8.47	7.34	6.76	6.86	7.36	201 14	
193	8.56	10.06	11.46	12.50	13.02	12.96	12.57	11.86	10.96	10.04	9.33	9.52	9.76	10.73	11.74	12.78	13.04	12.50	10.20	8.76	7.52	6.90	6.76	7.25	202 16	
194	8.50	10.20	11.86	13.24	13.97	13.87	13.28	12.22	11.04	10.07	9.54	9.50	9.87	10.64	11.70	12.60	12.66	11.42	10.20	8.76	7.52	6.90	6.76	7.14	203 16	
195	8.62	10.44	12.07	13.40	14.20	14.14	13.28	12.08	10.74	9.52	8.94	8.94	9.48	10.50	11.72	13.06	12.60	11.28	9.36	7.66	6.38	5.86	6.06	7.07	204 17	
196	8.94	10.96	13.07	14.58	15.07	14.54	13.34	11.84	10.26	9.14	8.46	8.46	9.16	11.74	13.14	13.32	12.81	11.24	9.13	7.31	5.74	5.33	6.10	7.65	205 18	
197	9.76	12.02	14.00	15.20	15.33	14.58	12.97	11.01	9.35	8.37	8.18	9.62	10.95	12.64	13.76	13.92	12.56	10.36	8.02	6.14	5.26	5.24	6.52	8.36	206 19	
198	10.60	12.96	14.83	16.05	15.68	14.35	12.14	9.94	8.56	8.20	8.73	9.99	11.82	13.73	14.66	14.04	11.84	8.90	6.50	5.04	4.74	5.78	7.22	9.33	207 20	
199	11.77	14.22	15.86	16.07	15.15	13.18	10.77	7.57	7.18	7.78	8.96	10.77	12.83	14.27	14.50	13.28	10.70	7.76	5.53	4.56	4.86	6.26	8.20	10.44	208 21	
200	13.14	15.37	16.51	16.11	14.47	9.36	7.58	6.88	7.16	8.00	9.72	11.80	13.84	14.90	14.32	12.37	9.57	6.96	5.10	4.56	5.42	7.13	9.26	11.96	209 22	
201	14.36	15.96	16.14	14.14	12.96	8.01	6.67	6.34	6.89	8.16	10.14	12.46	14.24	14.84	13.50	10.90	8.02	5.86	4.76	5.04	6.32	8.34	10.66	13.15	210 23	
202	15.27	16.14	15.82	11.47	8.96	7.02	6.16	6.33	7.34	9.23	11.44	13.54	14.58	14.24	12.42	9.84	7.44	5.64	5.14	5.97	7.54	9.60	11.76	13.95	212 0	
203	15.50	14.93	12.72	10.10	7.72	6.16	5.77	6.54	7.96	9.86	12.04	13.74	14.37	13.56	11.51	8.97	7.02	5.96	5.96	7.12	8.61	10.53	12.64	15.55	213 2	
204	15.26	13.84	11.46	8.86	6.95	5.97	6.05	5.97	8.56	10.54	12.48	13.67	13.96	12.84	10.98	9.00	7.60	6.88	7.24	8.26	9.66	11.37	14.57	15.10	214 3	
205	14.32	12.72	10.34	8.27	6.67	6.12	6.40	7.34	8.74	10.52	12.26	13.26	13.32	12.36	10.84	9.38	8.24	7.77	8.12	8.86	11.76	13.33	14.29	14.38	215 4	
206	13.46	11.64	9.64	7.76	6.48	6.10	6.50	7.54	9.00	10.63	12.05	12.96	13.18	12.64	11.47	10.24	9.16	8.76	9.66	10.72	12.02	13.24	14.10	14.04	216 5	
207	13.02	11.29	9.63	7.96	6.84	6.50	6.73	7.66	9.04	10.52	12.10	13.14	13.55	13.28	12.50	11.34	10.26	9.35	9.67	10.59	11.83	12.88	13.62	13.44	217 6	
208	12.54	11.15	9.50	7.86	6.50	5.94	6.16	7.10	8.50	10.20	11.94	13.44	14.14	14.16	13.42	10.76	9.56	9.05	9.15	9.96	11.33	12.62	13.38	13.55	218 7	
209	12.96	11.68	9.90	7.96	6.26	5.30	5.46	6.46	8.25	10.24	12.44	14.18	15.26	14.64	12.94	10.78	9.16	8.56	8.76	9.78	11.16	12.57	13.70	14.26	219 8	
210	14.02	12.80	10.52	8.01	5.84	4.76	4.81	5.98	7.77	10.32	13.02	16.66	16.76	15.58	13.24	10.54	8.38	7.60	7.78	8.76	10.54	12.56	14.24	15.18	220 9	
211	14.86	13.21	10.40	7.41	4.97	3.62	3.84	5.16	7.44	13.54	16.14	17.54	17.44	15.84	12.90	9.72	7.44	6.60	6.85	8.10	10.22	12.92	15.15	16.26	221 10	
212	15.72	13.66	10.33	6.96	4.40	3.04	3.33	7.86	11.08	14.56	17.20	18.37	18.04	16.16	12.38	8.82	6.46	5.54	5.95	7.72	10.60	13.60	16.07	17.04	222 11	
213	16.38	13.96	10.25	6.47	3.74	3.20	5.12	8.18	11.74	15.30	17.66	18.50	17.76	14.76	10.60	7.27	5.06	4.48	5.07	7.18	10.36	13.94	16.34	17.16	223 12	
Sum	850.16794	40834.07	773.34	740.77	738.25	669.89	720.18	702.16	784.95	833.44	798.44	878.60	805.26	847.29	775.60	741.31	743.97	687.88	742.40	719.35	778.12	816.92	788.45	No. of Days.		
No.	76	71	76	74	73	77	71	77	72	76	77	71	77	71	77	74	73	76	71	76	72	75	76	71	18574.70	

FORMS FOR SHORT-PERIOD TIDES.

SERIES M<sub>2</sub>N.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
214	16.04	13.12	9.20	5.80	3.36 2.36	3.60	5.73	9.03	12.78	15.94	17.78	18.04	16.74	13.32	9.36	6.05	4.18	3.80	4.90	7.56	11.10	14.46	16.66	16.88	224 13	
215	15.39	12.15	8.23 5.44	3.52	3.32	4.58	7.04	10.14	13.35	16.16	17.52	17.26	15.28	11.80	8.22	5.32	3.80	4.02	5.58	8.40	11.50	14.52	16.18	16.06	225 14	
216	14.18 11.26	7.98	5.62	4.54	4.80	6.25	8.27	11.00	13.96	16.32	17.26	16.42	14.32	10.85	7.62	5.16	4.10	4.64	6.45	8.92	12.05	14.70	15.80	15.18 13.36	226 16	
217	10.62	7.94	6.32	5.74	6.44	7.77	9.72	12.07	14.12	15.66	15.72	14.46	12.06	9.36	6.96	5.40	5.07	5.84	7.33	9.54	11.87	13.60 14.46	13.96	12.48	227 17	
218	10.40	8.65	7.45	7.28	8.00	9.26	10.72	12.27	13.74	14.47	14.18	12.78	10.82	8.78	6.78	5.83	5.86	6.74	8.34	10.14 12.02	13.26	13.57	12.85	11.76	228 18	
219	10.70	9.74	9.12	8.90	9.34	10.06	10.94	12.10	12.88	13.72	13.38	11.88	10.06	8.17	7.02	6.68	7.00	7.70 8.77	10.10	11.44	12.33	12.66	12.46	12.00	229 19	
220	11.36	10.62	10.07	9.67	9.77	10.12	10.82	11.54	12.43	12.67	12.12	11.23	9.96	8.64	7.77	7.46	7.69 8.30	9.04	10.10	11.17	12.34	12.90	12.90	12.34	230 20	
221	11.72	11.15	10.62	10.30	10.00	10.14	10.50	11.34	11.96	12.26	11.97	11.38	10.53	9.44	8.35 7.66	7.57	8.12	9.06	10.48	11.57	12.72	13.42	13.56	13.18	231 21	
222	12.30	11.45	10.72	10.26	9.92	9.63	10.00	10.71	11.62	12.32	12.18	11.42	10.36 9.08	8.15	7.53	7.24	7.70	8.54	9.82	11.43	12.72	13.64	13.66	13.26	232 22	
223	12.36	11.22	10.18	9.34	8.97	9.08	9.88	10.76	11.64	12.26	12.35	11.85 10.40	8.78	7.36	6.44	6.28	7.14	8.37	10.20	11.94	13.38	14.40	14.54	13.58	233 23	
224	12.17	10.70	9.34	8.82	8.84	9.26	10.00	11.16	12.50	13.30 13.42	12.06	10.16	8.40	6.86	6.06	6.14	7.20	8.95	10.80	12.76	13.96	14.91	14.84	13.64	235 0	
225	11.84	9.97	8.77	8.36	8.48	8.96	10.06	11.56 13.12	13.97	13.64	12.06	9.70	7.27	5.96	5.56	6.35	7.80	9.76	11.70	13.66	15.10	15.46	14.62	12.86	236 1	
226	10.57	8.64	7.46	7.31	7.76 10.72	12.64	14.21	14.62	13.44	11.00	8.24	6.24	5.17	5.36	6.54	8.54	10.66	13.00	15.02	15.96	15.50	14.08	11.60	237 2		
227	8.97	7.34	6.70	6.84	6.10 9.62	11.70	13.76	14.95	14.67	12.76	10.00	7.37	5.56	4.97	5.74	7.38	9.36	11.94	14.36	16.04	16.27	15.32	13.08	10.11	238 3	
228	7.72	6.36	6.94	8.63	10.83	13.20	15.21	15.71	14.43	11.89	8.54	6.26	4.97	5.06	6.36	8.22	10.64	13.40	15.80	16.62	16.16	14.21	11.38	8.34	239 4	
229	6.35 5.46	5.74	7.13	9.22	11.84	14.36	15.71	15.48	13.64	10.66	7.60	5.70	4.96	5.70	7.24	9.54	12.02	14.56	16.24	16.56	15.34	12.80	9.60	7.06 5.50	240 6	
230	5.18	5.94	7.72	10.28	13.04	15.14	15.90	14.88	12.52	9.63	7.07	5.74	5.64	6.67	8.36	10.62	13.17	15.30	16.38	15.97	14.06	11.04 8.16	6.11	5.05	241 7	
231	5.41	6.72	8.83	11.26	13.77	15.36	15.38	14.00	11.50	8.72	6.86	5.97	6.34	7.52	9.30	11.47	13.80	15.46	15.84	14.77 12.44	9.37	7.06	5.37	4.85	242 8	
232	5.64	7.12	9.24	11.64	13.96	15.06	14.75	13.17	10.76	8.64	7.30	6.86	7.44	8.64	10.38	12.36	14.06	15.73 15.10	13.64	11.26	8.61	6.5c	5.32	5.38	243 9	
233	6.34	7.85	9.86	11.96	13.64	14.58	14.07	12.68	10.68	8.97	8.02	7.81	8.36	9.26	10.60	12.24	13.73 14.44	13.86	12.25	10.02	8.06	6.46	5.62	5.78	244 10	
234	6.47	7.80	9.63	11.38	12.97	13.74	13.44	12.44	11.04	9.83	8.84	8.57	8.87	9.67	10.67 11.96	13.06	13.46	13.08	11.68	9.86	8.26	6.87	6.17	6.26	245 11	
235	7.02	8.17	9.66	11.26	12.55	13.37	13.57	12.94	11.92	10.73	9.67	9.16	9.18 9.63	10.54	11.48	12.46	12.92	12.66	11.74	10.42	8.87	7.44	6.44	6.21	246 12	
236	6.66	7.76	9.20	10.76	12.36	13.54	14.05	13.67	12.68	11.26	10.02	9.22 8.90	9.14	9.86	10.86	12.02	12.84	12.98	12.36	11.16	9.57	7.60	6.24	5.63	247 13	
237	5.97	7.17	8.80	10.66	12.80	14.28	14.96	14.74	13.66	11.85 10.04	8.66	8.02	8.14	9.04	10.38	12.00	13.14	13.74	13.40	12.04	10.04	7.64	5.76	4.78	248 14	
238	5.02	6.24	8.16	10.78	13.20	15.04	15.98	15.74 14.33	11.96	9.30	7.37	6.55	6.70	8.06	9.98	12.06	13.93	14.86	14.44	12.80	10.18	7.37	5.17	3.90	249 15	
239	4.03	5.50	7.96	10.88	13.80 16.04	17.04	16.46	14.44	11.04	8.24	6.27	5.15	5.63	7.24	9.64	12.52	14.74	15.98	15.40	13.29	9.94	6.63	4.34	3.17	250 16	
240	2.53	5.38	8.20	11.40	14.56 16.82	17.44	16.36	13.83	9.98	6.70	4.46	3.84	4.58	6.80	10.06	13.28	15.76	16.64	15.75	12.94	9.26	6.06	3.66	2.67	251 17	
241	3.72	5.66	8.70 12.20	15.53	17.33	17.53	15.87	12.42	8.56	5.32	3.44	3.17	4.55	7.26	10.87	14.22	16.50	17.05	15.47	12.37	8.44	5.52	3.48	3.10	252 18	
242	4.46 6.74	9.94	13.47	16.22	17.47	17.02	14.77	10.84	7.23	4.52	3.00	3.30	5.07	8.06	11.72	14.94	16.86	16.90	14.94	11.54	8.00	5.38	3.90	4.20 5.52	253 20	
243	7.95	11.06	14.30	16.51	17.04	15.88	12.99	9.17	5.97	3.70	2.94	3.94	6.16	9.14	12.45	15.42	16.68	16.10	13.81	10.56	7.46	5.47 4.87	5.60	7.04	254 21	
244	9.54	12.25	14.81	16.16	16.06	14.44	11.07	7.87	5.34	3.84	3.92	5.16	7.43	10.36	13.44	15.47	16.04	14.92	12.66	9.98 7.74	6.47	6.36	7.02	8.54	255 22	
245	10.58	12.80	14.58	15.36	14.73	12.52	9.86	7.17	5.31	4.44	5.02	6.44	8.50	11.04	13.56	14.79	14.77	13.46	11.46 9.44	8.00	7.36	7.56	8.36	9.51	256 23	
246	11.10	12.60	13.73	13.94	12.90	11.02	8.73	6.90	5.70	5.63	6.34	7.60	9.36	11.36	13.14	13.88	13.60 12.43	10.94	9.64	8.76	8.44	8.70	9.18	9.95	258 0	
247	10.88	12.06	12.76	12.71	11.64	9.87	8.26	7.04	6.44	6.67	7.34	8.36	9.74	11.16	12.22 12.70	12.20	11.38	10.60	9.88	9.34	9.16	9.13	9.34	9.87	259 1	
248	10.66	11.30	11.62	11.37	10.56	9.48	8.44	7.52	7.14	7.33	7.86	8.66	9.84 10.90	11.62	11.97	11.87	11.54	11.08	10.42	9.92	9.60	9.42	9.54	9.86	260 2	



249	10.24	10.70	10.91	10.80	10.34	9.74	9.06	8.35	7.72	7.46	7.67	8.44	10.73	11.52	11.88	13.06	11.88	11.53	10.97	10.23	9.48	9.04	9.01	9.38	261	3	
250	10.01	10.64	11.05	11.18	10.94	10.46	9.52	8.56	7.74	7.42	8.34	9.42	10.67	11.65	12.46	13.84	12.62	12.04	10.96	9.85	8.96	8.54	8.42	8.86	262	4	
251	9.64	10.44	11.33	11.67	11.00	10.92	9.74	8.36	6.68	6.86	7.74	9.24	10.86	12.34	13.24	13.55	13.17	13.08	10.64	9.21	8.06	7.54	7.74	8.74	263	5	
252	9.92	11.30	12.38	12.82	12.42	11.17	7.86	6.55	6.10	6.54	7.88	9.68	11.56	13.16	14.03	14.06	13.18	11.60	9.86	8.07	6.97	6.64	7.14	8.38	264	6	
253	10.20	11.92	13.16	13.44	12.50	8.70	6.90	5.75	5.50	6.36	8.04	10.20	12.32	13.87	14.61	14.36	12.87	10.73	8.45	6.71	5.90	6.17	7.29	9.02	265	7	
254	11.07	13.02	14.14	14.68	10.30	7.96	6.07	5.14	5.48	6.87	9.06	11.46	13.66	15.18	15.37	14.28	12.24	9.67	7.34	5.74	5.30	6.12	7.84	9.97	266	8	
255	12.54	15.33	14.46	13.23	9.34	6.94	5.36	4.94	5.94	8.06	10.08	12.62	14.76	15.76	15.26	13.16	10.67	7.88	5.74	4.48	4.66	6.00	8.44	11.24	267	10	
256	14.50	15.07	15.66	14.20	11.46	8.47	6.20	4.97	5.22	8.86	11.54	14.06	15.76	16.07	14.86	12.14	9.06	6.37	4.56	3.93	4.93	6.93	12.77	15.34	268	11	
257	16.35	15.80	13.61	10.52	7.73	5.58	4.88	5.77	7.56	10.04	12.74	14.90	15.94	15.62	13.71	10.64	7.47	5.10	3.54	3.83	4.93	6.67	14.16	16.01	269	12	
258	16.37	15.04	12.33	9.34	6.97	5.54	5.42	6.51	8.50	11.14	13.77	15.60	15.98	14.86	12.14	8.87	6.16	4.30	3.67	4.44	9.01	12.27	14.84	16.21	270	13	
259	15.96	14.09	11.42	8.56	6.75	5.80	6.17	7.42	9.65	12.22	14.26	15.46	15.24	13.48	10.57	7.95	5.42	4.06	5.34	7.30	9.97	12.69	14.83	15.87	271	14	
260	15.16	13.24	10.76	8.47	7.04	6.68	7.20	8.44	10.38	12.56	14.16	14.83	14.05	12.07	9.24	5.34	4.44	6.61	5.87	7.97	10.37	13.07	14.81	15.06	272	15	
261	14.13	12.37	10.44	8.86	7.87	7.56	7.92	8.94	10.67	12.44	13.74	13.97	12.81	8.83	7.10	5.78	5.25	5.76	6.66	8.34	10.76	12.86	14.16	14.44	273	16	
262	13.68	12.40	10.86	9.52	8.53	8.21	8.56	9.40	10.68	12.08	13.04	13.08	10.54	9.05	7.64	6.61	6.06	6.30	7.07	8.81	10.63	12.30	13.68	14.16	274	17	
263	13.66	12.66	11.46	10.12	9.18	8.77	8.56	9.10	10.17	11.30	12.30	12.14	11.16	9.92	8.44	7.14	6.37	6.38	7.34	8.76	10.57	12.10	13.44	13.92	275	18	
264	13.88	13.56	12.37	11.18	9.72	8.32	7.60	7.94	10.84	12.94	12.52	12.48	11.98	11.16	9.77	7.94	6.58	6.06	6.50	7.97	9.84	11.56	13.26	14.17	276	19	
265	14.66	14.52	13.27	11.31	9.06	7.37	6.82	8.74	10.60	12.11	13.20	14.04	13.84	12.76	10.92	8.58	6.74	5.94	6.30	7.68	9.72	11.97	13.90	15.26	277	20	
266	15.99	15.54	13.97	13.80	8.63	6.62	6.37	7.97	10.25	12.66	14.44	15.38	15.04	13.48	11.07	8.36	6.38	5.47	5.87	7.36	9.62	12.14	14.54	16.28	278	21	
267	16.98	16.37	10.49	7.50	5.61	5.14	5.74	7.77	10.54	13.45	15.71	16.85	16.30	14.16	10.84	7.77	5.85	5.07	5.66	7.50	9.87	12.74	15.25	16.92	279	22	
268	17.15	15.62	8.60	5.94	4.14	3.96	5.28	7.85	11.15	14.38	16.70	17.32	16.33	13.48	9.84	7.20	5.47	4.98	5.96	7.74	10.58	13.66	16.26	17.40	280	0	
269	14.56	10.89	7.40	4.72	3.37	3.98	5.86	8.86	12.43	15.47	17.34	17.64	16.26	12.76	9.26	6.56	5.24	5.38	6.54	8.77	11.76	16.82	17.12	15.72	282	1	
270	12.71	9.14	6.06	3.77	3.17	4.42	6.67	9.72	13.44	16.25	17.55	17.22	15.06	11.70	8.40	6.26	5.44	6.06	7.47	10.01	15.12	16.37	16.06	14.21	288	2	
271	11.04	7.43	4.80	3.12	3.62	5.50	8.04	11.13	14.40	16.25	17.22	16.16	13.58	10.36	7.77	6.24	6.04	6.91	10.52	13.06	15.02	15.64	14.36	11.93	284	3	
272	8.64	6.01	4.31	3.47	4.52	6.20	8.94	11.94	14.56	16.24	16.32	14.74	12.13	9.47	7.47	6.58	6.90	9.30	11.26	13.26	14.41	14.26	12.74	10.35	285	4	
273	7.88	5.80	4.44	4.58	5.92	7.85	10.30	12.70	14.67	15.54	15.01	13.36	11.14	9.11	7.80	7.74	8.64	10.04	11.80	13.04	13.64	13.06	11.36	9.07	286	5	
274	7.14	5.84	5.47	6.20	7.44	9.04	10.97	13.06	14.36	14.36	13.40	11.82	10.44	9.16	8.24	8.54	9.26	10.30	11.46	12.12	12.22	11.46	10.00	8.37	287	6	
275	7.08	6.36	6.44	7.32	8.34	9.60	11.24	12.72	13.46	13.28	12.32	11.06	9.27	8.07	8.94	9.08	9.61	10.14	11.01	11.52	11.46	10.73	9.52	8.47	288	7	
276	7.66	7.41	7.56	8.04	8.76	9.91	11.17	12.30	12.88	12.66	11.92	10.10	9.37	9.76	9.36	9.12	9.08	9.27	9.86	10.44	10.68	10.66	10.30	9.78	9.22	289	8
277	8.56	8.06	7.74	8.02	8.86	10.06	11.16	12.02	12.40	12.40	11.04	10.37	9.76	9.36	9.12	9.08	8.96	9.55	10.22	10.70	10.88	10.82	10.57	10.03	290	9	
278	9.26	8.44	7.90	8.07	8.80	9.84	10.90	12.36	12.58	12.54	12.07	11.12	9.97	9.24	8.77	8.68	8.96	9.27	10.10	10.90	11.50	11.78	11.53	10.67	291	10	
279	9.30	8.14	7.56	7.77	8.55	11.07	12.15	12.94	13.28	13.04	12.24	10.77	9.14	7.88	7.18	7.36	8.12	8.56	9.27	10.10	10.90	11.78	11.53	10.67	291	10	
280	8.86	7.70	7.28	8.65	10.02	11.54	12.81	13.77	14.04	13.50	12.16	10.00	8.34	6.96	6.50	6.88	7.96	9.76	11.52	13.07	13.96	13.77	12.48	10.32	298	12	
281	8.76	7.36	7.26	8.52	10.36	12.17	13.66	14.56	14.48	13.40	11.12	8.84	6.87	5.64	5.46	6.30	8.06	10.30	12.80	14.34	15.00	14.16	12.26	9.06	294	14	
282	6.50	6.22	7.10	8.82	10.86	13.12	14.54	15.07	14.56	12.60	9.98	7.47	5.46	4.56	4.96	6.60	9.03	11.80	14.15	15.84	15.96	14.52	9.24	7.24	295	15	
283	6.16	6.40	6.67	9.66	11.93	14.14	15.62	15.76	14.36	11.76	8.61	6.02	4.24	3.86	5.14	7.32	10.15	13.10	15.67	16.78	16.26	14.16	11.00	6.36	296	16	
284	5.84	6.47	8.16	10.16	12.84	15.02	16.10	15.46	13.28	9.87	6.84	4.45	3.04	3.57	5.44	8.15	11.37	14.60	16.81	16.28	13.64	10.44	7.71	6.07	297	17	
Sum	763.22	723.48	742.65	684.37	754.49	750.38	774.90	824.95	783.66	842.03	772.06	801.67	761.62	701.25	721.91	672.12	732.60	733.30	777.03	824.70	772.57	841.55	763.68	804.51	No. of Days.		
No.	76	73	77	71	77	73	74	76	71	76	71	76	76	72	76	71	76	71	76	77	71	77	71	77	77	18344.52	

FORMS FOR SHORT-PERIOD TIDES.

SERIES M<sub>3</sub>N.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	
285	5.84	6.88	8.87	11.47	14.13	15.94	16.22	14.81	11.87	8.55	5.46	3.46	2.87	4.17	6.35	9.32	13.00	17.47	17.44	15.74	12.68	9.66	7.28	5.94	298 18	
286	6.04	7.36	9.64	12.45	14.84	16.04	15.00	13.70	10.52	7.15	4.66	2.92	3.10	4.72	7.47	13.92	16.35	17.36	16.74	14.57	11.67	8.85	6.76	5.94	299 19	
287	6.48	7.70	9.92	12.68	14.78	15.58	14.78	13.36	9.16	6.36	4.20	3.07	3.72	5.35	11.05	14.10	16.17	16.96	16.12	14.06	11.35	8.82	7.14	6.57	800 20	
288	7.02	8.46	10.56	13.14	14.64	15.04	13.76	11.47	8.74	6.42	4.70	4.22	6.80	9.02	11.88	14.60	16.14	16.22	15.16	13.26	10.86	8.86	7.58	7.14	301 21	
289	7.44	8.84	10.92	12.84	13.84	13.86	12.57	10.68	8.54	6.84	5.37	5.98	7.33	9.36	11.72	14.00	15.22	15.38	14.58	12.98	11.01	9.42	8.12	7.64	302 22	
290	7.92	8.94	10.40	11.82	12.91	13.12	12.36	12.40	7.60	6.08	6.30	6.72	7.86	9.44	11.50	13.34	14.46	14.66	13.96	12.74	11.30	9.76	8.54	7.93	303 23	
291	7.84	8.40	9.60	10.88	12.06	11.66	11.47	10.10	8.76	7.08	7.01	7.06	7.90	9.22	10.97	12.56	13.72	14.38	14.04	13.04	11.45	9.76	8.12	7.22	305 0	
292	7.02	7.48	8.84	10.32	11.48	12.87	12.46	11.36	9.70	8.28	7.14	6.80	7.40	8.84	10.74	12.56	13.87	14.54	14.38	13.40	11.67	9.60	7.53	6.30	306 1	
293	5.88	6.50	8.20	11.93	13.36	14.04	13.66	12.30	10.26	8.61	7.37	6.86	7.24	8.35	10.36	12.50	14.13	15.08	14.96	13.80	11.64	9.03	6.96	5.44	307 2	
294	5.04	5.86	7.70	10.12	12.60	14.54	15.37	14.86	13.04	10.66	8.56	7.12	6.44	6.77	8.02	10.14	12.62	14.56	15.55	15.25	13.56	10.92	8.12	4.22	308 4	
295	5.32	7.70	10.85	13.60	15.51	16.05	15.06	12.86	10.40	8.16	6.53	5.96	6.51	8.24	10.85	13.27	15.16	15.84	15.03	12.98	9.78	7.04	3.46	3.86	309 5	
296	5.60	8.44	11.74	14.04	16.50	16.72	15.38	12.86	9.98	7.70	6.35	5.93	6.71	8.67	11.25	13.84	15.52	15.84	14.55	11.68	8.46	3.63	3.01	4.08	310 6	
297	6.50	9.76	13.08	15.81	17.12	16.72	14.87	12.03	9.20	7.26	6.32	6.37	7.46	9.60	12.20	14.35	15.67	15.28	13.15	7.00	4.47	3.03	3.22	5.03	311 7	
298	7.60	10.76	14.05	16.38	17.05	16.14	13.92	11.10	8.66	6.87	6.16	6.46	8.00	10.44	13.10	14.76	15.10	11.40	8.36	5.66	3.69	2.94	3.94	6.18	312 8	
299	9.01	11.24	14.92	16.53	16.56	15.16	12.66	10.06	7.96	6.74	6.60	7.35	9.00	11.24	13.43	14.36	12.66	9.94	7.20	4.97	3.56	3.77	5.34	7.72	313 9	
300	10.56	13.46	15.04	16.34	15.71	13.92	11.46	9.28	7.66	6.86	6.98	7.98	9.96	12.00	14.50	13.37	11.18	8.81	6.52	4.86	4.33	5.20	6.90	9.14	314 10	
301	11.80	14.20	15.72	15.81	14.68	13.32	10.71	8.96	7.82	7.36	7.92	9.16	12.24	13.26	13.26	13.06	10.17	8.00	6.25	5.31	5.50	6.66	8.34	10.52	315 11	
302	12.80	14.44	15.16	14.68	13.32	11.56	10.02	8.76	8.10	8.00	9.65	10.96	12.18	12.58	12.23	11.04	9.16	7.62	6.54	6.20	6.84	7.96	9.38	11.14	316 12	
303	12.91	14.18	14.40	13.64	12.37	10.90	9.58	8.78	8.46	8.68	10.00	10.94	11.57	11.80	11.36	10.28	8.94	7.84	7.18	7.20	7.86	8.80	9.98	11.46	317 13	
304	12.86	13.86	13.83	12.96	11.72	10.53	9.66	8.92	8.96	9.17	9.66	10.40	11.10	11.37	11.01	10.20	9.26	8.46	8.10	8.14	8.66	9.44	10.56	11.74	318 14	
305	12.76	13.34	13.26	12.61	11.52	9.76	9.04	8.80	8.85	9.16	9.64	10.14	10.74	11.18	11.32	11.06	10.38	9.58	8.94	8.71	8.90	9.50	10.42	11.46	319 15	
306	12.48	13.10	12.64	11.84	10.76	9.71	8.88	8.35	8.19	8.42	9.04	9.96	10.86	11.50	11.80	11.55	10.96	9.98	9.08	8.64	8.75	9.38	10.38	11.46	320 16	
307	12.41	13.07	12.64	11.72	10.14	8.38	7.03	6.27	6.31	7.08	8.83	10.03	11.16	12.23	12.80	12.64	11.66	10.25	9.04	8.36	8.34	8.96	10.38	11.46	321 18	
308	13.23	13.47	13.00	11.72	10.14	8.38	7.03	6.27	6.31	7.08	8.52	10.23	11.92	13.17	13.63	13.10	11.86	10.18	8.76	7.98	7.96	8.75	10.38	11.46	322 19	
309	13.94	13.94	13.04	11.34	9.30	7.45	5.86	5.13	5.46	6.76	8.80	11.15	13.20	14.66	14.98	13.87	11.70	9.58	8.10	7.27	7.36	10.13	11.76	13.33	323 20	
310	14.28	14.14	12.87	10.56	7.98	5.77	4.14	3.74	4.67	6.71	9.27	12.02	14.40	15.66	15.44	13.71	11.16	8.74	7.02	6.78	8.22	10.37	12.22	13.88	324 21	
311	14.74	14.20	12.26	9.36	6.51	4.12	2.75	2.94	4.56	7.03	10.05	13.27	15.65	16.62	15.90	13.76	10.86	6.45	5.84	6.36	8.12	10.44	12.84	14.46	325 22	
312	15.08	13.97	11.41	8.07	4.96	2.57	1.63	2.58	4.74	7.64	11.12	14.22	16.47	17.07	12.96	9.86	7.26	5.65	5.46	6.44	8.40	11.20	13.57	15.11	326 23	
313	15.17	13.27	9.96	6.40	3.62	1.76	1.54	3.26	6.02	9.35	12.97	15.66	17.40	15.75	12.23	9.00	6.75	5.63	5.63	6.88	9.32	12.22	14.44	15.50	328 0	
314	14.60	12.31	8.84	5.46	3.00	1.66	2.20	4.15	6.95	10.46	13.81	17.54	16.82	14.56	11.38	8.50	6.32	5.44	5.74	7.26	10.06	12.76	14.67	15.26	329 1	
315	14.06	11.32	8.05	5.16	2.94	2.16	3.11	5.16	7.96	11.23	16.57	17.22	16.23	13.81	10.68	8.07	6.16	5.50	5.88	7.64	10.23	12.77	14.49	14.72	330 2	
316	13.35	10.74	7.81	5.32	3.66	3.26	4.42	6.34	8.86	14.30	16.33	16.57	15.28	12.84	9.93	7.47	6.23	5.72	6.26	7.94	10.30	12.38	13.76	13.96	331 3	
317	12.68	10.56	8.18	6.38	4.97	4.83	5.73	9.38	12.05	14.37	15.76	15.80	14.56	12.28	9.94	8.13	6.64	6.14	6.54	8.04	10.04	11.78	12.86	13.16	332 4	
318	12.24	10.73	8.96	7.30	5.96	6.24	6.50	7.80	9.84	12.15	13.88	14.87	13.77	11.77	10.06	8.23	6.86	6.34	6.56	7.70	9.30	10.84	12.16	12.76	333 5	
319	12.53	11.48	10.14	7.52	7.06	7.44	8.47	10.17	11.91	13.34	14.21	14.40	13.72	12.30	10.42	8.41	6.88	6.14	6.37	7.32	8.81	10.45	11.84	12.86	334 6	

No.	70	75	73	72	75	70	75	70	73	71	69	75	69	75	72	72	75	69	74	69	74	74	69	74	No. of Days.	729 g.	17766.04																				
320	13.08	12.42	9.75	8.54	7.84	7.88	8.64	10.03	11.65	13.16	14.14	14.30	13.64	12.17	10.31	8.37	6.68	5.72	5.86	6.88	8.64	10.40	12.07	13.31	385	8																					
321	13.61	12.36	10.67	9.06	8.12	7.90	8.54	9.72	11.26	12.78	13.82	14.20	13.74	12.14	10.05	7.76	6.00	5.04	5.23	6.52	8.50	10.50	12.60	13.88	386	9																					
322	13.86	12.58	10.80	8.97	7.94	7.68	8.24	9.50	11.14	12.75	13.98	14.44	13.73	11.85	9.10	6.84	5.06	4.41	5.04	6.57	8.66	10.52	12.61	13.94	387	10																					
323	13.98	13.13	10.86	9.00	7.82	7.54	8.05	9.36	11.14	12.94	14.20	14.46	13.36	11.58	8.58	5.98	4.22	3.96	5.07	6.54	8.66	10.54	12.26	13.84	388	11																					
324	15.17	12.88	10.26	8.38	7.53	7.40	8.14	9.77	11.52	13.36	14.60	14.56	12.94	10.26	7.33	5.11	3.87	3.87	5.64	7.81	10.61	13.20	15.47	16.24	389	12																					
325	14.70	12.20	9.81	8.08	7.33	7.37	8.31	10.05	12.02	13.86	14.76	14.17	12.16	8.93	6.32	4.31	4.64	6.56	9.06	11.87	14.55	16.23	16.72	15.97	340	13																					
326	13.94	11.34	8.98	7.71	7.36	7.70	9.02	10.97	12.94	14.40	14.70	13.44	10.64	8.93	6.32	4.16	5.63	7.85	10.36	13.16	15.34	16.56	16.48	15.11	341	14																					
327	12.72	10.27	8.26	7.37	7.26	8.12	9.82	11.91	13.58	14.48	14.07	12.12	6.72	4.74	3.96	4.91	6.70	9.02	11.70	14.07	15.87	16.56	15.80	13.96	342	15																					
328	11.44	9.32	7.80	7.24	7.44	8.72	10.57	12.53	14.00	14.24	14.07	8.06	5.93	4.58	4.74	6.03	8.20	10.34	12.88	15.05	16.23	16.28	14.89	12.64	343	16																					
329	10.30	8.54	7.57	7.44	8.17	9.64	11.50	13.03	13.80	13.24	9.47	7.26	5.64	5.07	5.86	7.45	9.20	11.48	13.56	15.17	15.82	15.18	13.58	11.42	344	17																					
330	9.46	7.98	7.36	7.62	8.50	10.02	11.60	13.00	12.14	10.36	8.34	6.54	5.59	5.67	6.77	8.43	10.27	12.17	13.90	14.96	14.86	13.76	12.00	10.22	345	18																					
331	8.66	7.73	7.38	7.80	8.82	11.48	12.26	12.24	11.15	9.47	8.01	6.87	6.45	6.75	7.83	9.14	10.75	12.56	13.86	14.46	14.06	12.87	11.31	9.72	346	19																					
332	8.40	7.76	7.73	8.27	9.54	11.48	12.02	11.81	10.84	9.56	8.46	7.76	7.56	8.00	8.95	10.05	11.60	13.13	14.50	14.42	13.82	12.50	10.98	9.56	347	20																					
333	8.76	8.24	8.80	9.36	10.53	11.27	11.70	11.62	11.14	10.38	9.49	8.78	8.48	8.71	9.47	10.70	12.04	13.16	13.78	13.79	13.14	11.94	10.54	8.17	348	22																					
334	7.83	8.04	8.58	9.36	10.22	11.00	11.54	11.74	11.57	10.96	10.14	9.44	9.04	9.10	9.74	10.90	12.24	13.16	13.57	13.38	12.64	11.55	10.54	8.30	349	23																					
335	7.22	7.36	7.86	8.85	10.11	11.13	11.95	12.42	12.30	11.78	10.77	9.72	9.06	9.01	9.55	10.76	11.97	12.94	13.38	13.14	12.44	11.22	10.50	7.04	351	1																					
336	6.26	6.15	6.82	8.20	9.97	11.56	12.90	13.50	13.36	12.36	10.92	9.68	8.84	8.68	9.14	10.18	11.57	12.76	13.22	13.42	13.45	12.54	10.86	8.50	352	2																					
337	4.90	4.92	6.07	7.94	10.07	12.03	13.66	14.38	14.16	12.76	10.77	9.04	7.98	7.73	8.23	9.70	12.74	13.42	13.45	12.54	10.86	8.50	7.18	4.47	353	3																					
338	3.64	4.12	5.82	8.20	10.84	13.27	14.95	15.70	14.97	13.05	10.60	8.64	7.50	7.36	8.16	9.80	13.38	14.33	14.26	13.00	10.50	7.72	5.17	3.42	354	3																					
339	2.93	4.16	6.37	9.77	13.27	16.13	17.72	17.51	15.78	13.11	10.34	8.06	6.98	7.06	7.94	9.04	10.00	12.15	14.04	15.14	15.03	13.10	10.20	7.00	4.37	355	4																				
340	2.20	3.93	6.57	9.77	13.27	16.13	17.72	17.51	15.78	13.11	10.34	7.27	6.36	7.50	8.86	12.72	14.77	15.81	15.20	12.64	9.26	5.91	4.37	1.55	356	5																					
341	1.93	4.00	7.06	10.68	14.30	17.04	18.34	17.72	15.47	13.00	9.74	6.14	6.00	7.50	9.06	13.10	15.24	16.17	14.94	12.16	8.55	5.06	2.64	1.50	357	6																					
342	2.57	5.14	8.44	11.93	15.00	17.66	18.34	17.37	14.51	13.77	5.66	5.14	5.64	7.65	10.63	13.44	15.46	15.86	14.14	10.98	7.68	4.48	2.36	1.77	358	7																					
343	3.30	5.83	8.90	12.30	15.50	17.50	16.62	13.58	9.97	6.94	5.14	4.70	5.52	7.63	10.73	13.70	15.36	15.32	13.24	9.92	6.64	4.73	3.07	3.08	359	8																					
344	4.74	6.97	9.86	13.01	15.80	17.48	15.95	12.86	9.53	6.72	5.22	4.90	5.87	8.03	10.96	13.30	14.68	14.83	13.24	10.55	7.68	5.43	4.33	4.63	360	9																					
345	5.97	8.02	10.57	13.25	16.00	16.14	14.11	11.13	8.76	6.38	5.17	5.13	6.30	8.60	10.76	12.74	13.74	13.62	12.37	10.30	8.14	6.53	5.84	6.14	361	10																					
346	7.14	8.74	13.13	14.96	15.71	15.12	13.32	10.86	8.44	6.53	5.48	5.27	6.00	7.98	9.85	11.62	12.84	13.10	12.38	10.74	9.22	7.96	7.33	7.28	362	12																					
347	9.16	10.97	13.12	14.54	14.68	13.66	12.28	10.12	8.24	6.78	5.82	5.70	6.37	7.92	9.40	11.06	12.32	12.86	12.50	11.47	10.24	8.42	8.24	8.54	363	13																					
348	9.54	11.12	12.64	13.57	13.57	12.88	11.44	9.87	8.24	6.74	5.77	5.52	6.12	7.27	8.94	10.64	12.10	13.01	13.12	12.46	10.02	9.06	8.58	8.66	364	14																					
349	9.44	10.68	11.96	12.92	13.14	12.66	11.54	10.06	8.36	6.86	5.72	5.37	5.87	7.17	8.94	11.00	12.70	13.68	13.81	11.57	10.28	9.14	8.62	8.63	365	15																					
350	9.20	10.44	11.66	12.53	12.92	12.58	11.61	9.77	7.86	6.12	5.02	4.78	5.62	7.06	8.91	11.26	13.23	14.32	13.94	11.78	10.34	9.17	8.44	8.24	366	16																					
351	8.62	9.76	11.04	12.36	13.08	12.90	11.65	9.64	7.34	5.52	4.45	4.52	5.76	7.66	9.97	12.43	15.18	14.97	13.73	11.82	10.16	8.86	8.24	8.26	367	17																					
352	8.96	10.32	11.70	12.96	13.58	13.16	11.26	8.91	6.66	4.96	4.33	4.86	6.36	8.55	13.44	15.21	15.84	15.17	13.56	11.44	9.66	8.38	7.80	7.97	368	18																					
353	9.00	10.56	12.24	13.46	13.82	12.72	10.52	7.90	5.74	4.34	4.11	5.34	9.78	12.44	14.65	15.94	14.74	12.37	10.23	8.53	7.47	7.31	7.97	369	19																						
364	9.38	11.36	13.14	14.17	14.00	12.18	9.43	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	370	2																				
Sum	668	13.7	45.51	761	14.78	530	841.04	787	50	825.43	734	66	729	26	698	87	625	63	678	61	641	45	333	82	724	99	785	00	850	23	784	208	13	57	27	10	738	31	709	48	647	33	693	33	No. of Days.	729 g.	17766.04

FORMS FOR SHORT-PERIOD TIDES.

BOMBAY—Commencing 0 hours, Astronomical Time, 1st January, 1885.

SERIES M<sub>2</sub>K<sub>1</sub>. Motion per mean Solar hour = 44°.0251728.

Argument (3γ - 2σ).

Table with 36 columns (Day, 0h-23h) and 36 rows. Each column represents an hour of the day, and each row represents a day. The cells contain numerical values in feet. The final column (23h) contains the Solar Hour and the corresponding day number.

No.	75	74	74	75	74	74	74	75	74	74	75	74	74	75	74	74	75	74	75	74	75	74	75	No. of Days.	
86	9.30	7.54	6.26	6.13	6.68	7.86	9.28	10.86	12.27	13.10	12.94	11.93	10.66	9.72	9.12	9.06	9.26	10.60	11.82	12.86	13.34	12.82	11.45	87.18	
87	10.03	8.74	7.48	6.86	6.78	7.17	7.94	9.05	10.30	11.34	11.97	11.92	11.42	10.84	10.34	10.07	9.97	9.77	10.44	11.32	12.06	12.26	11.78	10.88	88.19
88	9.87	8.84	7.86	7.24	6.94	7.18	8.03	9.07	10.14	11.00	11.56	11.85	11.77	11.46	11.12	10.57	10.07	9.94	10.70	10.13	10.80	11.27	11.45	11.25	89.19
89	10.76	9.97	9.00	8.00	7.11	6.58	6.74	7.44	8.51	9.84	10.90	11.76	12.34	12.55	12.30	10.57	9.76	9.34	9.17	9.56	10.24	10.94	11.36	11.44	90.20
90	10.97	10.10	9.07	7.87	6.85	6.30	6.50	7.26	8.50	10.16	11.44	12.65	13.26	13.32	12.56	11.36	10.08	9.16	8.67	8.64	9.01	9.76	10.58	11.25	41.20
41	11.66	11.34	10.36	8.82	7.36	6.12	5.54	5.82	6.94	8.54	10.36	13.46	13.97	13.64	12.30	10.76	9.26	8.14	7.84	8.12	8.96	10.24	11.52	12.40	42.21
42	12.66	12.07	10.47	8.56	6.64	5.46	5.20	5.93	7.55	9.56	11.72	14.85	15.64	15.23	13.64	11.13	9.02	7.54	6.79	7.00	8.13	9.87	11.85	13.60	44.22
43	13.62	13.60	12.30	10.24	7.77	5.88	4.84	4.96	8.27	10.66	13.07	14.85	15.82	15.96	14.78	12.26	9.64	7.46	6.24	5.96	6.74	8.48	10.85	13.07	45.22
44	14.38	13.88	11.93	9.10	6.54	4.66	4.00	4.90	8.66	9.20	11.97	14.34	16.64	16.01	13.87	10.90	8.00	6.17	5.46	5.74	7.26	9.70	12.25	14.42	46.23
45	14.56	14.85	13.63	10.90	7.86	5.57	4.04	5.46	7.84	10.63	13.64	15.83	16.64	16.01	13.87	10.90	8.00	6.17	5.46	5.74	7.26	9.70	12.25	14.42	46.23
46	15.50	15.15	13.08	9.90	6.94	4.75	3.92	4.66	6.62	9.46	12.60	15.08	16.60	16.64	15.00	11.93	8.96	6.76	5.63	5.06	5.84	7.84	10.54	13.30	47.23
47	15.12	15.66	11.76	8.44	5.86	4.26	4.25	5.52	7.84	10.68	13.68	15.84	16.68	15.86	13.15	10.22	7.36	5.65	4.25	4.46	6.07	8.56	11.57	14.06	49.0
48	15.54	15.51	13.57	10.53	7.47	5.38	4.52	5.04	6.70	9.14	12.18	14.74	16.26	16.26	14.64	11.74	8.68	6.38	4.54	4.14	5.97	7.06	9.74	12.44	50.0
49	14.55	14.76	12.57	9.68	7.24	5.84	5.60	6.54	8.40	10.77	13.32	15.42	16.26	15.47	13.18	10.24	7.54	5.62	4.54	4.69	5.80	7.87	10.40	12.80	51.1
50	14.50	15.06	14.03	11.86	9.36	7.58	6.64	6.76	7.86	9.60	11.66	13.73	15.08	15.32	14.12	11.86	9.24	6.90	5.18	4.58	5.06	6.46	8.24	10.33	52.2
51	13.86	14.34	13.44	11.46	9.53	8.05	7.40	7.66	8.58	9.92	11.68	13.36	14.16	14.12	12.82	10.83	8.73	6.87	5.45	4.92	5.44	6.63	8.23	10.14	53.2
52	11.77	12.96	13.40	12.76	11.56	10.24	9.04	8.45	8.28	8.67	9.76	11.20	12.50	13.18	13.06	11.88	10.25	8.57	5.77	5.38	5.64	6.37	7.82	9.54	54.3
53	11.17	12.38	13.02	12.96	12.16	11.07	10.02	8.94	8.44	8.48	9.57	10.44	11.57	12.34	12.34	11.70	10.50	8.90	7.32	5.98	5.24	5.12	5.86	7.17	55.3
54	8.90	10.63	12.10	13.16	13.50	13.13	11.86	10.27	8.88	8.08	7.98	8.42	9.56	10.87	11.93	12.44	11.27	9.76	7.96	6.27	5.06	4.55	5.02	6.47	56.4
55	8.52	10.67	12.72	14.44	14.86	14.44	12.70	10.66	8.80	7.60	7.21	7.64	9.18	11.00	12.40	13.36	13.52	12.60	8.63	6.40	4.63	4.06	4.70	57.4	
56	6.46	8.84	11.30	13.80	15.56	16.25	15.33	12.96	10.26	7.95	6.54	6.18	7.03	11.00	12.96	14.40	14.74	13.76	11.70	8.84	6.08	4.05	3.42	4.14	58.5
57	6.18	8.80	12.06	14.93	16.76	17.15	15.84	12.87	9.66	7.00	5.18	5.12	6.26	8.52	11.16	13.67	15.86	14.57	11.93	8.26	4.05	3.42	2.92	2.92	59.5
58	4.14	6.52	9.58	13.16	16.04	17.62	17.34	15.27	11.66	8.27	4.16	4.32	5.84	8.66	11.92	14.74	16.46	16.54	14.66	11.26	7.66	4.94	3.20	3.27	60.6
59	4.70	7.52	10.86	14.63	17.06	17.98	16.96	13.90	10.20	6.96	4.47	3.56	4.02	6.04	9.40	12.86	15.55	16.86	16.36	13.86	10.44	6.92	4.54	3.37	61.6
60	3.90	5.80	8.56	12.33	15.44	17.27	17.40	15.46	11.66	8.27	3.74	3.37	4.33	7.10	10.34	13.76	15.97	16.76	15.76	12.96	9.44	6.74	4.67	4.23	62.7
61	5.26	7.43	10.37	13.82	16.13	17.08	16.40	13.86	10.50	7.26	4.84	3.56	3.86	5.60	8.27	11.55	14.34	16.02	16.28	14.66	11.66	8.60	6.46	5.26	63.7
62	5.46	6.56	8.80	11.44	15.97	16.18	14.88	12.00	8.80	6.28	4.57	4.66	4.86	6.67	9.40	12.24	14.39	15.64	15.33	13.25	10.46	8.22	6.76	6.34	64.8
63	7.00	8.36	10.22	12.44	14.42	15.27	14.71	12.72	10.14	7.72	5.93	4.86	5.00	6.10	8.03	10.30	12.47	13.97	14.58	13.92	12.03	10.14	8.54	7.56	65.8
64	7.56	8.42	11.34	12.96	14.04	14.24	13.22	11.36	9.36	7.56	6.27	5.84	6.34	7.46	9.00	10.76	12.44	13.56	13.74	12.74	11.40	10.07	9.16	8.96	66.9
65	9.27	9.77	10.46	11.36	12.44	13.07	13.03	12.12	10.40	8.86	7.68	7.02	7.02	7.66	8.54	9.66	10.96	12.24	12.88	12.88	12.24	11.43	10.24	10.16	67.10
66	10.24	10.47	10.86	11.44	12.02	12.40	12.24	11.36	10.18	8.87	7.97	7.07	7.94	8.50	9.00	9.78	10.74	11.76	12.46	12.67	12.27	11.74	11.26	10.87	68.10
67	10.56	10.36	10.22	10.36	10.76	11.26	11.56	11.38	10.86	9.96	9.14	8.40	7.98	7.80	7.86	8.34	9.30	10.46	11.44	12.08	12.27	12.03	11.50	10.78	69.11
68	10.20	9.73	9.58	9.87	10.35	10.89	11.10	11.10	10.78	10.32	9.72	8.86	7.97	7.28	7.26	7.87	8.97	10.32	11.56	12.46	13.04	13.10	11.68	70.11	
69	10.56	9.64	9.08	8.82	9.16	9.88	10.74	11.40	11.75	11.70	11.14	10.07	8.84	7.56	6.74	6.70	7.63	10.02	12.06	13.26	13.78	13.68	11.34	71.12	
70	9.88	8.86	8.16	8.03	8.46	9.64	10.86	12.06	12.78	12.56	11.57	9.92	8.17	6.67	5.98	6.16	7.20	8.87	10.76	13.26	13.78	14.06	14.06	12.53	72.12
71	10.68	8.96	7.55	6.88	7.05	8.07	9.84	11.76	12.97	13.54	13.03	11.46	9.42	7.27	5.30	5.90	7.44	9.66	11.92	14.02	15.17	15.16	13.87	11.66	73.13
72	9.44	7.56	6.34	6.07	6.86	8.68	10.80	12.96	14.26	14.55	13.37	11.16	8.45	6.26	5.16	5.12	6.24	8.10	10.63	13.22	15.15	15.86	15.17	13.22	74.18
73	10.40	7.86	6.06	5.25	5.54	6.90	9.24	11.72	13.93	15.20	15.12	13.39	7.57	5.44	4.44	4.96	6.46	8.94	11.85	14.34	16.00	16.06	14.53	11.64	75.14
Sum	781.78	858.51	791.85	794.77	802.45	814.07	828.77	844.75	862.84	883.84	907.25	933.75	963.77	997.53	1040.07	1092.79	1157.99	1239.09	1339.75	1454.37	1598.24	1774.05	1985.36	2490.56	No.
No.	75	74	74	74	75	74	74	75	74	74	74	70	74	74	76	75	74	75	75	75	74	75	74	74	154

FORMS FOR SHORT-PERIOD TIDES.  
 SERIES M<sub>2</sub>K<sub>1</sub>.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour d h
74	8.54	5.76	4.22	3.97	5.24	7.30	10.10	13.02	15.04	16.00	15.20	12.86	9.54	6.67	4.92	4.38	5.52	7.55	10.33	13.50	15.75	16.73	16.07	13.66	76 14
75	10.42	7.22	4.92	3.64	4.00	5.66	8.33	11.52	14.36	16.52	15.06	12.13	8.73	6.13	4.66	4.99	6.52	8.92	11.86	14.66	16.40	16.56	15.07	11.90	77 15
76	8.47	5.62	3.74	3.22	4.26	6.00	9.60	12.85	15.23	16.56	16.25	14.26	10.83	8.00	5.75	5.11	5.88	7.84	10.46	13.38	15.68	16.60	15.80	13.36	78 15
77	10.12	7.06	4.83	3.54	3.76	5.34	8.00	11.00	13.93	16.74	15.74	13.36	10.24	7.64	6.12	6.08	7.14	9.00	11.56	13.90	15.66	15.98	14.76	12.06	79 16
78	8.90	6.13	4.34	3.62	4.36	6.06	8.47	11.31	13.87	15.62	16.12	14.97	12.74	10.02	8.05	6.96	7.06	7.93	9.67	12.07	14.08	15.23	15.08	13.57	80 16
79	11.16	8.26	6.08	4.70	4.70	6.49	9.48	11.88	13.90	15.36	15.50	14.66	12.67	10.54	8.74	7.94	8.14	9.06	10.62	12.40	13.77	14.52	14.20	12.80	81 17
80	10.64	8.47	6.76	5.86	5.82	6.49	7.75	9.52	11.71	13.54	14.73	14.90	14.06	12.63	11.05	9.70	8.86	8.72	9.12	10.24	11.76	13.06	13.60	12.06	82 16
81	10.56	8.92	7.40	6.43	6.30	6.68	7.68	9.46	11.24	13.02	14.08	14.52	14.22	13.04	11.70	10.34	9.24	8.84	9.04	9.84	10.96	12.05	12.86	12.96	83 18
82	12.44	11.22	9.67	8.30	7.06	6.48	6.64	7.48	8.86	10.64	12.34	13.74	14.48	14.44	13.62	12.12	10.36	8.96	8.11	7.96	8.44	9.76	11.26	12.36	84 19
83	12.78	11.94	10.30	8.78	7.20	6.06	5.92	6.72	8.34	10.26	12.20	13.86	15.00	15.14	14.16	12.20	9.88	8.00	6.90	6.56	7.46	9.22	11.16	12.56	85 19
84	13.57	14.06	13.37	11.72	9.38	7.17	5.72	5.38	6.17	7.82	10.00	12.50	14.54	15.84	15.94	14.64	12.14	9.36	6.97	5.63	6.67	8.88	11.24	13.46	86 20
85	14.86	15.36	14.34	12.05	9.44	6.93	5.38	5.00	5.82	7.83	10.50	13.30	15.60	16.72	16.28	14.37	11.37	8.36	6.97	5.74	6.00	8.40	9.20	12.06	87 20
86	14.62	16.11	16.16	14.90	12.22	9.12	6.60	5.05	4.86	5.87	8.10	11.14	14.15	16.35	17.15	13.58	10.14	7.06	4.83	3.96	4.67	7.70	9.92	13.20	88 21
87	15.64	17.04	16.75	14.92	11.81	8.56	6.27	5.14	5.64	6.94	9.43	12.61	15.44	17.03	17.08	15.36	11.92	8.64	6.18	4.48	4.25	5.24	7.57	11.00	89 21
88	14.10	16.44	17.34	16.56	14.28	10.82	7.84	5.95	5.42	6.12	7.87	10.62	16.10	17.14	16.46	13.96	10.44	7.12	4.80	3.83	4.41	6.43	8.78	12.04	90 22
89	14.74	16.66	17.13	15.64	12.86	9.53	7.16	5.81	5.93	7.22	9.26	12.02	14.66	16.44	16.67	15.06	12.02	8.56	5.84	4.04	3.84	4.93	7.24	10.09	91 22
90	13.22	15.56	16.90	16.56	14.74	11.68	8.84	7.02	6.48	7.04	10.50	13.00	14.94	15.83	15.12	12.96	9.87	7.14	5.16	4.22	4.76	6.40	8.73	11.37	92 23
91	14.00	15.82	16.34	15.34	13.10	10.40	8.36	7.32	7.28	8.03	9.50	11.53	13.48	14.74	14.92	13.67	11.34	8.76	6.67	5.40	5.22	6.16	7.85	9.97	93 23
92	12.30	14.30	15.48	15.46	14.27	12.24	10.20	8.26	7.47	9.24	10.52	12.04	13.48	14.16	13.84	12.27	10.16	8.14	6.47	5.74	6.22	7.44	9.20	10.85	95 0
93	12.64	14.05	14.67	14.27	12.97	11.44	10.04	9.16	8.84	9.16	9.84	10.95	11.96	12.80	12.96	12.28	10.94	9.24	7.80	6.78	6.70	7.30	8.37	9.54	96 0
94	10.90	12.34	13.52	13.80	13.26	12.13	10.94	9.60	9.33	9.54	9.90	10.56	11.44	11.92	12.05	11.54	10.36	8.14	6.47	5.74	6.22	7.44	8.52	9.46	97 1
95	10.73	11.93	12.74	12.98	12.60	11.86	11.07	10.34	9.94	9.77	9.87	10.02	10.36	10.83	11.14	11.27	10.92	10.30	9.34	8.36	7.74	7.58	7.98	8.76	98 1
96	9.87	11.04	12.50	12.66	12.42	11.96	11.34	10.55	9.91	9.47	9.34	9.52	9.94	10.53	10.94	11.12	11.02	10.62	10.00	9.22	8.40	8.01	8.13	8.63	99 2
97	9.70	10.66	11.77	12.66	13.06	12.94	12.40	11.47	10.50	9.62	8.94	8.54	8.74	9.48	10.45	11.36	11.88	11.89	11.44	10.50	9.40	8.46	7.76	7.76	100 3
98	9.46	10.86	12.36	13.36	13.82	13.66	12.66	11.42	10.02	8.72	7.96	7.82	8.36	9.47	10.86	11.90	12.70	12.87	12.44	11.06	9.52	8.12	7.40	7.40	101 3
99	8.26	9.54	11.08	12.70	14.06	14.56	14.22	12.80	10.96	8.88	7.46	6.81	6.84	7.92	9.62	11.52	13.00	13.97	14.12	13.00	9.05	7.48	6.74	6.92	102 4
100	7.97	9.72	11.72	13.58	14.86	15.12	14.21	12.35	9.67	7.47	5.98	5.58	6.14	7.76	9.84	12.16	14.02	15.18	15.06	13.40	10.95	8.28	6.66	6.02	103 4
101	6.46	7.88	10.06	12.53	14.55	15.72	15.49	13.80	11.08	8.22	5.93	4.52	4.32	5.47	7.72	10.54	13.37	16.20	15.32	13.00	9.88	7.34	5.76	5.40	104 5
102	6.24	8.22	10.70	13.40	15.52	16.25	15.36	12.80	9.46	6.56	4.47	3.42	3.91	5.74	8.31	11.40	14.40	16.28	16.72	15.47	12.68	9.44	6.81	5.47	105 5
103	5.38	6.52	8.91	11.80	14.40	15.97	16.08	14.35	11.30	7.80	4.97	2.93	2.46	6.21	9.51	12.97	15.58	17.14	17.04	14.94	11.68	8.36	6.14	5.06	106 6
104	5.57	7.24	10.07	13.10	15.40	16.44	15.82	13.44	9.74	6.67	4.03	2.50	2.77	4.44	7.56	10.96	14.33	16.70	17.72	16.91	13.47	10.87	8.10	6.15	107 6
105	5.71	6.50	8.36	11.33	14.12	15.97	16.50	15.10	12.22	8.67	5.24	3.56	3.47	5.74	8.64	12.02	15.12	16.94	17.54	16.24	13.40	10.32	7.62	6.17	108 7
106	6.07	7.04	9.13	12.00	14.47	15.69	15.54	13.66	10.74	7.44	4.88	3.28	3.04	4.36	6.67	9.40	12.47	15.00	16.74	16.94	15.60	13.03	10.01	7.87	109 7
107	6.76	6.80	7.71	9.70	12.14	14.15	15.02	14.50	12.53	7.24	5.36	4.17	4.16	5.20	7.26	9.89	12.40	14.57	15.77	15.74	14.47	12.12	9.90	8.97	110 8
108	7.14	7.11	7.83	9.54	11.58	13.16	13.74	13.74	11.76	9.56	7.60	5.96	4.93	5.02	5.86	7.52	9.74	12.00	13.87	14.87	14.77	13.76	12.06	10.26	111 6

109	8.74	7.82	7.54	8.00	9.34	11.00	12.96	12.72	11.58	10.14	8.48	6.94	6.06	5.96	6.60	7.87	9.72	11.62	13.34	14.34	14.44	13.66	13.26	10.62	11.2	9		
110	9.10	8.03	7.66	7.76	8.68	10.20	11.63	13.43	12.66	12.10	10.96	9.47	8.14	7.03	6.51	6.88	7.94	9.57	11.42	13.00	14.07	14.44	13.93	12.76	11.8	9		
111	11.00	9.18	7.74	6.96	7.85	9.40	10.96	12.36	13.06	13.12	12.22	10.65	8.87	7.52	6.74	6.84	7.66	9.26	11.04	12.88	14.12	14.66	14.30	12.64	11.4	9		
112	10.64	8.60	6.78	5.94	5.93	7.08	9.00	11.04	12.64	13.72	13.87	12.97	11.36	9.32	7.66	6.62	6.47	7.28	8.88	10.96	12.96	14.54	15.17	14.54	11.5	11		
113	10.22	7.74	5.76	4.88	5.14	6.58	8.88	11.33	13.36	14.66	14.94	13.86	11.70	9.34	7.26	6.22	6.20	7.24	9.00	11.22	13.36	14.86	15.37	14.44	11.6	11		
114	12.10	9.16	6.48	4.70	4.20	4.74	6.70	9.17	11.77	14.02	15.37	15.54	14.03	11.54	8.80	6.96	6.07	6.31	7.48	9.44	11.06	15.48	15.37	13.84	11.7	12		
115	10.92	7.66	5.31	3.77	3.70	5.12	7.30	10.10	12.94	15.14	16.26	15.76	13.86	11.00	8.24	6.47	5.97	6.34	7.98	10.16	12.70	14.64	15.66	14.96	11.8	12		
116	12.70	9.46	6.57	4.32	3.42	4.04	5.86	8.48	11.42	14.32	16.17	16.57	15.46	12.94	10.06	7.64	6.36	6.82	8.40	10.90	13.45	15.07	15.35	13.81	11.9	13		
117	11.00	7.70	5.15	3.44	3.36	4.67	6.96	9.52	12.56	14.92	16.36	16.28	14.70	11.93	9.06	7.20	6.40	6.70	7.74	9.37	11.47	13.86	15.04	15.06	12.0	13		
118	12.96	9.73	7.17	4.24	3.42	4.04	5.68	8.27	10.68	13.46	15.48	16.23	15.62	13.50	10.52	6.20	6.40	7.02	8.34	10.44	12.60	14.08	14.45	13.26	12.1	14		
119	10.82	7.87	5.57	3.94	3.86	4.88	6.80	9.18	11.76	14.24	15.56	15.54	14.30	11.86	9.46	7.76	6.94	7.06	7.86	9.36	11.24	13.06	13.96	13.66	12.2	14		
120	11.90	9.20	6.72	5.07	4.36	4.90	6.32	8.22	10.36	12.80	14.56	15.43	14.76	10.84	8.96	7.76	7.44	7.70	8.80	10.26	11.91	13.06	13.30	12.28	12.3	15		
121	10.40	8.28	6.46	5.35	5.20	6.00	7.54	9.26	11.42	13.34	14.60	14.86	13.86	12.06	10.14	8.84	8.15	8.06	8.40	9.36	10.55	11.36	11.86	12.46	12.4	15		
122	11.36	9.38	7.94	6.74	6.04	6.20	7.12	8.46	10.24	13.38	14.08	13.92	12.90	11.41	10.00	8.90	8.46	8.30	9.00	9.74	10.55	11.36	11.86	12.46	12.4	15		
123	10.72	9.26	7.86	6.96	6.92	7.41	8.22	9.26	10.47	12.10	13.34	13.78	13.40	12.16	10.87	9.94	9.24	8.96	8.94	9.17	9.58	10.34	10.96	11.44	12.6	16		
124	11.34	10.58	9.56	8.46	7.76	7.66	7.87	9.74	10.97	12.22	13.24	13.54	13.24	12.12	10.96	9.98	9.27	8.94	8.74	8.80	9.24	10.03	10.80	11.26	12.7	17		
125	11.29	10.79	10.06	9.26	8.46	8.06	8.04	8.56	9.72	10.94	12.20	12.06	13.22	12.94	12.14	11.17	9.96	8.96	8.20	7.92	8.00	8.62	9.56	10.46	12.8	17		
126	11.34	11.77	11.44	10.70	10.74	10.70	8.17	8.10	8.66	10.93	12.30	13.21	13.50	13.18	12.36	11.16	9.68	8.30	7.26	6.90	7.45	8.52	10.00	11.40	12.9	18		
127	12.36	12.92	12.66	11.62	10.20	8.85	8.06	7.83	8.24	9.37	10.96	12.50	13.57	14.02	13.54	12.37	10.74	8.97	7.34	6.24	5.98	6.71	8.26	10.20	13.0	18		
128	12.12	14.22	13.67	12.20	10.16	8.55	7.53	7.27	7.93	9.36	11.30	13.16	14.26	14.66	13.94	12.24	9.97	7.60	5.85	4.92	5.06	6.42	8.60	10.95	13.1	19		
129	13.28	14.84	15.34	14.46	12.38	10.01	8.14	6.95	6.96	8.01	9.74	11.84	13.66	14.84	15.16	14.10	11.76	8.83	6.14	4.18	3.66	4.53	6.46	11.92	13.2	20		
130	14.30	15.96	16.28	14.95	12.41	9.36	7.14	6.17	6.50	7.92	10.02	12.44	14.46	15.64	15.47	13.76	10.66	7.20	4.46	2.86	2.74	4.17	6.63	9.77	13.3	20		
131	13.00	15.72	17.16	16.96	15.18	11.90	8.78	6.57	5.95	6.52	7.94	10.30	12.84	15.02	15.97	15.24	12.56	8.80	5.70	3.17	2.43	4.23	7.22	10.62	13.4	21		
132	13.96	16.50	17.69	17.06	14.58	10.90	8.02	5.94	5.84	6.30	8.25	10.90	13.74	15.64	16.06	14.62	11.54	7.86	4.52	2.14	1.42	2.56	5.03	8.20	13.5	21		
133	11.45	14.68	16.97	17.83	16.77	14.06	10.36	7.60	5.84	5.52	6.20	8.20	11.20	14.02	15.72	15.74	13.76	7.86	4.07	2.24	1.86	3.24	5.60	8.58	13.6	22		
134	12.24	15.14	17.16	17.74	16.33	13.21	10.00	7.30	5.76	5.60	6.58	8.80	11.97	14.34	15.47	15.07	12.82	9.66	6.56	4.08	2.67	2.88	4.46	6.78	13.7	22		
135	9.71	12.92	15.50	17.10	17.16	15.40	12.67	9.57	7.36	6.16	6.11	7.20	9.40	12.06	14.98	14.36	12.18	9.28	6.58	4.76	3.86	4.30	5.66	7.78	13.8	23		
136	10.44	13.15	15.36	16.54	16.23	14.86	11.94	9.56	7.54	6.48	6.38	7.36	9.30	11.76	13.38	13.98	13.42	11.66	9.36	7.30	5.74	4.98	5.26	6.33	13.9	23		
137	8.08	10.42	12.87	14.66	15.72	15.46	14.00	11.78	9.46	7.72	6.82	7.44	8.91	10.74	12.30	13.13	12.92	11.76	10.08	8.18	6.84	6.28	6.46	7.26	14.1	0		
138	8.54	10.38	12.48	14.22	14.94	14.74	13.52	11.62	9.46	7.84	6.66	5.72	7.44	8.91	10.74	12.30	13.13	12.92	11.76	10.08	8.18	6.84	6.28	6.46	7.26	14.1	0	
139	7.36	8.54	10.16	11.86	13.27	14.14	13.98	11.14	9.14	7.48	6.36	5.86	6.83	8.02	9.54	11.12	12.28	12.33	12.07	10.86	9.35	7.86	6.87	6.74	14.2	0		
140	7.70	8.44	10.00	11.62	13.06	13.93	13.82	12.68	10.82	9.01	7.20	5.72	5.93	7.12	8.94	10.74	12.22	12.86	12.65	11.60	10.06	8.56	7.47	7.24	14.3	1		
141	7.47	7.63	8.26	9.76	11.56	13.14	14.05	13.96	12.62	10.76	6.66	5.32	5.17	5.56	6.97	8.92	10.90	12.46	13.44	13.42	12.46	10.72	9.12	8.02	14.4	1		
142	7.52	7.50	8.44	10.16	11.93	13.46	14.20	13.97	12.62	10.50	7.84	5.72	4.46	4.54	5.90	7.82	10.17	12.67	14.36	15.22	14.76	13.34	11.12	9.16	14.6	2		
143	7.84	7.36	8.72	10.32	12.06	13.66	14.36	13.76	11.92	9.27	6.82	4.82	3.97	4.57	6.16	8.40	11.03	13.46	15.10	15.52	14.67	12.94	10.67	8.77	14.7	3		
144	7.60	7.38	7.93	9.10	10.86	12.73	14.28	14.53	13.00	10.66	7.86	5.58	4.22	4.13	5.24	7.24	9.70	12.30	14.40	15.74	15.70	14.12	12.14	9.74	14.8	4		
145	7.64	7.54	8.20	9.70	11.80	13.62	14.54	14.16	12.22	9.68	6.84	4.84	3.94	4.50	6.00	8.33	10.94	13.60	15.42	16.13	15.62	13.90	11.47	9.48	14.9	4		
Sum	764.60	765.01	775.40	762.54	773.08	759.32	753.59	741.94	752.55	752.99	751.73	749.21	786.09	782.56	766.03	779.76	765.55	729.65	718.63	720.51	722.85	733.23	763.80	782.11	No. of Days.	79° 14'	35	
No.	73	73	75	73	74	74	74	73	74	74	74	72	74	74	72	74	74	73	73	74	73	73	74	75	75	75	1814	35

FORMS FOR SHORT-PERIOD TIDES.

SERIES M<sub>2</sub>K<sub>1</sub>—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
146	7.84	7.40	7.74	8.92	10.62	12.60	14.02	14.77	13.22	10.78	8.10	5.76	4.27	4.17	5.26	7.20	9.70	12.28	14.66	15.94	14.86	10.04	12.64	10.27	8.44	150.5
147	7.54	7.34	8.10	9.52	11.55	13.36	14.27	13.92	12.06	9.48	6.90	5.12	4.32	4.97	6.54	8.70	11.00	13.46	15.32	16.07	15.07	14.17	11.77	9.56	151.5	
148	8.16	7.68	7.83	8.74	10.50	12.26	13.66	14.02	12.96	10.86	8.34	6.24	5.04	4.82	5.84	7.60	9.46	11.87	15.30	15.60	14.66	12.78	10.74	9.03	152.6	
149	7.96	7.73	8.24	9.44	11.07	12.62	13.44	13.16	11.96	9.94	7.67	6.16	5.18	5.56	6.86	8.64	10.66	12.74	14.30	15.12	15.06	13.65	11.84	10.00	153.6	
150	8.46	7.75	7.78	8.46	9.93	11.36	12.37	12.84	12.22	10.98	9.18	7.32	6.03	5.94	8.17	9.67	11.58	13.28	14.64	14.97	14.22	12.62	11.08	9.47	154.7	
151	8.38	8.08	8.30	9.20	10.24	11.40	12.12	12.84	12.05	10.38	8.77	7.37	6.70	6.93	7.78	8.83	10.30	11.90	13.54	14.68	14.80	13.77	12.16	10.50	155.7	
152	9.20	8.47	8.28	8.60	9.36	10.36	11.26	11.83	12.05	11.56	10.60	9.20	7.72	7.83	8.62	9.82	11.10	12.64	13.94	14.46	14.16	13.26	11.74	10.42	156.8	
153	9.26	8.54	8.34	8.46	9.33	10.30	11.26	11.83	12.05	11.72	11.06	9.98	8.86	8.32	9.36	10.00	10.04	11.34	12.92	13.86	14.25	13.85	12.88	11.48	157.8	
154	10.08	8.74	7.93	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	10.17	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158.9	
155	10.03	8.74	7.93	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	10.17	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158.9	
156	10.03	8.74	7.93	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	10.17	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158.9	
157	10.03	8.74	7.93	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	10.17	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158.9	
158	10.03	8.74	7.93	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	10.17	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158.9	
159	10.03	8.74	7.93	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	10.17	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158.9	
160	10.03	8.74	7.93	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	10.17	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158.9	
161	10.03	8.74	7.93	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	10.17	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158.9	
162	10.03	8.74	7.93	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	10.17	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158.9	
163	10.03	8.74	7.93	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	10.17	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158.9	
164	10.03	8.74	7.93	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	10.17	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158.9	
165	10.03	8.74	7.93	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	10.17	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158.9	
166	10.03	8.74	7.93	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	10.17	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158.9	
167	10.03	8.74	7.93	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	10.17	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158.9	
168	10.03	8.74	7.93	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	10.17	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158.9	
169	10.03	8.74	7.93	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	10.17	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158.9	
170	10.03	8.74	7.93	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	10.17	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158.9	
171	10.03	8.74	7.93	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	10.17	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158.9	
172	10.03	8.74	7.93	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	10.17	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158.9	
173	10.03	8.74	7.93	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	10.17	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158.9	
174	10.03	8.74	7.93	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	10.17	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158.9	
175	10.03	8.74	7.93	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	10.17	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158.9	
176	10.03	8.74	7.93	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	10.17	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158.9	
177	10.03	8.74	7.93	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	10.17	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158.9	
178	10.03	8.74	7.93	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	10.17	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158.9	
179	10.03	8.74	7.93	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	10.17	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158.9	
180	10.03	8.74	7.93	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.86	13.28	12.03	10.56	9.66	10.17	10.37	11.98	13.44	14.22	14.34	13.94	12.86	11.59	158.9	



181	10.00	11.48	13.23	14.36	14.44	13.38	11.42	9.60	8.02	6.94	6.56	6.92	7.79	9.26	10.80	11.92	12.43	12.16	11.12	9.70	8.48	7.63	7.56	8.14	185 23	
182	9.04	10.41	11.98	13.30	13.98	13.72	12.51	10.84	8.96	7.47	6.70	6.48	6.84	7.36	8.16	9.16	10.36	11.46	12.28	11.46	10.38	8.34	8.14	8.38	187 0	
183	8.04	10.37	11.82	13.16	13.66	13.27	11.87	10.24	8.57	7.03	6.14	5.87	6.26	7.22	8.72	10.36	11.70	13.56	12.86	12.14	11.14	9.86	8.86	8.32	188 0	
184	8.34	9.03	10.46	11.88	13.12	13.48	12.96	11.86	10.30	8.58	7.00	5.74	5.74	6.86	8.67	10.62	12.30	13.47	13.96	13.31	12.10	10.48	9.04	8.28	189 1	
185	8.37	9.08	10.28	11.72	13.02	13.62	13.24	12.02	10.14	8.20	6.16	4.76	4.31	4.90	6.40	8.62	10.94	13.04	14.57	15.22	14.64	12.87	10.58	8.66	190 1	
186	7.68	7.62	8.40	10.00	11.70	13.12	13.97	13.69	10.27	7.76	5.44	3.88	3.19	3.88	5.80	8.60	11.46	13.90	15.54	16.06	15.08	12.92	10.40	8.23	191 2	
187	7.07	6.90	7.82	9.54	11.60	13.35	14.38	14.34	12.76	10.16	7.15	4.46	2.56	2.37	3.49	5.92	8.80	12.36	15.04	17.66	17.06	15.90	13.27	10.08	192 2	
188	7.42	6.93	6.04	7.17	9.30	11.84	13.92	14.90	13.08	9.91	6.43	3.53	1.84	1.84	3.58	6.20	9.54	13.00	15.92	17.60	17.55	15.88	13.54	9.04	193 3	
189	6.46	5.24	5.54	6.76	9.24	12.48	14.76	16.12	15.46	13.17	9.32	5.65	2.96	1.56	1.90	3.97	6.70	10.13	13.94	16.80	18.22	17.87	15.72	12.00	194 3	
190	8.47	5.86	4.66	6.66	9.72	13.12	15.46	16.44	15.54	12.76	8.60	5.17	2.76	1.62	2.37	4.50	7.60	11.14	14.80	17.30	18.38	17.46	14.77	11.14	195 4	
191	7.30	5.12	4.24	4.66	6.66	9.96	13.24	15.56	16.37	15.10	12.10	8.47	5.36	3.22	2.47	3.46	5.71	8.66	12.13	15.36	17.38	17.97	16.76	13.80	196 4	
192	10.38	4.79	4.26	5.04	7.14	10.42	13.85	15.77	16.14	14.53	11.60	8.45	5.84	4.20	3.82	5.12	6.97	9.80	13.00	15.56	17.04	17.17	15.44	12.60	197 5	
193	9.26	6.86	5.22	4.84	5.76	8.06	10.85	13.97	15.36	15.40	13.86	11.04	8.20	6.43	5.40	5.54	6.64	7.95	10.24	12.80	15.30	15.86	14.11	11.28	198 6	
194	8.50	6.30	5.34	5.40	6.24	8.00	10.50	12.97	14.30	14.44	12.94	10.92	9.08	7.74	7.24	7.56	8.14	9.16	11.11	13.10	14.71	15.40	14.72	12.96	199 6	
195	10.60	8.38	6.86	5.92	6.02	6.82	8.26	10.28	12.30	13.38	13.40	12.62	11.34	10.16	9.24	8.58	8.59	8.86	10.96	12.55	13.78	14.07	13.40	11.92	200 7	
196	10.10	8.37	6.87	6.38	6.51	7.24	8.41	9.82	11.28	12.52	12.90	12.68	11.87	10.93	10.01	9.34	9.14	9.27	9.97	10.90	12.12	13.14	13.41	12.71	201 7	
197	11.34	9.77	8.47	7.34	6.76	6.86	7.36	8.56	10.06	11.46	12.50	13.02	12.96	12.57	11.86	10.96	10.04	9.54	9.52	9.76	10.73	11.74	12.78	13.04	202 8	
198	11.42	10.20	8.76	7.52	6.96	6.70	7.25	8.50	10.20	11.86	13.24	13.87	13.87	13.28	12.22	11.04	10.07	9.54	9.50	9.87	10.73	11.74	12.60	12.94	203 8	
199	12.66	11.70	10.10	8.56	7.16	6.24	6.28	7.14	8.62	10.44	12.07	13.40	14.20	14.14	12.08	10.74	9.52	8.94	8.94	9.48	10.50	11.72	12.63	13.06	204 9	
200	12.60	11.28	9.36	7.66	6.38	5.86	6.06	7.07	8.94	10.96	13.07	14.58	15.07	14.54	13.34	11.84	10.26	9.14	8.46	8.46	9.16	10.36	11.74	13.14	205 9	
201	13.32	12.81	11.24	9.13	7.31	5.74	5.33	6.10	7.65	9.76	14.00	15.20	15.33	14.58	12.97	11.01	9.35	8.37	8.18	8.73	9.62	10.95	12.64	13.76	206 10	
202	13.92	12.56	10.36	8.02	6.14	5.26	5.24	6.52	8.36	10.60	12.96	14.83	16.03	15.68	14.38	12.14	9.94	8.56	8.04	8.20	8.78	9.99	11.82	13.73	207 10	
203	14.66	14.04	11.84	8.90	6.50	5.04	4.74	7.22	9.33	11.77	14.22	15.86	16.07	15.15	13.18	10.77	8.67	7.57	7.18	7.78	8.96	10.77	12.83	14.27	208 11	
204	14.50	13.28	10.70	7.76	5.53	4.56	4.86	6.26	8.20	10.44	13.14	15.37	16.51	16.11	14.47	11.94	9.36	7.58	6.88	7.16	8.00	9.72	11.80	13.84	209 11	
205	14.90	14.32	12.37	9.57	5.10	4.56	5.42	7.13	9.26	11.96	14.36	15.96	16.14	15.17	12.96	10.35	8.01	6.67	6.34	6.89	8.16	10.14	12.46	14.24	210 12	
206	14.84	13.50	10.90	8.02	5.86	4.76	5.04	6.52	8.34	10.66	13.15	15.27	16.14	15.82	14.14	11.47	8.96	7.02	6.16	6.33	7.34	9.23	11.44	13.54	211 12	
207	14.58	12.42	9.84	7.44	5.64	5.14	5.97	7.54	9.60	11.76	13.95	15.50	15.83	14.93	12.72	10.10	7.72	6.16	5.77	6.54	7.96	9.86	12.04	13.74	212 13	
208	14.37	13.56	11.31	8.97	7.02	5.96	5.96	7.12	8.61	10.53	12.64	14.44	15.55	15.26	13.84	11.46	8.86	6.95	5.97	6.05	7.05	8.56	10.54	12.48	213 13	
209	13.96	12.84	10.98	9.00	7.60	6.88	7.24	8.26	9.66	11.37	13.15	14.57	15.10	14.32	12.72	10.34	8.27	6.67	6.12	6.10	7.34	8.74	10.52	12.26	214 14	
210	13.26	13.32	12.36	10.84	9.38	8.24	7.77	8.12	8.86	10.16	11.76	13.33	14.29	14.38	13.46	11.64	9.64	7.76	6.48	6.10	6.50	7.54	9.00	10.63	215 15	
211	12.96	13.18	12.64	11.47	10.24	9.16	8.76	9.04	9.66	10.72	12.02	13.24	14.10	14.04	13.02	11.29	9.63	7.96	6.84	6.50	6.73	7.66	9.04	10.52	216 15	
212	12.10	13.14	13.55	13.28	12.50	11.34	10.26	9.52	9.35	9.67	10.59	11.83	12.88	13.62	13.44	12.54	11.15	7.86	6.50	5.94	6.16	7.10	8.50	10.20	217 16	
213	11.94	13.44	14.14	14.16	13.42	12.16	10.76	9.56	9.05	9.15	9.96	11.33	12.62	13.38	13.55	12.96	11.68	7.96	6.26	5.30	5.46	6.46	8.25	218 16		
214	10.24	12.44	14.18	15.26	15.50	14.64	12.94	10.78	9.16	8.56	8.76	9.78	11.16	12.57	14.26	14.02	12.80	10.52	8.01	5.84	4.76	4.81	5.98	7.77	219 17	
215	10.32	13.02	15.24	16.66	16.76	15.58	13.24	10.54	8.38	7.66	7.78	8.76	10.54	12.56	14.24	15.18	14.86	13.21	10.40	7.41	4.97	3.62	3.84	5.16	220 17	
216	7.44	10.44	13.54	16.14	17.54	17.44	15.84	12.90	9.72	7.44	6.60	6.85	10.22	12.92	15.15	16.26	15.72	13.66	10.33	6.96	4.40	3.04	3.33	5.32	221 18	
217	7.86	11.08	14.56	17.20	18.37	18.04	16.16	12.38	8.82	6.46	5.54	5.95	7.72	10.60	13.60	16.07	17.04	16.38	13.96	10.25	6.47	3.74	2.56	3.20	222 18	
Sum	708.16	780.21	734.29	729.30	733.03	715.16	749.27	756.64	761.77	772.68	791.99	790.74	791.00	812.56	809.25	774.39	754.66	762.43	732.82	731.70	764.66	784.22	783.48	786.50	No. of Days.	
No.	74	74	74	74	74	74	74	74	74	74	74	74	74	74	74	74	74	74	74	74	74	74	74	73	73	18,199.71

FORMS FOR SHORT-PERIOD TIDES.

SERIES M<sub>2</sub>K<sub>1</sub>.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
218	5.12	8.18	11.74	15.30	17.66	18.50	17.76	14.76	10.60	5.06	4.48	5.07	7.18	10.36	13.94	16.34	17.16	16.04	13.12	9.20	5.80	3.36	2.56	3.60	223 19	
219	5.73	9.03	12.78	15.94	17.78	18.04	16.74	13.32	9.36	6.05	4.18	3.80	4.90	7.56	11.10	14.46	16.66	16.88	15.39	12.15	8.23	5.44	3.52	3.32	224 19	
220	4.56	7.04	10.14	13.35	16.16	17.36	15.28	11.86	8.22	5.32	3.80	4.02	5.58	8.40	11.50	14.54	16.16	16.06	14.38	11.26	7.98	5.62	4.54	4.86	225 20	
221	6.25	8.27	11.00	13.96	16.32	17.26	16.43	14.32	10.85	7.62	5.16	4.10	4.64	6.45	8.92	12.05	14.70	15.80	15.18	13.36	10.62	7.94	6.32	5.74	226 20	
222	6.44	7.77	9.72	12.07	15.66	15.72	14.46	12.06	9.36	6.96	5.40	5.07	5.84	7.33	9.54	11.87	13.60	14.46	13.96	12.48	10.40	8.65	7.45	7.28	227 21	
223	8.00	9.16	10.72	12.27	13.74	14.47	14.18	12.78	10.82	8.78	6.78	5.83	5.86	6.74	8.34	10.14	12.02	13.26	13.57	12.85	11.76	10.70	9.74	9.12	228 21	
224	8.90	10.06	10.94	12.10	12.88	13.72	13.38	12.67	12.12	11.23	9.96	8.64	7.46	7.69	8.30	9.04	10.14	12.33	12.66	12.46	12.00	11.36	10.62	10.07	229 22	
225	9.34	9.77	10.12	10.82	11.54	12.43	12.67	12.12	11.23	9.96	8.64	7.77	7.46	7.69	8.30	9.04	10.14	12.33	12.66	12.46	12.00	11.36	10.62	10.07	230 23	
226	10.30	10.00	10.14	10.50	11.34	11.96	12.26	11.97	11.23	9.96	8.64	8.35	7.66	7.57	8.12	9.06	10.48	11.57	12.72	13.42	13.56	13.18	12.30	11.45	231 23	
227	10.72	10.26	9.92	9.61	10.00	10.71	11.62	12.32	12.18	11.42	10.36	9.08	8.15	7.53	7.24	7.70	8.54	9.82	11.43	12.72	13.64	13.66	13.26	12.36	11.22	232 0
228	10.18	9.34	8.97	9.08	9.88	10.76	11.64	12.26	12.35	11.85	10.40	8.78	7.36	6.44	6.28	7.14	8.37	10.20	11.94	13.38	14.40	14.54	13.58	12.17	12.17	233 0
229	10.70	9.34	8.83	8.84	9.26	10.00	11.16	12.50	13.30	13.42	12.06	10.16	8.40	6.86	6.06	6.14	8.95	10.80	12.76	13.96	14.91	14.84	13.64	11.84	235 1	
230	9.97	8.77	8.36	8.48	8.96	10.06	11.36	13.12	13.97	13.64	12.06	9.70	7.27	5.96	5.56	6.35	7.80	9.76	11.70	13.66	15.10	15.46	14.62	12.86	236 1	
231	10.57	8.64	7.46	7.31	7.76	8.84	10.72	12.64	14.21	14.62	13.44	11.00	8.24	5.17	5.36	6.54	8.54	10.66	13.00	15.02	15.96	15.50	14.08	11.60	237 2	
232	8.97	7.34	6.70	6.84	7.80	9.62	11.70	13.76	14.95	14.67	12.76	10.00	6.24	5.17	5.56	6.97	7.38	9.36	11.94	14.36	16.04	16.27	15.32	13.08	238 2	
233	10.11	7.72	6.36	6.10	6.94	8.63	10.81	13.20	15.21	15.71	14.43	8.54	6.26	4.97	5.06	6.36	8.22	10.64	13.40	15.80	16.62	16.16	14.21	11.38	239 3	
234	8.34	6.35	5.46	5.74	7.13	9.22	11.84	14.36	15.71	15.48	13.64	10.66	7.60	5.70	4.96	5.70	7.24	9.54	12.02	14.56	16.24	16.56	15.34	12.80	240 3	
235	9.60	7.06	5.50	5.18	5.94	7.72	10.28	13.04	15.90	14.88	12.52	9.53	7.07	5.74	5.64	6.67	8.36	10.62	13.17	15.30	16.38	15.97	14.06	11.04	241 4	
236	8.16	6.11	5.05	5.41	6.72	8.83	11.26	13.77	15.36	15.38	14.00	11.50	8.72	6.86	5.97	6.34	7.52	9.30	11.47	13.80	15.46	15.84	14.77	13.44	242 4	
237	9.37	7.06	5.37	4.85	5.64	7.24	11.64	13.96	15.06	14.75	13.17	10.76	8.64	7.30	6.86	7.44	8.64	10.38	12.36	14.06	15.24	15.10	13.64	11.26	243 5	
238	8.61	6.56	5.32	5.38	6.34	7.85	9.86	11.96	13.64	14.58	14.07	12.68	10.68	8.97	8.02	7.81	8.36	9.26	10.60	12.24	13.73	14.44	13.86	12.25	244 5	
239	10.02	6.46	5.62	5.78	6.47	7.80	9.63	11.38	12.97	13.74	13.44	12.44	11.04	9.83	8.84	8.57	8.87	9.67	10.67	11.96	13.06	13.46	13.06	11.68	245 6	
240	9.86	8.26	6.87	6.17	6.26	7.02	8.17	9.66	11.26	12.55	13.37	13.57	12.94	11.92	10.73	9.67	9.16	9.18	9.63	10.54	11.48	12.46	12.66	11.74	246 7	
241	10.42	8.87	7.44	6.44	6.21	6.66	7.76	9.20	10.76	12.36	13.54	14.95	13.67	12.68	11.26	10.02	9.22	8.90	9.14	9.86	10.86	12.02	12.84	12.98	247 7	
242	12.36	11.16	9.57	7.60	6.24	5.63	5.97	7.17	8.80	10.66	12.80	14.28	14.96	14.71	13.66	11.85	10.04	8.66	8.02	8.04	10.38	12.00	13.14	13.74	248 8	
243	13.40	12.04	10.04	7.64	5.76	4.78	5.02	6.24	8.16	10.78	13.20	15.04	15.98	15.74	14.33	11.96	9.30	7.37	6.55	6.70	8.06	9.98	12.06	13.93	249 8	
244	14.86	14.44	12.80	10.18	7.37	5.17	3.90	4.03	5.50	7.96	10.88	13.80	16.04	17.04	16.46	14.41	8.24	6.27	5.15	5.63	7.24	9.64	12.52	14.71	250 9	
245	15.98	15.46	13.29	9.94	6.61	4.34	3.17	2.53	3.38	8.20	11.40	14.56	16.82	17.41	16.36	13.83	9.98	6.70	4.46	3.84	4.58	6.80	10.06	13.28	251 9	
246	15.76	16.64	15.75	12.94	9.26	6.06	3.66	2.67	3.72	5.66	8.70	12.20	15.53	17.33	17.53	12.42	8.56	5.32	3.44	3.17	4.55	7.26	10.87	14.22	252 10	
247	16.50	17.05	15.47	12.37	8.44	5.52	3.48	3.10	4.26	6.74	9.94	13.47	16.22	17.47	17.02	14.77	10.84	7.23	4.52	3.00	3.30	5.07	8.06	11.72	253 10	
248	14.94	16.86	16.90	14.94	11.54	8.00	5.38	3.90	4.20	5.52	7.95	11.06	15.51	17.04	15.88	12.99	9.17	5.97	3.70	2.94	3.94	6.16	9.14	12.45	254 11	
249	15.44	16.68	16.10	13.81	10.56	7.46	5.47	4.87	5.60	7.04	9.54	12.25	14.81	16.16	15.06	14.44	11.07	7.87	5.31	3.84	3.92	5.16	7.43	10.36	255 11	
250	13.44	15.47	16.04	14.92	12.66	9.98	7.74	6.47	6.36	8.54	10.58	12.80	14.58	15.36	14.73	12.52	9.86	7.17	5.31	4.44	5.02	6.44	8.50	11.04	256 12	
251	13.56	14.79	14.77	13.46	11.46	9.44	8.00	7.36	7.56	8.36	9.51	11.10	12.60	13.73	13.94	12.90	11.02	8.73	6.90	5.70	5.63	6.34	7.60	9.36	257 12	
252	11.36	13.14	13.88	13.60	12.43	10.94	8.76	8.44	8.70	9.18	9.95	10.88	12.06	12.76	12.71	11.64	9.87	8.26	7.04	6.44	6.67	7.34	8.36	9.74	258 13	

253	11.16	13.22	12.70	13.20	11.38	10.60	9.88	9.34	9.16	9.13	9.34	9.87	10.66	11.30	11.62	11.37	10.56	9.48	8.44	7.52	7.14	7.33	7.86	8.66	259 13		
254	9.84	10.90	11.62	11.87	11.54	11.08	10.42	9.92	9.60	9.42	9.54	9.86	10.24	10.70	10.91	10.80	10.34	9.74	9.06	8.35	7.72	7.46	7.67	8.44	260 14		
255	9.64	10.73	11.52	11.88	12.06	11.88	11.53	10.97	10.23	9.48	9.04	9.01	9.38	10.01	10.64	11.05	11.18	10.94	10.46	9.52	8.56	7.74	7.42	8.34	261 15		
256	9.42	10.67	11.65	12.46	12.82	12.62	12.04	10.96	9.85	8.96	8.54	8.42	8.86	9.64	10.44	11.33	11.67	11.60	10.92	9.74	8.36	7.26	6.68	8.86	262 15		
257	7.74	9.24	10.86	12.34	13.24	13.55	13.17	12.08	10.64	9.21	8.06	7.54	7.74	8.74	9.92	11.30	12.38	12.82	12.42	11.17	9.62	7.86	6.10	6.54	263 16		
258	7.88	9.68	11.56	13.16	14.03	14.06	13.18	11.60	9.86	8.07	6.97	6.64	7.14	8.38	10.20	11.92	13.16	13.44	12.50	10.70	8.70	6.90	5.75	5.50	264 16		
259	6.36	8.04	10.20	12.32	13.87	14.61	14.36	12.87	10.73	8.45	6.71	5.90	6.17	7.29	9.02	11.07	13.02	14.14	14.04	10.30	7.96	6.07	5.14	5.48	265 17		
260	6.87	9.06	11.46	13.08	15.18	15.37	14.28	12.24	9.67	7.34	5.74	5.30	6.12	7.84	9.97	12.54	14.50	15.33	14.46	12.23	9.34	6.94	5.36	4.94	266 17		
261	5.94	8.06	10.08	12.62	14.76	15.76	15.26	13.46	10.67	7.88	5.74	4.48	4.66	6.00	8.44	13.07	15.67	15.66	14.20	11.46	8.47	6.20	4.97	5.22	267 18		
262	6.65	8.86	11.54	14.06	15.76	16.07	14.86	12.14	9.06	6.37	4.56	3.93	4.93	6.93	9.67	12.77	15.34	16.35	15.80	13.61	10.52	7.73	5.58	4.88	268 18		
263	5.77	7.56	10.04	12.74	14.90	15.94	15.62	13.71	10.64	7.47	5.10	3.54	3.83	5.50	7.97	11.14	14.16	16.01	16.37	15.04	12.33	9.34	6.97	5.54	269 19		
264	6.51	8.50	11.14	13.77	15.60	15.98	14.86	12.14	8.87	6.16	4.30	3.67	4.60	6.44	9.03	12.27	14.84	16.21	15.96	14.09	11.42	8.56	6.75	5.80	270 19		
265	6.17	7.42	9.65	12.22	14.26	15.46	15.24	13.48	10.57	7.65	3.96	4.06	5.34	7.30	9.97	12.69	14.83	15.87	15.16	13.24	10.76	8.47	7.04	6.68	271 20		
266	7.20	8.44	10.38	12.56	14.16	14.83	14.05	12.07	9.24	7.02	5.32	4.44	4.61	5.87	7.97	10.37	13.07	14.81	15.06	14.13	12.37	10.44	8.86	7.87	272 20		
267	7.56	7.92	8.94	10.67	12.44	13.74	13.07	10.83	8.83	7.10	5.78	5.25	5.76	6.66	8.34	10.76	12.86	14.16	14.44	13.68	12.40	10.86	9.52	8.53	273 21		
268	8.21	8.56	9.40	10.68	12.08	13.04	13.08	11.93	10.54	9.05	7.64	6.61	6.06	6.30	7.07	8.81	10.63	12.30	13.68	14.16	13.66	12.66	11.46	10.12	274 21		
269	9.18	8.77	8.56	9.10	10.17	12.30	12.61	12.14	11.16	9.92	8.44	7.14	6.37	6.38	7.34	8.76	10.57	12.10	13.44	13.92	13.88	13.56	12.37	11.18	275 22		
270	9.72	8.32	7.66	7.94	9.26	10.84	12.04	12.52	12.48	11.98	11.16	9.77	7.94	6.58	6.06	6.50	7.97	9.84	11.56	13.26	14.17	14.66	14.52	13.27	276 22		
271	11.31	9.06	6.82	7.46	8.74	10.60	12.11	13.20	14.04	13.84	12.76	10.92	8.58	6.74	5.94	6.30	7.68	9.72	11.97	13.90	15.26	15.99	15.54	13.97	277 23		
272	11.26	8.63	6.70	5.98	6.37	7.97	10.25	12.66	14.44	15.38	15.04	13.48	11.07	8.36	6.38	5.47	5.87	7.36	9.62	12.14	14.54	16.28	16.98	13.86	279 0		
273	10.49	7.50	5.61	5.14	5.74	7.77	10.54	13.45	15.71	16.85	16.30	14.16	10.84	7.77	5.85	5.07	5.66	7.96	9.87	12.74	15.25	16.92	17.15	15.62	280 1		
274	12.54	8.66	5.94	4.14	3.96	5.28	7.85	11.15	14.38	16.70	17.32	16.33	13.48	9.84	7.20	5.47	4.98	5.96	7.74	13.66	16.26	17.49	16.86	14.56	280 1		
275	10.89	7.40	4.72	3.37	3.98	5.86	8.86	12.43	15.47	17.34	17.64	16.26	12.76	9.26	6.56	5.24	5.38	6.54	8.77	11.76	14.62	16.82	17.12	15.72	282 1		
276	12.71	9.14	6.06	3.77	3.17	4.42	6.67	9.72	13.44	16.35	17.55	17.22	15.06	11.70	8.40	6.26	5.44	6.47	10.01	12.74	15.12	16.37	16.06	14.21	283 2		
277	11.94	7.42	4.80	3.12	3.62	5.50	8.04	11.13	14.40	16.50	17.22	16.16	13.58	10.36	7.77	6.24	6.04	6.91	8.53	10.52	13.06	15.02	15.64	14.36	284 2		
278	11.93	8.64	6.01	4.31	3.47	4.52	6.20	8.94	11.94	14.56	16.24	16.32	14.74	12.13	7.47	6.58	6.90	7.84	9.30	11.26	13.26	14.41	14.26	12.74	285 3		
279	10.35	7.88	5.80	4.44	4.58	5.92	7.85	10.30	12.70	14.67	15.54	15.01	13.36	11.14	9.11	7.80	7.42	7.74	8.64	10.04	11.80	13.04	13.64	13.06	286 3		
280	11.36	9.07	7.14	5.84	5.47	6.20	7.44	9.04	10.97	13.06	14.36	13.46	11.82	10.44	9.16	8.44	8.24	8.54	9.26	10.30	11.46	13.12	12.22	11.46	287 4		
281	10.00	8.37	7.08	6.36	6.44	7.32	8.34	9.60	11.24	12.72	13.46	13.28	12.32	11.06	10.10	9.27	8.97	8.94	9.08	9.61	10.14	11.01	11.52	11.46	288 4		
282	10.73	9.52	8.47	7.66	7.41	7.56	8.04	8.76	9.91	12.30	12.88	12.66	11.92	11.04	10.37	9.76	9.36	9.12	9.08	9.27	9.86	10.44	10.68	10.66	289 5		
283	10.30	9.78	9.22	8.56	8.06	7.74	8.02	8.86	10.06	11.16	12.02	12.40	12.34	12.06	11.48	10.82	9.97	9.24	8.77	8.68	8.96	9.55	10.22	10.70	290 5		
284	10.88	10.82	10.57	10.03	9.26	7.90	8.44	8.07	8.80	9.84	10.90	12.36	12.58	12.54	12.07	11.12	9.97	8.90	8.23	8.12	8.56	9.27	10.10	10.90	291 6		
285	11.50	11.78	11.53	10.67	9.30	8.14	7.56	7.77	8.55	9.74	11.07	12.15	12.94	13.28	13.04	12.24	10.77	9.14	7.88	7.18	7.36	8.12	9.26	10.61	292 6		
286	11.94	12.78	12.06	10.48	8.86	7.70	7.28	7.65	8.65	10.02	11.54	12.81	13.77	14.04	13.50	12.16	10.00	8.34	6.96	6.50	6.88	7.96	9.76	11.52	298 7		
287	13.07	13.96	13.77	12.48	10.52	8.76	7.36	6.77	7.26	8.52	10.36	12.17	13.66	14.56	14.48	13.40	11.12	8.84	6.87	5.64	5.46	6.30	8.06	10.30	294 8		
288	14.34	15.00	14.16	12.26	9.96	7.92	6.59	6.22	7.10	8.82	10.86	13.12	14.54	15.07	14.56	12.60	9.98	7.47	5.46	4.56	4.06	6.60	9.03	11.80	295 8		
289	14.15	15.84	15.96	14.52	12.00	9.24	7.24	6.16	6.40	7.67	9.66	11.93	14.14	15.62	15.76	14.36	11.76	8.61	6.02	4.24	3.86	6.00	9.03	13.10	206 9		
290	15.67	16.78	16.26	14.16	11.00	8.32	6.36	5.84	6.47	8.16	10.16	12.84	15.02	16.10	15.46	13.48	9.87	6.84	4.45	3.04	3.57	5.44	8.15	11.37	297 9		
Sum	755.82	747.60	747.56	734.08	744.58	777.64	767.21	776.91	797.38	777.38	774.20	773.75	746.31	739.01	748.30	762.19	766.54	757.39	787.53	784.90	775.45	794.08	804.38	787.02	No. of Days.		
No.	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100

FORMS FOR SHORT-PERIOD TIDES.  
 SERIES M<sub>2</sub>K<sub>1</sub>.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
291	14.60	16.81	17.35	16.38	13.64	10.44	7.71	6.07	5.84	6.88	8.87	11.47	14.12	15.94	16.22	14.81	11.87	8.55	5.46	2.87	4.17	6.35	9.32	13.00	298 10	
292	15.95	17.47	17.44	15.72	12.68	9.66	7.18	5.94	6.04	7.36	9.64	12.45	14.84	16.04	15.60	13.70	10.52	7.15	4.66	2.92	3.10	4.72	7.47	10.55	299 10	
293	13.92	16.35	17.36	16.74	14.57	11.67	8.85	6.76	5.94	6.18	7.70	9.92	12.68	14.78	15.58	12.30	9.26	6.36	4.20	3.07	3.72	5.55	8.04	11.05	300 11	
294	14.10	16.17	16.96	16.12	14.06	11.35	8.82	7.14	6.57	7.02	8.46	10.56	13.14	14.64	15.04	13.76	11.47	8.74	6.42	4.70	4.22	5.00	6.80	9.02	301 11	
295	11.88	14.60	16.14	16.22	15.16	13.26	10.86	8.86	7.58	7.14	7.44	8.84	10.92	13.84	13.86	12.57	10.68	8.54	6.84	5.56	5.27	5.98	7.33	9.36	302 12	
296	11.72	14.90	15.22	15.38	14.58	13.88	11.01	9.42	8.12	7.64	7.92	8.94	10.40	11.85	12.91	13.12	12.26	10.75	9.22	7.66	6.68	6.30	6.72	7.86	303 12	
297	9.44	11.50	13.34	14.46	14.66	13.96	13.74	11.30	9.76	7.93	7.84	8.40	9.60	10.88	12.06	12.64	12.40	11.47	10.10	8.76	7.68	7.01	7.06	7.90	304 13	
298	9.22	10.97	12.56	13.72	14.38	14.04	13.04	11.45	9.76	8.15	7.22	7.02	7.48	8.84	10.32	11.48	12.55	12.87	12.46	11.36	9.70	8.28	7.14	6.80	305 13	
299	7.40	8.94	10.74	12.56	13.87	14.54	13.40	11.67	9.60	7.53	6.30	5.88	6.50	8.20	10.07	11.93	13.36	14.04	13.66	12.30	10.26	8.61	7.37	6.86	306 14	
300	7.24	8.35	10.36	12.50	14.13	15.08	14.96	13.80	11.64	9.03	6.96	5.44	5.04	5.86	7.79	10.12	12.66	14.54	15.37	14.86	13.04	10.66	8.56	7.12	307 14	
301	6.44	6.77	8.02	10.14	12.56	15.55	15.25	13.56	10.91	8.12	5.82	4.22	4.10	5.32	7.70	10.85	13.60	15.51	16.05	15.06	12.86	10.40	8.16	6.53	308 15	
302	5.96	6.51	8.24	10.85	13.27	15.16	15.84	15.03	12.98	9.78	7.04	4.71	3.46	3.86	5.60	8.44	11.74	14.64	16.50	16.72	15.38	12.86	9.98	7.70	309 15	
303	6.25	5.93	8.67	11.25	13.84	15.52	15.84	14.55	11.68	8.46	5.64	3.63	3.01	4.08	6.50	9.62	13.08	15.81	17.12	16.72	14.87	12.03	9.20	7.26	310 16	
304	6.32	6.37	7.46	9.60	12.20	14.32	15.67	15.28	13.15	10.15	7.00	4.47	3.03	3.22	5.03	7.60	10.76	14.05	16.38	17.05	16.14	13.92	11.10	6.87	311 17	
305	6.16	6.46	8.00	10.44	13.10	14.76	15.16	13.92	11.40	8.36	5.66	3.69	2.94	3.94	6.18	9.01	12.24	14.92	16.53	16.56	15.16	12.66	10.06	7.96	312 17	
306	6.74	6.60	7.35	9.00	11.24	13.43	14.50	14.36	12.66	9.94	7.20	4.97	3.56	3.77	5.34	7.72	10.56	13.46	15.64	15.71	13.92	11.46	9.28	7.66	313 18	
307	6.86	6.98	7.98	9.96	12.00	13.52	14.02	13.37	11.18	8.81	6.52	4.86	4.33	5.20	6.90	9.14	11.80	14.20	15.72	15.81	14.66	11.72	10.71	8.96	314 18	
308	7.82	7.56	7.92	9.16	10.68	12.24	13.26	13.26	12.06	10.17	8.00	6.25	5.31	5.50	6.66	8.34	10.82	14.44	15.16	14.68	13.32	11.56	10.02	8.76	315 19	
309	8.10	8.00	8.60	9.65	10.96	12.18	12.58	12.23	11.04	9.16	7.62	6.54	6.20	6.84	7.96	9.80	11.46	12.86	13.86	13.83	12.96	11.72	10.53	9.66	316 19	
310	8.78	8.46	8.68	9.30	10.00	10.94	11.57	11.80	11.36	10.28	8.94	7.84	7.18	7.86	8.80	9.98	11.46	12.86	14.18	14.40	13.64	12.37	10.90	9.58	317 20	
311	9.14	8.92	8.96	9.17	9.66	10.40	11.10	11.37	11.01	10.20	9.26	8.46	8.10	8.14	8.66	9.44	10.36	11.74	12.76	13.34	13.26	12.61	11.72	10.86	318 20	
312	9.76	9.04	8.80	8.85	9.16	9.64	10.14	10.74	11.18	11.32	11.06	9.58	8.94	7.20	7.86	8.80	9.98	11.46	12.48	13.10	13.15	12.64	11.84	10.76	319 21	
313	9.71	8.88	8.35	8.19	8.42	9.04	9.60	10.86	11.50	11.80	11.55	10.96	9.98	9.68	8.64	8.75	9.38	10.38	11.46	12.41	13.07	13.16	12.84	11.84	320 21	
314	10.56	9.24	8.13	7.50	7.43	7.86	8.83	10.03	12.23	12.80	12.64	11.66	10.25	9.04	8.36	8.34	8.96	10.02	11.20	12.46	13.23	13.47	13.00	11.72	321 22	
315	10.14	8.38	7.03	6.27	6.31	7.08	8.52	10.23	11.92	13.17	13.63	13.10	11.86	10.18	8.76	7.98	7.96	8.75	10.13	11.64	13.14	13.94	13.94	13.04	322 22	
316	11.34	9.30	7.45	5.86	5.13	6.76	8.80	11.15	13.20	14.66	14.98	13.87	11.76	9.58	8.10	7.27	7.36	8.22	9.82	11.76	13.33	14.28	14.14	12.87	323 23	
317	10.56	7.98	5.77	4.14	3.74	4.67	6.71	9.27	12.02	14.40	15.66	15.44	13.71	11.16	8.74	7.02	6.40	6.78	8.22	10.37	12.25	13.88	14.74	14.20	324 23	
318	12.26	9.36	4.12	2.75	2.94	4.56	7.03	10.05	13.27	15.65	16.62	15.90	13.76	10.86	8.17	6.45	5.84	6.36	8.12	10.44	12.84	14.46	15.08	13.97	326 0	
319	11.41	8.07	4.96	2.57	1.63	2.58	4.74	7.64	11.12	14.22	16.47	17.07	15.75	12.96	9.86	7.26	5.65	5.46	6.44	8.40	11.20	13.57	15.11	15.17	327 1	
320	9.96	6.40	3.62	1.76	1.54	3.26	6.02	9.25	12.97	15.66	17.40	17.25	15.37	12.23	9.00	6.75	5.65	5.63	6.88	9.32	12.22	14.44	15.59	14.80	328 1	
321	12.31	8.84	5.46	3.00	1.66	2.20	4.15	6.95	10.46	13.81	16.44	17.54	16.82	14.56	11.38	8.50	6.32	5.44	5.74	7.26	10.00	14.67	15.36	14.06	329 2	
322	11.32	8.05	5.16	2.94	2.16	3.11	5.16	7.96	11.23	14.30	16.57	17.22	16.23	13.81	10.68	8.07	6.16	5.50	5.88	7.64	10.25	12.77	14.59	14.72	330 2	
323	13.33	10.74	7.81	5.32	3.66	3.26	4.42	6.34	8.86	11.67	14.58	16.33	16.57	15.28	12.28	9.93	7.47	6.23	6.26	7.94	10.30	12.38	13.76	13.96	331 3	
324	12.68	10.56	8.18	6.26	4.97	4.83	5.73	7.34	9.38	12.05	14.37	15.76	15.80	14.56	12.84	9.94	8.13	6.64	6.14	6.54	8.04	10.04	11.78	12.86	332 3	
325	13.16	12.24	10.73	8.96	7.30	6.24	5.96	6.50	7.80	9.84	12.15	13.88	14.87	14.84	11.77	10.06	8.23	6.86	6.34	6.56	7.70	9.30	10.84	12.16	333 4	

326	13.76	12.53	11.48	10.14	8.66	7.52	7.06	7.44	8.47	10.17	11.91	13.34	14.21	14.40	13.72	12.30	10.42	8.41	6.88	6.14	6.37	7.32	8.81	10.45	384 4	
327	11.84	12.86	13.08	12.42	11.25	9.75	8.54	7.84	7.88	8.64	10.02	11.65	13.16	14.30	13.64	12.17	10.31	8.37	6.68	5.72	5.86	6.88	8.64	10.40	385 5	
328	13.07	13.31	13.88	13.62	12.36	10.67	9.06	8.12	7.90	8.54	9.72	11.26	12.78	13.82	14.20	13.74	12.14	10.10	7.76	6.00	5.04	5.23	6.52	8.50	386 6	
329	10.56	12.60	14.12	14.40	13.86	12.58	10.80	8.97	7.94	7.08	9.50	11.14	12.75	13.90	14.44	13.73	11.85	11.28	8.84	5.06	4.41	5.04	6.57	8.66	387 6	
330	11.20	13.52	15.24	15.84	15.08	13.13	10.86	9.00	7.82	7.54	8.05	9.36	11.14	12.94	14.20	14.46	13.36	11.28	8.58	5.98	4.22	3.96	6.97	9.37	388 6	
331	9.34	12.26	14.54	16.11	16.34	15.17	12.88	8.38	7.53	7.40	8.14	9.77	11.52	13.36	14.60	14.56	12.94	10.26	7.33	5.11	3.87	4.05	5.64	7.81	389 7	
332	10.61	13.20	15.47	16.54	16.21	14.70	12.20	9.81	8.08	7.33	7.37	8.31	10.05	12.02	13.86	14.76	14.17	12.16	8.93	6.32	4.31	3.72	4.64	6.56	340 7	
333	9.06	11.87	14.55	16.23	15.97	13.94	11.34	8.98	7.71	7.36	7.70	9.02	10.97	12.94	14.40	14.70	13.44	10.64	7.77	5.58	4.12	4.16	5.63	7.85	341 8	
334	10.36	13.16	15.34	16.56	16.48	15.11	12.72	10.27	8.26	7.37	7.26	8.12	9.82	11.91	13.58	14.48	14.07	12.12	9.32	6.72	4.74	3.96	4.91	6.70	342 8	
335	9.02	11.70	14.07	15.82	15.18	13.58	11.42	9.46	7.98	7.36	7.62	8.50	10.02	11.60	12.67	13.00	12.14	10.36	8.34	6.54	5.59	5.67	6.77	8.43	345 10	
336	10.34	12.88	15.05	16.23	16.28	14.89	12.63	10.30	8.54	7.57	7.44	8.17	9.64	11.50	13.03	13.80	13.45	11.78	9.47	7.26	5.64	5.07	7.43	9.20	344 10	
337	11.48	13.56	15.7	15.82	15.18	13.58	11.42	9.46	7.98	7.36	7.62	8.50	10.02	11.60	12.67	13.00	12.14	10.36	8.34	6.54	5.59	5.67	6.77	8.43	345 10	
338	10.27	12.17	13.90	14.96	14.86	13.76	12.00	10.22	8.66	7.73	7.38	7.80	8.81	10.22	11.48	12.26	12.24	11.15	9.47	6.87	6.45	6.75	7.83	9.14	346 11	
339	10.75	12.56	13.86	14.46	14.06	12.87	11.31	9.72	8.40	7.76	7.73	8.27	9.36	10.54	11.48	12.02	11.81	10.84	9.56	8.46	7.76	7.56	8.00	8.95	347 11	
340	10.05	11.60	13.13	14.20	14.42	13.83	12.50	10.98	9.76	8.76	8.24	8.24	8.80	9.62	10.53	11.27	11.70	11.14	10.38	9.49	8.58	8.48	8.71	9.47	348 12	
341	10.70	12.04	13.16	13.78	13.79	13.14	11.94	10.54	9.17	8.30	7.83	8.04	8.58	9.36	10.22	11.00	11.54	11.74	11.57	10.96	10.14	9.44	9.04	9.10	349 12	
342	9.74	10.90	12.24	13.16	13.57	13.38	12.64	11.55	10.26	8.86	7.83	7.22	7.36	8.05	8.20	9.07	11.56	12.42	12.30	11.78	10.77	9.72	9.06	9.01	350 13	
343	9.55	10.76	11.97	12.94	13.38	13.14	12.44	11.22	9.78	8.36	7.04	6.26	6.15	6.82	8.20	9.97	11.56	12.90	13.50	13.36	12.36	10.92	9.68	8.84	351 13	
344	8.68	9.14	10.18	11.57	12.76	13.30	13.22	12.46	11.00	9.17	7.18	4.90	4.92	6.07	7.94	10.07	12.03	13.66	14.48	14.16	12.76	10.77	9.04	7.98	352 14	
345	7.73	8.23	9.70	11.10	12.74	13.42	13.45	12.54	10.80	8.50	6.30	4.47	3.64	4.12	5.82	8.20	10.84	13.27	14.95	15.70	14.97	13.05	10.60	8.64	353 14	
346	7.50	7.36	8.16	9.80	11.80	13.38	14.33	13.00	10.50	7.72	5.17	3.42	2.93	4.16	6.37	9.00	12.12	14.97	16.74	16.96	15.68	13.11	10.34	8.06	354 15	
347	6.98	7.04	8.06	10.00	12.15	14.04	15.14	15.03	13.10	10.20	7.00	4.27	2.40	2.20	3.93	6.57	9.77	13.27	16.13	17.72	17.51	15.78	12.57	9.74	355 15	
348	7.27	6.14	6.36	7.56	12.72	15.81	15.20	12.64	9.26	5.91	3.10	1.55	1.93	4.00	4.00	6.06	10.68	14.30	17.04	18.34	17.72	15.47	12.00	8.88	356 16	
349	6.58	5.67	6.00	10.14	13.10	15.24	16.17	14.94	12.16	8.55	5.06	2.64	1.50	2.57	5.14	8.41	11.93	15.00	17.66	18.34	17.37	14.51	10.93	8.57	357 16	
350	7.77	5.66	5.14	7.65	10.63	13.44	15.46	15.86	14.14	10.98	7.68	4.48	2.36	1.77	3.30	5.83	8.90	12.30	15.56	17.50	17.88	16.62	13.58	9.97	358 17	
351	6.94	5.14	4.70	5.52	7.63	10.73	13.70	15.36	15.32	13.24	9.92	6.64	4.73	3.07	3.08	4.74	6.97	9.86	13.01	15.80	17.38	17.48	15.95	12.86	359 18	
352	6.72	5.22	4.90	5.87	8.03	10.96	13.30	14.68	14.83	13.24	10.55	7.68	5.43	3.33	4.63	5.97	8.02	10.57	13.25	15.58	16.60	16.14	14.11	11.13	300 18	
353	8.76	6.38	5.17	5.13	6.30	8.60	10.76	12.74	13.74	13.62	12.37	10.30	8.14	6.53	5.84	6.14	7.14	8.74	10.77	13.13	15.71	14.96	15.12	13.32	10.86	361 19
354	8.44	6.53	5.48	5.27	6.00	7.78	9.85	11.62	12.84	13.10	12.28	10.74	9.22	7.96	7.33	7.48	7.93	9.16	10.97	13.12	14.54	14.68	13.66	12.28	362 19	
355	10.12	8.24	6.78	5.82	5.70	6.37	7.72	9.40	11.06	12.32	12.86	12.50	11.47	10.24	9.12	8.42	8.24	8.54	11.12	12.64	13.57	13.57	12.88	11.44	363 20	
356	9.87	8.24	6.74	5.77	5.52	6.12	7.27	8.94	10.64	12.10	13.01	13.12	12.46	11.26	10.02	9.06	8.58	8.66	9.44	10.68	11.96	12.92	13.14	12.66	364 20	
357	11.54	10.06	8.36	6.86	5.72	5.37	5.87	7.17	9.14	11.00	12.70	13.68	13.81	12.94	10.28	9.14	8.62	8.63	9.20	10.44	11.66	12.53	12.92	12.58	365 21	
358	11.64	9.77	7.86	6.12	5.05	4.78	5.62	7.06	9.15	11.26	13.23	14.30	14.32	13.36	11.78	10.34	9.17	8.44	8.24	8.62	9.76	11.04	12.36	13.08	366 21	
359	12.90	11.65	9.64	7.34	5.82	4.45	4.52	5.76	7.66	9.97	12.43	14.27	14.97	13.73	11.82	10.16	8.86	8.24	8.26	8.96	10.32	11.70	12.96	13.58	367 22	
360	13.16	11.26	8.91	6.66	4.96	4.33	4.86	6.36	8.55	11.00	13.44	15.21	15.84	15.17	13.56	11.44	9.66	8.38	7.80	7.97	9.00	10.56	12.24	13.46	368 22	
361	13.82	12.72	10.52	7.90	5.74	4.34	4.11	5.34	7.23	9.78	14.65	15.93	15.94	14.74	12.37	10.23	8.53	7.47	7.31	7.97	9.38	11.36	13.14	14.17	369 23	
362	14.00	12.18	9.43	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	370 2
Sum	734.56	729.86	739.21	759.66	755.75	759.88	778.28	767.68	746.65	735.55	710.75	696.56	707.06	729.72	734.99	759.65	762.37	758.89	780.36	782.26	753.57	746.55	746.78	729.17	1786.94	
No.	73	73	74	73	72	72	73	73	71	74	73	72	73	73	73	72	73	73	72	73	73	72	73	72	73	1786.94

FORMS FOR SHORT-PERIOD TIDES.

B O M B A Y—Commencing 0 hours, Astronomical Time, 1st January, 1885.

S E R I E S 2M<sub>3</sub>K<sub>1</sub>.

Motion per mean Solar hour = 42°-92'71398.

Argument (3γ - 1α).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
1	15.52	13.06	9.13	5.76	3.03	1.68	2.28	4.80	7.90	11.70	15.50	18.85	18.08	15.14	11.54	8.50	6.21	5.53	6.08	8.20	11.31	14.16	16.06	16.66	2 0	
2	15.40	13.16	8.40	4.86	2.56	1.71	2.90	5.56	12.94	16.44	18.58	18.97	17.67	14.24	10.56	7.53	5.57	5.16	6.10	8.63	11.84	14.68	16.63	16.96	3 1	
3	15.24	11.92	8.00	4.87	2.57	4.24	6.84	10.20	14.07	17.26	18.86	18.84	17.06	13.20	9.77	6.90	5.23	4.96	6.16	8.86	12.14	14.87	16.40	16.40	4 2	
4	14.28	11.00	7.63	4.88	3.55	5.55	8.01	11.30	14.83	17.16	18.38	17.93	15.80	12.16	8.68	6.10	5.05	5.25	6.68	9.24	12.28	14.51	15.58	13.48	5 4	
5	10.47	7.54	5.76	5.07	6.84	7.54	8.67	9.17	12.11	15.02	17.02	17.55	16.63	14.11	10.96	8.16	6.22	5.47	5.84	7.18	12.12	14.04	15.00	14.45	12.62	6 5
6	10.24	8.07	7.04	6.84	7.54	8.67	10.60	12.84	15.06	16.36	16.35	15.24	12.76	10.11	8.00	6.17	6.55	7.86	9.76	11.80	13.27	14.00	13.64	12.22	7 6	
7	10.47	9.05	8.44	8.46	9.03	9.97	11.20	13.05	14.64	15.46	15.18	13.87	9.76	8.10	7.16	7.03	7.40	8.29	9.82	11.16	12.55	13.24	13.07	12.20	8 7	
8	11.16	10.27	9.64	9.60	9.90	10.60	11.70	12.96	14.02	14.44	12.27	10.82	9.20	7.93	7.24	7.06	7.34	8.07	9.14	10.55	11.74	12.48	12.66	12.27	9 8	
9	11.60	10.93	10.34	9.98	9.86	11.07	12.14	13.06	13.36	12.72	11.71	10.43	9.14	7.91	7.14	6.75	6.94	7.74	8.96	10.26	11.64	13.67	13.14	12.97	10 9	
10	12.20	11.24	10.13	10.05	10.23	10.84	11.64	12.57	12.68	12.37	11.53	10.43	8.97	7.80	6.96	6.38	6.34	7.28	8.73	10.47	12.14	13.23	13.84	12.58	11 11	
11	11.38	10.27	9.77	9.61	9.89	10.44	11.24	11.97	12.52	12.50	11.87	10.54	8.76	7.34	6.16	5.74	6.34	7.62	9.54	11.46	14.24	14.58	13.94	12.72	12 12	
12	11.24	10.02	9.34	9.14	9.46	10.37	11.48	12.46	13.04	12.84	11.80	10.23	8.20	6.52	5.62	5.56	6.14	8.16	12.34	14.10	15.20	15.17	13.97	12.37	13 13	
13	10.58	9.35	8.75	8.76	9.26	10.34	11.68	12.96	13.64	13.36	11.80	10.23	7.32	5.82	5.14	5.44	6.74	8.86	11.26	13.66	15.38	15.24	13.66	11.54	14 14	
14	9.82	8.71	8.16	8.36	9.30	10.74	12.46	13.64	13.98	13.00	8.24	6.20	4.76	4.46	5.40	7.36	9.78	12.37	14.82	16.13	15.97	14.56	12.25	10.05	15 15	
15	8.46	7.82	7.74	8.41	9.71	11.76	13.30	14.00	14.26	14.00	7.00	5.12	4.20	4.63	6.12	8.44	11.24	14.04	15.74	16.36	15.71	13.82	11.22	8.94	16 16	
16	7.54	6.94	8.40	10.27	12.44	14.06	14.68	13.84	12.54	11.50	5.94	4.37	4.02	5.06	7.26	9.66	12.72	15.20	16.55	16.63	15.27	12.77	9.97	7.86	17 18	
17	6.68	7.56	9.32	11.40	13.55	14.80	14.78	13.22	10.43	7.48	5.34	4.30	4.66	6.25	8.54	11.38	14.15	16.15	16.88	16.08	14.04	8.54	6.76	6.12	18 19	
18	6.34	7.60	9.76	12.14	14.06	14.84	14.14	12.06	9.06	6.46	4.67	4.24	5.16	7.15	9.68	12.56	14.87	16.44	15.00	12.42	9.50	7.22	5.80	5.43	19 20	
19	6.26	8.16	10.65	12.88	14.28	14.56	13.33	10.92	8.30	6.04	4.87	5.06	6.54	8.66	13.64	15.62	16.36	15.76	13.82	11.00	8.37	6.37	5.54	5.64	20 21	
20	6.83	8.93	11.46	13.32	14.42	14.25	12.47	10.10	7.91	6.34	5.70	7.70	9.76	12.17	14.36	15.74	15.96	14.86	12.76	10.13	7.78	6.17	5.70	6.11	21 22	
21	7.62	9.70	11.76	13.36	14.14	13.72	12.06	9.94	7.22	7.01	7.74	8.97	10.80	12.97	14.62	15.30	15.17	13.80	11.46	9.14	7.34	6.17	6.00	6.68	22 23	
22	8.02	9.76	11.65	13.04	13.76	13.34	12.14	10.65	9.07	8.15	8.68	9.86	11.56	13.36	14.56	15.02	14.37	12.76	10.76	8.71	6.96	6.23	6.09	6.68	24 0	
23	7.86	11.24	12.66	13.36	13.34	12.38	11.08	9.94	9.11	8.88	9.28	10.22	11.70	13.06	14.14	14.41	13.60	12.06	10.26	8.46	7.10	6.23	6.56	7.64	25 2	
24	9.14	10.84	12.34	13.44	13.81	13.33	12.18	10.75	9.76	9.24	9.34	10.07	11.16	12.40	13.38	13.66	13.03	11.87	8.47	7.00	5.83	5.38	5.68	6.78	26 3	
25	8.55	10.33	12.22	13.56	14.30	14.16	13.05	11.56	10.66	9.11	8.87	9.40	10.46	11.87	13.44	13.33	12.40	10.74	8.86	6.83	5.22	4.41	4.77	6.10	27 4	
26	8.10	10.50	12.63	14.53	15.56	15.33	13.76	11.64	9.23	8.28	7.92	9.53	11.24	12.70	13.80	14.14	13.30	11.34	8.72	6.20	4.24	3.38	3.76	5.30	28 5	
27	7.76	10.55	13.50	15.72	16.74	16.12	14.36	11.40	8.83	6.86	7.53	9.20	11.11	12.97	14.55	15.08	14.17	11.84	8.82	5.70	3.60	2.56	3.06	5.04	29 6	
28	7.88	11.48	14.56	17.04	17.86	14.36	10.96	8.07	6.27	5.77	6.57	8.62	11.35	13.92	15.74	16.28	14.96	12.18	8.44	5.42	3.22	2.16	3.07	5.52	30 7	
29	8.75	16.01	18.10	18.47	17.26	13.80	10.14	7.09	5.27	5.02	6.02	8.40	11.85	14.65	16.52	16.84	15.28	11.68	7.88	4.80	2.74	2.38	4.00	6.66	31 9	
30	13.98	17.01	18.64	18.38	16.30	12.42	8.97	6.01	4.46	4.57	6.12	9.14	12.56	15.46	17.00	16.86	14.76	11.06	7.36	4.72	2.99	4.86	7.74	11.40	32 10	
31	14.94	17.54	18.47	17.66	14.67	11.08	7.54	5.01	3.93	4.32	6.55	9.62	13.04	15.80	16.84	16.08	13.73	10.16	6.82	4.54	3.58	4.41	6.36	9.36	33 11	
32	15.86	17.74	17.94	16.48	13.27	9.84	6.84	4.96	4.33	5.26	7.44	10.66	15.74	16.43	15.42	12.82	9.66	6.90	5.42	5.14	6.20	8.06	10.66	13.66	34 12	
33	16.02	17.12	16.74	14.88	11.68	8.76	6.34	4.92	4.74	8.26	11.07	13.66	15.16	15.34	14.06	11.68	9.04	7.34	6.56	6.94	8.04	9.56	11.76	14.24	35 13	
34	15.66	16.04	15.34	13.02	10.16	7.86	6.27	5.54	5.86	7.18	11.36	13.26	14.34	14.26	12.88	11.00	9.39	8.26	7.92	8.30	9.05	10.36	12.06	13.76	36 14	
35	14.66	14.44	11.12			7.54	6.26	6.13	6.68	7.86	9.28	10.86	13.10	12.54	11.93	10.66	9.72	9.12	9.06	9.26	9.66	10.60	11.82	13.34	37 16	

36	13.82	11.45	10.03	8.74	7.48	6.86	6.78	7.17	7.94	9.05	10.30	11.34	11.97	11.93	11.42	10.84	10.34	10.07	9.97	9.77	10.44	11.32	12.06	12.26	38 17	
37	11.78	10.88	9.87	8.84	7.86	7.24	6.94	7.18	8.03	9.07	10.14	11.00	11.56	11.85	11.77	11.46	11.12	10.77	10.70	9.70	9.70	10.13	10.80	11.27	11.45	38 18
38	11.25	10.76	9.97	9.00	8.00	7.11	5.58	6.74	7.44	8.31	9.84	10.90	11.76	12.34	12.30	11.60	10.57	9.76	9.34	9.17	9.56	10.24	10.94	11.36	40 19	
39	11.44	10.97	10.10	9.07	7.87	6.85	6.30	6.50	7.26	8.30	10.16	12.65	13.26	13.22	12.56	11.36	10.08	9.16	8.67	8.64	9.01	9.76	10.58	11.25	41 20	
40	11.66	11.34	10.36	8.82	7.36	6.12	5.54	6.94	8.54	10.36	12.06	13.46	13.97	13.64	12.30	10.76	9.26	8.14	7.84	8.12	8.96	10.24	11.52	12.40	42 21	
41	12.66	12.01	10.47	8.56	5.46	5.20	5.93	7.55	9.56	11.72	13.53	14.67	14.84	13.98	12.14	10.00	8.54	7.66	7.53	8.16	9.56	11.03	12.66	13.62	43 22	
42	13.60	10.24	7.77	5.88	4.84	4.96	4.96	6.33	8.27	10.66	13.07	14.85	15.64	15.23	13.64	11.13	9.02	7.54	6.79	7.00	8.13	11.85	14.38	13.88	45 0	
43	11.93	9.10	6.54	4.66	4.00	4.90	6.86	9.20	11.97	14.34	15.82	15.96	14.78	12.26	9.64	7.46	6.24	5.96	8.48	10.85	13.07	14.56	14.85	13.63	46 1	
44	10.90	7.86	5.37	4.07	4.04	5.46	7.84	10.63	13.64	15.83	16.64	16.01	13.87	10.90	8.00	5.46	5.74	7.26	9.70	12.25	14.42	15.50	15.15	13.08	47 2	
45	9.90	6.94	4.75	3.92	4.66	6.62	9.46	12.60	15.08	16.60	16.64	15.00	11.93	8.96	6.76	5.63	5.06	5.54	7.84	10.54	13.30	15.12	15.66	14.46	48 3	
46	8.44	5.86	4.26	4.25	5.32	7.84	10.68	13.68	16.68	15.86	13.15	10.22	7.36	5.65	4.23	4.46	6.07	8.56	11.57	14.06	15.54	15.51	13.57	10.53	49 4	
47	7.47	5.38	4.54	5.04	6.70	12.18	14.74	16.26	16.26	14.64	11.74	8.68	6.28	4.54	4.14	5.97	7.06	9.74	12.44	14.55	15.46	14.76	12.57	9.68	50 5	
48	7.24	5.60	6.54	8.40	10.77	13.32	15.42	16.26	15.47	13.18	10.24	7.54	5.62	4.54	4.69	5.80	7.87	10.40	12.41	14.50	15.06	11.86	9.36	7.58	51 7	
49	6.64	6.70	7.86	9.60	11.66	13.73	15.08	15.32	14.12	11.86	9.24	6.90	5.18	4.58	5.06	6.40	8.24	10.33	13.86	14.34	13.41	11.46	9.53	8.05	52 8	
50	7.40	7.66	8.58	9.92	11.68	13.36	14.16	14.12	12.82	10.83	8.73	6.98	5.45	4.92	5.44	6.63	10.14	11.77	12.96	13.40	12.76	11.56	10.24	9.04	53 9	
51	8.45	8.28	8.67	9.76	11.20	12.50	13.18	13.06	11.88	10.25	8.57	5.77	5.38	5.64	6.37	7.82	9.54	11.17	12.38	13.02	12.96	12.16	11.07	10.02	54 10	
52	8.94	8.44	8.48	9.27	10.44	11.57	12.34	12.34	11.70	8.90	7.32	5.96	5.24	5.12	5.86	7.17	8.90	10.63	12.10	13.16	13.56	13.13	11.86	10.27	55 11	
53	8.88	8.08	7.87	8.42	9.56	10.87	12.44	12.26	11.27	9.76	7.96	6.27	5.06	4.55	5.02	6.47	8.52	10.67	12.72	14.14	14.86	14.44	12.70	10.66	56 12	
54	8.80	7.60	7.21	7.21	9.18	11.00	12.40	13.36	13.52	12.60	8.63	6.40	4.63	4.06	4.70	6.46	8.84	11.30	13.80	15.56	16.25	15.33	10.26	7.95	57 14	
55	6.54	6.18	7.03	8.83	11.00	12.96	14.40	14.74	13.76	11.70	8.84	6.48	4.05	3.42	4.92	4.14	6.18	8.80	12.06	14.93	16.76	15.84	12.87	9.66	58 15	
56	5.18	5.12	6.26	8.52	11.16	13.67	15.38	15.86	14.57	11.93	8.36	5.48	3.42	2.92	4.14	6.52	9.58	16.04	17.62	17.34	15.27	11.66	8.27	5.56	59 16	
57	4.16	4.32	5.84	8.66	11.92	14.74	16.46	16.54	14.66	11.26	7.66	4.94	3.20	4.70	7.52	10.86	14.63	17.06	17.98	16.96	13.90	10.20	6.96	4.47	60 17	
58	3.56	4.02	6.04	9.40	12.86	15.55	16.86	16.36	13.86	10.44	4.54	3.37	3.90	5.80	8.56	12.33	15.44	17.27	17.40	15.46	12.93	8.50	5.70	3.74	61 18	
59	3.27	4.33	7.10	10.34	13.76	15.97	16.76	12.96	9.44	6.74	4.67	4.23	5.26	7.43	10.37	13.82	16.13	17.08	16.40	13.86	10.50	7.26	4.84	3.56	62 19	
60	3.86	5.60	8.27	11.55	16.02	16.28	14.66	11.66	8.60	6.46	5.26	5.46	6.56	8.86	11.44	14.36	15.97	16.18	14.88	12.00	8.86	6.28	4.06	4.86	63 21	
61	6.67	9.46	12.24	14.39	15.64	15.33	13.25	10.46	8.22	6.70	6.34	7.00	8.36	10.22	12.44	14.42	15.27	14.71	12.72	10.14	7.72	4.86	5.00	6.10	64 22	
62	8.03	10.30	12.47	13.97	14.58	13.92	12.93	10.14	8.54	7.56	7.56	8.42	9.82	11.34	12.96	14.04	14.24	13.22	9.36	7.56	6.27	5.84	6.34	7.46	65 23	
63	9.00	10.76	12.44	13.56	13.74	12.74	11.40	10.07	9.16	8.96	9.27	9.77	10.46	12.44	13.07	13.03	12.12	10.46	8.86	7.68	7.02	7.02	7.66	8.54	67 0	
64	9.66	10.96	12.24	12.88	12.88	12.24	11.43	10.66	10.24	10.16	10.24	10.86	11.44	12.02	12.40	12.24	11.36	10.18	8.87	7.97	7.67	7.94	8.50	9.00	68 1	
65	9.78	10.74	11.76	12.46	12.67	12.27	11.74	11.26	10.56	10.36	10.22	10.36	10.76	11.26	11.56	11.38	10.86	9.96	9.14	8.40	7.98	7.80	7.86	8.34	69 2	
66	9.30	10.46	11.44	12.08	12.36	12.03	11.50	10.78	10.20	9.75	9.58	9.87	10.35	10.89	11.10	11.10	10.78	10.32	9.72	8.86	7.97	7.28	7.26	7.87	70 3	
67	8.97	11.56	12.46	13.04	13.10	12.54	11.68	10.56	9.64	9.08	8.82	9.16	9.88	10.74	11.40	11.75	11.70	11.14	10.07	8.84	7.56	6.70	6.74	8.94	71 5	
68	10.62	12.06	13.26	13.78	13.68	12.86	11.34	9.88	8.86	8.16	8.03	8.46	9.64	10.86	12.06	12.78	12.56	11.57	9.92	8.17	6.67	5.98	6.16	7.20	8.87	72 6
69	10.76	12.70	14.08	14.61	14.06	12.53	10.68	8.96	7.55	6.88	7.05	8.07	9.84	11.76	13.54	13.03	11.46	9.42	7.27	5.74	5.30	5.90	7.44	9.66	73 7	
70	11.92	14.02	15.17	15.16	13.87	11.66	9.44	7.56	6.34	6.07	6.86	10.80	12.96	14.26	14.55	13.37	11.16	8.45	6.26	5.16	5.12	6.24	8.10	10.63	74 8	
71	13.22	15.15	15.86	15.17	13.22	10.40	7.80	6.06	5.25	6.90	9.24	11.72	13.95	15.20	15.12	13.39	10.64	7.57	5.44	4.44	4.96	6.46	8.94	11.85	75 9	
Sum	744.23	730.16	754.05	784.12	808.42	804.43	808.31	804.33	784.12	751.65	752.78	755.05	728.04	746.40	757.16	763.46	772.71	781.34	789.32	778.15	760.31	756.70	734.90	722.86	No. of Days.	
No.	75	74	74	74	75	74	74	75	75	74	75	76	74	74	74	74	74	74	74	76	74	75	74	74	74	1838.83

## FORMS FOR SHORT-PERIOD TIDES.

SERIES  $2M_2K_1$ —(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Rolar Hour	
72	14.34	16.00	16.06	14.53	11.64	8.54	4.22	3.97	5.24	7.30	10.10	13.02	15.04	16.00	15.20	12.86	9.54	6.67	4.92	4.38	5.52	7.55	10.33	13.50	16.10	76 10
73	15.75	16.73	13.66	10.42	7.22	4.92	3.64	4.00	5.66	8.33	11.52	14.30	16.06	16.52	15.06	12.13	8.73	6.13	4.66	4.99	6.52	8.92	11.86	14.66	16.40	77 12
74	16.56	15.07	11.90	8.47	5.62	3.74	3.22	4.26	6.00	9.60	12.85	15.23	16.56	16.25	14.26	10.83	8.00	5.75	5.11	5.88	10.40	13.38	15.68	16.66	17.18	78 18
75	15.80	13.36	10.12	7.06	4.81	3.54	3.76	5.34	7.86	11.09	13.93	15.92	16.74	15.74	13.36	7.64	6.12	6.08	7.14	9.00	11.56	13.90	15.66	15.98	17.14	79 14
76	14.76	13.06	8.90	6.13	4.34	3.62	4.36	6.06	8.47	11.31	13.87	15.62	16.12	12.74	10.02	8.05	6.96	7.06	7.93	9.67	12.07	14.08	15.23	15.08	80 15	
77	13.57	11.16	8.26	6.08	4.76	4.47	5.46	7.26	9.48	11.88	13.90	15.50	14.66	12.67	10.54	8.74	7.94	8.14	9.06	10.62	12.40	13.77	14.52	14.20	81 16	
78	12.86	10.64	8.47	6.76	5.86	5.82	7.75	9.52	11.71	13.54	14.73	14.90	14.06	12.63	11.05	9.70	8.86	8.72	9.12	10.24	11.76	13.06	13.66	13.34	82 17	
79	12.06	10.56	7.40	6.43	6.30	6.68	7.68	9.46	11.24	13.02	14.08	14.52	14.44	13.62	12.12	10.36	8.96	8.11	7.96	8.44	11.26	12.36	12.86	12.44	83 19	
80	11.22	9.67	8.30	7.00	6.48	6.64	7.48	8.86	10.64	12.34	13.74	14.48	14.44	13.62	12.12	10.36	8.00	6.56	7.46	9.22	11.16	12.56	13.57	14.06	84 20	
81	11.94	10.50	8.78	7.30	6.06	5.92	6.72	8.34	10.26	12.20	13.86	15.00	15.14	14.16	12.20	9.88	6.90	6.67	8.88	11.24	13.46	14.86	15.36	14.86	85 21	
82	13.37	11.72	9.38	7.17	5.72	5.38	6.17	7.82	10.00	12.50	14.54	15.84	15.94	14.64	12.14	9.36	6.97	5.74	6.67	9.22	13.20	15.64	17.04	16.75	86 22	
83	14.34	12.05	9.44	6.93	5.38	5.00	5.82	7.83	10.50	13.30	15.60	16.28	14.37	11.37	8.36	6.00	4.67	4.80	6.40	9.20	12.06	14.62	16.12	16.16	87 23	
84	14.90	12.22	9.12	6.60	5.05	4.86	5.87	8.10	11.14	14.15	16.35	17.15	16.24	13.58	10.14	7.06	4.83	3.96	4.70	6.72	9.92	13.20	15.64	17.04	16.75	89 0
85	14.92	11.81	8.56	6.27	5.64	6.94	9.43	12.61	15.44	17.03	17.08	15.36	11.92	8.64	6.18	4.48	4.25	5.24	7.57	11.00	14.10	16.43	17.34	16.56	90 1	
86	14.38	7.84	5.95	5.42	5.93	7.22	9.26	12.02	14.66	16.44	16.67	15.66	13.96	10.44	7.12	4.80	3.83	4.41	6.43	8.78	12.04	14.74	16.66	15.64	12.86	91 3
87	9.53	7.16	5.81	5.93	7.04	8.26	10.50	13.00	14.94	15.83	15.12	12.94	9.87	7.14	5.16	4.22	6.40	8.73	11.37	14.00	15.82	16.34	13.10	10.40	93 5	
88	8.36	7.32	7.28	8.03	9.50	11.53	13.48	14.74	14.92	13.67	11.34	8.76	7.14	5.16	4.22	6.40	8.73	11.37	14.00	15.82	16.34	13.10	10.40	94 6		
89	8.78	8.26	8.47	9.24	10.52	12.04	13.48	14.16	12.27	10.16	8.14	6.47	5.74	6.22	7.44	9.20	10.85	12.64	14.05	14.67	14.27	12.97	11.44	10.04	96 7	
90	9.16	8.84	9.16	9.84	10.95	12.80	12.96	12.28	10.94	9.24	7.80	6.78	6.70	7.30	8.37	9.54	10.90	12.34	13.32	13.80	13.26	12.13	10.96	10.04	96 8	
91	9.60	9.54	9.90	10.56	11.44	11.92	12.05	11.54	10.36	9.16	8.12	7.47	7.44	7.87	8.52	9.46	10.73	11.93	12.74	12.98	12.60	11.86	11.07	9.94	97 10	
92	9.77	9.87	10.02	10.36	10.81	11.14	11.27	10.92	10.30	9.34	8.36	7.74	7.58	7.98	8.76	9.87	11.04	11.96	12.50	12.42	11.96	11.34	10.55	9.91	98 11	
93	9.47	9.34	9.52	9.94	10.53	10.94	11.12	11.02	10.62	10.00	9.22	8.40	8.01	8.13	8.63	9.70	11.77	12.66	13.06	12.94	12.40	11.47	10.50	9.62	99 12	
94	8.94	8.54	8.74	9.48	10.45	11.36	11.88	11.89	11.44	10.50	9.40	8.46	7.76	7.84	8.43	9.46	10.86	12.30	13.36	13.82	13.66	12.66	11.42	10.02	8.72	100 13
95	7.96	7.82	8.36	9.47	10.86	11.90	12.70	12.87	11.00	9.52	8.12	7.40	7.47	8.26	9.54	11.08	12.70	14.06	14.56	14.22	12.80	10.96	8.88	7.46	101 14	
96	6.81	6.84	7.02	9.62	11.52	13.00	14.12	13.00	11.02	9.05	7.48	6.74	6.92	7.97	9.72	11.72	13.58	14.86	15.12	14.21	12.35	9.67	7.47	5.98	102 15	
97	5.58	6.14	7.06	12.16	14.02	15.18	15.06	13.40	10.95	8.28	6.66	6.02	6.46	7.88	10.06	12.53	14.55	15.72	15.49	13.80	11.08	8.22	5.93	4.32	103 17	
98	5.47	7.72	10.54	13.27	15.36	16.20	15.32	13.00	9.88	7.34	5.76	5.40	6.24	8.22	10.70	13.40	15.32	16.25	15.36	9.46	6.56	4.47	3.42	3.91	104 18	
99	5.74	8.31	11.40	14.40	16.28	16.72	15.47	12.68	9.44	6.81	5.47	5.38	6.52	8.91	11.80	14.40	16.08	14.35	11.30	7.80	4.97	2.93	2.46	3.76	105 19	
100	6.21	9.51	12.97	15.58	17.14	17.04	14.94	11.68	8.36	6.14	5.06	5.57	7.24	10.07	15.40	16.44	15.82	13.44	9.74	6.67	4.03	2.50	2.77	4.44	106 20	
101	7.50	10.96	14.33	16.70	17.72	16.91	14.37	10.87	8.10	5.71	6.50	8.36	11.33	13.10	15.40	16.44	15.82	13.44	9.74	6.67	4.03	2.50	2.77	4.44	107 21	
102	8.64	12.02	15.12	16.94	17.54	16.24	13.40	10.32	7.62	6.17	6.97	7.04	12.00	14.47	15.69	15.54	13.66	10.74	7.44	4.88	3.28	3.04	4.36	6.67	108 22	
103	9.40	12.47	15.00	16.74	15.60	13.03	10.31	7.87	6.76	6.80	7.71	9.70	12.14	14.15	15.02	14.50	12.53	9.92	7.24	5.36	4.17	4.16	5.20	7.26	110 0	
104	12.40	14.57	15.77	15.74	14.47	12.12	9.90	8.97	7.14	7.11	7.83	9.54	11.58	13.16	13.74	13.28	11.76	9.56	7.60	5.96	5.02	4.52	4.52	9.74	111 1	
105	12.00	13.97	14.87	14.77	13.76	13.06	10.26	8.74	7.82	7.54	8.00	9.34	11.00	12.36	12.96	12.72	11.58	10.14	6.94	6.06	5.96	6.06	7.87	9.72	112 2	





FORMS FOR SHORT-PERIOD TIDES.  
 SERIES 2M<sub>3</sub>K<sub>1</sub>—(Continued).

Day	0 <sup>a</sup>	1 <sup>a</sup>	2 <sup>a</sup>	3 <sup>a</sup>	4 <sup>a</sup>	5 <sup>a</sup>	6 <sup>a</sup>	7 <sup>a</sup>	8 <sup>a</sup>	9 <sup>a</sup>	10 <sup>a</sup>	11 <sup>a</sup>	12 <sup>a</sup>	13 <sup>a</sup>	14 <sup>a</sup>	15 <sup>a</sup>	16 <sup>a</sup>	17 <sup>a</sup>	18 <sup>a</sup>	19 <sup>a</sup>	20 <sup>a</sup>	21 <sup>a</sup>	22 <sup>a</sup>	23 <sup>a</sup>	Solar Hour	
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h
143	9.70	13.38	14.66	15.94	16.04	14.86	13.64	10.27	8.44	7.54	7.34	8.10	9.52	11.55	13.36	14.27	13.92	12.06	9.48	6.90	4.32	4.97	6.54	8.70	150 21	
144	11.00	13.46	15.12	16.07	15.67	14.17	11.77	9.56	8.16	7.68	7.83	8.74	10.50	12.26	13.06	14.02	12.96	10.86	8.34	6.24	5.04	4.82	5.84	7.60	9.46	151 22
145	11.87	14.10	15.30	15.60	14.66	12.78	10.74	9.03	7.96	7.73	8.24	9.44	11.07	12.62	13.16	11.96	9.94	7.67	6.16	5.18	5.56	6.86	8.64	10.66	152 23	
146	12.74	14.30	15.12	15.06	13.65	11.84	10.00	8.46	7.75	8.46	9.92	11.36	12.37	12.84	12.22	10.98	9.18	7.32	6.03	5.94	6.87	8.17	9.67	11.58	154 0	
147	13.28	14.64	14.97	14.22	12.62	11.08	9.47	8.08	8.30	9.20	10.24	11.40	12.12	12.46	11.72	10.38	8.77	7.37	6.70	6.93	7.78	8.83	10.30	11.90	155 1	
148	13.54	14.68	14.80	13.77	10.50	9.20	8.47	8.28	8.60	9.36	10.36	11.26	11.83	12.05	11.56	10.60	9.20	8.14	7.72	7.83	8.62	9.82	11.10	12.64	156 2	
149	13.94	14.16	13.26	11.74	10.42	9.26	8.54	8.34	8.46	9.23	10.10	10.93	11.70	11.97	11.72	11.06	9.98	8.86	8.32	8.36	9.00	11.54	12.92	13.86	157 4	
150	14.25	13.85	13.88	11.48	10.08	8.98	8.20	8.20	8.37	9.12	10.03	11.29	12.14	12.58	12.36	11.84	11.02	9.23	8.78	9.20	10.37	11.98	13.44	14.22	158 5	
151	14.34	13.94	12.86	11.59	10.03	8.74	7.92	7.54	7.76	8.67	9.96	11.54	12.84	13.87	13.28	12.03	10.56	9.66	9.64	10.17	11.38	12.77	13.98	14.67	159 6	
152	15.14	14.88	13.86	12.46	10.48	8.83	7.82	7.50	8.19	9.46	11.28	14.76	15.82	15.76	14.97	13.34	11.70	10.67	10.27	10.56	11.52	12.90	14.12	15.30	160 7	
153	15.65	15.48	14.17	12.02	9.86	8.00	7.09	6.83	7.34	11.40	13.77	15.84	16.86	16.85	15.76	13.60	11.52	9.95	9.55	9.80	10.84	12.57	14.21	15.47	161 8	
154	16.06	15.22	13.50	10.84	8.22	6.16	5.15	4.90	5.50	11.37	14.18	16.48	17.54	17.17	15.60	12.50	10.07	8.34	8.17	8.96	10.27	12.23	14.24	15.74	162 9	
155	16.29	12.77	9.46	6.34	4.44	3.62	4.30	6.30	8.54	11.95	15.02	17.28	17.95	17.20	15.02	11.76	9.04	7.44	7.22	7.81	9.55	12.08	14.24	16.07	163 11	
156	14.76	11.87	8.16	5.07	3.07	2.74	3.80	5.94	9.24	12.80	15.92	18.07	18.53	17.65	14.65	10.90	8.00	6.62	6.55	7.50	9.65	12.45	14.89	16.40	164 12	
157	14.28	10.90	7.10	4.31	2.62	2.37	3.68	6.11	10.40	13.95	16.74	17.95	16.07	12.81	9.60	7.05	5.72	5.77	7.00	9.60	12.79	15.16	16.42	15.96	165 13	
158	13.80	10.33	6.77	4.00	2.33	2.54	4.18	7.10	10.40	16.44	17.72	17.40	15.44	12.07	9.02	6.70	5.67	5.93	7.41	10.07	13.02	14.92	15.57	14.68	167 15	
159	12.76	9.20	6.14	3.33	2.88	3.47	5.52	7.93	11.04	16.44	17.20	16.60	14.54	11.30	8.66	6.74	6.05	6.16	7.65	10.05	12.50	14.32	14.83	14.03	168 16	
160	12.28	9.20	6.52	4.77	4.20	4.94	8.80	11.67	14.34	16.42	17.20	15.74	13.76	10.84	8.61	6.86	6.32	6.58	7.80	9.82	12.04	13.55	14.17	12.03	169 18	
161	11.96	9.47	7.26	5.80	6.39	7.66	9.64	11.92	14.25	15.90	16.46	15.74	12.66	10.40	8.31	7.04	6.60	6.77	7.78	9.93	10.90	12.32	13.46	12.40	170 19	
162	10.34	8.60	7.57	7.26	7.62	8.44	9.92	12.12	14.20	15.46	15.54	14.58	12.66	10.40	8.31	7.04	6.60	6.70	7.50	9.03	10.90	12.32	13.38	12.92	171 20	
163	10.90	9.62	8.66	8.31	8.49	9.03	10.30	12.04	13.70	14.74	14.75	13.73	12.02	10.10	8.46	7.12	6.53	6.70	7.50	9.06	10.90	12.32	13.20	13.38	12.92	172 21
164	11.94	10.67	9.60	8.94	8.82	9.24	10.33	11.90	13.24	14.06	14.10	13.34	11.84	8.26	6.94	6.44	6.67	7.49	9.00	10.94	12.50	13.66	14.10	13.63	172 21	
165	12.46	11.06	10.06	9.30	9.05	9.33	10.22	11.60	12.90	13.85	13.08	11.64	9.76	8.00	6.70	6.08	6.22	7.28	9.00	10.94	12.77	14.05	14.63	14.37	173 22	
166	12.86	11.33	10.04	9.14	8.86	9.20	10.08	12.44	13.30	13.52	12.80	11.00	8.85	7.06	5.67	5.05	5.60	7.15	9.26	11.30	13.28	14.45	14.84	13.95	174 23	
167	12.40	10.90	9.46	8.24	8.56	9.64	11.12	12.55	13.40	13.37	12.07	10.97	8.20	6.17	4.94	4.74	5.62	7.74	9.76	12.14	14.01	15.00	14.86	12.06	176 1	
168	10.27	8.84	8.10	7.94	8.52	9.68	11.18	12.64	13.37	13.05	11.52	9.17	6.76	5.11	4.16	4.64	6.10	8.00	10.50	12.90	14.56	14.70	13.32	11.14	177 2	
169	9.44	8.17	7.54	7.57	8.34	9.81	11.05	13.20	13.60	12.56	10.40	7.97	5.83	4.38	4.04	4.96	6.82	9.02	13.86	15.24	15.44	14.56	12.56	10.36	178 3	
170	8.63	7.62	7.30	7.74	8.86	10.67	12.47	13.67	13.60	12.02	9.66	6.93	4.96	3.94	5.70	7.84	10.40	12.82	14.74	15.56	15.33	13.86	11.44	9.35	179 4	
171	7.79	7.04	7.03	7.90	9.44	11.66	13.22	13.92	13.00	10.74	8.00	4.04	3.83	4.76	6.70	9.02	11.37	13.67	15.12	15.46	14.48	12.44	9.96	8.16	180 5	
172	6.86	6.42	6.94	8.42	10.44	12.57	13.67	12.22	9.64	6.86	4.96	3.98	4.36	5.65	7.72	10.02	12.26	14.31	15.28	15.12	13.77	11.30	9.01	7.37	181 6	
173	6.64	6.56	7.46	9.06	12.70	13.51	13.01	11.07	8.44	6.12	4.72	4.42	5.32	6.94	8.97	11.17	13.22	14.74	15.17	14.22	12.16	9.74	7.86	6.74	182 7	
174	6.51	8.16	9.92	11.66	12.82	13.10	11.86	9.72	7.36	5.70	5.02	5.24	6.42	8.07	10.12	11.98	13.73	14.86	14.72	13.40	11.17	7.55	6.51	6.57	183 9	
175	7.34	8.72	10.61	12.04	12.77	12.64	11.27	9.34	7.48	6.30	5.87	6.54	7.66	9.24	10.97	12.94	14.38	14.88	14.20	10.34	8.44	7.22	6.77	6.97	184 10	
176	7.87	9.34	10.94	12.19	12.66	12.22	10.84	9.25	7.90	6.96	6.92	7.56	8.50	10.00	11.48	14.36	14.44	13.38	11.42	9.60	8.02	6.94	6.56	6.91	185 11	
177	7.79	9.26	10.80	11.92	12.43	12.16	11.12	9.70	8.48	7.63	7.56	8.14	10.41	11.98	13.30	13.98	13.72	12.51	10.84	9.96	8.96	7.47	6.48	6.84	186 12	



FORMS FOR SHORT-PERIOD TIDES.  
 SERIES 2M<sub>3</sub>K<sub>1</sub>—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour	
213	4.48	5.07	7.18	10.36	13.94	16.34	17.16	16.04	13.12	9.20	5.80	3.36	2.56	3.60	5.73	9.03	12.78	15.94	17.78	18.04	16.74	13.32	9.36	6.95	4.18	224 0
214	3.80	4.90	7.36	11.10	14.46	16.66	16.88	15.39	12.15	8.23	5.44	3.52	3.32	4.58	7.04	10.14	13.35	16.16	17.52	17.26	15.28	11.80	8.22	5.32	3.80	225 7
215	4.01	5.58	8.40	11.50	14.52	16.18	16.06	14.38	11.26	7.98	5.62	4.80	6.25	8.27	11.00	13.96	16.32	17.26	16.42	14.32	10.85	7.62	5.16	4.10	226 8	
216	4.64	6.45	8.92	12.05	14.70	15.80	15.18	13.36	10.62	7.94	6.32	5.74	7.77	9.72	12.07	14.12	15.66	15.72	14.46	12.06	9.36	6.96	5.40	5.07	227 9	
217	5.84	7.33	9.54	11.87	13.60	13.96	12.48	10.40	8.65	7.45	7.28	8.00	9.26	10.72	12.27	13.74	14.47	14.18	12.78	10.82	8.78	6.78	5.83	5.86	228 10	
218	6.74	10.14	12.02	13.26	13.57	12.85	11.76	10.70	9.74	9.12	8.90	9.34	10.06	10.94	12.10	12.88	13.72	13.38	11.88	10.06	8.17	7.02	7.00	7.70	229 12	
219	8.71	10.10	11.44	12.33	12.66	12.46	12.00	11.36	10.62	10.07	9.67	9.77	10.12	10.82	11.54	12.43	12.67	12.12	11.22	9.90	8.64	7.77	7.46	7.09	8.30	230 18
220	9.04	10.10	11.17	12.34	12.90	12.90	12.34	11.72	11.15	10.62	10.30	10.00	10.14	10.50	11.34	12.26	11.97	11.38	10.53	9.44	8.35	7.66	7.57	7.24	8.12	231 14
221	9.06	10.48	11.57	12.72	13.42	13.56	13.18	12.30	11.45	10.72	10.26	9.92	10.00	10.71	11.62	12.32	12.18	11.42	10.36	9.08	8.15	7.53	7.24	7.70	7.70	232 15
222	8.54	9.82	11.43	12.72	13.64	13.66	13.26	12.36	11.22	9.34	8.97	9.08	9.88	10.76	11.64	12.36	12.35	11.85	10.40	8.78	7.36	6.44	6.28	7.14	7.14	233 16
223	8.37	10.20	11.94	13.38	14.40	14.54	13.58	12.17	10.70	9.34	8.84	9.26	10.00	11.16	12.50	13.30	13.42	12.06	10.16	8.40	6.86	6.06	6.14	7.20	7.20	234 17
224	8.95	12.76	13.96	14.91	14.84	13.64	11.84	9.97	8.77	8.36	8.48	8.96	10.06	11.56	13.12	13.97	13.64	12.06	9.70	7.27	5.96	5.56	6.35	9.76	9.76	235 19
225	11.70	13.66	15.10	15.46	14.62	12.86	10.57	8.64	7.46	7.31	7.76	8.84	10.72	12.04	14.21	14.62	13.44	11.00	8.24	5.17	5.36	6.54	8.54	10.66	10.66	236 20
226	13.00	15.02	15.96	15.50	14.08	11.60	8.97	7.34	6.70	6.84	7.80	9.62	11.70	13.76	14.95	12.76	10.00	7.37	5.56	4.97	5.06	6.36	8.22	10.64	13.40	238 22
227	14.36	16.04	16.17	15.32	13.08	10.11	7.72	6.36	6.10	6.94	8.63	10.83	13.20	15.71	17.43	11.89	8.54	6.26	4.97	5.06	6.36	8.22	10.64	13.40	14.56	239 23
228	15.80	16.61	16.16	14.21	11.38	8.34	6.35	5.46	5.74	7.13	11.84	14.36	15.90	14.88	12.52	9.63	7.07	5.74	5.64	6.67	8.36	10.62	13.17	15.30	15.30	241 0
229	16.24	16.56	15.34	12.80	9.60	7.06	5.50	5.94	7.72	10.28	13.04	15.14	15.90	14.88	12.52	9.63	7.07	5.74	5.64	6.67	8.36	10.62	13.17	15.30	15.30	242 2
230	16.38	15.97	14.06	8.16	6.11	5.05	5.41	6.72	8.83	11.26	13.77	15.36	15.38	14.00	11.50	8.72	6.86	5.97	6.34	7.52	9.30	11.47	13.80	15.46	15.46	242 2
231	14.77	13.44	9.37	7.06	5.37	4.85	5.64	7.12	9.24	11.64	13.96	15.06	14.75	13.17	10.76	8.64	7.30	6.86	7.44	8.64	10.36	14.06	15.24	15.10	15.10	243 3
232	13.64	11.26	8.61	6.50	5.32	5.38	6.34	7.85	9.86	11.96	13.64	14.58	14.07	12.68	10.68	8.97	8.02	8.36	9.26	10.60	12.24	13.73	14.44	13.86	13.86	244 4
233	12.25	10.02	8.06	6.46	5.62	5.78	6.47	7.80	9.63	11.38	12.97	13.74	13.44	12.44	11.04	9.83	8.84	8.57	8.87	9.67	10.67	11.96	13.06	13.46	13.08	245 6
234	11.68	9.86	8.26	6.87	6.17	6.26	7.02	8.17	9.66	11.26	12.55	13.57	12.94	11.92	10.73	9.67	9.16	9.18	9.63	10.54	11.48	12.46	12.92	12.66	12.66	246 6
235	11.74	10.42	8.87	7.44	6.44	6.21	6.66	7.76	9.66	11.26	13.37	14.05	13.67	12.68	11.26	10.02	9.22	8.90	9.14	9.86	10.86	12.02	12.84	12.98	12.98	247 7
236	12.36	11.16	9.57	6.24	5.63	5.97	7.17	8.80	10.66	12.80	14.28	14.96	14.74	13.66	11.85	10.04	8.66	8.02	8.14	9.04	10.38	12.00	13.14	13.74	13.74	248 8
237	13.04	10.04	7.64	5.76	4.78	5.02	6.24	8.16	10.78	13.20	15.04	15.98	15.74	14.33	11.96	9.30	7.37	6.55	6.70	8.06	9.98	13.06	14.86	14.44	14.44	249 10
238	12.80	10.18	7.37	5.17	3.90	4.03	5.50	7.96	10.88	13.80	16.04	17.04	16.46	14.44	11.04	8.24	6.27	5.63	5.74	7.24	9.64	12.52	14.74	15.98	15.46	250 11
239	13.29	9.94	6.63	4.34	3.17	3.53	5.38	8.20	11.40	14.56	16.82	17.44	16.36	13.83	9.98	4.46	3.84	4.58	6.80	10.06	13.28	15.76	16.64	15.75	15.75	251 12
240	12.94	9.26	6.06	3.66	2.67	3.72	5.66	8.70	12.20	15.53	17.33	15.87	12.42	8.56	5.32	3.44	3.17	4.55	7.26	10.87	14.22	16.50	17.95	15.47	15.47	252 13
241	12.37	8.41	5.52	3.48	3.10	4.46	6.74	9.94	16.22	17.47	17.02	14.77	10.84	7.23	4.52	3.00	3.30	5.07	8.06	11.72	14.94	16.86	16.90	14.94	14.94	253 14
242	11.54	8.00	5.38	3.90	5.52	7.95	11.06	14.30	16.51	17.04	15.88	12.99	9.17	5.97	3.70	2.94	3.94	6.16	9.14	12.45	15.42	16.68	16.10	13.81	13.81	254 15
243	10.56	5.47	4.87	5.60	7.04	9.54	12.25	14.81	16.16	16.06	14.44	11.07	7.87	5.34	3.84	3.92	5.16	7.43	9.36	13.45	15.47	16.68	13.66	9.98	9.98	255 17
244	7.74	6.47	6.36	7.02	8.54	10.58	12.80	14.58	15.36	14.73	12.51	9.86	7.17	5.31	4.44	5.02	6.44	8.50	11.04	14.79	14.77	13.46	11.46	9.44	9.44	256 18
245	8.00	7.36	7.56	8.36	9.51	11.10	12.60	13.73	13.94	12.90	11.02	8.73	6.90	5.70	5.63	6.34	8.36	11.36	13.14	13.88	13.60	12.43	10.94	9.64	9.64	257 19
246	8.76	8.44	8.70	9.18	9.95	10.88	12.06	12.76	13.71	11.64	9.87	8.26	6.44	6.67	7.34	8.36	9.74	11.16	12.22	12.70	13.20	11.38	10.60	9.88	9.88	258 20
247	9.34	9.16	9.12	9.34	9.87	10.66	11.30	11.62	11.37	9.48	8.44	7.52	7.14	7.33	7.86	8.66	9.84	10.90	11.62	11.97	11.87	11.54	11.08	10.42	10.42	259 21



FORMS FOR SHORT-PERIOD TIDES.

SERIES 2M<sub>2</sub>K<sub>1</sub>.—(Continued).

Day	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>	Solar Hour		
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	d h	
284	7.71	6.07	5.84	6.88	8.87	11.47	14.12	15.94	16.22	14.81	11.87	8.55	3.46	2.87	4.17	6.35	9.32	13.00	15.95	17.47	17.44	15.72	12.68	9.66	298 16		
285	7.28	5.94	6.04	7.36	9.64	12.45	14.84	16.04	15.60	10.52	7.15	4.66	2.92	3.10	4.72	7.47	10.55	13.92	16.35	17.36	16.74	14.57	11.67	8.85	299 17		
286	6.76	5.94	6.28	7.70	9.92	12.68	14.78	15.58	14.78	12.36	9.26	6.36	4.20	3.07	3.72	5.55	8.04	11.05	14.10	16.17	16.96	16.12	14.06	11.35	8.82	300 18	
287	7.14	6.57	8.46	10.56	13.14	14.64	15.04	13.76	11.47	8.74	6.42	4.70	4.22	5.00	6.80	9.02	11.88	14.60	16.14	16.22	15.16	13.26	10.86	8.86	7.58	301 20	
288	7.14	7.44	8.84	10.92	12.84	13.84	13.86	12.57	10.68	8.54	6.84	5.56	5.27	5.98	7.33	9.36	11.72	14.00	15.22	14.58	12.88	11.01	9.42	8.12	302 21		
289	7.64	7.92	8.94	10.40	11.85	12.91	13.12	12.26	10.75	9.22	7.66	6.68	6.30	6.72	7.86	9.44	11.50	13.34	14.46	14.66	13.96	12.74	11.30	9.76	8.54	303 22	
290	7.93	7.84	8.40	9.60	10.88	12.06	12.64	12.40	11.47	10.10	8.76	7.68	7.06	7.90	9.22	10.97	12.56	13.72	14.38	14.04	13.04	11.45	9.76	8.15	304 23		
291	7.22	7.02	7.48	8.84	10.32	11.48	12.55	12.87	12.46	11.36	8.28	7.14	6.80	7.40	8.84	10.74	12.56	13.87	14.54	14.38	13.40	11.67	9.60	7.53	306 0		
292	6.30	5.88	6.50	8.20	10.07	11.93	13.36	14.04	13.66	12.30	10.26	8.61	7.37	6.86	7.24	8.35	10.36	12.50	14.13	15.08	14.96	13.80	11.64	9.03	6.96	307 1	
293	5.44	5.04	5.86	7.79	10.12	12.66	14.54	15.37	14.86	13.04	10.66	8.56	7.12	6.44	6.77	8.02	10.14	12.62	14.56	15.55	15.25	13.56	10.92	8.12	5.82	308 3	
294	4.10	5.32	7.70	10.85	13.60	15.51	16.05	15.06	12.86	10.40	8.16	6.53	5.96	6.51	8.24	10.85	13.27	15.16	15.84	15.03	12.98	9.78	7.04	4.71	3.46	309 4	
295	3.86	5.60	8.44	11.74	14.64	16.50	16.72	15.38	12.86	9.98	7.70	6.25	5.93	6.71	8.67	11.25	13.84	15.52	15.84	14.55	11.68	8.46	5.64	3.63	3.01	310 5	
296	4.08	6.50	9.62	13.08	15.81	17.12	16.72	14.87	12.03	9.20	7.26	6.32	6.37	7.46	12.20	14.35	15.67	15.28	13.15	10.15	7.00	4.47	3.03	3.22	311 6		
297	5.03	7.60	10.76	14.05	16.38	17.05	16.14	13.92	11.10	8.66	6.87	6.46	8.00	10.44	13.10	14.76	15.16	13.92	11.40	8.36	5.66	3.69	2.94	3.94	312 7		
298	6.18	9.01	12.24	14.92	16.53	16.56	15.16	12.66	10.06	7.96	6.74	6.60	7.35	9.00	11.24	13.43	14.50	14.36	12.66	9.94	7.20	4.97	3.56	3.77	5.34	313 8	
299	7.72	10.56	13.46	15.64	15.71	13.92	11.46	9.28	7.66	6.86	6.98	7.98	9.96	12.00	13.52	14.02	13.37	11.18	8.81	6.52	4.86	4.33	5.20	6.90	314 9		
300	9.14	11.80	14.20	15.72	15.81	14.66	12.72	10.71	8.96	7.82	7.56	7.92	9.16	10.68	12.24	13.26	13.26	12.06	10.17	8.00	6.25	5.31	5.50	6.66	8.34	10.52	315 11
301	12.80	14.44	15.18	14.68	13.32	11.56	10.02	8.76	8.10	8.00	8.60	9.65	10.96	12.18	12.58	12.23	11.04	9.16	7.62	6.54	6.20	6.84	7.96	9.38	11.14	316 12	
302	12.91	14.18	14.40	13.64	12.37	10.90	9.58	8.78	8.46	8.68	9.30	10.00	10.94	11.57	11.80	10.28	8.94	7.84	7.18	7.20	7.86	8.80	9.98	11.46	317 13		
303	12.86	13.86	13.83	12.96	11.72	10.53	9.66	9.14	8.92	8.96	9.17	9.66	10.40	11.10	11.37	11.01	10.20	9.26	8.46	8.10	8.14	8.60	9.44	10.56	11.74	318 14	
304	12.76	13.34	13.26	12.61	11.72	10.86	9.76	9.04	8.85	9.16	9.64	10.14	10.74	11.18	11.32	11.06	10.38	9.58	8.94	8.71	8.90	9.50	10.42	11.46	319 15		
305	12.48	13.10	13.15	12.64	11.84	10.76	9.71	8.88	8.35	8.19	8.42	9.04	9.96	10.86	11.50	11.80	11.55	10.96	9.98	9.08	8.64	8.75	9.38	10.38	11.46	320 16	
306	12.41	13.07	13.16	12.84	11.84	10.56	9.24	8.13	7.50	7.43	7.86	8.83	10.03	11.16	12.23	12.80	12.64	11.66	10.25	9.04	8.36	8.34	8.96	10.02	11.20	12.46	321 18
307	13.23	13.47	13.00	11.72	10.14	8.38	7.03	6.27	6.31	7.08	8.52	10.23	11.92	13.17	13.63	13.10	11.86	10.18	8.76	7.98	7.96	8.75	10.13	11.64	13.14	322 19	
308	13.94	13.94	13.04	11.34	9.30	7.45	5.86	5.13	5.46	6.76	8.80	11.15	13.20	14.66	14.98	13.87	11.76	9.58	8.10	7.27	7.36	8.22	9.82	11.76	13.33	323 20	
309	14.28	14.14	12.87	10.56	7.98	5.77	4.14	3.74	4.67	6.71	9.27	12.02	14.40	15.66	15.44	13.71	11.16	8.74	7.02	6.40	6.78	8.22	10.37	12.25	13.88	324 21	
310	14.74	14.20	12.26	9.36	6.51	4.12	2.75	2.94	4.56	7.03	10.05	13.27	15.65	16.62	15.90	13.76	10.86	8.17	6.45	5.84	6.36	8.12	10.44	12.84	14.46	325 22	
311	15.08	13.97	11.41	8.07	4.96	2.57	1.63	2.58	4.74	7.64	11.12	14.22	16.47	17.07	15.75	12.96	9.86	7.26	5.65	5.46	6.44	8.40	11.20	13.57	15.11	326 23	
312	15.17	13.27	9.96	6.40	3.62	1.76	1.54	3.26	6.02	9.25	12.97	15.66	17.40	17.25	15.37	12.23	9.00	6.75	5.63	5.63	6.88	9.32	12.22	14.44	14.80	328 1	
313	12.31	8.84	5.46	3.00	1.66	2.20	4.15	6.95	10.46	13.81	16.44	17.54	16.82	14.56	11.38	8.50	6.32	5.44	5.74	7.26	10.06	12.76	14.67	15.26	14.06	329 2	
314	11.32	8.05	5.16	2.94	2.16	3.11	5.16	7.96	11.23	14.30	16.57	17.22	16.23	13.81	10.68	8.07	6.16	5.50	5.88	7.64	10.25	12.77	14.29	14.72	13.33	330 3	
315	10.74	7.81	5.32	3.66	3.26	4.42	6.34	8.86	11.67	14.58	16.33	16.57	15.28	12.84	9.93	7.47	6.23	5.72	6.26	7.94	10.30	12.38	13.76	13.96	12.68	331 4	
316	10.56	8.18	6.28	4.97	4.83	5.73	7.34	9.38	12.05	14.37	15.80	14.56	12.28	9.94	8.13	6.64	6.14	6.54	8.04	10.04	11.78	12.86	13.16	12.24	12.53	332 5	
317	10.73	8.96	7.30	6.24	5.96	6.50	7.80	9.84	12.15	13.88	14.87	14.84	13.77	11.77	10.06	8.23	6.86	6.34	6.56	8.04	10.04	10.84	12.16	12.76	12.53	333 6	
318	11.48	10.14	8.60	7.52	7.44	8.47	10.17	11.91	13.34	14.21	14.40	13.72	12.30	10.42	8.41	6.88	6.14	6.37	7.32	8.81	10.45	11.84	12.86	13.08	12.42	334 8	

319	11.25	9.75	8.54	7.84	7.88	8.64	10.02	11.65	13.16	14.14	14.30	13.64	12.17	10.31	8.37	6.68	5.72	5.86	6.88	8.64	10.00	13.31	13.88	13.62	385	9		
320	12.36	10.67	9.06	8.12	7.90	8.54	9.72	11.26	12.78	13.82	14.20	13.74	12.14	10.05	7.76	6.00	5.04	5.23	6.52	8.50	10.56	13.00	14.40	13.86	386	10		
321	12.58	10.80	8.97	7.94	7.68	8.24	9.50	11.14	12.75	13.98	14.44	13.73	11.85	9.10	5.06	4.41	5.04	6.57	8.66	11.20	13.32	15.24	15.84	15.08	387	11		
322	13.13	10.86	9.00	7.82	7.54	8.05	9.36	11.14	12.91	14.20	14.46	11.28	8.58	5.98	4.22	3.96	5.07	6.97	9.54	12.26	14.54	16.11	16.34	15.17	388	12		
323	12.88	10.26	8.38	7.33	7.40	8.14	9.77	11.52	14.60	14.56	12.94	10.26	7.33	5.11	3.87	4.05	5.64	7.81	10.61	13.20	15.47	16.54	16.21	14.70	389	13		
324	12.20	9.81	8.08	7.33	7.37	8.31	10.05	12.02	13.86	14.76	14.17	12.16	6.32	4.13	3.72	4.64	6.56	9.06	11.87	14.55	16.37	16.72	15.97	13.94	340	14		
325	11.34	7.71	7.36	7.70	9.02	10.97	12.94	14.40	14.70	13.44	10.64	7.77	5.58	4.12	4.16	5.63	7.85	10.36	13.16	15.34	16.56	16.48	12.72	10.27	341	16		
326	8.98	7.37	7.26	8.12	9.82	11.91	13.58	14.48	14.07	12.12	9.32	6.72	4.74	3.96	4.91	6.70	9.02	11.70	14.07	16.56	15.80	13.96	11.44	9.32	342	17		
327	7.80	7.24	7.44	8.72	10.57	12.55	14.00	14.24	13.24	10.72	8.06	5.93	4.58	4.74	6.03	10.34	12.88	15.05	16.23	16.28	14.89	12.63	10.30	8.54	343	18		
328	7.57	7.44	8.17	9.64	11.50	13.03	13.80	13.45	11.78	9.47	7.26	5.64	4.58	7.43	8.20	11.48	13.56	15.17	15.82	15.18	13.58	11.42	9.46	7.98	344	19		
329	7.36	7.62	8.30	10.02	11.60	12.67	13.00	13.14	10.36	6.54	5.59	5.07	6.77	8.43	10.27	12.17	13.90	14.96	14.86	13.76	12.00	10.22	8.66	7.73	345	20		
330	7.36	7.80	8.82	10.22	11.48	12.24	11.15	9.47	8.01	6.87	6.45	6.75	7.83	9.14	10.75	12.56	13.86	14.46	14.06	12.87	11.31	9.72	8.40	7.76	346	21		
331	7.73	8.27	10.54	11.48	12.02	11.81	10.84	9.56	8.46	7.76	8.48	8.71	9.47	10.70	12.04	13.16	13.78	13.79	13.14	10.54	10.98	9.76	8.76	8.24	347	23		
332	8.80	9.62	10.53	11.27	11.70	11.62	11.14	10.38	9.49	8.78	8.48	8.71	9.47	10.70	12.04	13.16	13.78	12.64	11.55	10.26	8.86	7.83	7.22	7.36	350	1		
333	8.58	9.36	10.22	11.00	11.51	11.74	11.57	10.96	10.14	9.44	9.04	9.10	9.74	10.90	12.24	13.37	13.38	12.44	11.22	9.78	8.36	7.04	6.26	6.15	351	2		
334	7.86	8.85	10.11	11.13	11.95	12.42	12.30	11.78	10.77	9.72	9.06	9.01	9.55	11.97	12.94	13.38	13.14	12.44	11.22	9.78	8.36	7.04	6.26	6.15	351	2		
335	6.82	8.20	9.97	11.56	12.90	13.50	13.36	12.36	10.92	8.84	8.68	9.14	10.18	11.57	12.76	13.36	13.22	12.46	11.00	9.17	7.18	5.75	4.90	4.92	352	3		
336	6.07	7.94	10.07	12.03	13.66	14.38	12.76	10.77	9.04	7.98	7.73	8.23	9.70	11.40	12.74	13.42	13.45	12.54	10.80	8.50	6.30	4.47	3.64	4.12	353	4		
337	5.82	8.20	10.84	14.95	15.70	14.97	13.05	10.60	8.64	7.50	7.36	8.16	9.80	11.80	13.38	14.33	14.26	13.00	10.50	7.72	5.17	3.42	2.93	4.16	354	6		
338	9.00	12.12	14.97	16.74	16.96	15.68	13.11	10.34	8.06	6.98	7.04	8.06	10.00	12.15	14.04	15.14	15.08	13.10	10.20	7.00	4.37	2.20	3.93	6.37	355	7		
339	9.77	13.27	16.13	17.72	17.51	15.78	12.57	9.74	7.27	6.14	6.36	7.56	9.86	12.72	14.77	15.81	12.64	9.26	5.91	3.10	1.55	1.93	4.00	7.06	356	8		
340	10.68	14.30	17.04	18.34	17.37	14.51	10.92	8.88	6.58	5.67	6.00	7.50	10.14	13.10	16.17	14.94	12.16	8.55	5.06	2.64	1.50	2.57	5.14	8.44	357	9		
341	11.93	15.00	17.66	18.34	17.37	14.51	10.92	8.88	6.58	5.67	6.00	7.50	10.14	13.10	16.17	14.94	12.16	8.55	5.06	2.64	1.50	2.57	5.14	8.44	357	9		
342	12.30	15.56	17.50	17.88	16.62	13.58	9.97	5.14	4.70	5.52	7.63	10.73	13.70	15.36	15.32	13.24	10.98	6.64	4.73	3.07	3.08	4.74	6.97	9.86	358	10		
343	13.01	15.80	17.38	15.95	12.86	9.53	6.72	5.22	4.90	5.87	8.03	10.96	13.30	14.68	14.83	13.24	10.55	7.68	5.43	4.33	4.63	5.97	8.02	10.57	359	11		
344	15.58	16.60	16.14	14.11	11.13	8.76	6.38	5.17	5.13	6.30	8.60	10.76	12.74	13.74	13.62	12.37	10.30	8.14	6.53	5.84	6.14	8.74	10.77	13.13	361	14		
345	14.96	15.71	15.12	13.32	10.86	8.44	6.53	5.48	5.27	6.00	7.78	9.85	11.62	12.84	13.10	12.28	10.74	9.22	7.33	7.28	7.93	9.16	10.97	13.12	362	15		
346	14.54	14.68	13.66	12.28	10.12	8.24	6.78	5.82	5.70	6.37	7.72	9.40	11.06	12.32	12.86	11.47	10.24	9.12	8.42	8.24	8.54	9.54	11.12	12.64	363	16		
347	13.57	13.57	12.88	11.44	9.87	8.24	6.74	5.77	5.52	6.12	7.27	10.64	12.10	13.01	13.12	12.46	11.26	10.02	9.06	8.58	8.66	9.44	10.68	11.96	364	17		
348	12.92	13.14	12.66	11.54	10.06	8.36	6.86	5.72	5.87	7.17	9.14	11.00	12.70	13.68	13.81	12.94	11.57	10.28	9.14	8.62	8.63	9.20	10.44	11.66	365	18		
349	12.53	12.92	12.58	11.64	9.77	8.12	5.95	5.37	5.62	7.06	9.15	11.26	13.23	14.30	14.32	13.36	11.78	10.34	9.17	8.44	8.24	8.62	9.76	11.04	366	19		
350	12.36	13.08	11.65	9.64	7.34	5.52	4.45	4.53	5.76	7.66	9.97	12.43	14.27	15.18	14.97	13.73	11.82	10.16	8.86	8.24	8.26	8.96	10.32	12.96	367	21		
351	13.58	13.16	11.26	8.91	6.66	4.96	4.33	4.86	6.36	8.55	11.00	13.44	15.21	15.84	15.17	13.56	11.44	9.66	8.38	7.80	7.97	9.00	10.56	11.70	368	22		
352	13.82	12.72	10.52	7.90	5.74	4.34	4.11	5.34	7.23	9.78	12.44	14.65	15.93	15.94	14.74	12.37	8.53	7.47	7.31	7.97	9.38	11.36	13.14	14.17	369	23		
353	14.00	12.18	9.43	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	...	370	2	
Sum	754.84	775.43	769.80	779.09	774.44	767.05	736.57	711.53	698.42	694.30	689.37	708.60	745.91	755.41	774.94	787.48	772.00	743.83	751.69	722.89	696.75	710.39	727.80	718.20	No.			
No.	73	74	73	73	73	73	72	72	72	72	72	73	73	72	72	73	72	72	72	73	72	72	73	73	72	No.		
																										729	116	
																											17773	82

FORMS FOR SHORT-  
BOMBAY—Summations and Means of

		0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>
SERIES G.	Sum (pp. 80-81)	<i>feet</i> 814.09	<i>feet</i> 807.47	<i>feet</i> 768.68	<i>feet</i> 713.90	<i>feet</i> 656.10	<i>feet</i> 612.63	<i>feet</i> 601.16	<i>feet</i> 628.55	<i>feet</i> 691.30	<i>feet</i> 776.04	<i>feet</i> 866.90	<i>feet</i> 936.49
	" (pp. 82-83)	885.27	889.48	864.56	818.97	767.77	731.08	714.25	726.49	762.13	811.55	860.03	891.16
	" (pp. 84-85)	943.28	948.07	928.91	889.06	838.11	788.76	748.57	726.62	726.18	746.27	773.80	793.58
	" (pp. 86-87)	937.59	911.22	852.77	773.80	692.27	628.64	595.34	600.56	643.42	708.54	779.87	831.26
	" (pp. 88-89)	814.95	774.00	708.99	629.27	572.10	540.36	545.06	587.93	658.53	742.96	822.19	880.63
	Sum (pp. 80-89)	4395.18	4330.24	4123.91	3825.00	3526.35	3301.47	3204.38	3270.15	3481.56	3785.36	4102.79	4333.12
No. of Obs. ...	370	370	370	369	369	369	369	369	369	369	369	369	
Means ...	11.879	11.703	11.146	10.366	9.557	8.947	8.684	8.862	9.435	10.258	11.119	11.743	
		0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>
SERIES K.	Sum (pp. 110-111)	<i>feet</i> 723.67	<i>feet</i> 769.74	<i>feet</i> 798.21	<i>feet</i> 798.65	<i>feet</i> 762.13	<i>feet</i> 720.27	<i>feet</i> 665.02	<i>feet</i> 622.68	<i>feet</i> 607.77	<i>feet</i> 627.02	<i>feet</i> 667.96	<i>feet</i> 758.10
	" (pp. 112-113)	570.44	551.64	568.43	618.93	680.36	756.30	830.55	870.19	879.69	860.79	823.73	771.49
	" (pp. 114-116)	769.73	738.35	721.10	680.42	642.70	620.46	605.70	645.71	699.54	763.58	829.96	887.21
	" (pp. 116-117)	617.23	654.72	698.28	764.60	807.84	825.07	812.56	780.34	723.32	704.58	688.28	691.72
	" (pp. 118-119)	670.87	618.09	583.62	568.88	596.11	647.59	715.26	782.36	840.22	865.32	889.31	881.87
	Sum (pp. 110-119)	3351.94	3332.54	3369.64	3431.48	3498.14	3569.69	3629.09	3701.28	3750.54	3821.29	3899.24	3990.39
No. of Obs. ...	370	370	370	369	369	369	369	369	369	369	369	369	
Means ...	9.059	9.007	9.107	9.299	9.480	9.674	9.835	10.031	10.164	10.356	10.567	10.814	
		0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>
SERIES L.	Sum (pp. 120-121)	<i>feet</i> 743.72	<i>feet</i> 718.78	<i>feet</i> 706.28	<i>feet</i> 675.00	<i>feet</i> 674.86	<i>feet</i> 696.17	<i>feet</i> 737.20	<i>feet</i> 796.85	<i>feet</i> 836.16	<i>feet</i> 874.43	<i>feet</i> 894.54	<i>feet</i> 893.37
	" (pp. 122-123)	765.35	780.58	802.43	818.37	826.64	805.16	775.77	738.35	698.73	664.17	643.97	655.10
	" (pp. 124-125)	758.50	725.12	691.31	657.84	633.01	627.22	644.31	681.17	745.69	791.37	841.75	875.48
	" (pp. 126-127)	683.96	676.63	701.39	742.61	805.54	846.95	879.65	888.81	886.43	825.84	769.07	711.23
	" (pp. 128-129)	770.71	802.26	798.49	773.28	734.99	690.39	625.86	587.29	575.29	601.92	644.62	709.32
	Sum (pp. 120-129)	3722.24	3703.37	3700.40	3667.10	3675.04	3665.89	3662.79	3692.47	3742.30	3757.73	3793.95	3844.50
No. of Obs. ...	370	370	370	368	370	369	368	369	370	369	368	369	
Means ...	10.060	10.009	10.001	9.965	9.933	9.935	9.953	10.007	10.114	10.184	10.310	10.419	
		0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>
SERIES M OR 2 MS.	Sum (pp. 190-191)	<i>feet</i> 789.10	<i>feet</i> 761.54	<i>feet</i> 724.19	<i>feet</i> 701.96	<i>feet</i> 720.79	<i>feet</i> 713.01	<i>feet</i> 694.59	<i>feet</i> 734.49	<i>feet</i> 733.71	<i>feet</i> 750.75	<i>feet</i> 771.98	<i>feet</i> 782.62
	" (pp. 192-193)	800.65	786.16	769.81	790.17	781.19	761.18	763.01	755.73	755.50	728.19	738.55	730.58
	" (pp. 194-195)	806.79	806.60	812.33	806.72	792.57	775.12	796.98	810.84	774.19	807.97	796.20	756.78
	" (pp. 196-197)	772.62	751.66	767.12	757.22	732.52	765.92	777.83	762.45	808.90	813.02	803.52	799.98
	" (pp. 198-199)	700.30	724.13	717.75	679.85	724.83	733.43	735.74	760.51	768.13	744.32	744.70	774.97
	Sum (pp. 190-199)	3869.46	3830.09	3791.20	3735.92	3751.90	3748.66	3768.15	3824.02	3840.43	3844.25	3854.95	3844.93
No. of Obs. ...	370	370	371	368	369	369	369	370	369	369	368	369	
Means ...	10.458	10.352	10.219	10.152	10.168	10.159	10.212	10.335	10.408	10.418	10.475	10.410	



PERIOD TIDES.

Series S, K, P, and  $\mu$  or 2 MS.

12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>		
<i>feet</i> 975.00	<i>feet</i> 976.40	<i>feet</i> 939.65	<i>feet</i> 873.58	<i>feet</i> 794.64	<i>feet</i> 719.55	<i>feet</i> 662.98	<i>feet</i> 634.76	<i>feet</i> 641.91	<i>feet</i> 681.53	<i>feet</i> 734.50	<i>feet</i> 786.21		18294.02
889.23	848.64	777.93	694.49	619.85	560.27	555.03	578.32	633.64	709.45	788.20	850.54		18237.33
793.05	769.34	722.70	666.49	620.53	596.14	604.10	640.99	705.26	783.60	857.11	913.59		18524.11
854.14	845.43	805.24	749.88	695.89	659.99	659.79	691.62	747.19	815.87	881.94	926.37		18288.63
912.48	915.78	892.52	849.63	799.14	754.68	726.45	720.34	734.38	761.88	791.71	808.45		17944.41
4423.90	4355.59	4138.04	3834.07	3530.05	3299.63	3208.35	3266.03	3462.38	3752.33	4053.46	4285.16		91288.50
369	369	369	369	369	369	369	369	369	369	369	369		
11.989	11.804	11.214	10.390	9.567	8.942	8.695	8.851	9.383	10.169	10.985	11.613		
<i>feet</i> 843.55	<i>feet</i> 919.92	<i>feet</i> 973.32	<i>feet</i> 986.21	<i>feet</i> 945.71	<i>feet</i> 887.75	<i>feet</i> 817.96	<i>feet</i> 736.38	<i>feet</i> 671.32	<i>feet</i> 637.88	<i>feet</i> 629.45	<i>feet</i> 666.34		18237.01
742.30	726.11	737.99	770.45	815.94	858.86	874.14	890.72	859.37	798.26	718.33	626.24		18210.25
914.17	945.43	935.76	904.46	859.81	810.17	766.70	727.42	726.27	733.12	751.09	768.07		18446.93
722.35	755.99	828.47	884.66	921.14	927.27	897.33	832.70	770.54	696.55	637.83	603.82		18247.19
858.64	828.38	792.71	765.16	776.25	780.49	792.29	804.99	795.42	798.40	770.62	724.27		18147.12
4081.01	4175.83	4268.25	4310.94	4318.85	4264.54	4148.42	3992.21	3822.92	3664.21	3507.32	3388.74		91288.50
369	369	369	369	369	369	369	368	369	370	369	369		
11.060	11.317	11.567	11.683	11.704	11.557	11.242	10.848	10.360	9.903	9.505	9.184		
<i>feet</i> 872.66	<i>feet</i> 838.37	<i>feet</i> 811.25	<i>feet</i> 758.37	<i>feet</i> 723.67	<i>feet</i> 703.57	<i>feet</i> 708.17	<i>feet</i> 707.86	<i>feet</i> 726.33	<i>feet</i> 742.58	<i>feet</i> 757.68	<i>feet</i> 748.31		18346.18
665.06	697.24	738.53	788.71	809.26	827.16	829.40	825.28	802.42	785.13	771.52	779.76		18294.09
902.52	882.87	863.18	836.11	813.57	781.59	762.62	753.46	770.31	765.53	770.30	765.89		18341.22
670.97	649.89	657.99	686.26	729.49	790.89	809.39	827.21	817.18	787.58	747.06	708.59		18300.32
779.56	859.60	887.44	907.40	898.25	864.39	817.12	769.86	732.94	720.86	717.84	737.01		18006.69
3890.77	3927.97	3958.10	3976.85	3974.24	3967.60	3926.70	3883.67	3849.18	3801.68	3764.40	3739.56		91288.50
370	369	369	369	369	369	369	369	369	369	369	369		
10.516	10.645	10.727	10.777	10.770	10.752	10.641	10.525	10.431	10.303	10.202	10.134		
<i>feet</i> 788.62	<i>feet</i> 754.95	<i>feet</i> 752.98	<i>feet</i> 774.99	<i>feet</i> 755.78	<i>feet</i> 779.99	<i>feet</i> 795.27	<i>feet</i> 793.64	<i>feet</i> 785.61	<i>feet</i> 820.56	<i>feet</i> 819.36	<i>feet</i> 793.54		18294.02
696.54	703.17	732.62	734.36	737.45	760.70	772.33	754.56	798.87	810.38	798.35	793.41		18253.46
762.42	753.69	737.14	694.92	718.68	717.71	707.38	744.73	779.56	769.99	790.25	806.92		18526.48
806.10	791.47	744.97	751.18	718.14	720.00	728.12	723.82	739.64	741.67	751.35	756.37		18285.59
777.25	756.28	772.11	764.56	786.66	770.57	787.08	782.80	747.09	739.75	729.35	706.79		17928.95
3830.93	3759.56	3739.82	3720.01	3716.71	3748.97	3790.18	3799.55	3850.77	3882.35	3888.66	3857.03		91288.50
370	368	369	369	369	369	370	368	369	370	369	368		
10.354	10.216	10.135	10.081	10.072	10.160	10.244	10.325	10.436	10.493	10.538	10.481		

SERIES S.

SERIES K.

SERIES P.

SERIES  $\mu$  OR 2 MS.

FORMS FOR SHORT.  
BOMBAY—Summations and Means of

	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	
SERIES M.	Sum (pp. 90-91)	<i>feet</i> 1020·87	<i>feet</i> 900·44	<i>feet</i> 752·96	<i>feet</i> 600·02	<i>feet</i> 497·60	<i>feet</i> 465·12	<i>feet</i> 502·71	<i>feet</i> 600·78	<i>feet</i> 765·87	<i>feet</i> 901·35	<i>feet</i> 1016·37	<i>feet</i> 1068·59
	„ (pp. 92-93)	1024·63	914·06	744·98	586·08	476·79	447·90	489·12	604·61	755·24	907·73	1036·36	1107·56
	„ (pp. 94-95)	1027·69	892·75	725·74	583·23	502·54	476·45	523·48	615·47	754·55	913·26	1051·87	1066·39
	„ (pp. 96-97)	1032·54	910·43	760·26	608·18	501·65	473·80	511·80	621·28	762·12	907·49	1021·76	1072·60
	„ (pp. 98-99)	1014·95	885·30	738·49	593·11	478·97	448·53	593·53	595·16	750·39	893·87	1015·57	1078·27
Sum (pp. 90-99)	5120·68	4502·98	3722·43	2970·62	2457·55	2311·80	2530·64	3037·30	3788·17	4523·70	5141·93	5393·41	
No. of Obs. ...	369	369	371	370	369	368	369	369	372	368	369	369	
Means ...	13·877	12·203	10·034	8·029	6·660	6·282	6·858	8·231	10·183	12·293	13·935	14·616	
SERIES O.		0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>
	Sum (pp. 100-101)	<i>feet</i> 745·01	<i>feet</i> 691·67	<i>feet</i> 695·23	<i>feet</i> 687·13	<i>feet</i> 680·95	<i>feet</i> 730·71	<i>feet</i> 722·78	<i>feet</i> 789·33	<i>feet</i> 788·74	<i>feet</i> 803·03	<i>feet</i> 774·59	<i>feet</i> 813·78
	„ (pp. 102-103)	744·58	744·14	745·38	733·90	753·80	700·15	747·98	708·24	728·23	716·84	751·36	754·60
	„ (pp. 104-105)	750·62	738·47	702·83	693·10	664·46	703·65	700·15	741·62	756·99	779·83	810·97	810·04
	„ (pp. 106-107)	716·99	703·85	701·16	715·55	748·94	769·12	784·15	788·73	757·19	780·21	739·58	752·49
	„ (pp. 108-109)	755·04	734·74	751·60	689·56	708·52	694·75	703·48	684·89	727·13	728·87	756·86	776·57
	Sum (pp. 100-109)	3712·24	3612·87	3596·20	3519·24	3556·67	3598·38	3658·54	3712·81	3758·28	3808·78	3833·36	3907·48
No. of Obs. ...	371	370	371	368	368	369	370	370	368	369	368	370	
Means ...	10·006	9·765	9·693	9·563	9·665	9·752	9·888	10·035	10·213	10·322	10·417	10·561	
SERIES J.		0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>
	Sum (pp. 130-131)	<i>feet</i> 762·81	<i>feet</i> 771·19	<i>feet</i> 763·32	<i>feet</i> 757·94	<i>feet</i> 768·36	<i>feet</i> 742·42	<i>feet</i> 745·02	<i>feet</i> 746·89	<i>feet</i> 740·06	<i>feet</i> 729·58	<i>feet</i> 732·71	<i>feet</i> 749·20
	„ (pp. 132-133)	755·67	750·24	740·17	758·79	737·14	736·63	754·33	742·58	748·16	775·97	758·38	779·80
	„ (pp. 134-135)	769·97	761·46	759·40	765·29	765·97	782·88	770·07	774·24	798·18	787·97	788·89	797·91
	„ (pp. 136-137)	770·20	754·83	755·15	768·99	750·37	757·72	766·45	767·85	763·27	751·63	766·70	740·98
	„ (pp. 138-139)	751·35	757·98	769·15	743·83	753·45	772·13	754·10	763·62	765·09	760·54	763·39	773·08
	Sum (pp. 130-139)	3810·00	3795·70	3787·19	3794·84	3775·29	3791·78	3789·97	3795·18	3814·76	3805·69	3809·97	3840·97
No. of Obs. ...	370	371	370	371	370	371	370	370	371	370	370	372	
Means ...	10·297	10·231	10·236	10·229	10·203	10·220	10·243	10·257	10·282	10·286	10·297	10·325	
SERIES Q.		0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>
	Sum (pp. 140-141)	<i>feet</i> 747·98	<i>feet</i> 740·35	<i>feet</i> 747·10	<i>feet</i> 742·53	<i>feet</i> 763·46	<i>feet</i> 739·17	<i>feet</i> 764·06	<i>feet</i> 778·00	<i>feet</i> 780·85	<i>feet</i> 765·81	<i>feet</i> 754·39	<i>feet</i> 746·88
	„ (pp. 142-143)	769·09	740·33	773·60	721·18	740·99	745·29	768·76	735·74	742·12	749·25	764·15	771·41
	„ (pp. 144-145)	764·31	787·43	750·82	777·22	768·42	755·54	742·48	728·93	770·21	759·73	787·09	779·64
	„ (pp. 146-147)	750·39	773·17	758·51	768·46	732·67	767·55	771·09	785·69	755·65	758·63	752·33	740·08
	„ (pp. 148-149)	750·90	757·95	743·99	755·91	761·36	782·39	766·39	756·46	743·89	757·48	757·41	797·17
	Sum (pp. 140-149)	3782·67	3799·23	3774·02	3765·30	3766·90	3789·94	3812·78	3784·82	3792·72	3790·90	3815·37	3835·18
No. of Obs. ...	369	371	369	370	370	371	372	370	371	369	370	370	
Means ...	10·251	10·241	10·228	10·176	10·181	10·215	10·249	10·219	10·223	10·273	10·312	10·365	

PERIOD TIDES.

Series M, O, J, and Q.

12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>		
<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>		
1045'66	921'58	748'92	586'33	476'86	459'09	492'81	595'88	744'51	912'16	1021'90	1075'13	18173'51	SERIES M.
1038'74	937'98	779'46	599'48	499'89	451'76	494'27	610'92	770'90	916'80	1048'80	1093'78	18357'84	
1021'39	899'21	742'68	599'35	494'34	482'75	533'46	650'77	799'94	940'31	1041'05	1070'88	18409'55	
1060'31	924'04	744'15	591'06	495'43	460'89	511'58	610'72	763'36	946'14	1054'15	1072'91	18418'65	
1033'88	910'94	761'64	592'07	476'85	437'85	478'26	584'39	738'21	878'16	989'11	1051'45	17928'95	
5219'98	4593'75	3776'85	2968'29	2443'37	2292'34	2510'38	3052'68	3816'92	4593'57	5155'01	5364'15	91288'50	
370	369	371	368	368	369	369	368	369	369	368	369		
14'108	12'449	10'180	8'066	6'640	6'212	6'803	8'295	10'344	12'449	14'008	14'537		
<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>		
745'79	764'28	763'48	760'84	779'48	782'19	832'47	816'07	838'97	801'49	803'77	738'84	18350'62	SERIES O.
777'61	804'95	814'93	824'98	812'14	820'54	774'60	795'55	779'96	755'00	757'02	755'77	18302'25	
821'23	808'73	788'43	770'37	769'74	758'91	793'22	799'07	798'23	803'96	779'79	784'21	18328'62	
745'90	763'61	772'47	786'92	811'51	832'13	840'80	821'35	770'38	754'72	741'66	709'07	18308'48	
787'04	780'12	786'89	786'56	785'66	782'46	760'00	765'24	764'66	764'68	766'75	756'46	17998'53	
3877'57	3921'69	3926'20	3929'67	3958'53	3976'23	4001'09	3997'28	3952'20	3879'85	3848'99	3744'35	91288'50	
368	370	370	368	369	368	370	370	369	367	370	368		
10'537	10'599	10'611	10'678	10'728	10'805	10'814	10'803	10'711	10'572	10'403	10'175		
<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>		
745'64	742'01	768'91	774'83	746'57	777'49	768'34	760'60	755'80	738'47	764'47	741'40	18094'03	SERIES J.
783'39	780'79	779'34	787'09	769'15	771'73	768'24	757'15	752'14	766'26	750'58	757'83	18261'45	
776'78	778'93	784'36	757'58	770'02	765'98	745'04	775'30	744'58	773'91	780'60	763'40	18538'71	
718'34	753'48	742'69	751'19	770'36	759'39	773'99	786'32	780'88	788'02	776'86	766'77	18302'43	
780'94	777'30	769'74	790'39	768'99	774'15	782'99	766'54	767'24	758'51	735'08	753'06	18352'64	
3825'09	3832'51	3845'04	3861'08	3825'09	3848'74	3838'60	3845'91	3800'64	3825'17	3807'59	3782'46	91549'26	
370	370	371	372	368	370	370	371	368	370	370	369		
10'338	10'358	10'364	10'379	10'394	10'402	10'375	10'366	10'328	10'338	10'291	10'251		
<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>	<i>feet</i>		
750'22	787'54	746'59	773'31	769'37	783'82	751'20	779'06	757'21	777'05	774'22	732'98	18253'15	SERIES Q.
788'42	756'35	763'27	769'01	749'10	775'62	761'21	780'98	756'62	792'66	743'04	765'72	18223'91	
772'88	772'18	780'18	771'08	776'86	776'52	774'13	790'96	779'33	775'94	776'29	792'73	18510'90	
780'04	756'52	779'19	758'40	775'27	752'88	772'08	740'38	751'69	766'59	746'32	748'12	18241'70	
756'01	759'53	781'47	777'74	790'50	749'28	770'69	763'27	776'05	744'37	749'23	770'16	18319'60	
3847'57	3832'12	3850'70	3849'54	3861'10	3838'12	3829'31	3854'65	3820'90	3856'61	3789'10	3809'71	91549'26	
372	370	372	371	370	369	368	370	368	372	369	372		
10'343	10'357	10'351	10'376	10'435	10'401	10'406	10'418	10'383	10'367	10'269	10'241		

FORMS FOR SHORT-  
BOMBAY—Summations and Means of

		0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>
SERIES L.	Sum (pp. 150-151)	<i>feet</i> 767'45	<i>feet</i> 775'49	<i>feet</i> 790'38	<i>feet</i> 795'81	<i>feet</i> 775'44	<i>feet</i> 765'23	<i>feet</i> 765'55	<i>feet</i> 762'71	<i>feet</i> 764'99	<i>feet</i> 758'26	<i>feet</i> 754'06	<i>feet</i> 771'84
	„ (pp. 152-153)	781'94	769'25	781'62	775'65	772'92	774'30	748'58	741'30	772'33	772'27	753'41	752'06
	„ (pp. 154-155)	744'20	733'19	711'16	731'34	740'36	768'40	785'65	776'33	768'16	753'67	754'56	763'77
	„ (pp. 156-157)	757'40	783'38	817'68	801'03	787'31	777'56	766'91	785'93	767'18	752'00	747'92	752'45
	„ (pp. 158-159)	645'19	639'71	621'95	643'14	641'99	632'37	648'86	660'85	672'34	672'17	669'20	657'44
	Sum (pp. 150-159)	3696'18	3701'02	3722'79	3746'97	3718'02	3717'86	3715'55	3727'12	3745'00	3708'37	3679'15	3697'56
No. of Obs. ...	369	359	357	360	358	358	350	359	359	359	358	358	
Means ...	10'296	10'309	10'428	10'408	10'386	10'385	10'350	10'382	10'432	10'330	10'277	10'328	
SERIES N.	Sum (pp. 160-161)	<i>feet</i> 783'91	<i>feet</i> 741'93	<i>feet</i> 710'19	<i>feet</i> 709'60	<i>feet</i> 684'10	<i>feet</i> 693'37	<i>feet</i> 732'72	<i>feet</i> 748'53	<i>feet</i> 791'19	<i>feet</i> 830'15	<i>feet</i> 840'57	<i>feet</i> 818'68
	„ (pp. 162-163)	853'32	826'32	788'18	704'52	672'72	654'78	687'53	715'07	755'90	811'69	818'81	860'01
	„ (pp. 164-165)	824'98	806'89	800'14	756'21	712'03	703'03	690'51	703'39	737'45	805'95	824'51	839'99
	„ (pp. 166-167)	786'84	778'90	729'00	690'22	695'83	719'77	727'18	755'69	801'68	796'19	800'35	786'08
	„ (pp. 168-169)	744'70	732'90	684'61	651'26	620'19	564'80	561'73	592'35	640'28	659'68	694'11	747'68
	Sum (pp. 160-169)	3993'75	3886'94	3712'12	3511'81	3384'87	3335'75	3399'67	3515'03	3726'50	3903'66	4008'35	4052'44
No. of Obs. ...	357	359	360	358	358	359	360	357	359	360	358	358	
Means ...	11'187	10'827	10'311	9'810	9'455	9'292	9'444	9'846	10'380	10'844	11'197	11'320	
SERIES A.	Sum (pp. 170-171)	<i>feet</i> 805'33	<i>feet</i> 779'93	<i>feet</i> 769'55	<i>feet</i> 794'05	<i>feet</i> 770'85	<i>feet</i> 773'79	<i>feet</i> 754'69	<i>feet</i> 739'87	<i>feet</i> 740'77	<i>feet</i> 772'47	<i>feet</i> 804'96	<i>feet</i> 812'35
	„ (pp. 172-173)	729'58	750'10	763'88	784'78	751'80	743'68	751'85	738'00	744'66	730'62	713'40	709'54
	„ (pp. 174-175)	777'01	757'60	745'75	747'40	779'76	804'32	832'18	826'31	812'11	795'82	812'94	774'66
	„ (pp. 176-177)	767'08	766'50	757'45	761'02	729'94	707'88	695'14	698'96	725'36	744'78	791'32	778'57
	„ (pp. 178-179)	543'81	523'35	533'19	549'04	559'76	593'98	604'87	598'03	586'54	579'28	561'87	556'56
	Sum (pp. 170-179)	3622'81	3577'48	3569'82	3636'29	3592'11	3623'65	3638'73	3601'17	3609'44	3622'97	3684'49	3631'68
No. of Obs. ...	353	349	348	353	350	350	353	349	348	350	353	350	
Means ...	10'263	10'251	10'258	10'301	10'263	10'353	10'308	10'319	10'372	10'351	10'438	10'376	
SERIES P.	Sum (pp. 180-181)	<i>feet</i> 791'28	<i>feet</i> 776'61	<i>feet</i> 818'85	<i>feet</i> 785'56	<i>feet</i> 727'80	<i>feet</i> 661'77	<i>feet</i> 670'27	<i>feet</i> 719'60	<i>feet</i> 768'73	<i>feet</i> 790'99	<i>feet</i> 763'82	<i>feet</i> 794'45
	„ (pp. 182-183)	682'71	719'43	684'25	727'93	818'70	880'24	875'62	789'39	754'54	789'51	723'54	689'66
	„ (pp. 184-185)	789'41	809'09	802'44	758'56	708'49	678'49	729'56	784'69	822'44	777'45	795'34	865'76
	„ (pp. 186-187)	840'73	786'15	738'93	740'84	775'03	753'94	688'49	681'39	736'85	783'00	812'76	757'39
	„ (pp. 188-189)	479'15	535'61	575'11	611'05	577'88	584'12	613'64	623'08	557'65	499'96	483'21	522'49
	Sum (pp. 180-189)	3583'28	3626'89	3619'58	3623'94	3607'90	3558'56	3577'58	3598'15	3640'21	3640'91	3578'67	3629'75
No. of Obs. ...	346	349	352	353	351	346	350	352	353	350	346	351	
Means ...	10'356	10'393	10'283	10'266	10'279	10'285	10'222	10'222	10'312	10'403	10'343	10'341	

PERIOD TIDES.

Series L, N, λ, and ν.

12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>			
<i>feet</i> 800.60	<i>feet</i> 796.45	<i>feet</i> 810.02	<i>feet</i> 790.80	<i>feet</i> 763.78	<i>feet</i> 766.14	<i>feet</i> 754.45	<i>feet</i> 725.41	<i>feet</i> 726.65	<i>feet</i> 726.90	<i>feet</i> 711.50	<i>feet</i> 720.83	18340.74	SERIES L.	
743.78	734.36	748.64	748.56	742.33	743.79	738.09	753.74	764.34	776.73	786.00	804.00	18279.99		
754.36	749.89	752.91	773.56	778.27	798.17	796.67	805.67	792.94	781.54	764.43	740.97	18320.17		
770.82	788.49	779.87	783.29	777.60	751.13	745.10	732.96	732.43	713.15	722.45	728.20	18322.24		
632.31	613.85	619.54	606.11	617.49	615.29	619.11	634.50	650.24	654.79	670.21	654.81	15393.46		
3701.87.	3683.04	3710.98	3702.32	3679.47	3674.52	3653.42	3652.28	3666.60	3653.11	3654.59	3648.81	88656.60		
360	358	358	358	357	358	358	357	357	359	358	357			
10.283	10.288	10.366	10.342	10.307	10.264	10.205	10.230	10.271	10.176	10.208	10.221			
<i>feet</i> 775.35	<i>feet</i> 756.44	<i>feet</i> 712.26	<i>feet</i> 701.39	<i>feet</i> 704.93	<i>feet</i> 703.75	<i>feet</i> 731.39	<i>feet</i> 771.67	<i>feet</i> 803.35	<i>feet</i> 819.91	<i>feet</i> 834.91	<i>feet</i> 843.62	18243.91		SERIES N.
850.38	810.82	764.66	701.03	659.25	636.86	667.19	709.45	750.90	796.40	836.62	857.46	18219.87		
848.43	833.50	795.99	755.48	729.70	709.59	693.46	709.14	727.67	786.15	841.37	859.94	18493.50		
802.02	759.83	726.80	716.36	697.70	704.38	747.63	774.14	795.36	805.31	820.31	793.00	18210.57		
733.94	700.42	653.34	615.20	575.45	545.14	543.44	561.20	593.16	651.90	698.64	722.63	15488.75		
4010.12	3861.01	3653.05	3487.46	3367.03	3299.72	3383.11	3525.60	3670.44	3859.67	4031.85	4076.65	88656.60		
359	359	357	358	359	356	358	359	356	356	359	359			
11.170	10.755	10.233	9.742	9.379	9.269	9.450	9.821	10.310	10.842	11.231	11.356			
<i>feet</i> 805.13	<i>feet</i> 785.61	<i>feet</i> 772.60	<i>feet</i> 783.82	<i>feet</i> 756.64	<i>feet</i> 762.68	<i>feet</i> 725.23	<i>feet</i> 700.59	<i>feet</i> 697.14	<i>feet</i> 723.64	<i>feet</i> 761.76	<i>feet</i> 768.59	18362.04	SERIES λ.	
725.28	764.05	763.26	798.01	779.57	774.97	780.37	784.90	788.60	766.78	739.39	724.67	18101.74		
776.02	756.57	726.13	717.66	738.72	772.17	775.09	779.31	769.78	767.43	787.13	778.31	18610.18		
782.39	787.15	787.51	788.20	771.88	750.72	725.21	723.00	753.41	751.06	783.80	765.56	18093.89		
552.06	548.36	528.05	539.74	551.71	581.57	590.40	590.02	572.95	556.94	531.93	527.69	13461.70		
3640.88	3641.74	3577.55	3627.43	3598.52	3642.11	3596.30	3577.82	3581.88	3565.85	3604.01	3564.82	86629.55		
350	352	347	349	349	352	349	348	349	349	349	349			
10.403	10.346	10.310	10.394	10.311	10.347	10.305	10.281	10.263	10.217	10.327	10.214			
<i>feet</i> 836.44	<i>feet</i> 836.42	<i>feet</i> 742.44	<i>feet</i> 700.41	<i>feet</i> 697.55	<i>feet</i> 731.65	<i>feet</i> 723.79	<i>feet</i> 689.67	<i>feet</i> 709.32	<i>feet</i> 706.03	<i>feet</i> 840.00	<i>feet</i> 846.71	18220.16		SERIES ν.
645.90	671.73	761.21	706.88	832.07	799.12	842.15	836.50	809.86	697.59	653.43	660.90	18142.86		
873.47	817.80	729.26	703.49	739.23	731.48	717.37	713.51	763.46	867.42	872.08	842.15	18692.44		
765.96	826.76	826.65	784.56	712.35	707.19	739.00	748.65	744.34	712.16	751.51	793.05	18207.68		
560.63	516.09	530.96	559.39	652.61	659.66	582.64	559.17	546.27	558.67	512.06	465.31	13366.41		
3682.40	3668.80	3590.52	3544.73	3633.81	3629.10	3604.95	3547.50	3573.25	3631.87	3629.08	3608.12	86629.55		
353	352	349	344	352	351	352	346	347	351	352	351			
10.432	10.423	10.318	10.304	10.323	10.339	10.241	10.253	10.298	10.347	10.310	10.280			

FORMS FOR SHORT.  
B O M B A Y—Summations and Means of

	0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>	
Series R.	Sum (pp. 200-201)	<i>feet</i> 767.64	<i>feet</i> 795.61	<i>feet</i> 794.06	<i>feet</i> 763.88	<i>feet</i> 717.33	<i>feet</i> 666.62	<i>feet</i> 622.12	<i>feet</i> 613.15	<i>feet</i> 634.65	<i>feet</i> 688.92	<i>feet</i> 766.40	<i>feet</i> 851.29
	„ (pp. 202-203)	677.15	754.91	822.66	856.51	861.67	863.83	828.80	782.65	743.51	724.16	729.96	758.66
	„ (pp. 204-205)	601.59	636.73	714.01	790.22	862.58	919.06	948.75	951.26	927.15	882.49	830.24	782.67
	„ (pp. 206-207)	688.15	651.82	640.93	664.78	718.87	791.73	869.71	931.75	962.30	949.12	893.06	800.04
	„ (pp. 208-209)	927.90	896.08	848.59	799.21	758.63	736.69	735.56	754.53	783.47	812.73	818.07	814.05
	Sum (pp. 200-209)	3662.43	3735.15	3820.25	3874.60	3919.08	3977.93	4004.94	4033.34	4051.08	4057.42	4037.73	4006.71
No. of Obs. ...	369	369	370	369	369	370	369	370	370	370	369	369	
Means ...	9.925	10.122	10.325	10.500	10.621	10.751	10.853	10.901	10.949	10.966	10.942	10.858	
Do. of 1884 ...	9.950	10.143	10.358	10.528	10.633	10.727	10.800	10.836	10.872	10.897	10.874	10.811	
Do. for 1884-85	9.938	10.133	10.342	10.514	10.627	10.739	10.827	10.869	10.911	10.932	10.908	10.835	
Series T.	Sum (pp. 210-211)	<i>feet</i> 802.24	<i>feet</i> 763.25	<i>feet</i> 708.83	<i>feet</i> 654.09	<i>feet</i> 616.55	<i>feet</i> 615.05	<i>feet</i> 642.43	<i>feet</i> 706.60	<i>feet</i> 789.02	<i>feet</i> 870.63	<i>feet</i> 931.53	<i>feet</i> 961.30
	„ (pp. 212-213)	807.59	758.35	724.77	714.54	731.84	769.22	815.55	855.21	872.02	873.99	809.99	742.41
	„ (pp. 214-215)	761.15	735.39	730.29	748.21	761.45	777.21	778.66	762.11	727.00	681.79	643.16	622.47
	„ (pp. 216-217)	684.65	730.53	775.97	806.80	819.31	808.65	778.61	753.03	708.68	690.76	701.45	733.96
	„ (pp. 218-219)	858.63	897.93	898.18	885.36	852.88	808.82	767.26	739.54	727.51	736.31	757.27	786.73
	Sum (pp. 210-219)	3914.26	3885.45	3838.04	3809.00	3782.03	3778.95	3782.51	3816.49	3824.23	3853.48	3843.40	3846.96
No. of Obs. ...	369	370	369	370	369	370	369	370	369	370	369	370	
Means ...	10.608	10.501	10.401	10.295	10.249	10.213	10.251	10.315	10.364	10.415	10.416	10.307	
Do. of 1884 ...	10.671	10.656	10.536	10.386	10.252	10.152	10.120	10.121	10.168	10.233	10.307	10.381	
Do. for 1884-85	10.640	10.579	10.460	10.341	10.251	10.183	10.186	10.218	10.266	10.324	10.362	10.389	
Series M.	Sum (pp. 220-221)	<i>feet</i> 780.48	<i>feet</i> 791.55	<i>feet</i> 784.03	<i>feet</i> 776.19	<i>feet</i> 756.55	<i>feet</i> 739.51	<i>feet</i> 739.98	<i>feet</i> 754.28	<i>feet</i> 739.34	<i>feet</i> 740.07	<i>feet</i> 775.30	<i>feet</i> 781.18
	„ (pp. 222-223)	764.71	758.18	744.83	750.08	753.14	774.85	803.07	771.79	759.95	735.54	733.69	736.75
	„ (pp. 224-225)	789.28	790.73	799.61	767.73	755.98	752.44	760.73	767.67	757.55	770.07	783.94	803.37
	„ (pp. 226-227)	759.72	757.68	747.32	738.03	754.25	781.97	793.89	796.22	787.52	782.28	749.69	748.59
	„ (pp. 228-229)	756.35	744.88	742.16	734.32	727.44	754.02	737.26	730.49	722.51	731.22	745.07	766.70
	Sum (pp. 220-229)	3850.54	3843.02	3817.95	3766.35	3747.36	3802.79	3834.93	3820.45	3766.87	3759.18	3787.69	3836.59
No. of Obs. ...	369	368	370	370	368	370	370	369	368	370	370	368	
Means ...	10.435	10.443	10.319	10.179	10.183	10.278	10.365	10.354	10.236	10.160	10.237	10.426	
Series 2 S.M.	Sum (pp. 230-231)	<i>feet</i> 755.17	<i>feet</i> 770.71	<i>feet</i> 736.02	<i>feet</i> 718.71	<i>feet</i> 720.68	<i>feet</i> 780.55	<i>feet</i> 717.69	<i>feet</i> 776.94	<i>feet</i> 735.19	<i>feet</i> 762.29	<i>feet</i> 734.14	<i>feet</i> 754.02
	„ (pp. 232-233)	794.81	752.76	805.37	752.80	797.38	743.69	776.69	756.27	749.30	750.90	750.64	762.48
	„ (pp. 234-235)	728.84	779.36	729.60	779.67	753.65	788.98	767.05	776.39	782.09	771.24	802.76	750.64
	„ (pp. 236-237)	788.17	747.44	781.64	762.08	763.36	764.37	762.95	782.60	746.24	794.36	732.62	794.82
	„ (pp. 238-239)	738.82	775.73	774.76	744.42	750.88	742.91	762.09	706.44	754.79	703.22	756.55	713.75
	Sum (pp. 230-239)	3805.81	3826.00	3827.39	3817.68	3785.95	3820.50	3786.47	3798.64	3767.61	3782.01	3776.71	3775.71
No. of Obs. ...	369	370	370	369	368	370	370	370	370	370	370	368	
Means ...	10.314	10.341	10.344	10.346	10.388	10.326	10.234	10.267	10.183	10.222	10.207	10.260	

PERIOD TIDES.

Series R, T, MS, and 2 SM.

12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>		
<i>feet</i> 923.85	<i>feet</i> 967.47	<i>feet</i> 976.31	<i>feet</i> 947.28	<i>feet</i> 888.49	<i>feet</i> 804.19	<i>feet</i> 735.85	<i>feet</i> 673.17	<i>feet</i> 640.65	<i>feet</i> 639.83	<i>feet</i> 668.92	<i>feet</i> 717.19		18264.87
804.03	851.91	887.95	899.21	857.45	815.32	734.97	653.54	588.64	554.03	559.85	600.82		18212.19
747.86	730.60	727.81	753.44	779.08	795.86	791.62	763.77	715.38	659.03	613.21	590.03		18514.64
714.63	622.52	583.60	572.26	606.03	672.81	753.21	824.17	866.86	867.76	832.87	773.14		18252.12
770.54	702.29	628.88	561.53	532.20	542.50	589.53	661.82	747.15	827.61	878.34	916.78		18044.68
3960.91	3874.79	3804.55	3733.72	3663.25	3630.68	3605.18	3576.47	3558.88	3548.26	3553.19	3597.96		91288.50
370	369	369	369	368	368	369	369	369	369	368	369		
10.705	10.501	10.310	10.118	9.954	9.866	9.770	9.692	9.645	9.616	9.655	9.751		
10.663	10.449	10.250	10.051	9.889	9.757	9.668	9.592	9.534	9.525	9.585	9.743		
10.684	10.475	10.280	10.085	9.922	9.812	9.719	9.642	9.590	9.571	9.620	9.747		
<i>feet</i> 956.40	<i>feet</i> 914.92	<i>feet</i> 859.06	<i>feet</i> 778.27	<i>feet</i> 714.90	<i>feet</i> 669.06	<i>feet</i> 650.91	<i>feet</i> 663.96	<i>feet</i> 701.29	<i>feet</i> 750.76	<i>feet</i> 792.18	<i>feet</i> 809.21		18322.53
670.45	610.56	579.07	580.59	614.75	673.79	753.76	814.62	864.55	887.62	882.68	867.30		18275.22
636.07	656.72	710.32	778.72	844.03	893.18	922.45	929.21	914.02	883.88	841.93	796.72		18536.14
780.80	830.13	870.70	888.13	889.11	848.73	799.61	741.31	687.48	653.13	653.86	656.28		18291.67
788.51	779.34	747.95	690.64	636.79	591.00	565.80	566.93	600.26	659.01	727.31	792.98		17862.94
3832.23	3791.67	3767.10	3716.35	3699.58	3675.76	3692.53	3716.03	3767.60	3834.40	3897.96	3922.49		91288.50
370	369	370	368	369	368	369	368	368	368	368	369		
10.357	10.276	10.181	10.099	10.026	9.988	10.007	10.008	10.238	10.420	10.564	10.630		
10.427	10.307	10.320	10.152	9.980	9.886	9.834	9.887	10.023	10.218	10.433	10.594		
10.392	10.337	10.251	10.126	10.008	9.937	9.921	9.993	10.131	10.319	10.499	10.612		
<i>feet</i> 798.51	<i>feet</i> 806.78	<i>feet</i> 798.63	<i>feet</i> 775.47	<i>feet</i> 745.83	<i>feet</i> 740.42	<i>feet</i> 725.86	<i>feet</i> 696.82	<i>feet</i> 707.13	<i>feet</i> 696.37	<i>feet</i> 715.24	<i>feet</i> 738.79		18104.31
736.99	744.06	727.51	727.84	759.37	771.30	790.55	809.98	806.69	784.09	782.49	789.12		18316.57
818.22	838.19	819.00	799.31	788.61	763.24	756.48	739.28	735.82	722.48	732.46	761.19		18573.38
735.87	713.44	705.92	705.90	736.03	763.99	790.44	825.82	866.03	794.53	793.70	781.00		18349.83
798.98	792.90	786.05	787.74	770.67	757.51	753.07	743.23	711.19	699.60	721.89	729.07		17944.41
3888.57	3895.37	3837.11	3796.26	3800.51	3796.46	3816.40	3815.13	3766.86	3697.16	3745.78	3799.17		91288.50
369	370	369	369	371	369	368	369	371	367	368	369		
10.538	10.528	10.399	10.288	10.244	10.289	10.371	10.339	10.153	10.074	10.179	10.296		
<i>feet</i> 764.70	<i>feet</i> 748.80	<i>feet</i> 774.19	<i>feet</i> 745.98	<i>feet</i> 794.17	<i>feet</i> 734.89	<i>feet</i> 797.60	<i>feet</i> 751.32	<i>feet</i> 775.74	<i>feet</i> 736.02	<i>feet</i> 763.71	<i>feet</i> 764.28		18173.51
728.26	781.55	735.82	783.90	734.45	788.40	759.96	766.66	757.82	784.66	788.57	754.70		18357.84
803.99	738.72	804.83	752.32	787.00	765.76	757.79	759.06	750.82	772.23	730.95	775.81		18409.55
750.16	797.48	759.05	777.70	772.73	754.30	782.03	750.70	778.21	729.88	785.84	728.36		18387.09
745.27	744.18	750.76	748.91	747.20	771.79	735.30	783.92	726.70	780.74	722.69	778.69		17960.51
3792.38	3810.73	3824.65	3808.81	3835.55	3815.14	3832.68	3811.66	3789.29	3803.53	3791.76	3801.84		91288.50
369	370	370	368	369	368	369	369	367	369	368	369		
10.277	10.299	10.337	10.350	10.394	10.367	10.387	10.330	10.325	10.308	10.304	10.303		

SERIES R.

SERIES T.

SERIES MS.

SERIES 2 SM.

FORMS FOR SHORT.  
BOMBAY—Summations and Means of

		0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>
SERIES 2N.	Sum (pp. 240-241)	<i>feet</i> 747'71	<i>feet</i> 694'17	<i>feet</i> 689'93	<i>feet</i> 694'26	<i>feet</i> 690'35	<i>feet</i> 720'01	<i>feet</i> 732'20	<i>feet</i> 740'10	<i>feet</i> 786'83	<i>feet</i> 800'63	<i>feet</i> 807'04	<i>feet</i> 784'97
	" (pp. 242-243)	753'59	728'67	742'32	746'48	732'84	732'41	725'03	731'56	728'62	734'37	716'89	741'07
	" (pp. 244-245)	771'66	787'20	751'76	713'79	707'19	675'03	701'71	723'74	725'52	770'91	772'60	818'81
	" (pp. 246-247)	725'25	709'21	714'11	715'11	718'09	748'25	757'39	774'00	777'74	745'74	771'49	753'66
	" (pp. 248-249)	771'43	769'90	752'24	727'62	704'70	702'99	694'10	670'79	681'10	706'39	705'04	734'50
Sum (pp. 240-249)	3770'64	3689'15	3650'36	3597'26	3553'17	3578'69	3610'43	3640'19	3699'81	3758'04	3773'06	3833'01	
No. of Obs. ...	370	369	371	371	368	369	370	369	369	369	368	369	
Means ...	10'191	9'998	9'839	9'696	9'655	9'698	9'758	9'865	10'027	10'184	10'253	10'388	
		0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>
SERIES M <sub>2</sub> N.	Sum (pp. 250-251)	<i>feet</i> 744'07	<i>feet</i> 765'35	<i>feet</i> 682'18	<i>feet</i> 726'53	<i>feet</i> 707'72	<i>feet</i> 711'87	<i>feet</i> 782'04	<i>feet</i> 755'36	<i>feet</i> 851'08	<i>feet</i> 818'28	<i>feet</i> 852'20	<i>feet</i> 849'37
	" (pp. 252-253)	723'70	742'55	743'25	828'93	802'15	869'38	821'74	798'11	771'06	676'94	696'88	642'33
	" (pp. 254-255)	850'16	794'49	834'07	773'34	740'77	738'25	669'89	729'18	702'16	784'95	833'44	798'44
	" (pp. 256-257)	763'22	723'28	742'65	684'37	754'49	750'38	774'90	824'95	783'66	842'03	772'06	801'67
	" (pp. 258-259)	668'13	745'51	761'14	785'39	841'04	787'50	825'43	734'66	729'26	698'87	625'63	678'61
Sum (pp. 250-259)	3749'28	3771'18	3763'29	3798'56	3846'17	3857'38	3874'00	3842'26	3837'22	3821'07	3780'21	3770'42	
No. of Obs. ...	369	371	369	370	370	370	370	368	369	369	369	370	
Means ...	10'161	10'165	10'199	10'266	10'395	10'425	10'470	10'441	10'399	10'355	10'244	10'190	
		0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>
SERIES M <sub>2</sub> K <sub>1</sub> .	Sum (pp. 260-261)	<i>feet</i> 781'78	<i>feet</i> 788'51	<i>feet</i> 791'85	<i>feet</i> 794'77	<i>feet</i> 802'45	<i>feet</i> 781'40	<i>feet</i> 778'77	<i>feet</i> 778'84	<i>feet</i> 753'27	<i>feet</i> 736'84	<i>feet</i> 758'25	<i>feet</i> 771'75
	" (pp. 262-263)	764'60	765'01	775'40	762'54	773'08	759'52	753'59	741'94	752'55	752'99	751'73	749'21
	" (pp. 264-265)	798'16	780'21	734'29	729'30	733'03	715'16	749'27	756'64	761'77	772'68	791'99	790'74
	" (pp. 266-267)	755'82	747'60	747'56	734'08	744'58	777'64	767'21	776'91	797'38	777'38	774'20	773'75
	" (pp. 268-269)	734'56	729'89	739'21	759'66	755'75	759'88	778'28	767'68	726'65	735'55	710'75	696'56
Sum (pp. 260-269)	3834'92	3811'22	3788'31	3780'35	3808'89	3793'60	3827'12	3822'01	3791'62	3775'44	3766'92	3782'01	
No. of Obs. ...	369	370	370	368	370	368	369	369	369	369	369	369	
Means ...	10'393	10'301	10'239	10'273	10'294	10'309	10'372	10'358	10'275	10'232	10'208	10'249	
		0 <sup>h</sup>	1 <sup>h</sup>	2 <sup>h</sup>	3 <sup>h</sup>	4 <sup>h</sup>	5 <sup>h</sup>	6 <sup>h</sup>	7 <sup>h</sup>	8 <sup>h</sup>	9 <sup>h</sup>	10 <sup>h</sup>	11 <sup>h</sup>
SERIES 2N <sub>1</sub> K <sub>1</sub> .	Sum (pp. 270-271)	<i>feet</i> 744'23	<i>feet</i> 739'16	<i>feet</i> 754'05	<i>feet</i> 784'12	<i>feet</i> 808'42	<i>feet</i> 804'42	<i>feet</i> 808'31	<i>feet</i> 804'33	<i>feet</i> 784'12	<i>feet</i> 751'65	<i>feet</i> 752'28	<i>feet</i> 755'05
	" (pp. 272-273)	746'70	739'98	726'62	724'56	746'21	771'16	768'42	786'97	780'20	786'85	773'81	755'51
	" (pp. 274-275)	808'66	798'15	780'79	781'47	737'80	732'60	734'46	726'08	747'26	764'39	768'96	797'78
	" (pp. 276-277)	785'38	797'35	772'13	759'62	757'78	748'47	731'42	757'51	741'65	758'63	790'11	801'85
	" (pp. 278-279)	754'84	775'43	769'80	779'09	774'44	767'05	736'57	711'53	698'42	694'30	689'37	708'60
Sum (pp. 270-279)	3839'81	3850'07	3803'39	3828'86	3824'65	3823'70	3779'18	3786'42	3751'65	3755'82	3775'03	3820'79	
No. of Obs. ...	370	371	369	369	369	370	368	370	368	369	369	370	
Means ...	10'378	10'378	10'307	10'376	10'365	10'334	10'270	10'234	10'195	10'178	10'230	10'326	



PERIOD TIDES.

Series 2N, M<sub>2</sub>N, M<sub>2</sub>K<sub>1</sub> and 2M<sub>2</sub>K<sub>1</sub>.

12 <sup>h</sup>	13 <sup>h</sup>	14 <sup>h</sup>	15 <sup>h</sup>	16 <sup>h</sup>	17 <sup>h</sup>	18 <sup>h</sup>	19 <sup>h</sup>	20 <sup>h</sup>	21 <sup>h</sup>	22 <sup>h</sup>	23 <sup>h</sup>		
<i>feet</i> 769'73	<i>feet</i> 769'60	<i>feet</i> 745'62	<i>feet</i> 768'17	<i>feet</i> 759'58	<i>feet</i> 795'87	<i>feet</i> 821'34	<i>feet</i> 832'74	<i>feet</i> 823'49	<i>feet</i> 803'67	<i>feet</i> 804'80	<i>feet</i> 763'37	18346'18	SERIES 2N.
774'16	777'63	810'66	789'71	828'49	817'00	801'22	801'81	775'74	773'18	776'86	753'78	18294'09	
836'86	831'11	822'89	796'02	778'33	787'64	778'57	777'03	812'92	819'81	812'76	818'97	18592'83	
733'03	746'95	729'65	772'71	800'69	815'81	817'37	814'37	829'91	812'02	776'11	749'42	18308'08	
745'73	745'38	775'50	772'30	776'06	759'07	739'00	773'61	760'90	761'94	764'52	751'51	17747'32	
3859'51	3870'67	3884'32	3898'91	3943'15	3975'39	3957'50	3999'56	4002'96	3970'62	3935'05	3837'05	91288'50	
370	369	368	368	370	370	367	369	369	369	370	368		
10'431	10'490	10'555	10'595	10'657	10'744	10'783	10'839	10'848	10'760	10'635	10'427		
<i>feet</i> 751'23	<i>feet</i> 762'11	<i>feet</i> 689'39	<i>feet</i> 723'23	<i>feet</i> 709'47	<i>feet</i> 707'52	<i>feet</i> 763'62	<i>feet</i> 739'34	<i>feet</i> 817'79	<i>feet</i> 790'47	<i>feet</i> 821'84	<i>feet</i> 818'68	18340'74	SERIES M <sub>2</sub> N.
700'96	726'46	736'65	837'64	800'17	881'37	821'07	808'08	786'27	690'16	721'72	661'34	18288'91	
878'60	805'26	847'29	775'60	741'31	743'97	687'88	742'40	719'35	778'12	816'92	788'45	18574'29	
761'64	701'25	721'91	672'12	732'60	733'30	777'03	824'70	772'57	841'55	763'68	804'51	18324'52	
641'45	733'82	754'99	785'06	850'23	784'20	813'57	727'10	738'31	709'48	647'33	693'33	17760'04	
3733'88	3728'90	3750'23	3793'65	3833'78	3850'36	3863'17	3841'62	3834'29	3809'78	3771'49	3766'31	91288'50	
368	369	368	370	369	368	369	368	370	369	368	369		
10'146	10'105	10'191	10'253	10'390	10'463	10'469	10'439	10'363	10'325	10'249	10'207		
<i>feet</i> 755'63	<i>feet</i> 771'53	<i>feet</i> 804'07	<i>feet</i> 797'63	<i>feet</i> 779'55	<i>feet</i> 779'09	<i>feet</i> 762'37	<i>feet</i> 752'86	<i>feet</i> 724'38	<i>feet</i> 729'05	<i>feet</i> 751'20	<i>feet</i> 749'56	18455'40	SERIES M <sub>2</sub> K <sub>1</sub> .
786'09	782'56	766'05	779'76	765'55	729'05	718'63	720'51	722'85	733'23	733'80	782'11	18142'35	
791'00	812'56	809'25	774'39	754'66	762'43	732'82	731'70	764'66	784'22	782'28	786'50	18399'71	
746'31	739'01	748'30	762'19	766'54	757'39	787'53	784'99	775'45	794'98	804'28	787'02	18428'10	
707'06	706'32	729'72	734'99	759'65	762'37	758'89	780'36	782'26	753'57	746'55	746'78	17862'94	
3786'09	3811'98	3857'39	3848'96	3825'95	3790'33	3760'24	3770'42	3769'60	3795'05	3838'11	3851'97	91288'50	
369	369	370	369	369	369	368	370	369	369	369	370		
10'260	10'331	10'425	10'431	10'368	10'272	10'218	10'190	10'216	10'285	10'401	10'411		
<i>feet</i> 728'04	<i>feet</i> 746'40	<i>feet</i> 757'16	<i>feet</i> 763'36	<i>feet</i> 772'71	<i>feet</i> 782'34	<i>feet</i> 789'32	<i>feet</i> 778'15	<i>feet</i> 760'31	<i>feet</i> 756'70	<i>feet</i> 734'90	<i>feet</i> 722'80	18382'83	SERIES 2M <sub>2</sub> K <sub>1</sub> .
762'78	743'93	735'57	759'25	758'79	767'70	781'15	785'47	792'32	798'43	796'12	768'59	18357'09	
794'93	795'31	784'24	748'72	733'38	713'58	719'04	743'99	787'44	791'33	798'15	801'88	18389'49	
812'49	799'41	802'83	774'35	747'43	747'90	737'77	719'36	728'56	759'18	766'50	785'59	18385'27	
745'91	755'41	774'94	794'48	772'00	743'83	751'69	722'89	696'75	710'39	727'80	718'29	17773'82	
3843'25	3840'46	3854'74	3840'16	3784'31	3755'35	3778'97	3749'86	3765'38	3816'03	3823'47	3797'15	91288'50	
369	368	369	369	369	368	371	368	369	369	370	368		
10'415	10'436	10'446	10'407	10'256	10'205	10'186	10'190	10'204	10'342	10'334	10'318		

FORMS FOR SHORT-PERIOD TIDES.

Analysis of Series S.

I		II		III		IV		V		VI		VII		IX		X		XII		XIII		XIV		XV		Values of Multipliers (M)							
				I+II		I-II		Lower half of IV reversed		IV+V		M		M×VI		IV-V		M		M×IX		XII First half of III		XIII Second half of III		XII+XIII		XII-XIII					
h	0	h	12	h	11	h	11	...	...	- .110	o	.000	- .110	1	- .110	23	.868	17	.379	41	.247	+ 6	.489	o	= nat. sin. 0° = .00000								
1	11	11	703	13	11	11	804	23	23	507	17	713	41	41	220	+ 5	794	S <sub>1</sub>	= nat. sin. 15° = .25882														
2	11	11	146	14	11	214	22	300	- .068	+ .134	+ .066	S <sub>2</sub>	+ .033	- .202	S <sub>3</sub>	- .175	23	360	18	818	41	178	+ 3	542	S <sub>2</sub>	= nat. sin. 30° = .50000							
3	10	10	366	15	10	390	20	756	- .024	+ .089	+ .065	S <sub>3</sub>	+ .046	- .113	S <sub>3</sub>	- .080	20	756	20	427	41	183	+ 0	329	S <sub>3</sub>	= nat. sin. 45° = .70711							
4	9	9	557	16	9	567	19	124	- .010	+ .042	+ .036	S <sub>4</sub>	+ .036	- .062	S <sub>2</sub>	- .031	19	124	22	104	41	228	- 2	980	S <sub>4</sub>	= nat. sin. 60° = .86603							
5	8	8	947	17	8	942	17	889	+ .005	+ .011	+ .016	S <sub>5</sub>	+ .015	- .006	S <sub>1</sub>	- .002	17	889	23	356	41	245	- 5	467	S <sub>5</sub>	= nat. sin. 75° = .96593							
6	8	8	684	18	8	695	17	379	- .011	...	- .011	1	- .011	- .011	o	.000																	
7	8	8	862	19	8	851	17	713	+ .011	...	...	...	...	...	...	...																	
8	9	9	435	20	9	383	18	818	+ .052	...	...	...	...	...	...	...																	
9	10	10	258	21	10	160	20	427	+ .089	...	...	...	...	...	...	...																	
10	11	11	119	22	10	985	22	104	+ .134	12		+ 0	.127	12		- 0	.621	24		247		301											
11	11	11	743	23	11	613	23	356	+ .130	B <sub>1</sub>		= + 0		.0106	A <sub>1</sub>		= - 0		.0518	A <sub>0</sub>		= 10		304									

XV		XVI		XVII		XVIII		XIX		XX		XXI		XXII		XXIII		XXIV		XXV		XXVI		XXVII																							
M		M×XV		M×XV		M×XV		M×XV		First half of XIV		Second half of XIV		XX-XXI		M×XXII		M×XXII		XX+XXI		M×XXV		M×XXV																							
+ 6	.489	o	.000	1	+ 6	.489	o	.000	1	+ 6	.489	41	41	.247	.183	+ .064	o	.000	1	+ .064	82	82	.450	o	.000	1	+ 82	.430																			
+ 5	.794	S <sub>2</sub>	+ 2	.897	S <sub>4</sub>	+ 5	.794	1	+ 5	.794	41	41	.220	.228	- .008	S <sub>4</sub>	- .007	S <sub>2</sub>	- .004	82	82	.448	S <sub>4</sub>	+ 71	.402	- S <sub>2</sub>	- 41	.224																			
+ 3	.542	S <sub>3</sub>	+ 3	.067	S <sub>2</sub>	+ 1	.771	o	.000	- 1	- 3	.542	41	41	.245	- .067	S <sub>4</sub>	- .058	- S <sub>2</sub>	+ .034	82	82	.423	- S <sub>4</sub>	- 71	.381	- S <sub>2</sub>	- 41	.212																		
+ 0	.329	1	+ 0	.329	o	.000	- 1	- 0	.329	o	.000																																				
- 2	.980	S <sub>4</sub>	- 2	.581	- S <sub>2</sub>	+ 1	490	o	.000	1	- 2	.980																																			
- 5	.467	S <sub>2</sub>	- 2	.734	- S <sub>4</sub>	+ 4	.735	1	- 5	.467	o	.000																																			
12		+ 0		.978		12		+ 19		.503		12		- 0		.002		12		- 0		.033		12		+ 0		.021		12		- 0		.006													
B <sub>2</sub>		= + 0		.0815		A <sub>2</sub>		= + 1		.623		B <sub>6</sub>		= - 0		.0002		A <sub>6</sub>		= - 0		.0028		B <sub>4</sub>		= - 0		.0054		A <sub>4</sub>		= + 0		.0078		B <sub>8</sub>		= + 0		.0018		A <sub>8</sub>		= - 0		.0005	

Analysis of Series M.

I		II		III		IV		V		VI		VII		VIII		IX		X		XI		XII		XIII		XIV		XV									
				I+II		I-II		Lower half of IV reversed		IV+V		M		M×VI		IV-V		M		M×IX		M×IX		XII First half of III		XIII Second half of III		XII+XIII		XII-XIII							
h	0	h	12	h	14	h	14	...	...	- .231	o	.000	o	.000	- .231	1	- .231	1	- .231	1	- .231	27	.985	13	.661	41	.646	+ 14	.324								
1	12	12	203	13	12	449	24	652	- .246	+ .079	- .167	S <sub>1</sub>	- .043	S <sub>3</sub>	- .118	- .325	S <sub>2</sub>	- .314	S <sub>2</sub>	- .230	24	652	16	526	41	178	+ 8	126									
2	10	10	034	14	10	180	20	214	- .146	- .073	- .219	- .110	1	- .219	- .073	o	.000	o	.000	20	214	20	527	40	741	- 0	313										
3	8	8	029	15	8	066	16	095	- .037	- .073	- .193	S <sub>3</sub>	- .136	S <sub>3</sub>	- .136	+ .119	S <sub>2</sub>	+ .084	- S <sub>2</sub>	- .084	16	095	24	742	40	837	- 8	647									
4	6	6	660	16	6	640	13	300	+ .020	- .161	- .141	S <sub>4</sub>	- .122	o	.000	+ .181	S <sub>2</sub>	+ .091	- 1	- .181	13	300	27	943	41	243	- 14	643									
5	6	6	282	17	6	212	12	494	+ .070	- .064	+ .006	S <sub>5</sub>	+ .006	- S <sub>3</sub>	- .004	+ .134	S <sub>1</sub>	+ .035	- S <sub>3</sub>	- .095	12	494	29	153	40	647	- 16	659									
6	6	6	858	18	6	803	13	661	+ .055	...	+ .055	1	+ .055	- 1	- .055	+ .055	o	.000	o	.000																	
7	8	8	231	19	8	295	16	526	- .064	...	...	...	...	...	...	...	...	...	...	...																	
8	10	10	183	20	10	344	20	527	- .161	...	...	...	...	...	...	...	...	...	...	...																	
9	12	12	203	21	12	440	24	742	- .156	...	...	...	...	...	...	...	...	...	...	...																	
10	13	13	935	22	14	008	27	943	- .073	12		- 0	.350	12		- 0	.532	12		- 0	.398	12		- 0	.821												
11	14	14	616	23	14	537	29	153	+ .079	B <sub>1</sub>		= - 0		.0291		B <sub>3</sub>		= - 0		.0443		A <sub>1</sub>		= - 0		.0332		A <sub>3</sub>		= - 0		.0683					

XV		XVI		XVII		XVIII		XIX		XX		XXI		XXII		XXIII		XXIV		XXV		XXVI		XXVII											
M		M×XV		M×XV		M×XV		M×XV		First half of XIV		Second half of XIV		XX-XXI		M×XXII		M×XXII		XX+XXI		M×XXV		M×XXV											
+ 14	.324	o	.000	1	+ 14	.324	o	.000	1	+ 14	.324	41	41	.646	.837	+ 0	.809	o	.000	1	+ .809	82	82	.483	o	.000	1	+ 82	.483						
+ 8	.126	S <sub>2</sub>	+ 4	.063	S <sub>4</sub>	+ 7	.037	1	+ 8	.126	41	41	.178	.243	- 0	.065	S <sub>4</sub>	- .056	S <sub>2</sub>	- .033	82	82	.421	S <sub>4</sub>	+ 71	.379	- S <sub>2</sub>	- 41	.211						
- 0	.313	S <sub>4</sub>	- 0	.271	S <sub>2</sub>	- 0	.157	o	.000	- 1	+ 0	.313	40	741	41	.647	- 0	.906	S <sub>4</sub>	- .785	- S <sub>2</sub>	+ .453	82	82	.388	- S <sub>4</sub>	- 71	.350	- S <sub>2</sub>	- 41	.194				
- 8	.647	1	- 8	.647	o	.000	- 1	+ 8	.647	o	.000																								
- 14	.643	S <sub>2</sub>	- 12	.681	- S <sub>2</sub>	+ 7	.322	o	.000	1	- 14	.643																							
- 16	.659	S <sub>2</sub>	- 8	.330	- S <sub>4</sub>	+ 14	.427	1	- 16	.659	o	.000																							
12		- 2		1555		A <sub>2</sub>		= + 3		5794		B <sub>8</sub>		= + 0		.0005		A <sub>6</sub>		= - 0		.0005		12		+ 0		.029		12		+ 0		.078	
B <sub>2</sub>		= - 2		1555		A <sub>2</sub>		= + 3		5794		B <sub>8</sub>		= + 0		.0005		A <sub>6</sub>		= - 0		.0005		12		+ 0		.029		12		+ 0		.078	



FORMS FOR SHORT-PERIOD TIDES.

Analysis of Series L.

I		II		III	XIII Second half of III	XV	XVI	XVII
				I + II		III - XIII	M	M × XV
h		h						
0	10° 296	12	10° 283	20° 579	20° 555	+ '024	0	+ '024
1	10° 309	13	10° 288	20° 597	20° 612	- '015	S <sub>2</sub>	- '013
2	10° 438	14	10° 366	20° 794	20° 703	+ '091	S <sub>1</sub>	+ '046
3	10° 408	15	10° 342	20° 750	20° 506	+ '244	1	+ '000
4	10° 386	16	10° 307	20° 693	20° 485	+ '208	S <sub>2</sub>	- '104
5	10° 385	17	10° 264	20° 649	20° 549	+ '100	S <sub>2</sub>	- '087
6	10° 350	18	10° 205	20° 555				
7	10° 382	19	10° 230	20° 612				
8	10° 432	20	10° 271	20° 703			12	+ '0545
9	10° 330	21	10° 176	20° 506				- '0134
10	10° 277	22	10° 208	20° 485				B <sub>2</sub> = + '0545; A <sub>2</sub> = - '0112
11	10° 358	23	10° 221	20° 549				

Analysis of Series N.

I		II		III	XIII Second half of III	XV	XVI	XVII
				I + II		III - XIII	M	M × XV
h		h						
0	11° 187	12	11° 170	22° 357	18° 894	+ '3463	0	+ '000
1	10° 827	13	10° 755	21° 582	19° 667	+ '1915	S <sub>2</sub>	+ '0958
2	10° 311	14	10° 233	20° 544	20° 600	- '0146	S <sub>1</sub>	- '0126
3	9° 810	15	9° 742	19° 552	21° 686	- '2134	1	- '000
4	9° 455	16	9° 379	18° 834	22° 428	- '3594	S <sub>1</sub>	- '3113
5	9° 292	17	9° 269	18° 561	22° 676	- '4115	S <sub>2</sub>	- '2058
6	9° 444	18	9° 450	18° 894				
7	9° 846	19	9° 821	19° 667				
8	10° 380	20	10° 310	20° 690			12	- '6473
9	10° 844	21	10° 842	21° 686				12 + '10409
10	11° 197	22	11° 231	22° 428				B <sub>2</sub> = - '05394; A <sub>2</sub> = + '08674
11	11° 320	23	11° 356	22° 676				

Analysis of Series J.

I		II		IV	V Lower half of IV reversed	VI	VII	IX	X
				I - II	IV + V	M	M × VI	IV - V	M × IX
h		h							
0	10° 297	12	10° 338	- '041	...	- '041	0	- '041	1
1	10° 231	13	10° 358	- '127	+ '074	- '053	- '014	- '201	S <sub>2</sub>
2	10° 236	14	10° 364	- '128	+ '066	- '122	- '061	- '134	S <sub>2</sub>
3	10° 229	15	10° 379	- '150	- '052	- '202	- '143	- '098	S <sub>2</sub>
4	10° 203	16	10° 394	- '101	- '046	- '237	- '205	- '145	S <sub>2</sub>
5	10° 220	17	10° 402	- '182	- '109	- '291	- '281	- '073	S <sub>1</sub>
6	10° 243	18	10° 375	- '132	...	- '132	1	- '132	0
7	10° 257	19	10° 366	- '109					
8	10° 282	20	10° 328	- '046			12	- '0836	
9	10° 286	21	10° 338	- '052					12 - '0512
10	10° 207	22	10° 291	+ '006					A <sub>1</sub> = - '0426
11	10° 325	23	10° 251	+ '074					B <sub>1</sub> = - '06607

Analysis of Series Q.

I		II		IV	V Lower half of IV reversed	VI	VII	IX	X
				I - II	IV + V	M	M × VI	IV - V	M × IX
h		h							
0	10° 251	12	10° 343	- '092	...	- '092	0	- '092	1
1	10° 241	13	10° 357	- '116	+ '124	+ '008	S <sub>1</sub>	+ '002	- '240
2	10° 228	14	10° 351	- '123	+ '043	- '080	S <sub>2</sub>	- '040	- '166
3	10° 176	15	10° 376	- '200	- '094	- '294	S <sub>2</sub>	- '208	- '106
4	10° 181	16	10° 435	- '254	- '160	- '414	S <sub>1</sub>	- '359	- '094
5	10° 215	17	10° 401	- '186	- '189	- '375	S <sub>2</sub>	- '362	+ '003
6	10° 240	18	10° 406	- '157	...	- '157	1	- '157	0
7	10° 229	19	10° 418	- '180					
8	10° 223	20	10° 383	- '160			12	- '1124	
9	10° 273	21	10° 367	- '094					12 - '0589
10	10° 312	22	10° 269	+ '043					A <sub>1</sub> = - '04091
11	10° 365	23	10° 241	+ '124					B <sub>1</sub> = - '00937

Analysis of Series R.

I		II		III	XIII Second half of III	XV	XVI	XVII
				I + II		III - XIII	M	M × XV
h		h						
0	9° 938	12	10° 684	20° 622	20° 546	+ '076	0	+ '076
1	10° 133	13	10° 473	20° 608	20° 511	+ '097	S <sub>2</sub>	+ '084
2	10° 142	14	10° 280	20° 622	20° 501	+ '121	S <sub>2</sub>	+ '061
3	10° 514	15	10° 085	20° 599	20° 503	+ '096	1	+ '000
4	10° 627	16	9° 912	20° 549	20° 528	+ '021	S <sub>1</sub>	+ '011
5	10° 739	17	9° 812	20° 551	20° 582	- '031	S <sub>2</sub>	- '027
6	10° 827	18	9° 719	20° 546				
7	10° 869	19	9° 642	20° 511				
8	10° 911	20	9° 590	20° 501			12	+ '0237
9	10° 912	21	9° 571	20° 501				
10	10° 908	22	9° 620	20° 518				
11	10° 835	23	9° 747	20° 582				
Means of 1884 and 1885								B <sub>2</sub> = + '0210; A <sub>2</sub> = + '0198

Analysis of Series T.

I		II		III	XIII Second half of III	XV	XVI	XVII
				I + II		III - XIII	M	M × XV
h		h						
0	10° 640	12	10° 392	21° 032	20° 107	+ '925	0	+ '000
1	10° 579	13	10° 337	20° 916	20° 211	+ '705	S <sub>2</sub>	+ '353
2	10° 469	14	10° 251	20° 720	20° 397	+ '323	S <sub>1</sub>	+ '280
3	10° 341	15	10° 126	20° 467	20° 643	- '176	1	- '000
4	10° 251	16	10° 008	20° 259	20° 861	- '602	S <sub>1</sub>	- '521
5	10° 183	17	9° 937	20° 120	21° 001	- '881	S <sub>2</sub>	- '441
6	10° 186	18	9° 921	20° 107				
7	10° 218	19	9° 993	20° 211			12	- '0505
8	10° 266	20	10° 131	20° 397				
9	10° 324	21	10° 319	20° 643				
10	10° 362	22	10° 499	20° 861				
11	10° 389	23	10° 612	21° 001				
Means of 1884 and 1885								B <sub>2</sub> = - '0421; A <sub>2</sub> = + '02301

FORMS FOR SHORT-PERIOD TIDES.

Analysis of Series  $\lambda$ .

I		II		III	XIII	XV	XVI	M	XVII	
		I + II		Second half of III	III - XIII	M	M × XV	M	M × XV	
h		h								
0	10° 263	12	10° 403	20° 666	20° 613	+ .053	0	.000	1 + .053	
1	10° 251	13	10° 346	20° 597	20° 600	- .003	$S_2$	- .002	$S_4$ - .003	
2	10° 258	14	10° 310	20° 568	20° 635	- .007	$S_4$	- .058	$S_2$ - .034	
3	10° 301	15	10° 394	20° 695	20° 568	+ .127	1	+ .127	0 .000	
4	10° 263	16	10° 311	20° 574	20° 765	- .191	$S_4$	- .165	- $S_2$ + .096	
5	10° 353	17	10° 347	20° 700	20° 590	+ .110	$S_2$	+ .055	- $S_4$ - .095	
6	10° 308	18	10° 395	20° 613						
7	10° 319	19	10° 281	20° 600						
8	10° 372	20	10° 263	20° 635						
9	10° 351	21	10° 217	20° 568						
10	10° 438	22	10° 327	20° 765						
11	10° 376	23	10° 214	20° 590						
							$B_2 = -0.0035$	$A_2 = +0.0014$		

Analysis of Series  $\nu$ .

I		II		III	XIII	XV	XVI	M	XVII	
		I + II		Second half of III	III - XIII	M	M × XV	M	M × XV	
h		h								
0	10° 356	12	10° 432	20° 788	20° 463	+ .325	0	.000	1 + .325	
1	10° 392	13	10° 423	20° 815	20° 475	+ .340	$S_2$	+ .170	$S_4$ + .294	
2	10° 283	14	10° 318	20° 601	20° 610	- .009	$S_4$	- .008	- $S_2$ - .005	
3	10° 266	15	10° 304	20° 570	20° 750	- .180	1	- .180	0 .000	
4	10° 279	16	10° 323	20° 602	20° 653	- .051	$S_4$	- .044	- $S_2$ + .026	
5	10° 285	17	10° 339	20° 624	20° 621	+ .003	$S_2$	+ .002	- $S_4$ - .003	
6	10° 222	18	10° 241	20° 463						
7	10° 222	19	10° 253	20° 475						
8	10° 312	20	10° 298	20° 610						
9	10° 403	21	10° 347	20° 750						
10	10° 343	22	10° 310	20° 653						
11	10° 341	23	10° 280	20° 621						
							$B_2 = -0.0050$	$A_2 = +0.0531$		

Analysis of Series  $\mu$  or 2MS.

I		II		III	XIII	XV	XVI	M	XVII	
		I + II		Second half of III	III - XIII	M	M × XV	M	M × XV	
h		h								
0	10° 458	12	10° 354	20° 812	20° 456	+ .356	0	.000	1 + .356	
1	10° 352	13	10° 216	20° 508	20° 660	- .092	$S_2$	- .046	$S_4$ - .080	
2	10° 219	14	10° 135	20° 354	20° 844	- .490	$S_4$	- .424	$S_2$ - .245	
3	10° 152	15	10° 081	20° 233	20° 911	- .678	1	- .678	0 .000	
4	10° 168	16	10° 072	20° 240	21° 013	- .773	$S_4$	- .669	- $S_2$ + .387	
5	10° 159	17	10° 160	20° 319	20° 901	- .582	$S_2$	- .291	- $S_4$ + .504	
6	10° 212	18	10° 244	20° 456						
7	10° 335	19	10° 325	20° 660						
8	10° 408	20	10° 436	20° 844						
9	10° 418	21	10° 493	20° 911						
10	10° 475	22	10° 538	21° 013						
11	10° 420	23	10° 481	20° 901						
							$B_2 = -0.1757$	$A_2 = +0.0768$		

Analysis of Series 2SM.

I		II		III	XIII	XV	XVI	M	XVII	
		I + II		Second half of III	III - XIII	M	M × XV	M	M × XV	
h		h								
0	10° 314	12	10° 277	20° 591	20° 621	- .030	0	.000	1 - .030	
1	10° 341	13	10° 299	20° 640	20° 597	+ .043	$S_2$	+ .022	$S_4$ + .037	
2	10° 344	14	10° 337	20° 681	20° 508	+ .173	$S_4$	+ .150	$S_2$ + .087	
3	10° 346	15	10° 350	20° 696	20° 530	+ .166	1	+ .166	0 .000	
4	10° 288	16	10° 394	20° 682	20° 511	+ .171	$S_4$	+ .148	- $S_2$ - .086	
5	10° 326	17	10° 367	20° 693	20° 563	+ .150	$S_2$	+ .065	- $S_4$ - .113	
6	10° 234	18	10° 387	20° 621						
7	10° 267	19	10° 330	20° 597						
8	10° 183	20	10° 325	20° 508						
9	10° 222	21	10° 308	20° 530						
10	10° 207	22	10° 304	20° 511						
11	10° 260	23	10° 303	20° 563						
							$B_2 = +0.0459$	$A_2 = -0.0088$		

Analysis of Series 2N.

I		II		III	XIII	XV	XVI	M	XVII	
		I + II		Second half of III	III - XIII	M	M × XV	M	M × XV	
h		h								
0	10° 191	12	10° 431	20° 622	20° 541	+ .081	0	.000	1 + .081	
1	9° 998	13	10° 490	20° 488	20° 704	- .216	$S_2$	- .108	$S_4$ - .187	
2	9° 839	14	10° 555	20° 394	20° 875	- .481	$S_4$	- .417	$S_2$ - .241	
3	9° 696	15	10° 595	20° 291	20° 944	- .653	1	- .653	0 .000	
4	9° 655	16	10° 657	20° 312	20° 888	- .576	$S_4$	- .499	- $S_2$ + .288	
5	9° 698	17	10° 744	20° 442	20° 815	- .373	$S_2$	- .187	- $S_4$ + .323	
6	9° 758	18	10° 783	20° 541						
7	9° 865	19	10° 839	20° 704						
8	10° 027	20	10° 848	20° 875						
9	10° 184	21	10° 760	20° 944						
10	10° 353	22	10° 635	20° 888						
11	10° 388	23	10° 427	20° 815						
							$B_2 = -0.1553$	$A_2 = +0.0220$		

Analysis of Series  $M_3N$ .

I		II		III	XIII	XV	XVI	M	XVII	
		I + II		Second half of III	III - XIII	M	M × XV	M	M × XV	
h		h								
0	10° 161	12	10° 146	20° 307	20° 939	- .632	0	.000	1 - .632	
1	10° 165	13	10° 105	20° 270	20° 880	- .610	$S_4$	- .528	$S_2$ - .305	
2	10° 199	14	10° 191	20° 390	20° 762	- .372	$S_4$	- .322	- $S_2$ + .186	
3	10° 266	15	10° 253	20° 519	20° 680	- .161	1	- .161	0 .000	
4	10° 395	16	10° 390	20° 785	20° 493	+ .292	$S_4$	- .253	- $S_2$ - .146	
5	10° 425	17	10° 463	20° 888	20° 397	+ .491	- $S_4$	- .425	- $S_2$ + .246	
6	10° 470	18	10° 460	20° 939						
7	10° 441	19	10° 439	20° 880						
8	10° 399	20	10° 363	20° 762						
9	10° 355	21	10° 325	20° 680						
10	10° 244	22	10° 249	20° 493						
11	10° 190	23	10° 207	20° 397						
							$B_4 = -0.1273$	$A_4 = -0.0400$		

FORMS FOR SHORT-PERIOD TIDES.

Analysis of Series  $M_2K_1$ .

Analysis of Series  $2M_2K_1$ .

I		II		IV		V	VI		M	VII		IX		M	X	
				I-II		Lower half of IV reversed	IV+V			M x VI		IV-V			M x IX	
h		h														
0	10° 393	12	10° 260	+ '133	...	...	0	'000		+ '133	1	+ '133				
1	10° 301	13	10° 431	- '030	- '162	- '192	$S_3$	- '136	+ '132	$S_3$		+ '093				
2	10° 430	14	10° 425	- '186	- '193	- '379	1	- '379	+ '007	0		'000				
3	10° 273	15	10° 431	- '158	- '053	- '211	$S_3$	- '149	- '105	- $S_3$		+ '074				
4	10° 294	16	10° 368	- '074	+ '059	- '015	0	'000	- '135	- 1		+ '133				
5	10° 309	17	10° 272	+ '037	+ '168	+ '205	- $S_3$	- '145	- '131	- $S_3$		+ '093				
6	10° 372	18	10° 218	+ '154	...	+ '154	- 1	- '154	'000	0		'000				
7	10° 358	19	10° 190	+ '168												
8	10° 275	20	10° 216	+ '059												
9	10° 232	21	10° 285	- '053			12	- '0963			12	+ '0526				
10	10° 208	22	10° 401	- '193												
11	10° 249	23	10° 411	- '162				$B_3 = - '0803$				$A_3 = + '0438$				

I		II		IV		V	VI		M	VII		IX		M	X	
				I-II		Lower half of IV reversed	IV+V			M x VI		IV-V			M x IX	
h		h														
0	10° 378	12	10° 415	- '037	...	...	- '037	0	'000	- '035	- '066	1	- '037			
1	10° 378	13	10° 436	- '058	+ '008	- '050	$S_3$	- '035	- '066	$S_3$		- '047				
2	10° 307	14	10° 440	- '139	- '104	- '243	1	- '243	- '035	0		'000				
3	10° 376	15	10° 407	- '031	- '164	- '195	$S_3$	- '138	+ '133	- $S_3$		+ '094				
4	10° 365	16	10° 256	+ '109	- '009	+ '109	0	'000	+ '118	- 1		- '118				
5	10° 334	17	10° 205	+ '129	+ '044	+ '173	- $S_3$	- '122	+ '085	- $S_3$		- '060				
6	10° 270	18	10° 186	+ '084	...	+ '084	- 1	- '084	+ '084	0		'000				
7	10° 234	19	10° 190	+ '044												
8	10° 195	20	10° 204	- '009												
9	10° 178	21	10° 342	- '164							12	- '0622		12	- '0356	
10	10° 230	22	10° 334	- '104												
11	10° 326	23	10° 318	+ '008								$B_3 = - '0518$			$A_3 = - '0520$	

VALUES OF  $V_0 + u$  FOR BOMBAY.

1885, 1st January, 0<sup>h</sup>. Lat. 18° 55' N., Long. 72° 50' E. (= 4<sup>h</sup> 856).

Average Long. Moon's Node for year beginning with  
 0<sup>h</sup> 1st January 1885, Date of mid-year = 2-3 July 1885  
 Auxiliary Tables N = 179° 557.

Average Long. Moon's Perigee for L Tide  
 (round numbers).  
 (from below)  $p_0 = 84° 144$   
 motion in 184<sup>d</sup> 13<sup>h</sup> = 20° 560  
 $P + \xi = 104° 704$   
 $-\xi = 359° 882$   
 $P = 104° 586$   
 $\cot \frac{1}{2} I = + 6\cdot 205$   
 $\cot^2 \frac{1}{2} I = + 38\cdot 502$   
 $\frac{1}{2} \cot^2 \frac{1}{2} I = + 6\cdot 417$   
 $-\cos 2P = + 0\cdot 873$   
 $\frac{1}{2} \cot^2 \frac{1}{2} I - \cos 2P = + 7\cdot 290$

Computation of R and Q (round numbers).  
 $\text{colog} [\frac{1}{2} \cot^2 \frac{1}{2} I - \cos 2P] = + 9\cdot 13747$   
 $\log \sin 2P = - 9\cdot 68791$   
 $\log \tan R = - 8\cdot 82518$   
 for L Tide,  $R = 356° 175$   
 $\log \tan P = - 10\cdot 58466$   
 $\log \frac{1}{2} = 9\cdot 69897$   
 $\log \tan Q = - 0\cdot 28165$   
 for M Tide,  $Q = 117° 494$

Extract from Auxiliary Tables.

$I = 18° 309$ ,  $\nu = + 0° 127$ ,  $\xi = + 0° 118$ .  
 For K Tides  $\nu' = + 0° 017$ ,  $2\nu'' = + 0° 031$ .

1885, 1st January, 0<sup>h</sup>. Mean Time at Greenwich.

Sid. Time at Mean Noon } = 18 45 12.37  
 (Naut. Alm., p. II.) }  
 = 18 45 20.61  
 = 18 45 34.35  
 = 281° 302  
 East Long. Correction = - 0° 199  
 $h_0 = 281° 103$   
 $\nu = 0° 127$   
 $h_0 - \nu = 280° 076$   
 $2h_0 = 201° 106$

Moon's mean longitude }  $s_0 = 103° 19' 1$   
 (Nautical Almanac) }  
 = 103° 318  
 East Long. Correction = - 2° 667  
 $s_0 = 100° 651$   
 $\xi = 0° 118$   
 $s_0 - \xi = 100° 533$   
 $2s_0 - 2\xi = 201° 066$   
 $2s_0 = 201° 302$

Hansen's Tables de la Lune, }  $p_0 = 83° 920$   
 p. 300.  $\pi$  for 1885, Jan. 0. }  
 Motion in interval from } = 0° 111  
 Jan. 0, or 1 day. }  
 Constant = 0° 136  
 Sum = 84° 167  
 East Long. Correction = 0° 023  
 $p_0 = 84° 144$   
 $s_0 = 100° 651$   
 $s_0 - p_0 = 16° 507$

Extract from Auxiliary Tables }  $p_1 = 280° 960$   
 }  $h_0 = 281° 103$   
 $h_0 - p_1 = 0° 134$   
 Motion per mean Solar hour. } East Long. Correction.  
 $\eta = 0° 0410686$  } (- 0° 199)  
 $\sigma = 0° 5490165$  } (- 2° 667)  
 $\omega = 0° 0046418$  } (- 0° 023)

FORMS FOR SHORT-PERIOD TIDES.

VALUES OF  $V_0 + u$  FOR BOMBAY—(Continued).

<p><b>M SERIES.</b></p> $\begin{aligned} \bar{h}_0 - \nu &= 280^{\circ}976 \\ - (s_0 - t) &= 259^{\circ}467 \end{aligned}$ <p>§ <math>M_1 = 180^{\circ}443</math>          (x 2) for <math>M_2 = 0^{\circ}886</math>          (x 3) for <math>M_3 = 181^{\circ}329</math>          (x 4) for <math>M_4 = 1^{\circ}772</math>          (x 6) for <math>M_6 = 2^{\circ}658</math>          (x 8) for <math>M_8 = 3^{\circ}544</math></p> <p>§ as above <math>M_1 = 180^{\circ}443</math>          (see above) + <math>Q = 117^{\circ}494</math>  <math>-\frac{1}{2}\pi = 270^{\circ}000</math></p> <p>for <math>M_1 = 207^{\circ}937</math></p>	<p><b>K<sub>2</sub> SERIES.</b></p> $\begin{aligned} 2\bar{h}_0 &= 202^{\circ}206 \\ - 2\nu'' &= 359^{\circ}969 \end{aligned}$ <p>for <math>K_2 = 202^{\circ}175</math></p> <p><b>K<sub>1</sub> SERIES.</b></p> $\begin{aligned} \bar{h}_0 &= 281^{\circ}103 \\ - \nu' &= 359^{\circ}983 \\ - \frac{1}{2}\pi &= 270^{\circ}000 \end{aligned}$ <p>for <math>K_1 = 191^{\circ}086</math></p>	<p><b>λ SERIES.</b></p> $\begin{aligned} \text{for } N &= 344^{\circ}379 \\ - 2\bar{h}_0 &= 157^{\circ}794 \\ + 2s_0 &= 201^{\circ}302 \\ + \pi &= 180^{\circ}000 \end{aligned}$ <p>for <math>\lambda = 163^{\circ}475</math></p> <p><b>ν SERIES.</b></p> $\begin{aligned} \text{for } M_2 &= 0^{\circ}886 \\ + (s_0 - p_0) &= 16^{\circ}507 \\ + 2h_0 &= 202^{\circ}206 \\ - 2s_0 &= 158^{\circ}698 \end{aligned}$ <p>for <math>\nu = 18^{\circ}297</math></p>	<p><b>M<sub>2</sub>N SERIES.</b></p> $\begin{aligned} \text{for } M_2 &= 0^{\circ}886 \\ + \text{for } N &= 344^{\circ}379 \end{aligned}$ <p>for <math>M_2N = 345^{\circ}265</math></p> <p><b>2M<sub>2</sub>K<sub>1</sub> SERIES.</b></p> $\begin{aligned} \text{for } M_1 &= 1^{\circ}772 \\ - \text{for } K_1 &= 168^{\circ}914 \end{aligned}$ <p>for <math>2M_2K_1 = 170^{\circ}686</math></p>	<p><b>Mm SERIES.</b></p> $s_0 - p_0 = 16^{\circ}507$ <p><b>Mf SERIES.</b></p> $(2s_0 - 2t) = 201^{\circ}066$
<p><b>S SERIES.</b></p> <p>All zero.</p>	<p><b>L SERIES.</b></p> $\begin{aligned} \text{for } M_2 &= 0^{\circ}886 \\ + (s_0 - p_0) &= 16^{\circ}507 \\ + \pi &= 180^{\circ}000 \end{aligned}$ <p>(see above) - <math>R = 3^{\circ}825</math></p> <p>for <math>L = 201^{\circ}218</math></p>	<p><b>O SERIES.</b></p> $\begin{aligned} \bar{h}_0 - \nu &= 280^{\circ}976 \\ - (2s_0 - 2t) &= 158^{\circ}934 \\ + \frac{1}{2}\pi &= 90^{\circ}000 \end{aligned}$ <p>for <math>O = 169^{\circ}910</math></p>	<p><b>M<sub>2</sub>K<sub>1</sub> SERIES.</b></p> $\begin{aligned} \text{for } M_2 &= 0^{\circ}886 \\ + \text{for } K_1 &= 191^{\circ}086 \end{aligned}$ <p>for <math>M_2K_1 = 191^{\circ}972</math></p>	<p><b>MSf as for 2SM = 359^{\circ}114</b></p>
<p><b>R SERIES.</b></p> $\begin{aligned} \bar{h}_0 - p_1 &= 0^{\circ}134 \\ + \pi &= 180^{\circ}000 \end{aligned}$ <p>for <math>R = 180^{\circ}134</math></p>	<p><b>N SERIES.</b></p> $\begin{aligned} \text{for } M_2 &= 0^{\circ}886 \\ - (s_0 - p_0) &= 343^{\circ}493 \end{aligned}$ <p>for <math>N = 344^{\circ}379</math></p>	<p><b>Q SERIES.</b></p> $\begin{aligned} \text{for } O &= 169^{\circ}910 \\ - (s_0 - p_0) &= 343^{\circ}493 \end{aligned}$ <p>for <math>Q = 153^{\circ}403</math></p>	<p><b>MS as for M<sub>2</sub> = 0^{\circ}886</b></p>	<p><b>Sa SERIES.</b></p> $\bar{h}_0 = 281^{\circ}103$
<p><b>T SERIES.</b></p> <p>for T, - (<math>h_0 - p_1</math>) = 359^{\circ}866</p>	<p><b>2N SERIES.</b></p> $\begin{aligned} \text{for } N &= 344^{\circ}379 \\ - (s_0 - p_0) &= 343^{\circ}493 \end{aligned}$ <p>for <math>2N = 327^{\circ}872</math></p>	<p><b>J SERIES.</b></p> $\begin{aligned} \bar{h}_0 - \nu &= 280^{\circ}976 \\ + (s_0 - p_0) &= 16^{\circ}507 \\ - \frac{1}{2}\pi &= 270^{\circ}000 \end{aligned}$ <p>for <math>J = 207^{\circ}483</math></p>	<p><b>2MS as for M<sub>1</sub> = 1^{\circ}772</b></p>	<p><b>Ssa SERIES.</b></p> $2h_0 = 202^{\circ}206$
<p><b>P SERIES.</b></p> $\begin{aligned} - \bar{h}_0 &= 78^{\circ}897 \\ + \frac{1}{2}\pi &= 90^{\circ}000 \end{aligned}$ <p>for <math>P = 168^{\circ}897</math></p>			<p><b>2SM as for - M<sub>2</sub> = 359^{\circ}114</b></p>	

EVALUATION OF SHORT-PERIOD TIDES.

<b>SERIES S.</b>				<b>SERIES R.</b>				<b>SERIES T.</b>							
Log B <sub>1</sub> = +8.02531	Log B <sub>2</sub> = +8.91116	Log B <sub>4</sub> = -7.73239	Log B <sub>6</sub> = -6.30103	Log B <sub>8</sub> = +7.25327	Log B <sub>2</sub> = +8.32222	Log B <sub>2</sub> = -8.62428	Log B <sub>2</sub> = +8.32222	Log A <sub>2</sub> = +8.29667	Log A <sub>2</sub> = +9.36192	L tan ζ <sub>2</sub> = +0.02555	L tan ζ <sub>2</sub> = -9.26236	L tan ζ <sub>2</sub> = -9.26236	L tan ζ <sub>2</sub> = +0.02555	L tan ζ <sub>2</sub> = +0.02555	L tan ζ <sub>2</sub> = -9.26236
Log A <sub>1</sub> = -8.71433	Log A <sub>2</sub> = +0.21093	Log A <sub>4</sub> = +7.89209	Log A <sub>6</sub> = -7.44716	Log A <sub>8</sub> = -6.69897	Log A <sub>2</sub> = +8.29667	Log A <sub>2</sub> = +9.36192	Log A <sub>2</sub> = +8.29667	Log A <sub>2</sub> = +8.29667	Log A <sub>2</sub> = +9.36192	L tan ζ <sub>2</sub> = +0.02555	L tan ζ <sub>2</sub> = -9.26236	L tan ζ <sub>2</sub> = -9.26236	L tan ζ <sub>2</sub> = +0.02555	L tan ζ <sub>2</sub> = +0.02555	L tan ζ <sub>2</sub> = -9.26236
L tan κ <sub>1</sub> = -9.31098	L tan κ <sub>2</sub> = +8.70023	L tan κ <sub>4</sub> = -9.84030	L tan κ <sub>6</sub> = +8.85387	L tan κ <sub>8</sub> = -0.55630	L tan κ <sub>2</sub> = +8.29667	L tan κ <sub>2</sub> = +9.36192	L tan κ <sub>2</sub> = +8.29667	L tan κ <sub>2</sub> = +8.29667	L tan κ <sub>2</sub> = +9.36192	L tan ζ <sub>2</sub> = +0.02555	L tan ζ <sub>2</sub> = -9.26236	L tan ζ <sub>2</sub> = -9.26236	L tan ζ <sub>2</sub> = +0.02555	L tan ζ <sub>2</sub> = +0.02555	L tan ζ <sub>2</sub> = -9.26236
κ <sub>1</sub> = 168.435	κ <sub>2</sub> = 2.871	κ <sub>4</sub> = 325.305	κ <sub>6</sub> = 184.086	κ <sub>8</sub> = 105.524	κ <sub>2</sub> = 2.871	κ <sub>2</sub> = 2.871	κ <sub>2</sub> = 2.871	κ <sub>2</sub> = 2.871	κ <sub>2</sub> = 2.871	κ <sub>2</sub> = 2.871	κ <sub>2</sub> = 2.871	κ <sub>2</sub> = 2.871	κ <sub>2</sub> = 2.871	κ <sub>2</sub> = 2.871	κ <sub>2</sub> = 2.871
(B <sub>1</sub> ) <sup>2</sup> = 0.00011236	(B <sub>2</sub> ) <sup>2</sup> = 0.00664225	(B <sub>4</sub> ) <sup>2</sup> = 0.00002916	(B <sub>6</sub> ) <sup>2</sup> = 0.00000004	(B <sub>8</sub> ) <sup>2</sup> = 0.00000324	(B <sub>2</sub> ) <sup>2</sup> = 0.00044100	(B <sub>2</sub> ) <sup>2</sup> = 0.00177241	(B <sub>2</sub> ) <sup>2</sup> = 0.00044100	(B <sub>2</sub> ) <sup>2</sup> = 0.00044100	(B <sub>2</sub> ) <sup>2</sup> = 0.00177241	(B <sub>2</sub> ) <sup>2</sup> = 0.00044100	(B <sub>2</sub> ) <sup>2</sup> = 0.00177241	(B <sub>2</sub> ) <sup>2</sup> = 0.00177241	(B <sub>2</sub> ) <sup>2</sup> = 0.00044100	(B <sub>2</sub> ) <sup>2</sup> = 0.00044100	(B <sub>2</sub> ) <sup>2</sup> = 0.00177241
(A <sub>1</sub> ) <sup>2</sup> = 0.00268324	(A <sub>2</sub> ) <sup>2</sup> = 2.64160009	(A <sub>4</sub> ) <sup>2</sup> = 0.00006084	(A <sub>6</sub> ) <sup>2</sup> = 0.00000784	(A <sub>8</sub> ) <sup>2</sup> = 0.00000025	(A <sub>2</sub> ) <sup>2</sup> = 0.00039204	(A <sub>2</sub> ) <sup>2</sup> = 0.05294601	(A <sub>2</sub> ) <sup>2</sup> = 0.00039204	(A <sub>2</sub> ) <sup>2</sup> = 0.00039204	(A <sub>2</sub> ) <sup>2</sup> = 0.05294601	(A <sub>2</sub> ) <sup>2</sup> = 0.00039204	(A <sub>2</sub> ) <sup>2</sup> = 0.05294601	(A <sub>2</sub> ) <sup>2</sup> = 0.05294601	(A <sub>2</sub> ) <sup>2</sup> = 0.00039204	(A <sub>2</sub> ) <sup>2</sup> = 0.00039204	(A <sub>2</sub> ) <sup>2</sup> = 0.05294601
(H <sub>1</sub> ) <sup>2</sup> = 0.00279560	(H <sub>2</sub> ) <sup>2</sup> = 2.64824234	(H <sub>4</sub> ) <sup>2</sup> = 0.00009000	(H <sub>6</sub> ) <sup>2</sup> = 0.00000788	(H <sub>8</sub> ) <sup>2</sup> = 0.00000349	(H <sub>2</sub> ) <sup>2</sup> = 0.00083304	(H <sub>2</sub> ) <sup>2</sup> = 0.05471842	(H <sub>2</sub> ) <sup>2</sup> = 0.00083304	(H <sub>2</sub> ) <sup>2</sup> = 0.00083304	(H <sub>2</sub> ) <sup>2</sup> = 0.05471842	(H <sub>2</sub> ) <sup>2</sup> = 0.00083304	(H <sub>2</sub> ) <sup>2</sup> = 0.05471842	(H <sub>2</sub> ) <sup>2</sup> = 0.05471842	(H <sub>2</sub> ) <sup>2</sup> = 0.00083304	(H <sub>2</sub> ) <sup>2</sup> = 0.00083304	(H <sub>2</sub> ) <sup>2</sup> = 0.05471842
H <sub>1</sub> = 0.0529	H <sub>2</sub> = 1.6273	H <sub>4</sub> = 0.0095	H <sub>6</sub> = 0.0028	H <sub>8</sub> = 0.0019	H <sub>2</sub> = 0.0289	H <sub>2</sub> = 0.2339	H <sub>2</sub> = 0.0289	H <sub>2</sub> = 0.0289	H <sub>2</sub> = 0.2339	H <sub>2</sub> = 0.0289	H <sub>2</sub> = 0.2339	H <sub>2</sub> = 0.2339	H <sub>2</sub> = 0.0289	H <sub>2</sub> = 0.0289	H <sub>2</sub> = 0.2339
Aug <sup>in</sup> = 0.0003				Aug <sup>in</sup> = 0.0003				Aug <sup>in</sup> = 0.0003							
Aug <sup>in</sup> R <sub>2</sub> } or H <sub>2</sub> } = 0.0292				Aug <sup>in</sup> R <sub>2</sub> } or H <sub>2</sub> } = 0.0292				Aug <sup>in</sup> R <sub>2</sub> } or H <sub>2</sub> } = 0.0292							
Aug <sup>in</sup> = 0.0003				Aug <sup>in</sup> = 0.0003				Aug <sup>in</sup> = 0.0003							
Aug <sup>in</sup> = 0.0003				Aug <sup>in</sup> = 0.0003				Aug <sup>in</sup> = 0.0003							

Augmenting Factors.—For A<sub>1</sub>, B<sub>1</sub> . . . 1.00286, A<sub>2</sub>, B<sub>2</sub> . . . 1.01152, A<sub>3</sub>, B<sub>3</sub> . . . 1.02617, A<sub>4</sub>, B<sub>4</sub> . . . 1.04720,

A<sub>6</sub>, B<sub>6</sub> . . . 1.11072, A<sub>8</sub>, B<sub>8</sub> . . . 1.20920.

## FORMS FOR SHORT-PERIOD TIDES.

## EVALUATION OF SHORT-PERIOD TIDES—(Continued).

## SERIES M.

Log B <sub>1</sub> = -8.46389	Log B <sub>2</sub> = -0.33355	Log B <sub>3</sub> = -8.64640	Log B <sub>4</sub> = -8.84572	Log B <sub>5</sub> = +7.97772	Log B <sub>6</sub> = +7.38021
Log A <sub>1</sub> = -8.52114	Log A <sub>2</sub> = +0.55381	Log A <sub>3</sub> = -8.83506	Log A <sub>4</sub> = +9.01072	Log A <sub>5</sub> = -6.69897	Log A <sub>6</sub> = +7.81291
L tan ζ <sub>1</sub> = +9.94275	L tan ζ <sub>2</sub> = -9.77974	L tan ζ <sub>3</sub> = +9.81134	L tan ζ <sub>4</sub> = -9.83500	L tan ζ <sub>5</sub> = -1.27875	L tan ζ <sub>6</sub> = +9.56730
ζ <sub>1</sub> = 221.234	ζ <sub>2</sub> = 328.944	ζ <sub>3</sub> = 212.929	ζ <sub>4</sub> = 325.631	ζ <sub>5</sub> = 93.013	ζ <sub>6</sub> = 20.266
V <sub>0</sub> + u = 207.937	V <sub>0</sub> + u = 0.886	V <sub>0</sub> + u = 181.329	V <sub>0</sub> + u = 1.772	V <sub>0</sub> + u = 2.658	V <sub>0</sub> + u = 3.544
κ <sub>1</sub> = 69.171	κ <sub>2</sub> = 329.830	κ <sub>3</sub> = 34.258	κ <sub>4</sub> = 327.403	κ <sub>5</sub> = 95.671	κ <sub>6</sub> = 23.810
(B <sub>1</sub> ) <sup>2</sup> = 0.00084681	(B <sub>2</sub> ) <sup>2</sup> = 4.64618025	(B <sub>3</sub> ) <sup>2</sup> = 0.00196249	(B <sub>4</sub> ) <sup>2</sup> = 0.00491401	(B <sub>5</sub> ) <sup>2</sup> = 0.00009025	(B <sub>6</sub> ) <sup>2</sup> = 0.0000576
(A <sub>1</sub> ) <sup>2</sup> = 0.00110224	(A <sub>2</sub> ) <sup>2</sup> = 12.81210436	(A <sub>3</sub> ) <sup>2</sup> = 0.00467856	(A <sub>4</sub> ) <sup>2</sup> = 0.01050625	(A <sub>5</sub> ) <sup>2</sup> = 0.00000025	(A <sub>6</sub> ) <sup>2</sup> = 0.00004225
(R <sub>1</sub> ) <sup>2</sup> = 0.00194905	(R <sub>2</sub> ) <sup>2</sup> = 17.45828461	(R <sub>3</sub> ) <sup>2</sup> = 0.00664105	(R <sub>4</sub> ) <sup>2</sup> = 0.01542026	(R <sub>5</sub> ) <sup>2</sup> = 0.00009050	(R <sub>6</sub> ) <sup>2</sup> = 0.00004801
R <sub>1</sub> = 0.0441	R <sub>2</sub> = 4.1783	R <sub>3</sub> = 0.0815	R <sub>4</sub> = 0.1242	R <sub>5</sub> = 0.0095	R <sub>6</sub> = 0.0069
Aug <sup>th</sup> = 0.0001	Aug <sup>th</sup> = 0.0481	Aug <sup>th</sup> = 0.0021	Aug <sup>th</sup> = 0.0059	Aug <sup>th</sup> = 0.0011	Aug <sup>th</sup> = 0.0014
Aug <sup>th</sup> R <sub>1</sub> = 0.0442	Aug <sup>th</sup> R <sub>2</sub> = 4.2264	Aug <sup>th</sup> R <sub>3</sub> = 0.0836	Aug <sup>th</sup> R <sub>4</sub> = 0.1301	Aug <sup>th</sup> R <sub>5</sub> = 0.0106	Aug <sup>th</sup> R <sub>6</sub> = 0.0083
$\frac{1}{f}$ = 1.1377	$\frac{1}{f}$ = 0.9635	$\frac{1}{f}$ = 0.9458	$\frac{1}{f}$ = 0.9283	$\frac{1}{f}$ = 0.8944	$\frac{1}{f}$ = 0.8618
H <sub>1</sub> = 0.0503	H <sub>2</sub> = 4.0721	H <sub>3</sub> = 0.0791	H <sub>4</sub> = 0.1208	H <sub>5</sub> = 0.0095	H <sub>6</sub> = 0.0072

## SERIES K.

## SERIES O.

## SERIES P.

## SERIES J.

## SERIES Q.

Log B <sub>1</sub> = -9.84255	Log B <sub>2</sub> = +9.25431	Log B <sub>1</sub> = -9.66671	Log B <sub>1</sub> = -9.52673	Log B <sub>1</sub> = -8.84323	Log B <sub>1</sub> = -8.97174
Log A <sub>1</sub> = -0.00552	Log A <sub>2</sub> = -9.39620	Log A <sub>1</sub> = -9.46300	Log A <sub>1</sub> = -9.38256	Log A <sub>1</sub> = -8.62941	Log A <sub>1</sub> = -8.69108
L tan ζ <sub>1</sub> = +9.83703	L tan ζ <sub>2</sub> = -9.85811	L tan ζ <sub>1</sub> = +0.20371	L tan ζ <sub>1</sub> = +0.14417	L tan ζ <sub>1</sub> = +0.21382	L tan ζ <sub>1</sub> = +0.28066
ζ <sub>1</sub> = 214.494	ζ <sub>2</sub> = 144.197	ζ <sub>1</sub> = 237.970	ζ <sub>1</sub> = 234.340	ζ <sub>1</sub> = 238.567	ζ <sub>1</sub> = 242.345
V <sub>0</sub> + u = 191.086	V <sub>0</sub> + u = 202.175	V <sub>0</sub> + u = 169.910	V <sub>0</sub> + u = 168.897	V <sub>0</sub> + u = 207.483	V <sub>0</sub> + u = 153.403
κ <sub>1</sub> = 45.580	κ <sub>2</sub> = 346.372	κ <sub>1</sub> = 47.880	κ <sub>1</sub> = 43.237	κ <sub>1</sub> = 86.050	κ <sub>1</sub> = 35.748
(B <sub>1</sub> ) <sup>2</sup> = 0.48427681	(B <sub>2</sub> ) <sup>2</sup> = 0.03225616	(B <sub>1</sub> ) <sup>2</sup> = 0.21548164	(B <sub>1</sub> ) <sup>2</sup> = 0.11309769	(B <sub>1</sub> ) <sup>2</sup> = 0.00485809	(B <sub>1</sub> ) <sup>2</sup> = 0.00877969
(A <sub>1</sub> ) <sup>2</sup> = 1.02576384	(A <sub>2</sub> ) <sup>2</sup> = 0.06200100	(A <sub>1</sub> ) <sup>2</sup> = 0.08433216	(A <sub>1</sub> ) <sup>2</sup> = 0.05822569	(A <sub>1</sub> ) <sup>2</sup> = 0.00181476	(A <sub>1</sub> ) <sup>2</sup> = 0.00241081
(R <sub>1</sub> ) <sup>2</sup> = 1.51004065	(R <sub>2</sub> ) <sup>2</sup> = 0.09425716	(R <sub>1</sub> ) <sup>2</sup> = 0.29981380	(R <sub>1</sub> ) <sup>2</sup> = 0.17132338	(R <sub>1</sub> ) <sup>2</sup> = 0.00667285	(R <sub>1</sub> ) <sup>2</sup> = 0.01119050
R <sub>1</sub> = 1.2288	R <sub>2</sub> = 0.3070	R <sub>1</sub> = 0.5476	R <sub>1</sub> = 0.4139	R <sub>1</sub> = 0.0817	R <sub>1</sub> = 0.1058
Aug <sup>th</sup> = 0.0034	Aug <sup>th</sup> = 0.0015	Aug <sup>th</sup> = 0.0015	Aug <sup>th</sup> = 0.0012	Aug <sup>th</sup> = 0.0002	Aug <sup>th</sup> = 0.0003
Aug <sup>th</sup> R <sub>1</sub> = 1.2322	Aug <sup>th</sup> R <sub>2</sub> = 0.3105	Aug <sup>th</sup> R <sub>1</sub> = 0.5491	Aug <sup>th</sup> R <sub>1</sub> } or H <sub>1</sub> } = 0.4151	Aug <sup>th</sup> R <sub>1</sub> = 0.0819	Aug <sup>th</sup> R <sub>1</sub> = 0.1061
$\frac{1}{f}$ = 1.1342	$\frac{1}{f}$ = 1.3376	$\frac{1}{f}$ = 1.2412		$\frac{1}{f}$ = 1.2095	$\frac{1}{f}$ = 1.2412
H <sub>1</sub> = 1.3976	H <sub>2</sub> = 0.4153	H <sub>1</sub> = 0.6815		H <sub>1</sub> = 0.0991	H <sub>1</sub> = 0.1317



FORMS FOR SHORT-PERIOD TIDES.

EVALUATION OF SHORT-PERIOD TIDES—(Continued).

SERIES L.	SERIES N.	SERIES 2N.	SERIES λ.	SERIES ν.
$\text{Log } B_2 = +8.65801$	$\text{Log } B_2 = -9.73191$	$\text{Log } B_2 = -9.19117$	$\text{Log } B_2 = -7.54407$	$\text{Log } B_2 = -7.69897$
$\text{Log } A_2 = -8.04922$	$\text{Log } A_2 = +9.93822$	$\text{Log } A_2 = +8.34242$	$\text{Log } A_2 = +7.14613$	$\text{Log } A_2 = +8.72509$
$L \tan \zeta_2 = -0.60879$	$L \tan \zeta_2 = -9.79369$	$L \tan \zeta_2 = -0.84875$	$L \tan \zeta_2 = -0.39794$	$L \tan \zeta_2 = -8.97388$
$\zeta_2 = 103.829$	$\zeta_2 = 328.124$	$\zeta_2 = 278.063$	$\zeta_2 = 291.801$	$\zeta_2 = 354.621$
$V_0 + u = 201.218$	$V_0 + u = 344.379$	$V_0 + u = 327.872$	$V_0 + u = 163.475$	$V_0 + u = 18.297$
$\kappa_2 = 305.047$	$\kappa_2 = 312.503$	$\kappa_2 = 245.935$	$\kappa_2 = 95.276$	$\kappa_2 = 12.918$
$(B_2)^2 = 0.00207025$	$(B_2)^2 = 0.29095236$	$(B_2)^2 = 0.02411809$	$(B_2)^2 = 0.00001225$	$(B_2)^2 = 0.00002500$
$(A_2)^2 = 0.00012544$	$(A_2)^2 = 0.75238276$	$(A_2)^2 = 0.00048400$	$(A_2)^2 = 0.00000196$	$(A_2)^2 = 0.00281961$
$(R_2)^2 = 0.00219569$	$(R_2)^2 = 1.04333512$	$(R_2)^2 = 0.02460209$	$(R_2)^2 = 0.00001421$	$(R_2)^2 = 0.00284461$
$R_2 = 0.0469$	$R_2 = 1.0214$	$R_2 = 0.1569$	$R_2 = 0.0038$	$R_2 = 0.0533$
$\text{Aug}^{\text{th}} R_2 = 0.0005$	$\text{Aug}^{\text{th}} R_2 = 0.0117$	$\text{Aug}^{\text{th}} R_2 = 0.0018$	$\text{Aug}^{\text{th}} R_2 = 0.0000$	$\text{Aug}^{\text{th}} R_2 = 0.0006$
$\frac{1}{f} = 0.8543$	$\frac{1}{f} = 0.9635$	$\frac{1}{f} = 0.9635$	$\frac{1}{f} = 0.9635$	$\frac{1}{f} = 0.9635$
$H_2 = 0.0405$	$H_2 = 0.9954$	$H_2 = 0.1529$	$H_2 = 0.0037$	$H_2 = 0.0519$

SERIES μ OF 2MS.	SERIES 2SM.	SERIES MS.	SERIES M <sub>2</sub> N.	SERIES 2M <sub>2</sub> K <sub>1</sub> .	SERIES M <sub>2</sub> K <sub>1</sub> .
$\text{Log } B_2 = -9.24477$	$\text{Log } B_2 = +8.66181$	$\text{Log } B_4 = +8.66370$	$\text{Log } B_4 = -9.10483$	$\text{Log } B_3 = -8.71433$	$\text{Log } B_3 = -8.90472$
$\text{Log } A_2 = +8.88536$	$\text{Log } A_2 = -7.94448$	$\text{Log } A_4 = +9.09968$	$\text{Log } A_4 = -8.61172$	$\text{Log } A_3 = -8.47276$	$\text{Log } A_3 = +8.64147$
$L \tan \zeta_2 = -0.35941$	$L \tan \zeta_2 = -0.71733$	$L \tan \zeta_1 = +9.56402$	$L \tan \zeta_4 = +0.49311$	$L \tan \zeta_3 = +0.24157$	$L \tan \zeta_3 = -0.26325$
$\zeta_2 = 293.611$	$\zeta_2 = 100.853$	$\zeta_1 = 20.126$	$\zeta_4 = 252.189$	$\zeta_3 = 240.172$	$\zeta_3 = 298.610$
$V_0 + u = 1.772$	$V_0 + u = 359.114$	$V_0 + u = 0.886$	$V_0 + u = 345.265$	$V_0 + u = 170.686$	$V_0 + u = 191.972$
$\kappa_2 = 295.383$	$\kappa_2 = 99.967$	$\kappa_4 = 21.012$	$\kappa_4 = 237.454$	$\kappa_3 = 50.858$	$\kappa_3 = 130.582$
$(B_2)^2 = 0.003087049$	$(B_2)^2 = 0.00210681$	$(B_4)^2 = 0.00212521$	$(B_4)^2 = 0.01620529$	$(B_3)^2 = 0.00268324$	$(B_3)^2 = 0.00644809$
$(A_2)^2 = 0.00589824$	$(A_2)^2 = 0.00007744$	$(A_4)^2 = 0.01582564$	$(A_4)^2 = 0.00167281$	$(A_3)^2 = 0.00088209$	$(A_3)^2 = 0.00191844$
$(R_2)^2 = 0.03676873$	$(R_2)^2 = 0.00218425$	$(R_4)^2 = 0.01795085$	$(R_4)^2 = 0.01787810$	$(R_3)^2 = 0.00356533$	$(R_3)^2 = 0.00836653$
$R_2 = 0.1918$	$R_2 = 0.0467$	$R_4 = 0.1340$	$R_4 = 0.1337$	$R_3 = 0.0597$	$R_3 = 0.0915$
$\text{Aug}^{\text{th}} R_2 = 0.0022$	$\text{Aug}^{\text{th}} R_2 = 0.0005$	$\text{Aug}^{\text{th}} R_4 = 0.0063$	$\text{Aug}^{\text{th}} R_4 = 0.0063$	$\text{Aug}^{\text{th}} R_3 = 0.0016$	$\text{Aug}^{\text{th}} R_3 = 0.0024$
$\frac{1}{f} = 0.9283$	$\frac{1}{f} = 0.9635$	$\frac{1}{f} = 0.9635$	$\frac{1}{f} = 0.9283$	$\frac{1}{f} = 1.0529$	$\frac{1}{f} = 1.0928$
$H_2 = 0.1801$	$H_2 = 0.0455$	$H_4 = 0.1352$	$H_4 = 0.1300$	$H_3 = 0.0645$	$H_3 = 0.1026$

FORMS FOR LONG-PERIOD TIDES.

TIDE Mm.

$\Sigma dh \sin(\sigma - \omega) t.$

Multiplier	1-0		-9		-8		-7		-6		-5		-4		-3		-2		-1		0		
	+	-	+	-	+	-	+	-	+	-	+	-	+	-	+	-	+	-	+	-	+	-	
No. of the day																							
7 to 0	.74	.66	.65	.49	.49	.32	.32	.32	.32	.32	.32	.32	.32	.32	.32	.32	.32	.32	.32	.32	.32	.32	.32
8-13	.35	.35	.35	.18	.18	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23
34-28	.43	.43	.33	.16	.16	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
35-41	.30	.30	.05	.11	.11	.19	.19	.19	.19	.19	.19	.19	.19	.19	.19	.19	.19	.19	.19	.19	.19	.19	.19
62-56	.21	.15	.42	.38	.38	.42	.42	.42	.42	.42	.42	.42	.42	.42	.42	.42	.42	.42	.42	.42	.42	.42	.42
63-68	.07	.07	.08	.20	.20	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34
80-83	.23	.23	.23	.05	.05	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07
90-96	.19	.19	.24	.33	.33	.47	.47	.47	.47	.47	.47	.47	.47	.47	.47	.47	.47	.47	.47	.47	.47	.47	.47
117-111	.32	.28	.29	.41	.41	.53	.53	.53	.53	.53	.53	.53	.53	.53	.53	.53	.53	.53	.53	.53	.53	.53	.53
118-124	.38	.38	.27	.36	.36	.32	.32	.32	.32	.32	.32	.32	.32	.32	.32	.32	.32	.32	.32	.32	.32	.32	.32
144-138	.18	.18	.25	.16	.16	.38	.38	.38	.38	.38	.38	.38	.38	.38	.38	.38	.38	.38	.38	.38	.38	.38	.38
145-151	.29	.29	.16	.18	.18	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17
172-166	.49	.43	.50	.38	.38	.58	.58	.58	.58	.58	.58	.58	.58	.58	.58	.58	.58	.58	.58	.58	.58	.58	.58
173-179	.09	.09	.16	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18
200-193	.13	.22	.28	.28	.28	.16	.16	.16	.16	.16	.16	.16	.16	.16	.16	.16	.16	.16	.16	.16	.16	.16	.16
201-206	.34	.34	.28	.34	.34	.16	.16	.16	.16	.16	.16	.16	.16	.16	.16	.16	.16	.16	.16	.16	.16	.16	.16
227-221	.23	.23	.18	.18	.18	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07
228-234	.24	.24	.31	.50	.50	.29	.29	.29	.29	.29	.29	.29	.29	.29	.29	.29	.29	.29	.29	.29	.29	.29	.29
255-248	.07	.05	.28	.37	.37	.47	.47	.47	.47	.47	.47	.47	.47	.47	.47	.47	.47	.47	.47	.47	.47	.47	.47
256-261	.07	.07	.24	.31	.31	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28
282-276	.05	.05	.16	.25	.25	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24
283-289	.15	.09	.10	.09	.09	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24
310-304	.19	.27	.08	.05	.05	.11	.11	.11	.11	.11	.11	.11	.11	.11	.11	.11	.11	.11	.11	.11	.11	.11	.11
311-316	.27	.27	.23	.07	.07	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
337-331	.05	.05	.05	.04	.04	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17
338-344	.01	.01	.10	.12	.12	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07
364-350	.17	.17	.17	.16	.16	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17
Total $\alpha$	5.16	2.94	3.84	2.80	2.50	2.81	1.97	0.99	1.91	2.20	1.53	1.27	1.63	1.32	1.34	0.77	0.59	1.96	1.60	0.94	1.60	0.94	1.60
	+3.22		+0.95		-0.31		+0.98		-0.59		+0.66		+0.31		+0.57		-1.37		+0.66		+0.66		+0.66

→	20 to 14	'07	.	'12	.	'21	.	'02	.	'00	.	'07	.	'02	←						
→	21-27	'26	'39	'39	.	'35	.	'23	.	'09	.	'08	.	'20	←						
	48-42	.	'42	'35	'24	'27	'34	'18	'28	'37	'46	'02	'29	←							
→	49-55	'15	'07	'15	'28	'37	'24	'22	'02	'55	'16	'03	'03	←							
	76-69	'36	'28	'53	'34	'19	'54	'53	'55	'20	'16	'05	'05	←							
→	77-82	'12	'02	'19	'27	'29	'20	'01	'00	'00	'03	'03	'03	←							
	103-97	'34	'10	'12	'27	'29	'20	'01	'00	'00	'03	'03	'03	←							
→	104-110	'41	'29	'05	'02	'12	'29	'20	'01	'00	'03	'03	'03	←							
	131-125	'02	'10	'09	'13	'00	'10	'30	'03	'03	'03	'03	'03	←							
→	132-137	'28	'45	'53	'51	'31	'13	'03	'03	'03	'03	'03	'03	←							
	158-152	1'78	'92	'67	'46	'31	'13	'03	'03	'03	'03	'03	'03	←							
→	159-165	1'93	1'34	'77	'34	'16	'12	'04	'04	'04	'04	'04	'04	←							
	186-180	'15	'17	'19	'41	'61	'58	'59	'59	'59	'59	'59	'59	←							
→	187-192	'26	'17	'36	'50	'58	'59	'59	'59	'59	'59	'59	'59	←							
	213-207	'14	'17	'36	'50	'58	'59	'59	'59	'59	'59	'59	'59	←							
→	214-220	'11	'10	'04	'01	'10	'08	'02	'02	'02	'02	'02	'02	←							
	241-235	'20	'47	'40	'45	'56	'31	'27	'27	'27	'27	'27	'27	←							
→	241-235	'13	'14	'10	'16	'07	'09	'09	'09	'09	'09	'09	'09	←							
	242-247	'09	'14	'10	'16	'07	'09	'09	'09	'09	'09	'09	'09	←							
→	242-247	'18	'03	'16	'19	'25	'17	'17	'17	'17	'17	'17	'17	←							
	268-262	'24	'22	'28	'25	'36	'42	'21	'18	'18	'18	'18	'18	←							
→	269-275	'18	'16	'16	'05	'07	'21	'18	'18	'18	'18	'18	'18	←							
	296-290	'02	'06	'06	'07	'02	'05	'05	'05	'05	'05	'05	'05	←							
→	297-303	'01	'06	'06	'07	'02	'05	'05	'05	'05	'05	'05	'05	←							
	324-317	'05	'09	'05	'15	'17	'21	'21	'21	'21	'21	'21	'21	←							
→	324-317	'39	'09	'04	'13	'17	'21	'21	'21	'21	'21	'21	'21	←							
	325-330	'58	'09	'04	'13	'17	'21	'21	'21	'21	'21	'21	'21	←							
→	325-330	'80	'68	'64	'58	'46	'30	'20	'15	'15	'15	'15	'15	←							
	351-345	'23	'24	'32	'30	'20	'15	'15	'15	'15	'15	'15	'15	←							
→	351-345	'07	'07	'19	'33	'35	'52	'33	'33	'33	'33	'33	'33	←							
	352-358	'19	'07	'19	'33	'35	'52	'33	'33	'33	'33	'33	'33	←							
	Total $\delta$	4'85	5'97	4'36	3'63	2'27	2'39	2'38	1'65	1'24	2'86	2'38	1'40	0'97	2'13	1'34	1'02	0'69	1'68	1'25	0'68
	$a-\delta$	-1'12	+0'73	-0'12	+0'73	-1'62	+0'98	-1'16	+0'32	-0'99	+0'57	-0'99	+0'57	-0'99	+0'57	-0'99	+0'57	-0'99	+0'57	-0'99	+0'57
	$(a-\delta) \times \text{Mult.}$	+3'34	+0'22	-0'19	+0'25	+1'33	-0'92	+1'47	+0'25	-0'38	+0'09	+0'09	+0'09	+0'09	+0'09	+0'09	+0'09	+0'09	+0'09	+0'09	+0'09
		-	-	-0'15	-	-	-0'46	-	-	-0'08	-	-	-	-	-	-	-	-	-	-	-

$$\sum (a-\delta) \times \text{Mult.} = + 5'19$$

$$\sum (a-\delta) \times \text{Mult.} = - 0'69$$

$$\sum d\delta \sin(\sigma - \omega) t = \sum_{374}^0 (a-\delta) \times \text{Mult.} = + 4'50$$

NOTE.—The arrows show the direction of the sequence of the entries of  $d\delta$  in the columns in which points are inserted, the values being entered under their proper signs—e.g., in the first row (marked 7 to 0) with arrow from right to left, the entry (irrespective of sign) for day 0 is to be entered in column 0, for day 1 in column 2, for day 2 in column 4, and so on. After filling in the first two rows of the upper half, the first two rows of the lower half are to be filled, and so on alternately, the alternation of entry being indicated by the curved arrows. In the spaces containing double points two successive entries are to be filled in—the first entry above, the second below; e.g., in row 7 to 0, column 1-0, there are double points, and the entry of  $d\delta$  for day 6 is to be made above the line and to left or right according as it is + or -, and for day 7 it is to be made below the line, and to left or right according as it is + or -.



1310	.22	.22	.23	.18	.25	.12	.05	.35	.07	.66								
14-20	.02	.00	.21	.11	.12	.05	.30	.07	.30									
41-85	.43	.37	.19	.24	.11	.05	.42	.30	.35									
42-48	.20	.18	.27	.24	.24	.08	.07	.07										
68-63	.06	.27	.34	.20	.34	.53	.24	.36										
69-75	.03	.22	.24	.34	.33	.27	.12	.19										
96-90	.10	.23	.36	.10	.10	.27	.38	.19										
97-103	.16	.20	.29	.41	.27	.09	.02	.34										
124-118	.13	.07	.24	.13	.16	.16	.24	.29										
125-130	.00	.10	.00	.09	.67	.16	.92	.178										
151-145	.05	.05	.04	.46	.38	.17	.24	.29										
152-158	.03	.13	.31	.51	.28	.17	.34	.09										
179-173	.54	.63	.44	.16	.04	.31	.10	.11										
180-186	.58	.61	.41	.19	.28	.17	.34	.24										
206-200	.16	.15	.16	.16	.28	.17	.10	.15										
207-213	.02	.08	.10	.01	.04	.22	.10	.11										
234-228	.22	.13	.13	.29	.31	.09	.10	.24										
235-241	.09	.07	.16	.50	.14	.14	.02	.13										
261-255	.25	.18	.18	.31	.24	.23	.10	.07										
262-268	.21	.36	.28	.25	.22	.09	.10	.27										
289-283	.42	.21	.22	.24	.09	.23	.02	.39										
290-296	.10	.10	.07	.06	.06	.12	.07	.01										
316-311	.02	.01	.07	.07	.23	.09	.10	.23										
317-323	.09	.17	.13	.04	.12	.09	.10	.01										
344-338	.22	.15	.16	.07	.24	.23	.07	.23										
345-351	.15	.15	.30	.32	.24	.07	.07	.23										
Total $b$	1'72	4'00	2'10	3'44	2'51	2'20	2'04	1'13	1'15	2'19	0'88	1'79	1'84	0'88	0'59	1'69	2'70	1'25
$a-b$	-2'28	+1'31	+2'00	-1'34	+0'31	-0'04	-0'11	-0'08	-1'04	-0'90	+0'04	+0'55	+1'57	+0'77	-1'10	+0'96	+1'45	+0'96
$(a-b) \times \text{Mult.}$	+1'31	+1'80	+1'80	-	-0'03	-	-0'08	-0'54	-	-	-	-	-	-	-	-	-	-

$$\Sigma(a-b) \times \text{Mult.} = +4.05 \quad \Sigma(a-b) \times \text{Mult.} = -0.80 \quad \Sigma \delta b \cos(\sigma - \omega) t = \Sigma_{\text{day}}(a-b) \times \text{Mult.} = +3.25$$

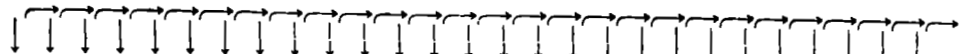
Note.—The arrows show the direction of the sequence of the entries of  $\delta b$  in the columns in which points are inserted, the values being entered under their proper signs— $a, b$ , in the first row (marked 0 to 6) with arrow from left to right, the entries for day 0 and for day 1 are to be entered in column 1.0, for day 2 in column .9, for day 3 in column .8, and so on. After filling in the first row of the upper half, the first two rows of the lower half are to be filled, and so on alternately, the alternation of entry being indicated by the curved arrows. In the spaces containing double points two successive entries are to be filled in—the first entry above, the second below;  $a, b$ , in row 0 to 6, column 1.0, there are double points, and the entry of  $\delta b$  for day 0 is to be made above the line and to left or right according as it is + or -, and for day 1 it is to be made below the line, and to left or right according as it is + or -. The entries in column 0 are made irrespective of sign.

FORMS FOR LONG-PERIOD TIDES.

TIDE Mf.

$\sum dh \sin 2\sigma t.$

Multiplier	1.0		.9		.8		.7		.6		.5		.4		.3		.2		.1		0	
	+	-	+	-	+	-	+	-	+	-	+	-	+	-	+	-	+	-	+	-	+	-
310-0	.12	.	.	.	.36	.	.65	.	.	.	.	.03	.	.74	.	.	.	.	.	.	.	.03
4-14	.40	.02	.	.00	.	.07	.	.	.	.07	.	.	.	.	.	.	.	.	.	.	.	.
14-20	.	.21	.	.21	.	.12	.	.	.	.12	.	.	.	.	.	.	.	.	.	.	.	.
31-29	.	.08	.	.04	.16	.18	.	.11	.	.	.	.33	.	.	.13	.	.	.	.	.	.	.
32-31	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
41-41	.	.14	.	.14	.	.14	.	.14	.	.20	.	.	.	.	.	.	.	.	.	.	.	.
45-47	.	.17	.	.18	.	.18	.	.18	.	.42	.	.	.	.	.	.	.	.	.	.	.	.
58-55	.	.39	.	.28	.	.42	.	.08	.	.	.	.	.	.	.	.	.	.	.	.	.	.
59-61	.	.38	.	.38	.	.34	.	.08	.	.	.	.	.	.	.	.	.	.	.	.	.	.
72-69	.	.24	.	.22	.18	.34	.	.	.	.	.	.53	.	.	.	.	.	.	.	.	.	.
73-75	.	.10	.	.	.18	.34	.	.	.	.	.	.33	.	.	.	.	.	.	.	.	.	.
85-82	.10	.	.	.	.	.	.05	.	.	.16	.	.	.	.93	.	.	.	.	.	.	.	.
86-88	.07	.	.	.10	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
90-96	.59	.	.	.17	.	.	.	.	.	.10	.	.	.	.	.	.	.	.	.	.	.	.
100-102	.	.00	.	.15	.	.	.	.	.	.10	.	.	.	.	.	.	.	.	.	.	.	.
113-110	.	.00	.	.15	.	.	.13	.	.	.10	.	.	.	.	.	.	.	.	.	.	.	.
114-116	.	.10	.	.15	.	.	.13	.	.	.10	.	.	.	.	.	.	.	.	.	.	.	.
125-123	.00	.	.	.07	.	.00	.13	.	.	.04	.36	.	.	.	.	.	.	.	.	.	.	.
127-120	.00	.	.	.07	.	.04	.13	.	.	.04	.36	.	.	.	.	.	.	.	.	.	.	.
141-137	.31	.	.	.13	.46	.	.03	.	.	.	.	.67	.	.	.	.	.	.	.	.	.	.
151-151	.43	.	.	.58	.36	.	.03	.	.	.	.	.04	.36	.	.	.	.	.	.	.	.	.
155-157	.	.61	.	.58	.36	.	.03	.	.	.	.	.04	.36	.	.	.	.	.	.	.	.	.
167-164	.	.41	.	.41	.36	.	.53	.	.	.	.	.04	.36	.	.	.	.	.	.	.	.	.
168-170	.	.41	.	.41	.36	.	.53	.	.	.	.	.04	.36	.	.	.	.	.	.	.	.	.
181-179	.	.03	.	.35	.17	.03	.47	.	.	.	.	.18	.	.	.	.	.	.	.	.	.	.
182-184	.	.03	.	.35	.17	.03	.47	.	.	.	.	.18	.	.	.	.	.	.	.	.	.	.
195-192	.08	.	.	.10	.16	.03	.01	.	.	.	.	.18	.	.	.	.	.	.	.	.	.	.
208-205	.08	.	.	.10	.16	.03	.01	.	.	.	.	.18	.	.	.	.	.	.	.	.	.	.
209-211	.07	.	.	.14	.16	.03	.01	.	.	.	.	.16	.	.	.	.	.	.	.	.	.	.
222-210	.09	.	.	.14	.16	.03	.01	.	.	.	.	.16	.	.	.	.	.	.	.	.	.	.
235-233	.07	.	.	.30	.16	.04	.23	.	.	.	.	.10	.	.	.	.	.	.	.	.	.	.
236-239	.07	.	.	.30	.16	.04	.23	.	.	.	.	.10	.	.	.	.	.	.	.	.	.	.
240-246	.	.42	.	.36	.43	.10	.47	.	.	.	.	.17	.	.	.	.	.	.	.	.	.	.
250-252	.	.48	.	.36	.43	.10	.47	.	.	.	.	.17	.	.	.	.	.	.	.	.	.	.
263-200	.47	.	.	.42	.43	.10	.47	.	.	.	.	.21	.	.	.	.	.	.	.	.	.	.
276-274	.47	.	.	.42	.43	.10	.47	.	.	.	.	.21	.	.	.	.	.	.	.	.	.	.
277-280	.47	.	.	.42	.43	.10	.47	.	.	.	.	.21	.	.	.	.	.	.	.	.	.	.
290-287	.05	.	.	.02	.43	.10	.07	.	.	.	.	.21	.22	.	.	.	.	.	.	.	.	.
291-293	.13	.	.	.15	.43	.10	.07	.	.	.	.	.21	.22	.	.	.	.	.	.	.	.	.
304-301	.09	.	.	.15	.43	.10	.07	.	.	.	.	.21	.22	.	.	.	.	.	.	.	.	.
305-307	.09	.	.	.15	.43	.10	.07	.	.	.	.	.21	.22	.	.	.	.	.	.	.	.	.
317-315	.09	.	.	.15	.43	.10	.07	.	.	.	.	.21	.22	.	.	.	.	.	.	.	.	.
318-321	.22	.	.	.13	.17	.20	.02	.	.	.	.	.13	.46	.	.	.	.	.	.	.	.	.
321-328	.15	.	.	.15	.17	.20	.02	.	.	.	.	.13	.46	.	.	.	.	.	.	.	.	.
322-324	.15	.	.	.15	.17	.20	.02	.	.	.	.	.13	.46	.	.	.	.	.	.	.	.	.
345-342	.33	.	.	.20	.08	.30	.52	.	.	.	.	.08	.46	.	.	.	.	.	.	.	.	.
346-348	.33	.	.	.20	.08	.30	.52	.	.	.	.	.08	.46	.	.	.	.	.	.	.	.	.
358-356	.19	.	.	.19	.13	.13	.52	.	.	.	.	.08	.46	.	.	.	.	.	.	.	.	.
359-362	.19	.	.	.19	.13	.13	.52	.	.	.	.	.08	.46	.	.	.	.	.	.	.	.	.
Total a	3.73	3.69	2.21	4.23	2.27	1.11	2.17	1.84	1.27	2.56	2.18	1.57	1.34	1.15	1.11	1.10	1.01	2.12	0.74	1.15	0.74	1.15
	+0.04		-2.02		+1.16		+0.33		-1.29		+0.61		+0.19		-0.08		-1.11		-0.41		-0.41	



10	.18	.33	.22	.35	.30	.35	.30	.35	.23	.26	.66									
11	.35	.39	.05	.09	.09	.22	.39	.22	.23	.26	.08									
21	.11	.19	.37	.07	.07	.05	.37	.15	.37	.15	.35									
31	.28	.34	.47	.28	.12	.36	.37	.19	.28	.46	.06									
41	.02	.34	.02	.02	.41	.36	.07	.19	.23	.15	.23									
51	.27	.47	.29	.28	.12	.36	.37	.19	.23	.34	.01									
61	.45	.35	.45	.38	.12	.36	.37	.19	.23	.34	.01									
71	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
81	.34	.34	.34	.34	.12	.36	.37	.19	.23	.34	.01									
91	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
100	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
110	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
120	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
130	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
140	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
150	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
160	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
170	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
180	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
190	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
200	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
210	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
220	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
230	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
240	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
250	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
260	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
270	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
280	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
290	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
300	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
310	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
320	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
330	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
340	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
350	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
360	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
370	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
380	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
390	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
400	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
410	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
420	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
430	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
440	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
450	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
460	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
470	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
480	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
490	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
500	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
510	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
520	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
530	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
540	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
550	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
560	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
570	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
580	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
590	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
600	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
610	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
620	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
630	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
640	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
650	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
660	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
670	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
680	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
690	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
700	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
710	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
720	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
730	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
740	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
750	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
760	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
770	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
780	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
790	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
800	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
810	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
820	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
830	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
840	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
850	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
860	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
870	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
880	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
890	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
900	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
910	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
920	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
930	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
940	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
950	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
960	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
970	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
980	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
990	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
1000	.16	.09	.16	.09	.12	.36	.37	.19	.23	.34	.01									
Total	5.05	4.44	2.83	3.31	4.48	2.40	1.38	2.95	1.06	1.12	1.36	1.10	3.54	2.31	1.40	1.83	0.48	0.77	1.91	1.66
$a-b$	+0.61	-0.57	-0.48	-0.48	+2.08	-0.92	-1.57	+1.90	-0.06	-1.23	+0.26	+0.35	+1.23	-0.43	-0.29	-0.43	-0.29	+0.25	+0.25	+0.25
$(a-b) \times \text{Mult.}$	+ .39	- .33	- .33	- .33	+ .84	- .46	- .74	+ .74	- .07	- .82	+ .26	+ .35	+ .82	- .18	- .18	- .18	- .18	+ .66	+ .66	+ .66
$\sum (a-b) \times \text{Mult.} = + 1.61$																				
$\sum (a-b) \times \text{Mult.} = - 4.09$																				
$\sum (a-b) \times \text{Mult.} = 2.34$																				
$\sum (a-b) \times \text{Mult.} = - 2.48$																				

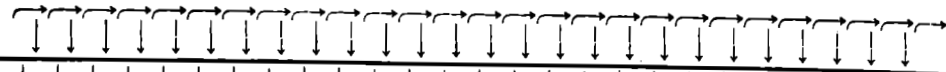
$\sum (a-b) \times \text{Mult.} = + 1.61$      $\sum (a-b) \times \text{Mult.} = - 4.09$      $\sum (a-b) \times \text{Mult.} = 2.34$      $\sum (a-b) \times \text{Mult.} = - 2.48$

FORMS FOR LONG-PERIOD TIDES.

TIDE Mf.

$\Sigma dh \cos 2\sigma t.$

Multiplier No. of the day	1.0		.9		.8		.7		.6		.5		.4		.3		.2		.1		0	
	+	-	+	-	+	-	+	-	+	-	+	-	+	-	+	-	+	-	+	-	+	-
0 to 3	.03	.	.03	.	.	.	.22	.	.16	.	.	.00	.	.23	.	.32	.	.	.	.	.	.
14-11	.02	.	.22	.	.07	.	.	.	.	.	.33	.	.	.	.	.	.	.	.	.	.	.02
15-17	.	.08	.	.13	.09	.	.11	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.35
27-24	.	.	.	.37	.	.20	.	.37	.	.	.	.	.	.	.	.	.	.	.	.	.	.
28-30	.	.43	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
41-38	.	.	.	.20	.	.20	.	.02	.	.	.	.	.	.	.	.	.	.	.	.	.	.
42-44	.	.46	.	.	.27	.	.36	.	.54	.	.34	.	.47	.	.19	.	.19	.	.	.	.	.30
54-52	.	.19	.	.	.	.	.	.	.18	.	.	.	.	.	.10	.	.34	.	.	.	.	.20
68-65	.06	.	.03	.	.27	.	.02	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
69-71	.	.	.53	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
82-79	.55	.	.32	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
83-85	.	.33	.	.	.16	.	.36	.	.18	.	.	.	.	.	.	.	.	.	.	.	.	.
95-93	.33	.	.	.	.16	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
96-99	.10	.	.01	.	.12	.	.13	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
109-106	.	.01	.	.05	.12	.	.13	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
110-112	.	.13	.	.24	.	.	.51	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
123-120	.	.07	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
124-126	.02	.	.30	.	.04	.	.03	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
136-134	.	.03	.	.03	.04	.	.04	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
137-140	.05	.	.05	.	.	.	.03	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
150-147	.	.12	.	.16	.	.16	.	.03	.	.	.	.	.	.	.	.	.	.	.	.	.	.
151-153	.	.	.04	.	.12	.	.13	.	.34	.	.09	.	.07	.	.10	.	.41	.	.	.	.	.
164-161	.12	.	.16	.	.04	.	.51	.	.26	.	.	.	.	.	.	.	.	.	.	.	.	.
165-167	.	.14	.	.04	.	.50	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
177-175	.	.54	.	.59	.	.63	.	.47	.	.	.	.	.	.	.	.	.	.	.	.	.	.
178-181	.	.58	.	.	.50	.	.	.45	.	.	.	.	.	.	.	.	.	.	.	.	.	.
191-188	.	.	.16	.	.	.27	.	.	.16	.	.36	.	.	.	.	.	.	.	.	.	.	.
192-194	.15	.	.16	.	.	.45	.	.	.02	.	.	.	.	.	.	.	.	.	.	.	.	.
205-202	.	.16	.	.16	.	.	.23	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
206-208	.56	.	.16	.	.	.45	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
218-216	.	.31	.	.22	.	.27	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
219-221	.31	.	.22	.	.29	.	.23	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
232-229	.13	.	.22	.	.29	.	.23	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
233-235	.25	.	.19	.	.29	.	.23	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
246-243	.	.28	.	.17	.	.31	.	.18	.	.	.	.	.	.	.	.	.	.	.	.	.	.
247-249	.	.18	.	.17	.	.25	.	.18	.	.	.	.	.	.	.	.	.	.	.	.	.	.
250-257	.	.07	.	.21	.	.05	.	.18	.	.	.	.	.	.	.	.	.	.	.	.	.	.
260-262	.	.21	.	.24	.	.05	.	.18	.	.	.	.	.	.	.	.	.	.	.	.	.	.
273-270	.	.21	.	.22	.	.05	.	.18	.	.	.	.	.	.	.	.	.	.	.	.	.	.
274-276	.	.21	.	.22	.	.05	.	.18	.	.	.	.	.	.	.	.	.	.	.	.	.	.
288-290	.15	.	.21	.	.05	.	.09	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
297-284	.17	.	.21	.	.07	.	.02	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
300-298	.	.03	.	.01	.	.07	.	.02	.	.	.	.	.	.	.	.	.	.	.	.	.	.
301-303	.	.58	.	.40	.	.07	.	.02	.	.	.	.	.	.	.	.	.	.	.	.	.	.
314-311	.	.07	.	.19	.	.08	.	.02	.	.	.	.	.	.	.	.	.	.	.	.	.	.
315-317	.	.33	.	.35	.	.12	.	.68	.	.	.	.	.	.	.	.	.	.	.	.	.	.
328-325	.	.16	.	.19	.	.08	.	.52	.	.	.	.	.	.	.	.	.	.	.	.	.	.
329-331	.	.16	.	.19	.	.08	.	.52	.	.	.	.	.	.	.	.	.	.	.	.	.	.
341-339	.	.16	.	.19	.	.08	.	.52	.	.	.	.	.	.	.	.	.	.	.	.	.	.
342-344	.	.16	.	.19	.	.08	.	.52	.	.	.	.	.	.	.	.	.	.	.	.	.	.
353-352	.	.16	.	.19	.	.08	.	.52	.	.	.	.	.	.	.	.	.	.	.	.	.	.
356-358	.	.16	.	.19	.	.08	.	.52	.	.	.	.	.	.	.	.	.	.	.	.	.	.
Total a	3.18	4.00	2.54	3.71	1.65	2.17	1.62	3.28	1.92	0.87	1.27	1.51	1.44	2.18	1.16	2.02	2.22	1.04	0.30	1.48	0.30	1.48
	-1.72		-1.17		-0.53		-1.66		+1.05		-0.24		-0.74		-0.86		+1.18		-1.09			





7 to 4																				
8-10																				
20-18																				
21-23																				
34-31																				
35-37																				
48-45																				
49-51																				
61-59																				
62-64																				
75-72																				
76-78																				
89-86																				
90-92																				
102-100																				
103-105																				
116-113																				
117-119																				
130-127																				
131-136																				
143-141																				
144-145																				
157-154																				
158-160																				
171-168																				
172-174																				
184-182																				
185-187																				
198-195																				
199-201																				
212-209																				
213-215																				
225-222																				
226-228																				
239-236																				
240-242																				
253-250																				
254-256																				
261-263																				
267-269																				
280-277																				
281-283																				
294-291																				
295-297																				
307-304																				
308-310																				
321-318																				
322-324																				
335-332																				
336-338																				
348-345																				
349-351																				
362-359																				
363-364																				
Total b	4.63	3.67	6.44	2.70	1.69	2.21	1.93	1.72	3.68	1.19	1.35	1.10	0.98	2.31	1.20	1.38	2.64	1.22	1.29	1.15
a-b	+0.96	-2.68	+3.74	-4.91	-0.52	-0.00	+0.21	-1.87	+2.49	-1.44	+0.25	-0.49	+0.59	-1.33	-0.18	+0.68	+1.42	-0.24	+0.14	-1.23
(a-b) × Mult.	+ .	-2.68	+ .	-4.91	-0.52	-0.00	+0.21	-1.87	+2.49	-1.44	+0.25	-0.49	+0.59	-1.33	-0.18	+0.68	+1.42	-0.24	+0.14	-1.23

$$\sum a^2 \cos 2\alpha t = \sum_{j=0}^n a^2 \times \text{Mult.} = -9.65$$

$$\sum (a-b) \times \text{Mult.} = -9.89$$

$$\sum (a-b) \times \text{Mult.} = +0.24$$



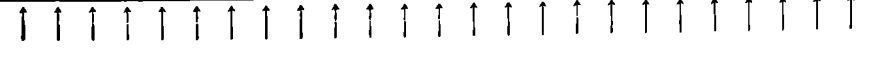
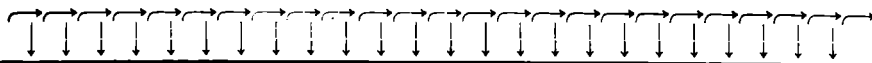


FORMS FOR LONG-PERIOD TIDES.

TIDE MSf.

$\Sigma \delta h \cos 2(\sigma - \eta) t.$

Multiplier	1.0		.9		.8		.7		.6		.5		.4		.3		.2		.1		0	
	+	-	+	-	+	-	+	-	+	-	+	-	+	-	+	-	+	-	+	-	+	-
No. of the day																						
0 to 8	.03	.07	.03	.	.26	.	.26	.	.	.	.26	.	.22	.	.32	.	.	.	.	.	.	.
16-18	.02	.00	.02	.	.22	.	.22	.	.	.	.22	.	.16	.	.08	.	.21	.	.09	.	.33	.
20-26	.11	.04	.13	.08	.18	.18	.24	.24	.28	.28	.24	.16	.08	.42	.20	.15	.43	.20	.33	.43	.20	.15
30-33	.34	.27	.39	.38	.42	.34	.34	.30	.28	.28	.24	.10	.05	.22	.15	.12	.12	.12	.23	.27	.23	.10
44-47	.53	.30	.05	.19	.12	.29	.41	.10	.51	.29	.05	.04	.05	.07	.05	.29	.29	.29	.33	.27	.33	.02
59-56	.23	.23	.34	.12	.29	.28	.24	.04	.38	.38	.32	.38	.38	.24	.04	.24	.29	.29	.05	.27	.05	.18
60-62	.34	.38	.28	.27	.41	.10	.53	.24	.51	.51	.32	.38	.38	.24	.04	.24	.29	.29	.05	.27	.05	.18
71-71	.45	.45	.28	.27	.41	.10	.53	.24	.51	.51	.32	.38	.38	.24	.04	.24	.29	.29	.05	.27	.05	.18
73-77	.16	.09	.16	.04	.24	.04	.24	.04	.38	.38	.32	.38	.38	.24	.04	.24	.29	.29	.05	.27	.05	.18
88-85	.34	.16	.77	.12	.12	.12	.12	.12	.12	.12	.12	.12	.12	.12	.12	.12	.12	.12	.12	.12	.12	.12
89-92	.16	.16	.12	.12	.12	.12	.12	.12	.12	.12	.12	.12	.12	.12	.12	.12	.12	.12	.12	.12	.12	.12
103-100	.44	.44	.54	.54	.63	.63	.50	.50	.35	.35	.10	.10	.05	.05	.29	.29	.29	.29	.05	.27	.05	.18
104-107	.59	.59	.58	.58	.50	.50	.47	.47	.35	.35	.10	.10	.05	.05	.29	.29	.29	.29	.05	.27	.05	.18
118-115	.02	.02	.16	.08	.15	.15	.15	.15	.10	.10	.31	.31	.07	.16	.03	.03	.01	.01	.56	.18	.56	.18
119-121	.24	.07	.08	.08	.10	.10	.08	.08	.10	.10	.31	.31	.07	.16	.03	.03	.01	.01	.56	.18	.56	.18
133-130	.07	.07	.09	.16	.14	.14	.14	.14	.23	.23	.23	.23	.07	.14	.04	.04	.22	.22	.18	.18	.18	.26
147-144	.47	.47	.16	.48	.10	.10	.10	.10	.23	.23	.23	.23	.07	.14	.04	.04	.22	.22	.18	.18	.18	.26
148-151	.34	.16	.16	.16	.10	.10	.10	.10	.23	.23	.23	.23	.07	.14	.04	.04	.22	.22	.18	.18	.18	.26
162-150	.47	.47	.37	.37	.28	.28	.28	.28	.23	.23	.23	.23	.07	.14	.04	.04	.22	.22	.18	.18	.18	.26
177-174	.28	.28	.25	.25	.36	.36	.36	.36	.24	.24	.24	.24	.08	.08	.08	.08	.64	.64	.05	.05	.05	.10
178-180	.25	.25	.25	.25	.36	.36	.36	.36	.24	.24	.24	.24	.08	.08	.08	.08	.64	.64	.05	.05	.05	.10
182-189	.25	.25	.25	.25	.36	.36	.36	.36	.24	.24	.24	.24	.08	.08	.08	.08	.64	.64	.05	.05	.05	.10
193-195	.25	.25	.25	.25	.36	.36	.36	.36	.24	.24	.24	.24	.08	.08	.08	.08	.64	.64	.05	.05	.05	.10
207-204	.02	.02	.16	.08	.15	.15	.15	.15	.10	.10	.31	.31	.07	.16	.03	.03	.01	.01	.56	.18	.56	.18
211-219	.24	.07	.08	.08	.10	.10	.10	.10	.10	.10	.31	.31	.07	.16	.03	.03	.01	.01	.56	.18	.56	.18
223-225	.07	.07	.09	.16	.14	.14	.14	.14	.23	.23	.23	.23	.07	.14	.04	.04	.22	.22	.18	.18	.18	.26
230-233	.47	.47	.16	.48	.10	.10	.10	.10	.23	.23	.23	.23	.07	.14	.04	.04	.22	.22	.18	.18	.18	.26
231-239	.47	.47	.16	.48	.10	.10	.10	.10	.23	.23	.23	.23	.07	.14	.04	.04	.22	.22	.18	.18	.18	.26
251-248	.28	.28	.25	.25	.36	.36	.36	.36	.24	.24	.24	.24	.08	.08	.08	.08	.64	.64	.05	.05	.05	.10
252-254	.25	.25	.25	.25	.36	.36	.36	.36	.24	.24	.24	.24	.08	.08	.08	.08	.64	.64	.05	.05	.05	.10
268-263	.25	.25	.25	.25	.36	.36	.36	.36	.24	.24	.24	.24	.08	.08	.08	.08	.64	.64	.05	.05	.05	.10
267-269	.25	.25	.25	.25	.36	.36	.36	.36	.24	.24	.24	.24	.08	.08	.08	.08	.64	.64	.05	.05	.05	.10
280-277	.25	.25	.25	.25	.36	.36	.36	.36	.24	.24	.24	.24	.08	.08	.08	.08	.64	.64	.05	.05	.05	.10
281-284	.02	.02	.16	.08	.15	.15	.15	.15	.10	.10	.31	.31	.07	.16	.03	.03	.01	.01	.56	.18	.56	.18
295-292	.01	.01	.06	.06	.05	.05	.05	.05	.08	.08	.08	.08	.08	.09	.09	.09	.09	.58	.58	.08	.08	.08
296-299	.01	.01	.06	.06	.05	.05	.05	.05	.08	.08	.08	.08	.08	.09	.09	.09	.09	.58	.58	.08	.08	.08
310-307	.19	.19	.00	.00	.23	.23	.23	.23	.39	.39	.16	.16	.19	.05	.05	.52	.52	.08	.08	.23	.33	.33
311-313	.80	.80	.58	.58	.39	.39	.39	.39	.64	.64	.16	.16	.19	.05	.05	.52	.52	.08	.08	.23	.33	.33
325-322	.10	.10	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07
326-328	.12	.12	.19	.19	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07
330-336	.12	.12	.19	.19	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07
340-343	.19	.19	.33	.33	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35
354-351	.33	.33	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35
355-358	.33	.33	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35	.35
Total $\alpha$	1.98	6.93	0.54	7.91	1.80	1.64	0.78	3.59	0.23	3.70	2.83	0.55	0.64	2.68	0.34	1.32	0.29	2.28	4.29	0.33	4.29	0.33
	-4.95		-7.37		+0.16		-2.81		-3.47		+2.28		-2.04		-0.98		-1.99		+3.96			



7 to 8	.66	.74	.65	.18	.49	.23	
8	.13	.25	.08	.15	.12	.35	
9	.39	.07	.03	.18	.02	.07	
23-25	.11	.30	.03	.12	.03	.01	
26-28	.15	.19	.08	.18	.09	.07	
29-31	.28	.37	.03	.12	.11	.01	
32-34	.34	.07	.03	.13	.13	.24	
35-37	.27	.37	.03	.13	.03	.09	
38-40	.53	.06	.03	.13	.03	.24	
41-43	.16	.32	.03	.13	.03	.09	
44-46	.13	.01	.03	.13	.03	.24	
47-49	.00	.07	.03	.13	.03	.09	
50-52	.07	.36	.03	.13	.03	.24	
53-55	.46	.31	.03	.13	.03	.09	
56-58	.56	.58	.03	.13	.03	.24	
59-61	.17	.19	.03	.13	.03	.09	
62-64	.15	.26	.03	.13	.03	.24	
65-67	.22	.34	.03	.13	.03	.09	
68-70	.20	.11	.03	.13	.03	.24	
71-73	.31	.47	.03	.13	.03	.09	
74-76	.03	.24	.03	.13	.03	.24	
77-79	.16	.50	.03	.13	.03	.09	
80-82	.31	.18	.03	.13	.03	.24	
83-85	.03	.18	.03	.13	.03	.09	
86-88	.16	.19	.03	.13	.03	.24	
89-91	.28	.34	.03	.13	.03	.09	
92-94	.20	.11	.03	.13	.03	.24	
95-97	.31	.47	.03	.13	.03	.09	
98-100	.03	.24	.03	.13	.03	.24	
101-103	.16	.50	.03	.13	.03	.09	
104-106	.31	.18	.03	.13	.03	.24	
107-109	.03	.18	.03	.13	.03	.09	
110-112	.16	.19	.03	.13	.03	.24	
113-115	.28	.34	.03	.13	.03	.09	
116-118	.20	.11	.03	.13	.03	.24	
119-121	.31	.47	.03	.13	.03	.09	
122-124	.03	.24	.03	.13	.03	.24	
125-127	.16	.50	.03	.13	.03	.09	
128-130	.31	.18	.03	.13	.03	.24	
131-133	.03	.18	.03	.13	.03	.09	
134-136	.16	.19	.03	.13	.03	.24	
137-139	.28	.34	.03	.13	.03	.09	
140-142	.20	.11	.03	.13	.03	.24	
143-145	.31	.47	.03	.13	.03	.09	
146-148	.03	.24	.03	.13	.03	.24	
149-151	.16	.50	.03	.13	.03	.09	
152-154	.31	.18	.03	.13	.03	.24	
155-157	.03	.18	.03	.13	.03	.09	
158-160	.16	.19	.03	.13	.03	.24	
161-163	.28	.34	.03	.13	.03	.09	
164-166	.20	.11	.03	.13	.03	.24	
167-169	.31	.47	.03	.13	.03	.09	
170-172	.03	.24	.03	.13	.03	.24	
173-175	.16	.50	.03	.13	.03	.09	
176-178	.31	.18	.03	.13	.03	.24	
179-181	.03	.18	.03	.13	.03	.09	
182-184	.16	.19	.03	.13	.03	.24	
185-187	.28	.34	.03	.13	.03	.09	
188-190	.20	.11	.03	.13	.03	.24	
191-193	.31	.47	.03	.13	.03	.09	
194-196	.03	.24	.03	.13	.03	.24	
197-199	.16	.50	.03	.13	.03	.09	
200-202	.31	.18	.03	.13	.03	.24	
203-205	.03	.18	.03	.13	.03	.09	
206-208	.16	.19	.03	.13	.03	.24	
209-211	.28	.34	.03	.13	.03	.09	
212-214	.20	.11	.03	.13	.03	.24	
215-217	.31	.47	.03	.13	.03	.09	
218-220	.03	.24	.03	.13	.03	.24	
221-223	.16	.50	.03	.13	.03	.09	
224-226	.31	.18	.03	.13	.03	.24	
227-229	.03	.18	.03	.13	.03	.09	
230-232	.16	.19	.03	.13	.03	.24	
233-235	.28	.34	.03	.13	.03	.09	
236-238	.20	.11	.03	.13	.03	.24	
239-241	.31	.47	.03	.13	.03	.09	
242-244	.03	.24	.03	.13	.03	.24	
245-247	.16	.50	.03	.13	.03	.09	
248-250	.31	.18	.03	.13	.03	.24	
251-253	.03	.18	.03	.13	.03	.09	
254-256	.16	.19	.03	.13	.03	.24	
257-259	.28	.34	.03	.13	.03	.09	
260-262	.20	.11	.03	.13	.03	.24	
263-265	.31	.47	.03	.13	.03	.09	
266-268	.03	.24	.03	.13	.03	.24	
269-271	.16	.50	.03	.13	.03	.09	
272-274	.31	.18	.03	.13	.03	.24	
275-277	.03	.18	.03	.13	.03	.09	
278-280	.16	.19	.03	.13	.03	.24	
281-283	.28	.34	.03	.13	.03	.09	
284-286	.20	.11	.03	.13	.03	.24	
287-289	.31	.47	.03	.13	.03	.09	
290-292	.03	.24	.03	.13	.03	.24	
293-295	.16	.50	.03	.13	.03	.09	
296-298	.31	.18	.03	.13	.03	.24	
299-301	.03	.18	.03	.13	.03	.09	
302-304	.16	.19	.03	.13	.03	.24	
305-307	.28	.34	.03	.13	.03	.09	
308-310	.20	.11	.03	.13	.03	.24	
311-313	.31	.47	.03	.13	.03	.09	
314-316	.03	.24	.03	.13	.03	.24	
317-319	.16	.50	.03	.13	.03	.09	
320-322	.31	.18	.03	.13	.03	.24	
323-325	.03	.18	.03	.13	.03	.09	
326-328	.16	.19	.03	.13	.03	.24	
329-331	.28	.34	.03	.13	.03	.09	
332-334	.20	.11	.03	.13	.03	.24	
335-337	.31	.47	.03	.13	.03	.09	
338-340	.03	.24	.03	.13	.03	.24	
341-343	.16	.50	.03	.13	.03	.09	
344-346	.31	.18	.03	.13	.03	.24	
347-349	.03	.18	.03	.13	.03	.09	
350-352	.16	.19	.03	.13	.03	.24	
353-355	.28	.34	.03	.13	.03	.09	
356-358	.20	.11	.03	.13	.03	.24	
359-361	.31	.47	.03	.13	.03	.09	
362-364	.03	.24	.03	.13	.03	.24	

Total  $\delta$   
 $a-b$   
 $(a-b) \times \text{Mult.}$

$\Sigma(a-b) \times \text{Mult.} = +1.31$        $\Sigma(a-b) \times \text{Mult.} = -30.70$        $\Sigma \delta \cos 2(\sigma-\eta) \delta = \Sigma_{364}^0 (a-b) \times \text{Mult.} = -29.39$

FORMS FOR LONG-PERIOD TIDES.

TIDE Sa.

$\sum dh \sin \eta t$ .

Multiplier	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
No. of the day	+	-	+	-	+	-	+	-	+	-	+	-	+	-	+	-	+	-	+	-
01 to 0	.07	.54	.34	.27	.42	.29	.07	.24	.20	.30	.13	.26	.07	.18	.49	.03				
	.05	.53	.53	.06	.21	.20	.15	.42	.18	.05	.11	.30	.00	.23	.65	.07				
	.23	.55	.36	.03	.15	.28	.28	.35	.34	.11	.04	.30	.02	.22	.74	.26				
	.23	.32	.28	.02	.07	.39	.37	.15	.27	.10	.08	.35	.02	.22	.66	.32				
	.19	.18	.12	.22	.08	.38	.46	.07	.27	.30	.16	.23	.12	.03	.35	.32				
	.24	.10	.04	.24	.20	.34	.34	.43	.42	.08	.09	.68	.07	.03	.25	.35				
	.13	.20	.41	.05	.28	.07	.09	.45	.04	.36	.04	.67	.34	.58	.16	.58				
	.47	.29	.29	.13	.38	.00	.02	.53	.07	.25	.05	.92	.16	.53	.38	.61				
	.36	.27	.51	.15	.27	.10	.10	.51	.07	.18	.05	.78	.12	.50	.51	.41				
	.23	.10	.02	.00	.41	.00	.28	.30	.32	.29	.03	.93	.04	.49	.44	.41				
	.10	.12	.12	.12	.35	.13	.03	.03	.32	.27	.13	.77	.26	.42	.54	.54				
	.16	.34	.01	.29	.24	.13	.29	.03	.27	.16	.36	.43	.43	.09	.63	.63				
	.32	.13	.32	.32	.13	.13	.32	.09	.09	.09	.46	.77	.77	.09	.63	.63				
	.66	.00	.46	.69	.62	.91	.61	.98	.38	.35	.91	.40	.42	.42	.42	.42				
Total a	+ 2.66	+ 3.02	- 2.08	- 0.52	- 2.29	- 1.38	- 1.00	- 2.98	- 1.27	- 2.62	+ 1.54	+ 9.04	+ 1.00	+ 3.48	+ 0.48					
	.24	.21	.07	.48	.03	.10	.22	.31	.18	.45	.01	.16	.28	.59	.26	.19				
	.18	.42	.24	.47	.16	.14	.23	.59	.15	.56	.04	.15	.13	.47	.14	.17				
	.16	.36	.31	.31	.19	.13	.07	.29	.23	.31	.10	.16	.22	.35	.17	.15				
	.05	.28	.18	.28	.25	.09	.07	.13	.24	.27	.11	.02	.34	.83	.36	.36				
	.07	.22	.25	.05	.17	.18	.16	.16	.24	.24	.20	.08	.28	.17	.50	.58				
	.21	.16	.21	.06	.15	.11	.27	.02	.13	.58	.13	.01	.15	.23	.52	.16				
	.18	.05	.22	.06	.17	.05	.23	.09	.04	.80	.04	.10	.20	.19	.33	.17				
	.47	.15	.10	.02	.21	.08	.07	.22	.04	.68	.15	.12	.30	.07	.19	.17				
	.47	.10	.05	.01	.16	.09	.03	.17	.39	.64	.17	.07	.32	.07	.10	.13				
	.43	.09	.02	.05	.13	.10	.01	.17	.01	.58	.04	.16	.24	.33	.17	.17				
	.25	.24	.07	.02	.15	.19	.01	.01	.26	.46	.05	.08	.07	.35	.17	.17				
	.29	.70	.21	.92	.14	.77	.61	.73	.00	.83	.72	.18	.25	.35	.35	.35				
	.21	.32	.09	.09	.77	.41	.77	.00	.97	.48	.18	.11	.25	.80	.00	.35				
Total b	+ 1.50	- 2.11	- 1.82	- 1.78	+ 1.43	+ 0.34	+ 0.16	+ 1.73	+ 0.49	- 2.39	+ 1.60	+ 0.86	+ 2.39	- 2.45	- 3.35					
a-b	+ 1.16	+ 4.73	- 0.26	+ 1.26	- 3.72	- 1.72	- 1.76	- 4.71	- 1.76	- 0.23	- 0.06	+ 8.18	- 1.39	+ 5.93	+ 3.83					
(a-b) * Mult.	{	+ 1.16	+ 4.73	+ 1.13	+ 1.35	- 1.38	- 1.41	- 3.30	- 1.23	- 0.14	- 0.03	- 0.86	- 1.39	+ 1.19	+ 3.83					
	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					

$\sum (a-b) \times \text{Mult.} = + 11.86$        $\sum dh \sin \eta t = \sum_{364} (a-b) \times \text{Mult.} = + 0.34$

NOTE.—To fill up this form.—Enter days 0, 1, 2, 3 in the last column 0, days 4 to 9 (inclusive) under their proper signs in last column but one; 1, days 10 to 14 (inclusive) in column 2; days 15 to 20 (inclusive) in column 3; next so on. The signs in column right to left (21 to 0), or left to right (92 to 182), fill up each short column before going on to the next, and a similar instruction applies to the filling up of all the rest of the form.

FORMS FOR LONG-PERIOD TIDES.

TIDE Sa.

$\Sigma dk \cos \eta t.$

Multiplier	1-0	1-0	1-0	1-0	1-0	1-0	1-0	1-0	1-0	1-0	1-0	1-0	1-0	1-0	1-0	1-0	1-0	0																							
No. of the day	+	-	+	-	+	-	+	-	+	-	+	-	+	-	+	-	+	0																							
0 to 91	.03 .03 .26 .32 .49 .65 .74	.66 .35 .25 .18 .23 .22	.22 .02 .07 .00 .02 .21	.08 .13 .30 .32 .39 .04 .08	.09 .07 .26 .59 .39 .04 .23	.12 .07 .07 .00 .02 .21	.08 .13 .30 .32 .39 .04 .23	.30 .32 .24 .07 .24 .23	.16 .33 .42 .11 .43	.11 .19 .30 .37 .43	.20 .18 .34 .27 .27	.24 .42 .35 .15	.07 .15 .28 .37 .46 .29 .28	.39 .38 .42 .21 .15 .07	.08 .20 .16 .13 .15 .01	.21 .09 .16 .27 .11 .01	.02 .02 .01 .05 .09 .15 .08	.12 .18 .10 .07 .05 .23	.33 .47 .36	.16 .05 .18 .24 .16 .21	.23 .10 .23 .16 .20 .29 .27	.28 .28 .07 .25 .21 .42 .31	.25 .28 .18 .22 .18 .18 .16	.16 .07 .16 .21 .18 .18 .16																	
364 to 274	.19 .13 .17 .16 .17 .17	.07 .30 .19 .32 .24 .33 .07	.07 .16 .08 .05 .15 .01 .10 .12	.17 .04 .05 .05 .15 .01 .10 .12	.17 .04 .05 .05 .15 .01 .10 .12	.46 .20 .13 .04 .15	.58 .80 .68 .64 .58	.13 .09 .22 .39 .17	.13 .04 .09 .09 .39 .17	.58 .80 .68 .64 .58	.13 .09 .22 .39 .17	.02 .09 .16 .13 .15 .01	.02 .09 .16 .13 .15 .01	.21 .09 .16 .13 .15 .01	.21 .09 .16 .13 .15 .01	.15 .43 .21 .21 .16 .05 .22	.15 .43 .21 .21 .16 .05 .22	.21 .18 .47 .47	.21 .18 .47 .47	.43 .21 .21 .16 .05 .22	.15 .43 .21 .21 .16 .05 .22	.15 .43 .21 .21 .16 .05 .22	.43 .21 .21 .16 .05 .22	.15 .43 .21 .21 .16 .05 .22	.15 .43 .21 .21 .16 .05 .22	.43 .21 .21 .16 .05 .22	.15 .43 .21 .21 .16 .05 .22	.43 .21 .21 .16 .05 .22	.15 .43 .21 .21 .16 .05 .22												
Total a	2.32 0.99 + 1.33	1.89 1.79 + 0.10	1.17 0.72 + 0.45	2.20 0.12 0.53 0.44 + 0.19	0.12 0.53 0.44 + 0.19	1.45 0.79 0.00 0.68 0.17 1.47 + 0.66	0.17 1.47 - 1.30	0.50 1.16 - 0.66	0.00 2.99 0.76 1.75 - 2.99	0.00 2.99 0.76 1.75 - 2.99	1.38 0.10 0.15 2.18 + 1.22	1.83 1.13 2.05 0.00 - 3.03	1.83 1.13 2.05 0.00 - 3.03	1.83 1.13 2.05 0.00 - 3.03	1.83 1.13 2.05 0.00 - 3.03	1.83 1.13 2.05 0.00 - 3.03	1.83 1.13 2.05 0.00 - 3.03	1.83 1.13 2.05 0.00 - 3.03	1.83 1.13 2.05 0.00 - 3.03	1.83 1.13 2.05 0.00 - 3.03	1.83 1.13 2.05 0.00 - 3.03	1.83 1.13 2.05 0.00 - 3.03	1.83 1.13 2.05 0.00 - 3.03	1.83 1.13 2.05 0.00 - 3.03	1.83 1.13 2.05 0.00 - 3.03	1.83 1.13 2.05 0.00 - 3.03	1.83 1.13 2.05 0.00 - 3.03	1.83 1.13 2.05 0.00 - 3.03	1.83 1.13 2.05 0.00 - 3.03	1.83 1.13 2.05 0.00 - 3.03	1.83 1.13 2.05 0.00 - 3.03	1.83 1.13 2.05 0.00 - 3.03									
182 to 92	.44 .54 .63 .58 .61 .41	.49 .42 .09 .16 .53 .51	.04 .26 .43 .58 .53 .50	.178 .93 .34 .77 .34 .16 .12	.05 .03 .13 .31 .16 .07 .03	.16 .09 .04 .05	.36 .25 .18 .29 .24	.04 .07 .07 .32	.45 .53 .51 .30 .03	.10 .00 .13 .24 .02 .10 .28	.27 .41 .35 .24 .13 .07 .00	.12 .29 .32 .28 .38 .15	.12 .29 .32 .28 .38 .15	.12 .29 .32 .28 .38 .15	.12 .29 .32 .28 .38 .15	.12 .29 .32 .28 .38 .15	.12 .29 .32 .28 .38 .15	.12 .29 .32 .28 .38 .15	.12 .29 .32 .28 .38 .15	.12 .29 .32 .28 .38 .15	.12 .29 .32 .28 .38 .15	.12 .29 .32 .28 .38 .15	.12 .29 .32 .28 .38 .15	.12 .29 .32 .28 .38 .15	.12 .29 .32 .28 .38 .15	.12 .29 .32 .28 .38 .15	.12 .29 .32 .28 .38 .15	.12 .29 .32 .28 .38 .15	.12 .29 .32 .28 .38 .15	.12 .29 .32 .28 .38 .15	.12 .29 .32 .28 .38 .15	.12 .29 .32 .28 .38 .15	.12 .29 .32 .28 .38 .15	.12 .29 .32 .28 .38 .15	.12 .29 .32 .28 .38 .15						
183 to 273	.19 .17 .15 .26 .14 .17	.56 .50 .58 .59 .47 .35	.03 .17 .18 .28 .13 .22	.08 .28 .01 .16 .15 .02	.08 .28 .01 .16 .15 .02	.47 .40 .45 .56 .31	.27 .24 .07 .14 .07	.18 .15 .23 .24	.31 .50 .59 .13	.22 .23 .09 .07 .16 .10 .14	.13 .09 .18 .03 .16 .19 .25	.17 .04 .30 .48 .47 .37	.28 .07 .25 .21 .42 .31	.28 .07 .25 .21 .42 .31	.28 .07 .25 .21 .42 .31	.28 .07 .25 .21 .42 .31	.28 .07 .25 .21 .42 .31	.28 .07 .25 .21 .42 .31	.28 .07 .25 .21 .42 .31	.28 .07 .25 .21 .42 .31	.28 .07 .25 .21 .42 .31	.28 .07 .25 .21 .42 .31	.28 .07 .25 .21 .42 .31	.28 .07 .25 .21 .42 .31	.28 .07 .25 .21 .42 .31	.28 .07 .25 .21 .42 .31	.28 .07 .25 .21 .42 .31	.28 .07 .25 .21 .42 .31	.28 .07 .25 .21 .42 .31	.28 .07 .25 .21 .42 .31	.28 .07 .25 .21 .42 .31	.28 .07 .25 .21 .42 .31	.28 .07 .25 .21 .42 .31	.28 .07 .25 .21 .42 .31	.28 .07 .25 .21 .42 .31	.28 .07 .25 .21 .42 .31	.28 .07 .25 .21 .42 .31	.28 .07 .25 .21 .42 .31			
Total b	0.00 4.29 - 4.29	3.32 0.03 + 3.29	7.71 0.08 3.06 0.15 + 2.91	2.24 0.29 0.51 1.60 0.91 0.39 + 1.95	2.24 0.29 0.51 1.60 0.91 0.39 + 1.95	1.60 0.91 0.39 + 0.52	1.23 1.82 - 0.59	1.35 0.38 + 0.97	1.03 1.47 - 0.44	1.03 1.47 - 0.44	0.17 3.05 0.45 1.05 - 2.88	0.10 2.91 1.25 1.33 - 0.60	0.10 2.91 1.25 1.33 - 0.60	0.10 2.91 1.25 1.33 - 0.60	0.10 2.91 1.25 1.33 - 0.60	0.10 2.91 1.25 1.33 - 0.60	0.10 2.91 1.25 1.33 - 0.60	0.10 2.91 1.25 1.33 - 0.60	0.10 2.91 1.25 1.33 - 0.60	0.10 2.91 1.25 1.33 - 0.60	0.10 2.91 1.25 1.33 - 0.60	0.10 2.91 1.25 1.33 - 0.60	0.10 2.91 1.25 1.33 - 0.60	0.10 2.91 1.25 1.33 - 0.60	0.10 2.91 1.25 1.33 - 0.60	0.10 2.91 1.25 1.33 - 0.60	0.10 2.91 1.25 1.33 - 0.60	0.10 2.91 1.25 1.33 - 0.60	0.10 2.91 1.25 1.33 - 0.60	0.10 2.91 1.25 1.33 - 0.60	0.10 2.91 1.25 1.33 - 0.60	0.10 2.91 1.25 1.33 - 0.60	0.10 2.91 1.25 1.33 - 0.60	0.10 2.91 1.25 1.33 - 0.60	0.10 2.91 1.25 1.33 - 0.60	0.10 2.91 1.25 1.33 - 0.60	0.10 2.91 1.25 1.33 - 0.60	0.10 2.91 1.25 1.33 - 0.60	0.10 2.91 1.25 1.33 - 0.60		
a-b	+ 5.82 + 5.82	- 2.90 + 3.00	- 7.71 - 2.72	- 2.24 - 1.29	- 2.24 - 1.29	- 1.09 - 3.59	- 0.52 - 1.82	- 0.59 - 0.07	- 0.44 - 0.55	- 0.44 - 0.55	- 2.88 + 4.10	- 0.60 + 3.51	- 0.60 + 3.51	- 0.60 + 3.51	- 0.60 + 3.51	- 0.60 + 3.51	- 0.60 + 3.51	- 0.60 + 3.51	- 0.60 + 3.51	- 0.60 + 3.51	- 0.60 + 3.51	- 0.60 + 3.51	- 0.60 + 3.51	- 0.60 + 3.51	- 0.60 + 3.51	- 0.60 + 3.51	- 0.60 + 3.51	- 0.60 + 3.51	- 0.60 + 3.51	- 0.60 + 3.51	- 0.60 + 3.51	- 0.60 + 3.51	- 0.60 + 3.51	- 0.60 + 3.51	- 0.60 + 3.51	- 0.60 + 3.51	- 0.60 + 3.51	- 0.60 + 3.51	- 0.60 + 3.51	- 0.60 + 3.51	
(a-b) x Mult.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

$\Sigma(a-b) \times \text{Mult.} = + 11.37$        $\Sigma(a-b) \times \text{Mult.} = - 18.94$        $\Sigma dk \cos \eta t = \Sigma^{364} (\alpha - b) \times \text{Mult.} = - 7.57$

NOTE.—To fill up this form:—Enter days 0 to 6 (inclusive) under their proper signs in first column 1-0; days 7 to 12 (inclusive) in second column 1-0; days 13 to 18 (inclusive) in third column 1-0; days 19 to 25 (inclusive) in first column -9; and so on. Thus in working from left to right (0 to 91), or right to left (364 to 274), fill up each short column before going on to the next, and a similar instruction applies to the filling up of all the rest of the form.

FORMS FOR LONG-PERIOD TIDES.

TIDE Ssa.

$\Sigma dh \sin 2\pi t.$

Multiplier	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
No. of the day	+	-	+	-	+	-	+	-	+	-	+	-	+	-	+	-	+	-	+	-
45 to 0	.47	.43	.40	.37	.34	.31	.28	.25	.22	.19	.16	.13	.10	.07	.04	.01	.00	.00	.00	.00
46 to 91	.42	.39	.36	.33	.30	.27	.24	.21	.18	.15	.12	.09	.06	.03	.00	.00	.00	.00	.00	.00
228 to 183	.44	.41	.38	.35	.32	.29	.26	.23	.20	.17	.14	.11	.08	.05	.02	.00	.00	.00	.00	.00
229 to 273	.45	.42	.39	.36	.33	.30	.27	.24	.21	.18	.15	.12	.09	.06	.03	.00	.00	.00	.00	.00
137 to 92	.46	.43	.40	.37	.34	.31	.28	.25	.22	.19	.16	.13	.10	.07	.04	.01	.00	.00	.00	.00
138 to 182	.47	.44	.41	.38	.35	.32	.29	.26	.23	.20	.17	.14	.11	.08	.05	.02	.00	.00	.00	.00
319 to 274	.48	.45	.42	.39	.36	.33	.30	.27	.24	.21	.18	.15	.12	.09	.06	.03	.00	.00	.00	.00
320 to 364	.49	.46	.43	.40	.37	.34	.31	.28	.25	.22	.19	.16	.13	.10	.07	.04	.01	.00	.00	.00
Total a	1.47	1.43	1.40	1.37	1.34	1.31	1.28	1.25	1.22	1.19	1.16	1.13	1.10	1.07	1.04	1.01	1.00	1.00	1.00	1.00
Total b	0.45	0.42	0.39	0.36	0.33	0.30	0.27	0.24	0.21	0.18	0.15	0.12	0.09	0.06	0.03	0.00	0.00	0.00	0.00	0.00
a-b	1.02	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01
a-b x Mult.	1.02	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01

NOTE.—To fill up this form:—Enter days 0 and 1 in the last column 0; days 2, 3, 4 under their proper signs in last column but one -1; days 5, 6, 7 in column .2; days 8, 9, 10 in column .3; and so on. Thus in working from right to left (46 to 91), fill up each short column before going on to the next, and a similar instruction applies to the filling up of all the rest of the form.

$\Sigma(a-b) \times \text{Mult.} = + 10.78$        $\Sigma(a-b) \times \text{Mult.} = - 8.38$        $\Sigma dh \sin 2\pi t = \Sigma \text{obs. } (a-b) \times \text{Mult.} = + 2.40$



FORMS FOR LONG-PERIOD TIDES.

TIDE Ssa.

$\Sigma dh \cos 2\eta t.$

Multiplier No. of the day	$\Sigma dh \cos 2\eta t$																			
	1-0	1-0	1-0	1-0	1-0	1-0	1-0	1-0	1-0	1-0	1-0	1-0								
0 to 45	+ .03 - .03 + .26 - .31	- .49 + .65 - .74 + .66	+ .35	- .22 + .02 - .07	+ .00 - .21 + .12	+ .26 - .39 + .30 - .35	- .07	+ .16 - .34 + .78 - .93 + .34 - .77	+ .16 - .15 + .16	+ .08 - .10 + .11 - .02	+ .23 - .09 + .46 - .67 + .92	- .33 + .33 - .42 + .30	- .11 + .04 - .08 + .13	- .05 + .09 - .29 + .04 - .16	- .11 + .33 - .42 + .30	+ .20 - .18 + .34	- .30 + .37 - .43	+ .36 - .25 + .18	- .07 + .07 - .18	- .32
182 to 137	+ .41	- .54 + .63 - .58 + .61	+ .16 - .38 + .51 - .44	+ .43 - .58 + .53 - .50	+ .26	+ .178 - .93 + .34 - .77	+ .16 - .16 + .16	+ .13 - .22 + .34 - .28	+ .13 - .10 + .10 - .04	+ .08 - .11 + .11 - .02	+ .46 - .67 + .92	- .05 + .09 - .29 + .04 - .16	+ .05 - .03 - .13 + .31	- .05 + .09 - .29 + .04 - .16	- .05 + .09 - .29 + .04 - .16	+ .20 - .18 + .34	- .30 + .37 - .43	+ .36 - .25 + .18	- .07 + .07 - .18	- .32
183 to 228	+ .19 - .17 + .15 - .26	- .14 + .32 - .51 + .44	+ .58 - .36 + .36 - .30	+ .17 - .47 + .35 - .03	+ .13 - .22 + .34 - .28	+ .16 - .16 + .16	+ .13 - .22 + .34 - .28	+ .13 - .22 + .34 - .28	+ .13 - .22 + .34 - .28	+ .13 - .22 + .34 - .28	+ .08 - .11 + .11 - .02	+ .46 - .67 + .92	- .05 + .09 - .29 + .04 - .16	+ .05 - .03 - .13 + .31	- .05 + .09 - .29 + .04 - .16	+ .20 - .18 + .34	- .30 + .37 - .43	+ .36 - .25 + .18	- .07 + .07 - .18	- .32
304 to 320	+ .16 - .16 + .17 - .17	- .17 + .33 - .33 + .19	+ .33 - .33 + .19	+ .19 - .07 + .24	+ .24	+ .15 - .20 + .30 - .32	+ .15 - .20 + .30 - .32	+ .15 - .20 + .30 - .32	+ .15 - .20 + .30 - .32	+ .15 - .20 + .30 - .32	+ .05 - .01 + .04 - .05	+ .05 - .01 + .04 - .05	+ .17 - .04 + .15	+ .17 - .04 + .15	+ .17 - .04 + .15	+ .17 - .04 + .15	+ .17 - .04 + .15	+ .17 - .04 + .15	+ .17 - .04 + .15	+ .17 - .04 + .15
Total $a$	+ .64 - .21	- .54 + .21	+ .35 - .72	+ .98 - .43	+ .56	+ .71	+ .56	+ .42	+ .21	+ .12	+ .47	+ .35	+ .12	+ .12	+ .12	+ .24	+ .24	+ .24	+ .24	+ .24
91 to 46	+ .05 - .23	- .32 + .18 - .10 + .07	+ .172	+ .28 - .12 + .02 - .19	+ .28	+ .22 - .24 + .34 - .53	+ .22 - .24 + .34 - .53	+ .22 - .24 + .34 - .53	+ .22 - .24 + .34 - .53	+ .22 - .24 + .34 - .53	+ .07 - .08 + .08 - .11	+ .07 - .08 + .08 - .11	+ .27 - .06 + .03 - .02	+ .27 - .06 + .03 - .02	+ .27 - .06 + .03 - .02	+ .27 - .06 + .03 - .02	+ .27 - .06 + .03 - .02	+ .27 - .06 + .03 - .02	+ .27 - .06 + .03 - .02	+ .27 - .06 + .03 - .02
92 to 136	+ .33 - .47 + .36 - .23	- .10 + .16 - .20 + .29	+ .27	+ .12 - .05 + .02 - .41	+ .12 - .05 + .02 - .41	+ .12 - .05 + .02 - .41	+ .12 - .05 + .02 - .41	+ .12 - .05 + .02 - .41	+ .12 - .05 + .02 - .41	+ .12 - .05 + .02 - .41	+ .29 - .29 + .29 - .32	+ .29 - .29 + .29 - .32	+ .00 - .12 + .29 - .32	+ .00 - .12 + .29 - .32	+ .00 - .12 + .29 - .32	+ .00 - .12 + .29 - .32	+ .00 - .12 + .29 - .32	+ .00 - .12 + .29 - .32	+ .00 - .12 + .29 - .32	+ .00 - .12 + .29 - .32
273 to 229	+ .33 - .47 + .36 - .23	- .16 + .16 - .05 + .07	+ .28 - .22 + .24 - .18	+ .28 - .18 + .18 - .21	+ .21 - .06 + .13	+ .28 - .18 + .18 - .21	+ .28 - .18 + .18 - .21	+ .28 - .18 + .18 - .21	+ .28 - .18 + .18 - .21	+ .28 - .18 + .18 - .21	+ .30 - .48 + .47 - .37	+ .30 - .48 + .47 - .37	+ .30 - .48 + .47 - .37	+ .30 - .48 + .47 - .37	+ .30 - .48 + .47 - .37	+ .30 - .48 + .47 - .37	+ .30 - .48 + .47 - .37	+ .30 - .48 + .47 - .37	+ .30 - .48 + .47 - .37	+ .30 - .48 + .47 - .37
274 to 319	+ .21 - .18 + .47 - .47	- .43 + .21 - .25 + .16	+ .05	+ .15 - .10 + .09 - .24	+ .05 - .06 + .07 - .06	+ .02 - .01 + .05 - .07	+ .02 - .01 + .05 - .07	+ .02 - .01 + .05 - .07	+ .02 - .01 + .05 - .07	+ .02 - .01 + .05 - .07	+ .09 - .02 + .10 - .09	+ .09 - .02 + .10 - .09	+ .11 - .05 + .13 - .19	+ .11 - .05 + .13 - .19	+ .11 - .05 + .13 - .19	+ .11 - .05 + .13 - .19	+ .11 - .05 + .13 - .19	+ .11 - .05 + .13 - .19	+ .11 - .05 + .13 - .19	+ .11 - .05 + .13 - .19
Total $b$ $a-b$ $(a-b) \times \text{Mult.}$	+ .296 - 4.17 + .47 - 4.17	+ 2.20 - 4.36 + .30 - 4.36	+ 0.07 - 1.79 + 0.30 - 1.79	+ 2.00 + 4.42 + 3.98 - 1.79	+ 0.64 + 1.76 + 1.41 - 1.79	+ 0.74 + 7.95 + 5.57 - 1.79	+ 1.59 + 3.15 + 2.52 - 1.79	+ 0.64 + 1.76 + 1.41 - 1.79	+ 0.64 + 1.76 + 1.41 - 1.79	+ 0.64 + 1.76 + 1.41 - 1.79	+ 2.00 + 4.42 + 3.98 - 1.79	+ 2.00 + 4.42 + 3.98 - 1.79	+ 2.00 + 4.42 + 3.98 - 1.79	+ 2.00 + 4.42 + 3.98 - 1.79	+ 2.00 + 4.42 + 3.98 - 1.79	+ 2.00 + 4.42 + 3.98 - 1.79	+ 2.00 + 4.42 + 3.98 - 1.79	+ 2.00 + 4.42 + 3.98 - 1.79	+ 2.00 + 4.42 + 3.98 - 1.79	+ 2.00 + 4.42 + 3.98 - 1.79

$\Sigma(a-b) \times \text{Mult.} = +18.47$        $\Sigma(a-b) \times \text{Mult.} = -11.07$        $\Sigma(h \cos 2\eta t = \Sigma_{364}^{304} (a-b) \times \text{Mult.} = +7.40$

NOTE.—To fill up this form:—Enter days 0, 1, 2, 3 under their proper signs in the first column 1-0; days 4, 5, 6, 7 in second column 1-0; day 8 in third column 1-0; days 9, 10, 11, 12 in first column -9; days 13, 14, 15 in second column -9; and so on. Thus in working from left to right (0 to 45), or right to left (182 to 137), fill up each short column before going on to the next, and a similar instruction applies to the filling up of all the rest of the form.



FORMS FOR LONG-PERIOD TIDES.

EVALUATION OF LONG-PERIOD TIDES.

$\sum_0^{360} dh \times \cos(\sigma - \omega)t =$	$+3.59 = +183.05A$	$+2.14B$	$+0.73C$	$+4.29D$	$+0.77C'$	$+5.04D'$	$+4.88E$	$-0.34F$	$+4.96G$	$-0.69H$
	$+3.59 = 183.05A$	$+0.04$	$-0.04$	$-0.06$	$-0.01$	$-0.27$	$-0.20$	$-0.00$	$+0.20$	$-0.01$
	$+3.94 = 183.05A$									
	$+0.022 = A$									
$\sum_0^{360} dh \times \sin(\sigma - \omega)t =$	$+3.79 = +2.14A$	$+181.95B$	$-4.15C$	$+1.02D$	$-4.90C'$	$+1.07D'$	$+3.80E$	$+0.34F$	$+3.88G$	$+0.69H$
	$+3.79 = +0.05$	$+181.95B$	$+0.21$	$-0.01$	$+0.06$	$-0.06$	$-0.16$	$+0.00$	$+0.16$	$+0.01$
	$+3.53 = 181.95B$									
	$+0.019 = B$									
$\sum_0^{360} dh \times \cos 2\sigma t =$	$-9.37 = +0.73A$	$-4.15B$	$+183.18C$	$+0.88D$	$+0.61C'$	$+0.92D'$	$-1.50E$	$-0.10F$	$-1.51G$	$-0.19H$
	$-9.37 = +0.02$	$-0.08$	$+183.18C$	$-0.01$	$-0.01$	$-0.05$	$+0.06$	$-0.00$	$-0.06$	$-0.00$
	$-9.24 = 183.18C$									
	$-0.050 = C$									
$\sum_0^{360} dh \times \sin 2\sigma t =$	$-2.47 = +4.29A$	$+1.02B$	$+0.88C$	$+181.82D$	$+6.92C'$	$-0.75D'$	$+3.05E$	$-0.08F$	$+3.06G$	$-0.17H$
	$-2.47 = +0.09$	$+0.02$	$-0.04$	$+181.82D$	$-0.01$	$-0.04$	$-0.13$	$-0.00$	$+0.12$	$-0.00$
	$-2.56 = 181.82D$									
	$-0.014 = D$									
$\sum_0^{360} dh \times \cos 2(\sigma - \eta)t =$	$-2.38 = +0.77A$	$-4.90B$	$+0.61C$	$+0.92D$	$+183.19C'$	$+0.97D'$	$-1.68E$	$-0.11F$	$-1.70G$	$-0.23H$
	$-2.38 = +0.02$	$-0.09$	$+0.03$	$-0.01$	$+183.19C'$	$+0.05$	$+0.07$	$-0.00$	$-0.07$	$-0.00$
	$-2.22 = 183.19C'$									
	$-0.012 = C'$									
$\sum_0^{360} dh \times \sin 2(\sigma - \eta)t =$	$-9.64 = +5.04A$	$+1.07B$	$+0.92C$	$-0.75D$	$+0.97C'$	$+181.81D'$	$+3.25E$	$-0.10F$	$+3.27G$	$-0.23H$
	$-9.64 = +0.11$	$+0.02$	$-0.05$	$+0.01$	$-0.01$	$+181.81D'$	$-0.14$	$-0.00$	$+0.13$	$-0.00$
	$-9.71 = 181.81D'$									
	$-0.053 = D'$									
$\sum_0^{360} dh \times \cos \eta t =$	$-7.66 = +4.88A$	$+3.80B$	$-1.50C$	$+3.05D$	$-1.68C'$	$+3.25D'$	$+182.43E$	$+0.00F$	$-0.14G$	$+0.00H$
	$-7.66 = +0.11$	$+0.07$	$+0.08$	$-0.04$	$+0.02$	$-0.17$	$+182.43E$	$+0.00$	$-0.01$	$+0.00$
	$-7.72 = 182.43E$									
	$-0.042 = E$									
$\sum_0^{360} dh \times \sin \eta t =$	$+0.32 = -0.34A$	$+0.34B$	$-0.10C$	$-0.08D$	$-0.11C'$	$-0.10D'$	$+0.00E$	$+182.57F$	$+0.00G$	$+0.00H$
	$+0.32 = -0.01$	$+0.01$	$+0.01$	$+0.00$	$+0.00$	$+0.01$	$-0.00$	$+182.57F$	$+0.00$	$+0.00$
	$+0.30 = 182.57F$									
	$+0.002 = F$									
$\sum_0^{360} dh \times \cos 2\eta t =$	$+7.31 = +4.96A$	$+3.88B$	$-1.51C$	$+3.06D$	$-1.70C'$	$+3.27D'$	$-0.14E$	$+0.00F$	$+182.43G$	$+0.00H$
	$+7.31 = +0.11$	$+0.07$	$+0.08$	$-0.04$	$+0.02$	$-0.17$	$+0.01$	$-0.00$	$+182.43G$	$+0.00$
	$+7.23 = 182.43G$									
	$+0.040 = G$									
$\sum_0^{360} dh \times \sin 2\eta t =$	$+2.36 = -0.69A$	$+0.69B$	$-0.19C$	$-0.17D$	$-0.23C'$	$-0.23D'$	$+0.00E$	$+0.00F$	$+0.00G$	$+182.57H$
	$+2.36 = -0.02$	$+0.01$	$+0.01$	$+0.00$	$+0.00$	$+0.01$	$-0.00$	$-0.00$	$+0.00$	$+182.57H$
	$+2.35 = 182.57H$									
	$+0.013 = H$									

LUNAR MONTHLY Mm.	LUNAR FORTNIGHTLY Mf.	LUNI-SOLAR FORTNIGHTLY MSf.	SOLAR ANNUAL Sa.	SOLAR SEMI-ANNUAL Ssa.
Log B = +8.27875	Log D = -8.14613	Log D' = -8.72428	Log F = +7.30103	Log H = +8.11394
Log A = +8.34242	Log C = -8.69897	Log C' = -8.07918	Log E = -8.62325	Log G = +8.60206
L tan $\zeta_1 = +9.93633$	L tan $\zeta_1 = +9.44716$	L tan $\zeta_1 = +0.64510$	Tan $\zeta_1 = -8.67778$	Tan $\zeta_1 = +9.51188$
$\zeta_1 = 40.815$	$\zeta_1 = 195.642$	$\zeta_1 = 257.243$	$\zeta_1 = 177.274$	$\zeta_1 = 18.004$
Motion for $11\frac{1}{4}^h = 6.260$	Motion for $11\frac{1}{4}^h = 12.627$	Motion for $11\frac{1}{4}^h = 11.683$	Motion for $11\frac{1}{4}^h = 0.472$	Motion for $11\frac{1}{4}^h = 0.945$
$\zeta = 47.075$	$\zeta = 208.269$	$\zeta = 268.926$	$\zeta = 177.746$	$\zeta = 18.949$
$V_0 + u = 16.507$	$V_0 + u = 201.066$	$V_0 + u = 359.114$	$V_0 + u = 281.103$	$V_0 + u = 202.206$
$\kappa = 63.582$	$\kappa = 49.315$	$\kappa = 268.040$	$\kappa = 98.849$	$\kappa = 221.155$
$B^2 = 0.000361$	$D^2 = 0.000196$	$(D')^2 = 0.000289$	$F^2 = 0.000004$	$H^2 = 0.000169$
$A^2 = 0.000484$	$C^2 = 0.000500$	$(C')^2 = 0.000144$	$E^2 = 0.001764$	$G^2 = 0.001600$
Sum = $R^2 = 0.000845$	Sum = $R^2 = 0.002696$	Sum = $R^2 = 0.002953$	Sum = $R^2 = 0.001768$	Sum = $R^2 = 0.001769$
$\frac{1}{f} = 0.884$	$\frac{1}{f} = 1.599$	$\frac{1}{f} = 0.964$	$B = H = 0.042$	$B = H = 0.042$
$H = 0.026$	$H = 0.083$	$H = 0.052$		
$B = 0.039$	$B = 0.052$	$B = 0.054$		

AUXILIARY TABLES.

TABLE II.—For converting Minutes and Seconds into Decimals of a Degree.

Minutes	Parts of a Degree	Seconds and Parts of a Degree	Parts of a Degree	Minutes and Seconds	Parts of a Degree	Minutes	Parts of a Degree	Seconds and Parts of a Degree	Parts of a Degree	Minutes	Parts of a Degree	Seconds and Parts of a Degree	Parts of a Degree	Minutes	Parts of a Degree	Seconds and Parts of a Degree	Parts of a Degree
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

TABLE I.—For converting Decimals of a Degree into Minutes and Seconds.

Parts of a Degree	Minutes	Parts of a Degree	Minutes and Seconds	Parts of a Degree	Minutes and Seconds	Parts of a Degree	Minutes	Parts of a Degree	Minutes and Seconds
0.10	6	0.20	12	0.30	18	0.40	24	0.50	30



AUXILIARY TABLES.

TABLE VII.—Products of Augmenting Factors  $R_1$ ,  $R_2$ , and  $R_3$ , and  $R_4$ , multiplied by 1 to 99.

$R_1 = \cdot 0028.$										
	0	10	20	30	40	50	60	70	80	90
0	.0000	.0080	.0160	.0240	.0320	.0400	.0480	.0560	.0640	.0720
1	.0028	.0108	.0188	.0268	.0348	.0428	.0508	.0588	.0668	.0748
2	.0056	.0136	.0216	.0296	.0376	.0456	.0536	.0616	.0696	.0776
3	.0084	.0164	.0244	.0324	.0404	.0484	.0564	.0644	.0724	.0804
4	.0112	.0192	.0272	.0352	.0432	.0512	.0592	.0672	.0752	.0832
5	.0140	.0220	.0300	.0380	.0460	.0540	.0620	.0700	.0780	.0860
6	.0168	.0248	.0328	.0408	.0488	.0568	.0648	.0728	.0808	.0888
7	.0196	.0276	.0356	.0436	.0516	.0596	.0676	.0756	.0836	.0916
8	.0224	.0304	.0384	.0464	.0544	.0624	.0704	.0784	.0864	.0944
9	.0252	.0332	.0412	.0492	.0572	.0652	.0732	.0812	.0892	.0972

$R_2 = \cdot 0115.$										
	0	10	20	30	40	50	60	70	80	90
0	.0000	.1150	.2300	.3450	.4600	.5750	.6900	.8050	.9200	.10350
1	.0115	.1265	.2415	.3565	.4715	.5865	.7015	.8165	.9315	.10465
2	.0230	.1380	.2530	.3680	.4830	.5980	.7130	.8280	.9430	.10580
3	.0345	.1495	.2645	.3795	.4945	.6095	.7245	.8395	.9545	.10695
4	.0460	.1610	.2760	.3910	.5060	.6210	.7360	.8510	.9660	.10810
5	.0575	.1725	.2875	.4025	.5175	.6325	.7475	.8625	.9775	.10925
6	.0690	.1840	.2990	.4140	.5290	.6440	.7590	.8740	.9890	.11040
7	.0805	.1955	.3105	.4255	.5405	.6555	.7705	.8855	.10005	.11155
8	.0920	.2070	.3220	.4370	.5520	.6670	.7820	.8970	.10120	.11270
9	.1035	.2185	.3335	.4485	.5635	.6785	.7935	.9085	.10235	.11385

$R_3 = \cdot 0472.$										
	0	10	20	30	40	50	60	70	80	90
0	.0000	.4720	.9440	1.4160	2.1880	3.0600	4.0320	5.1040	6.2760	7.5480
1	.0472	1.0192	2.0384	3.0576	4.0768	5.0960	6.1152	7.1344	8.1536	9.1728
2	.0944	1.9136	3.8272	5.7408	7.6544	9.5680	11.4816	13.3952	15.3088	17.2224
3	.1416	2.8160	5.6320	8.4480	12.2640	16.0800	19.8960	23.7120	27.5280	31.3440
4	.1888	3.7440	7.4880	11.2320	14.9760	18.6640	22.3520	26.0400	29.7280	33.4160
5	.2360	4.6720	9.3440	14.0160	19.6320	25.2480	30.8640	36.4800	42.0960	47.7120
6	.2832	5.5920	11.1840	16.7760	23.5040	30.2160	36.4320	42.0640	47.6320	53.2480
7	.3304	6.5120	13.0240	19.5200	27.2640	34.9280	41.6160	47.2160	52.7680	58.7840
8	.3776	7.4320	14.8640	22.2640	31.0080	39.4240	47.1600	52.7040	58.1920	64.3200
9	.4248	8.3520	16.7040	25.0080	33.7520	41.9200	49.1040	54.6400	60.1280	69.8560

TABLE VI.—Value of the Movement of  $p$  or  $\pi$  for differences of Longitude, Greenwich.

Difference of Longitude	Value of $\pi$	Actual values of $\pi$ corresponding to Degrees in Column 1	Difference of Longitude	Value of $\pi$	Actual values of $\pi$ corresponding to Degrees in Column 1
0	.000	.0000	88-865	.028	.0275
1-616	.001	.0005	92-097	.029	.0285
4-847	.002	.0015	95-328	.030	.0295
8-079	.003	.0025	98-560	.031	.0305
11-310	.004	.0035	101-791	.032	.0315
14-543	.005	.0045	105-023	.033	.0325
17-773	.006	.0055	108-254	.034	.0335
21-005	.007	.0065	111-486	.035	.0345
24-236	.008	.0075	114-717	.036	.0355
27-467	.009	.0085	117-949	.037	.0365
30-699	.010	.0095	121-180	.038	.0375
33-930	.011	.0105	124-411	.039	.0385
37-162	.012	.0115	127-643	.040	.0395
40-393	.013	.0125	130-874	.041	.0405
43-625	.014	.0135	134-106	.042	.0415
46-856	.015	.0145	137-337	.043	.0425
50-088	.016	.0155	140-569	.044	.0435
53-319	.017	.0165	143-800	.045	.0445
56-551	.018	.0175	147-032	.046	.0455
59-782	.019	.0185	150-263	.047	.0465
63-014	.020	.0195	153-495	.048	.0475
66-245	.021	.0205	156-726	.049	.0485
69-477	.022	.0215	159-958	.050	.0495
72-708	.023	.0225	163-189	.051	.0505
75-939	.024	.0235	166-421	.052	.0515
79-171	.025	.0245	169-652	.053	.0525
82-402	.026	.0255	172-884	.054	.0535
85-634	.027	.0265	176-115	.055	.0545
88-865		.0275	179-346	.056	.0555
			182-578		.0565

Correction for E. Longitude —, for W. Longitude +.

AUXILIARY TABLES.

TABLE VIII.—Products of  $S_1 \times .001$  up to  $S_1 \times 1.000$ .  $S_1 = \sin 15^\circ = .25982$ .

N <sup>o</sup> .	.000	.001	.002	.003	.004	.005	.006	.007	.008	.009	N <sup>o</sup> .
00	.000000	.002259	.005518	.009776	.015035	.021294	.028553	.036812	.046071	.056330	50
01	.002258	.004517	.008776	.014035	.020294	.027553	.035812	.045071	.055330	.066589	51
02	.004516	.008775	.014034	.020293	.027552	.035811	.045070	.055329	.066588	.078847	52
03	.006774	.011033	.017292	.024551	.032810	.042069	.052328	.063587	.075846	.089105	53
04	.009032	.013291	.020550	.028809	.038068	.048327	.059586	.071845	.085104	.100363	54
05	.011290	.015549	.023808	.033067	.043326	.054585	.066844	.080103	.095362	.112621	55
06	.013548	.017807	.027066	.037325	.048584	.060843	.074102	.089361	.106620	.125879	56
07	.015806	.020065	.030324	.041583	.053842	.067101	.082360	.099619	.118878	.140137	57
08	.018064	.022323	.033582	.045841	.059100	.074359	.091618	.110877	.132136	.155395	58
09	.020322	.024581	.036840	.050099	.065358	.082617	.101876	.123135	.146394	.172653	59
10	.022580	.026839	.040098	.054357	.070616	.088875	.109134	.131393	.156652	.184911	60
11	.024838	.029097	.043356	.058615	.075874	.095133	.117392	.142651	.170910	.202169	61
12	.027096	.031355	.046614	.062873	.081132	.101391	.124650	.150909	.180168	.212427	62
13	.029354	.033613	.048872	.065131	.085390	.106649	.130908	.158167	.188426	.221686	63
14	.031612	.035871	.051130	.067389	.091648	.113907	.140166	.169425	.201684	.232943	64
15	.033870	.038129	.053388	.070647	.094906	.118165	.146424	.176683	.209942	.243201	65
16	.036128	.040387	.055646	.072905	.097164	.121423	.149682	.180941	.215200	.246459	66
17	.038386	.042645	.057904	.075163	.100422	.124681	.154940	.187200	.219458	.250717	67
18	.040644	.044903	.060162	.077421	.102680	.127939	.160200	.194458	.230717	.257976	68
19	.042902	.047161	.062420	.079679	.104938	.130197	.164456	.200715	.235974	.268235	69
20	.045160	.049419	.064678	.081937	.107196	.132456	.168714	.205973	.243232	.276494	70
21	.047418	.051677	.066936	.084195	.109454	.134714	.172972	.211231	.248491	.284753	71
22	.049676	.053935	.069194	.086453	.111712	.136972	.177230	.216489	.253749	.293012	72
23	.051934	.056193	.071452	.088711	.113970	.139230	.181488	.221747	.259007	.299271	73
24	.054192	.058451	.073710	.090969	.116228	.141488	.186746	.227005	.264265	.305530	74
25	.056450	.060709	.075968	.093227	.118486	.143746	.192004	.232263	.269523	.311789	75
26	.058708	.062967	.078226	.095485	.120744	.146004	.197262	.237521	.274781	.318048	76
27	.060966	.065225	.080484	.097743	.123002	.148262	.202520	.242779	.280039	.324307	77
28	.063224	.067483	.082742	.100001	.125260	.150520	.207778	.248037	.285297	.330566	78
29	.065482	.069741	.084999	.102259	.127518	.152778	.213036	.253295	.290555	.336825	79
30	.067740	.071999	.087257	.104517	.129776	.155036	.218294	.258553	.295813	.343084	80
31	.070000	.074259	.089515	.106775	.132034	.157294	.223552	.263811	.301071	.349343	81
32	.072258	.076517	.091773	.109033	.134292	.159552	.228810	.269069	.306329	.355602	82
33	.074516	.078775	.094031	.111291	.136550	.161810	.234068	.274327	.311587	.361861	83
34	.076774	.081033	.096289	.113549	.138808	.164068	.239326	.279585	.316845	.368120	84
35	.079032	.083291	.098547	.115807	.141066	.166326	.244584	.284843	.322103	.374379	85
36	.081290	.085549	.100805	.118065	.143324	.168584	.249842	.290101	.327361	.380638	86
37	.083548	.087807	.103063	.120323	.145582	.170842	.255100	.295359	.332619	.386897	87
38	.085806	.090065	.105321	.122581	.147840	.173100	.260358	.300617	.337877	.393156	88
39	.088064	.092323	.107579	.124839	.150098	.175358	.265616	.305875	.343135	.399415	89
40	.090322	.094581	.109837	.127097	.152356	.177616	.270874	.311133	.348393	.405674	90
41	.092580	.096839	.112095	.129355	.154614	.179874	.276132	.316391	.353651	.411933	91
42	.094838	.099097	.114353	.131613	.156872	.182132	.281390	.321649	.358909	.418192	92
43	.097096	.101355	.116611	.133871	.159130	.184390	.286648	.326907	.364167	.424451	93
44	.099354	.103613	.118869	.136129	.161388	.186648	.291906	.332165	.369425	.430710	94
45	.101612	.105871	.121127	.138387	.163646	.188906	.297164	.337423	.374683	.436969	95
46	.103870	.108129	.123385	.140645	.165904	.191164	.302422	.342681	.379941	.443228	96
47	.106128	.110387	.125643	.142903	.168162	.193422	.307680	.347939	.385199	.449487	97
48	.108386	.112645	.127901	.145161	.170420	.195680	.312938	.353197	.390457	.455746	98
49	.110644	.114903	.130159	.147419	.172678	.197938	.318196	.358455	.395715	.462005	99
50	.112902	.117161	.132417	.149677	.174936	.200196	.323454	.363713	.400973	.468264	100

AUXILIARY TABLES.

TABLE IX.—Products of  $S_3 \times .001$  up to  $S_3 \times 1.000$ .  $S_3 = \sin 45^\circ = .70711$ .

No.	.000	.001	.002	.003	.004	.005	.006	.007	.008	.009	.010	No.
00	.000000	.000707	.001411	.002111	.002818	.003516	.004213	.004910	.005605	.006304	.007000	50
01	.000707	.001411	.002111	.002818	.003516	.004213	.004910	.005605	.006304	.007000	.007693	51
02	.001411	.002111	.002818	.003516	.004213	.004910	.005605	.006304	.007000	.007693	.008386	52
03	.002111	.002818	.003516	.004213	.004910	.005605	.006304	.007000	.007693	.008386	.009079	53
04	.002818	.003516	.004213	.004910	.005605	.006304	.007000	.007693	.008386	.009079	.009772	54
05	.003516	.004213	.004910	.005605	.006304	.007000	.007693	.008386	.009079	.009772	.010465	55
06	.004213	.004910	.005605	.006304	.007000	.007693	.008386	.009079	.009772	.010465	.011158	56
07	.004910	.005605	.006304	.007000	.007693	.008386	.009079	.009772	.010465	.011158	.011851	57
08	.005605	.006304	.007000	.007693	.008386	.009079	.009772	.010465	.011158	.011851	.012544	58
09	.006304	.007000	.007693	.008386	.009079	.009772	.010465	.011158	.011851	.012544	.013237	59
10	.007000	.007693	.008386	.009079	.009772	.010465	.011158	.011851	.012544	.013237	.013930	60
11	.007693	.008386	.009079	.009772	.010465	.011158	.011851	.012544	.013237	.013930	.014623	61
12	.008386	.009079	.009772	.010465	.011158	.011851	.012544	.013237	.013930	.014623	.015316	62
13	.009079	.009772	.010465	.011158	.011851	.012544	.013237	.013930	.014623	.015316	.016009	63
14	.009772	.010465	.011158	.011851	.012544	.013237	.013930	.014623	.015316	.016009	.016702	64
15	.010465	.011158	.011851	.012544	.013237	.013930	.014623	.015316	.016009	.016702	.017395	65
16	.011158	.011851	.012544	.013237	.013930	.014623	.015316	.016009	.016702	.017395	.018088	66
17	.011851	.012544	.013237	.013930	.014623	.015316	.016009	.016702	.017395	.018088	.018781	67
18	.012544	.013237	.013930	.014623	.015316	.016009	.016702	.017395	.018088	.018781	.019474	68
19	.013237	.013930	.014623	.015316	.016009	.016702	.017395	.018088	.018781	.019474	.020167	69
20	.013930	.014623	.015316	.016009	.016702	.017395	.018088	.018781	.019474	.020167	.020860	70
21	.014623	.015316	.016009	.016702	.017395	.018088	.018781	.019474	.020167	.020860	.021553	71
22	.015316	.016009	.016702	.017395	.018088	.018781	.019474	.020167	.020860	.021553	.022246	72
23	.016009	.016702	.017395	.018088	.018781	.019474	.020167	.020860	.021553	.022246	.022939	73
24	.016702	.017395	.018088	.018781	.019474	.020167	.020860	.021553	.022246	.022939	.023632	74
25	.017395	.018088	.018781	.019474	.020167	.020860	.021553	.022246	.022939	.023632	.024325	75
26	.018088	.018781	.019474	.020167	.020860	.021553	.022246	.022939	.023632	.024325	.025018	76
27	.018781	.019474	.020167	.020860	.021553	.022246	.022939	.023632	.024325	.025018	.025711	77
28	.019474	.020167	.020860	.021553	.022246	.022939	.023632	.024325	.025018	.025711	.026404	78
29	.020167	.020860	.021553	.022246	.022939	.023632	.024325	.025018	.025711	.026404	.027097	79
30	.020860	.021553	.022246	.022939	.023632	.024325	.025018	.025711	.026404	.027097	.027790	80
31	.021553	.022246	.022939	.023632	.024325	.025018	.025711	.026404	.027097	.027790	.028483	81
32	.022246	.022939	.023632	.024325	.025018	.025711	.026404	.027097	.027790	.028483	.029176	82
33	.022939	.023632	.024325	.025018	.025711	.026404	.027097	.027790	.028483	.029176	.029869	83
34	.023632	.024325	.025018	.025711	.026404	.027097	.027790	.028483	.029176	.029869	.030562	84
35	.024325	.025018	.025711	.026404	.027097	.027790	.028483	.029176	.029869	.030562	.031255	85
36	.025018	.025711	.026404	.027097	.027790	.028483	.029176	.029869	.030562	.031255	.031948	86
37	.025711	.026404	.027097	.027790	.028483	.029176	.029869	.030562	.031255	.031948	.032641	87
38	.026404	.027097	.027790	.028483	.029176	.029869	.030562	.031255	.031948	.032641	.033334	88
39	.027097	.027790	.028483	.029176	.029869	.030562	.031255	.031948	.032641	.033334	.034027	89
40	.027790	.028483	.029176	.029869	.030562	.031255	.031948	.032641	.033334	.034027	.034720	90
41	.028483	.029176	.029869	.030562	.031255	.031948	.032641	.033334	.034027	.034720	.035413	91
42	.029176	.029869	.030562	.031255	.031948	.032641	.033334	.034027	.034720	.035413	.036106	92
43	.029869	.030562	.031255	.031948	.032641	.033334	.034027	.034720	.035413	.036106	.036799	93
44	.030562	.031255	.031948	.032641	.033334	.034027	.034720	.035413	.036106	.036799	.037492	94
45	.031255	.031948	.032641	.033334	.034027	.034720	.035413	.036106	.036799	.037492	.038185	95
46	.031948	.032641	.033334	.034027	.034720	.035413	.036106	.036799	.037492	.038185	.038878	96
47	.032641	.033334	.034027	.034720	.035413	.036106	.036799	.037492	.038185	.038878	.039571	97
48	.033334	.034027	.034720	.035413	.036106	.036799	.037492	.038185	.038878	.039571	.040264	98
49	.034027	.034720	.035413	.036106	.036799	.037492	.038185	.038878	.039571	.040264	.040957	99
50	.034720	.035413	.036106	.036799	.037492	.038185	.038878	.039571	.040264	.040957	.041650	100



AUXILIARY TABLES.

TABLE X.—Products of  $S_4 \times .001$  up to  $S_4 \times 1.000$ .  $S_4 = \sin 60^\circ = .86603$ .

No.	.000	.001	.002	.003	.004	.005	.006	.007	.008	.009	No.
00	.00000	.00866	.01732	.02598	.03464	.04330	.05196	.06062	.06928	.07794	00
01	.00866	.01732	.02598	.03464	.04330	.05196	.06062	.06928	.07794	.08660	01
02	.01732	.02598	.03464	.04330	.05196	.06062	.06928	.07794	.08660	.09526	02
03	.02598	.03464	.04330	.05196	.06062	.06928	.07794	.08660	.09526	.10392	03
04	.03464	.04330	.05196	.06062	.06928	.07794	.08660	.09526	.10392	.11258	04
05	.04330	.05196	.06062	.06928	.07794	.08660	.09526	.10392	.11258	.12124	05
06	.05196	.06062	.06928	.07794	.08660	.09526	.10392	.11258	.12124	.12990	06
07	.06062	.06928	.07794	.08660	.09526	.10392	.11258	.12124	.12990	.13856	07
08	.06928	.07794	.08660	.09526	.10392	.11258	.12124	.12990	.13856	.14722	08
09	.07794	.08660	.09526	.10392	.11258	.12124	.12990	.13856	.14722	.15588	09
10	.08660	.09526	.10392	.11258	.12124	.12990	.13856	.14722	.15588	.16454	10
11	.09526	.10392	.11258	.12124	.12990	.13856	.14722	.15588	.16454	.17320	11
12	.10392	.11258	.12124	.12990	.13856	.14722	.15588	.16454	.17320	.18186	12
13	.11258	.12124	.12990	.13856	.14722	.15588	.16454	.17320	.18186	.19052	13
14	.12124	.12990	.13856	.14722	.15588	.16454	.17320	.18186	.19052	.19918	14
15	.12990	.13856	.14722	.15588	.16454	.17320	.18186	.19052	.19918	.20784	15
16	.13856	.14722	.15588	.16454	.17320	.18186	.19052	.19918	.20784	.21650	16
17	.14722	.15588	.16454	.17320	.18186	.19052	.19918	.20784	.21650	.22516	17
18	.15588	.16454	.17320	.18186	.19052	.19918	.20784	.21650	.22516	.23382	18
19	.16454	.17320	.18186	.19052	.19918	.20784	.21650	.22516	.23382	.24248	19
20	.17320	.18186	.19052	.19918	.20784	.21650	.22516	.23382	.24248	.25114	20
21	.18186	.19052	.19918	.20784	.21650	.22516	.23382	.24248	.25114	.25980	21
22	.19052	.19918	.20784	.21650	.22516	.23382	.24248	.25114	.25980	.26846	22
23	.19918	.20784	.21650	.22516	.23382	.24248	.25114	.25980	.26846	.27712	23
24	.20784	.21650	.22516	.23382	.24248	.25114	.25980	.26846	.27712	.28578	24
25	.21650	.22516	.23382	.24248	.25114	.25980	.26846	.27712	.28578	.29444	25
26	.22516	.23382	.24248	.25114	.25980	.26846	.27712	.28578	.29444	.30310	26
27	.23382	.24248	.25114	.25980	.26846	.27712	.28578	.29444	.30310	.31176	27
28	.24248	.25114	.25980	.26846	.27712	.28578	.29444	.30310	.31176	.32042	28
29	.25114	.25980	.26846	.27712	.28578	.29444	.30310	.31176	.32042	.32908	29
30	.25980	.26846	.27712	.28578	.29444	.30310	.31176	.32042	.32908	.33774	30
31	.26846	.27712	.28578	.29444	.30310	.31176	.32042	.32908	.33774	.34640	31
32	.27712	.28578	.29444	.30310	.31176	.32042	.32908	.33774	.34640	.35506	32
33	.28578	.29444	.30310	.31176	.32042	.32908	.33774	.34640	.35506	.36372	33
34	.29444	.30310	.31176	.32042	.32908	.33774	.34640	.35506	.36372	.37238	34
35	.30310	.31176	.32042	.32908	.33774	.34640	.35506	.36372	.37238	.38104	35
36	.31176	.32042	.32908	.33774	.34640	.35506	.36372	.37238	.38104	.38970	36
37	.32042	.32908	.33774	.34640	.35506	.36372	.37238	.38104	.38970	.39836	37
38	.32908	.33774	.34640	.35506	.36372	.37238	.38104	.38970	.39836	.40702	38
39	.33774	.34640	.35506	.36372	.37238	.38104	.38970	.39836	.40702	.41568	39
40	.34640	.35506	.36372	.37238	.38104	.38970	.39836	.40702	.41568	.42434	40
41	.35506	.36372	.37238	.38104	.38970	.39836	.40702	.41568	.42434	.43300	41
42	.36372	.37238	.38104	.38970	.39836	.40702	.41568	.42434	.43300	.44166	42
43	.37238	.38104	.38970	.39836	.40702	.41568	.42434	.43300	.44166	.45032	43
44	.38104	.38970	.39836	.40702	.41568	.42434	.43300	.44166	.45032	.45900	44
45	.38970	.39836	.40702	.41568	.42434	.43300	.44166	.45032	.45900	.46766	45
46	.39836	.40702	.41568	.42434	.43300	.44166	.45032	.45900	.46766	.47632	46
47	.40702	.41568	.42434	.43300	.44166	.45032	.45900	.46766	.47632	.48500	47
48	.41568	.42434	.43300	.44166	.45032	.45900	.46766	.47632	.48500	.49366	48
49	.42434	.43300	.44166	.45032	.45900	.46766	.47632	.48500	.49366	.50232	49
50	.43300	.44166	.45032	.45900	.46766	.47632	.48500	.49366	.50232	.51100	50



TABLE XII.—Constants for Long-Period Tide Computations.  
Motion of O, M, and N for certain periods.

Period.	Motion of O.	Motion of M.	Motion of N.	
For 11½ hours ...	160° 3449	333° 3172	327° 0569	
„ 1 day ...	334° 632854	335° 618501	322° 553510	
„ 100 days ...	343° 2854	81° 8501	215° 351	
„ 200 „ ...	326° 5709	163° 7002	70° 702	
„ 300 „ ...	309° 8563	245° 5502	286° 053	
„ 364 „ ...	126° 359002	125° 134291	49° 47779	
„ 1 day ...	25° 367146	24° 381499	37° 44649	Subtractive in using a 6-figure Arithmometer. See note below.

NOTE.—For O it would be necessary to add 334° 632854, or subtract 25° 367146 for each day's movement. This would only admit of 25° 3671 being used in a 6-figure Arithmometer. Adopting this plan, it is obvious that each daily position would be 0° 000046 too great, and it will be necessary to make an adjustment on this account. The position required is to be correct to three places of decimals of a degree.

Thus, 000046 would amount to { 00046 in 10 days } and as 0005 would affect the third place of decimals, the correction would be applied after 11 days' motion by subtracting 001 from the third place of decimals shown in the Arithmometer. Similarly, after 33 days' motion 001 would again have to be subtracted, and so on. The corrections will therefore be 001 after 11 days' motion, i.e. on 12th day, reckoning the starting day; after 33 days, or on 34th day; and after 55, 77, 98, 120, 142, 164, 185, 207, 229, 250, 272, 294, 316, 337, and 359 days' motion.

For M similarly 335° 618501 has to be added, or 24° 381499 to be subtracted, i.e. for the 6-figure Arithmometer 24° 3815 is subtracted. This would be 000001 too much to be subtracted daily, or in 365 days it would amount to 000365, which will not affect the third place of decimals. No correction is therefore required.

For N, 322° 553510 has to be added, or 37° 446490 to be subtracted. Thus 37° 4465 would be fixed in the Arithmometer. This would be 00001 too much to subtract daily, and the correction on this account would be arrived at by adding 001 after 50 days' motion, i.e. on 51st day, reckoning the starting day; and after 150, 250, and 350 days' motion, i.e. on 151st, 251st, and 351st day.

TABLE XIII.—Natural Numbers to three places of Decimals corresponding to Logarithms with Indices 6, 7, and 8.

Logarithms with Index 6 or 4.

Natural No.	Natural No. to 3 places of Decimals	Logarithms
00000	000	0000000
00050	001	6989700
00099	001	9999999

Logarithms with Index 7 or 3.

Nat. No.	Nat. No. to 3 places of Decimals	Logarithms	Nat. No.	Nat. No. to 3 places of Decimals	Logarithms	Nat. No.	Nat. No. to 3 places of Decimals	Logarithms
0010	001	0000000	0045	005	6532125	0085	009	9294189
0015	002	1760913	0055	006	7403627	0095	010	9777236
0025	003	3979400	0065	007	8129134	0099		9999999
0035	004	5440680	0075	008	8750613			
0045		6532127	0085		9294189			

Logarithms with Index 8 or 2.

Nat. No.	Nat. No. to 3 places of Decimals	Logarithms	Nat. No.	Nat. No. to 3 places of Decimals	Logarithms	Nat. No.	Nat. No. to 3 places of Decimals	Logarithms	Nat. No.	Nat. No. to 3 places of Decimals	Logarithms
0100	010	0000000	0325	033	5118834	0555	056	7442930	0785	079	8948697
0105	011	0211893	0335	034	5250448	0565	057	7520484	0795	080	9003671
0115	012	0606978	0345	035	5378191	0575	058	7596678	0805	081	9057959
0125	013	0969100	0355	036	5502284	0585	059	7671559	0815	082	9111576
0135	014	1303338	0365	037	5622929	0595	060	7745170	0825	083	9164339
0145	015	1613680	0375	038	5740313	0605	061	7817554	0835	084	9216865
0155	016	1903317	0385	039	5854607	0615	062	7888751	0845	085	9268467
0165	017	2174839	0395	040	5965971	0625	063	7958800	0855	086	9319661
0175	018	2430380	0405	041	6074550	0635	064	8027337	0865	087	9370161
0185	019	2671717	0415	042	6180481	0645	065	8095597	0875	088	9420081
0195	020	2900346	0425	043	6283889	0655	066	8162413	0885	089	9469433
0205	021	3117539	0435	044	6384893	0665	067	8228216	0895	090	9518230
0215	022	3324385	0445	045	6483600	0675	068	8293338	0905	091	9566486
0225	023	3521825	0455	046	6580114	0685	069	8356906	0915	092	9614211
0235	024	3710679	0465	047	6674530	0695	070	8419848	0925	093	9661417
0245	025	3891661	0475	048	6766936	0705	071	8481891	0935	094	9708116
0255	026	4054402	0485	049	6857417	0715	072	8543060	0945	095	9754318
0265	027	4212459	0495	050	6946052	0725	073	8603380	0955	096	9800034
0275	028	4393327	0505	051	7032914	0735	074	8662733	0965	097	9845273
0285	029	4548449	0515	052	7118072	0745	075	8721563	0975	098	9890046
0295	030	4698220	0525	053	7201593	0755	076	8779470	0985	099	9934362
0305	031	4842998	0535	054	7283538	0765	077	8836614	0995	100	9978231
0315	032	4983106	0545	055	7363965	0775	078	8893017	0999		9999999
0325		5118834	0555		7442930	0785		8948697			

TABLE XIV.—Values of N (Longitude of Moon's Ascending Node) for 0 hour Greenwich Mean Time, January 1.

Value on 0 hour G. M. T., January 1st, 1880 = 285° 936863. Motion per Julian year in 1880 = 19° 34146248. Motion for 365 days = 19° 31822387 and for 1 day = 0° 052954.

Table with 8 columns: Year, N, Year, N, Year, N, Year, N. It lists values for years 1850 through 1870, with two columns for each year.

TABLE XV.—Showing the Decrement of N (Longitude of Moon's Ascending Node) since 0 hour January 1 up to Midnight of each Day throughout the Year.

Daily Motion = 0° 0529541.

In Leap Years for all dates after February 28—March 1, use a mean value between the particular day and the day following.

Table with 12 columns: Date, Decrs., Date, Decrs., Date, Decrs., Date, Decrs., Date, Decrs., Date, Decrs. It shows decrements for various months including JAN., FEB., and AUG.

N.B.—In Table XV. The middle of the year of observations will occur at noon or midnight according as the 29th February is included in the period of observations or not. If the midnight falls on a date in a common year, or before the 29th February in a leap year, then the Decrement for N as given in the Table is correct: if, however, the midnight falls after the 29th February in a leap year, then take the value as that given for the succeeding date in the Table. If the noon falls in a common year or before the 29th February in a leap year, the

TABLE XV.—Showing the Decrement of N (Longitude of Moon's Ascending Node) since 0 hour January 1 up to Midnight of each Day throughout the Year—(Continued).

Daily Motion = 0° 0529541.

In Leap Years for all dates after February 28—March 1, use a mean value between the particular day and the day following.

Large table with 12 columns: Date, Decre., Date, Decre., Date, Decre., Date, Decre., Date, Decre., Date, Decre. It continues the data from Table XIV, covering months from MAY to NOV.

value to be taken from the Table is the mean between the preceding and succeeding midnights: but if the noon falls after the 29th February in a leap year, the mean between the values for the two midnights immediately following is to be taken.

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TABLE XVIII.—Values of  $I$ ,  $\nu$  and  $\xi$ , corresponding to  $N$ .

$N$	$I$	$\nu$	$\xi$	$N$	$I$	$\nu$	$\xi$	$N$	$I$	$\nu$	$\xi$	$N$	$I$	$\nu$	$\xi$	$N$								
0	28	002	0	000	360	0	30	528	005	5	564	5	015	320	5	60	526	351	10	31	9	106	209	5
1	28	002	0	004	359	5	31	527	008	5	563	5	014	320	5	61	526	351	10	31	9	106	209	5
2	28	002	0	008	358	10	31	527	005	5	562	5	013	320	5	62	526	351	10	31	9	106	209	5
3	28	002	0	012	357	15	31	527	002	5	561	5	012	320	5	63	526	351	10	31	9	106	209	5
4	28	002	0	016	356	20	31	527	000	5	560	5	011	320	5	64	526	351	10	31	9	106	209	5
5	28	002	0	020	355	25	31	527	000	5	559	5	010	320	5	65	526	351	10	31	9	106	209	5
6	28	002	0	024	354	30	31	527	000	5	558	5	009	320	5	66	526	351	10	31	9	106	209	5
7	28	002	0	028	353	35	31	527	000	5	557	5	008	320	5	67	526	351	10	31	9	106	209	5
8	28	002	0	032	352	40	31	527	000	5	556	5	007	320	5	68	526	351	10	31	9	106	209	5
9	28	002	0	036	351	45	31	527	000	5	555	5	006	320	5	69	526	351	10	31	9	106	209	5
10	28	002	0	040	350	50	31	527	000	5	554	5	005	320	5	70	526	351	10	31	9	106	209	5
11	28	002	0	044	349	55	31	527	000	5	553	5	004	320	5	71	526	351	10	31	9	106	209	5
12	28	002	0	048	348	60	31	527	000	5	552	5	003	320	5	72	526	351	10	31	9	106	209	5
13	28	002	0	052	347	65	31	527	000	5	551	5	002	320	5	73	526	351	10	31	9	106	209	5
14	28	002	0	056	346	70	31	527	000	5	550	5	001	320	5	74	526	351	10	31	9	106	209	5
15	28	002	0	060	345	75	31	527	000	5	549	5	000	320	5	75	526	351	10	31	9	106	209	5
16	28	002	0	064	344	80	31	527	000	5	548	5	000	320	5	76	526	351	10	31	9	106	209	5
17	28	002	0	068	343	85	31	527	000	5	547	5	000	320	5	77	526	351	10	31	9	106	209	5
18	28	002	0	072	342	90	31	527	000	5	546	5	000	320	5	78	526	351	10	31	9	106	209	5
19	28	002	0	076	341	95	31	527	000	5	545	5	000	320	5	79	526	351	10	31	9	106	209	5
20	28	002	0	080	340	100	31	527	000	5	544	5	000	320	5	80	526	351	10	31	9	106	209	5
21	28	002	0	084	339	105	31	527	000	5	543	5	000	320	5	81	526	351	10	31	9	106	209	5
22	28	002	0	088	338	110	31	527	000	5	542	5	000	320	5	82	526	351	10	31	9	106	209	5
23	28	002	0	092	337	115	31	527	000	5	541	5	000	320	5	83	526	351	10	31	9	106	209	5
24	28	002	0	096	336	120	31	527	000	5	540	5	000	320	5	84	526	351	10	31	9	106	209	5
25	28	002	0	100	335	125	31	527	000	5	539	5	000	320	5	85	526	351	10	31	9	106	209	5
26	28	002	0	104	334	130	31	527	000	5	538	5	000	320	5	86	526	351	10	31	9	106	209	5
27	28	002	0	108	333	135	31	527	000	5	537	5	000	320	5	87	526	351	10	31	9	106	209	5
28	28	002	0	112	332	140	31	527	000	5	536	5	000	320	5	88	526	351	10	31	9	106	209	5
29	28	002	0	116	331	145	31	527	000	5	535	5	000	320	5	89	526	351	10	31	9	106	209	5
30	28	002	0	120	330	150	31	527	000	5	534	5	000	320	5	90	526	351	10	31	9	106	209	5

$N, B, -I$  is always positive. When  $N$  is between  $0^\circ$  and  $180^\circ$ ,  $\nu$  and  $\xi$  are positive, when  $N$  is between  $180^\circ$  and  $360^\circ$ ,  $\nu$  and  $\xi$  are negative.

TABLE XVI.—Values of  $p_1$  (Mean Longitude of Solar Perigee) for 0 hour, January 1.

$p_1$  for 0 hour, January 1, 1880 =  $280^\circ 87' 48.02$ .  
Motion per Julian year =  $0^\circ 01' 17.10933$ .  
Motion for 365 days =  $0^\circ 01' 7.09295$ .

Year	$p_1$	Year	$p_1$	Year	$p_1$	Year	$p_1$
1850	$280^\circ 36' 14$	1875	$280^\circ 7' 892$	1900	$281^\circ 21' 71$	1925	$281^\circ 64' 50$
51	$3785$	76	$8603$	1	$2342$	26	$6631$
52	$3956$	77	$8535$	2	$2313$	27	$6792$
53	$4125$	78	$8466$	3	$2284$	28	$6953$
54	$4299$	79	$8397$	4	$2255$	29	$7115$
55	$4470$	80	$8328$	5	$3027$	30	$7276$
56	$4641$	81	$8259$	6	$3198$	31	$7437$
57	$4812$	82	$8190$	7	$3369$	32	$7598$
58	$4983$	83	$8121$	8	$3540$	33	$7759$
59	$5154$	84	$8052$	9	$3711$	34	$7920$
60	$5325$	85	$7983$	10	$3882$	35	$8081$
61	$5497$	86	$7914$	11	$4053$	36	$8242$
62	$5668$	87	$7845$	12	$4224$	37	$8403$
63	$5839$	88	$7776$	13	$4395$	38	$8564$
64	$6010$	89	$7707$	14	$4566$	39	$8725$
65	$6181$	90	$7638$	15	$4737$	40	$8886$
66	$6352$	91	$7569$	16	$4908$	41	$9047$
67	$6523$	92	$7500$	17	$5079$	42	$9208$
68	$6694$	93	$7431$	18	$5250$	43	$9369$
69	$6865$	94	$7362$	19	$5421$	44	$9530$
70	$7036$	95	$7293$	20	$5592$	45	$9691$
71	$7207$	96	$7224$	21	$5763$	46	$9852$
72	$7378$	97	$7155$	22	$5934$	47	$10013$
73	$7549$	98	$7086$	23	$6105$	48	$10174$
74	$7720$	99	$7017$	24	$6276$	49	$10335$

TABLE XVII.—Increment of  $p_1$  since 0 hour, January 1, for certain Days of the Year.

Motion for 1 day =  $0^\circ 00' 00.04683$ .

Date	Increment	Date	Increment	Date	Increment	Date	Increment
Jan. 10	$0^\circ 00' 42$	July 9	$0^\circ 08' 85$	Oct. 7	$0^\circ 13' 97$		
" 20	$00' 66$	" 19	$09' 32$	" 17	$14' 53$		
" 30	$01' 36$	" 29	$09' 79$	" 27	$16' 00$		
Feb. 9	$01' 83$	Aug. 6	$10' 26$	Nov. 6	$11' 47$		
" 19	$02' 51$	" 18	$11' 07$	" 16	$13' 41$		
" 30	$04' 09$	" 28	$11' 19$	" 26	$15' 35$		
Mar. 1	$04' 56$	Sept. 9	$11' 06$	Dec. 6	$16' 34$		
" 11	$05' 33$	June 9	$07' 45$	" 16	$17' 33$		
" 21	$06' 10$	" 19	$08' 71$	" 26	$18' 32$		
" 31	$06' 47$	" 29	$08' 38$	" 26	$19' 31$		

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TABLE XIX. (1).—Values of 1/f and f corresponding to various values of I, to be used in computing H and R for the Tides M<sub>2</sub>, N, 2N,  $\nu$ , MS, 2SM and Luni-Solar fortnightly.

Argument 1/f = Cor<sup>h</sup> + Cor<sup>k</sup> h.

Table with columns for Values of I, Differences, 1/f, f, Values of I, Differences, 1/f, f, and Differences. Includes numerical values for I, 1/f, and f across various arguments.

TABLE XVIII.—Values of I,  $\nu$  and  $\xi$ , corresponding to N.—(Continued).

Table with columns for N, I, nu, xi, N, I, nu, xi, N, I, nu, xi, N, I, nu, xi. Lists numerical values for these variables across multiple rows.

N, I, nu, xi are always positive. When N is between 0° and 180°, nu and xi are positive; when N is between 180° and 360°, nu and xi are negative.

AUXILIARY TABLES.

Argument 1/f = Sin ω Cos ω (1 - 3/4 Sin² ω) / Sin I Cos I

Table with columns: Values of I, 1/f, Differences for 1 of I, f, Differences for 1 of f, Values of I, 1/f, Differences for 1 of I, f, Differences for 1 of f.

Argument 1/f = Sin ω Cos² 1/2 ω Cos 1/2 I / Sin I Cos² 1/2 I

Table with columns: Values of I, 1/f, Differences for 1 of I, f, Differences for 1 of f, Values of I, 1/f, Differences for 1 of I, f, Differences for 1 of f.

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TABLE XIX. (5)—Values of 1/f and f corresponding to various values of I, to be used in computing H and R for the Tide Mm.

Argument 1/f = (1 - 3 sin^2 ω) (1 - 3/4 sin^2 I)

Table with columns: Values of I, 1/f, f, Differences for 0.1 of I, Values of I, 1/f, f, Differences for 0.1 of I.

TABLE XIX. (4)—Values of 1/f and f corresponding to various values of I, to be used in computing H and R for the Tide Mf.

Argument 1/f = (sin^2 ω cos^2 I) / sin^2 I

Table with columns: Values of I, 1/f, f, Differences for 0.1 of I, Values of I, 1/f, f, Differences for 0.1 of I.



AUXILIARY TABLES.

TABLE XIX. (7) — Values of 1/f and f corresponding to various values of I, to be used in computing H and R for the Tide K<sub>2</sub>.

Argument 1/f = {1 + (0.46407 \* k<sub>2</sub>)<sup>2</sup> + 0.92814k<sub>2</sub> Cos 2ν} 1/2 where k<sub>2</sub> = Sin<sup>2</sup> ω (1 - 3/4 Sin<sup>2</sup> ε)

Table with columns: Values of I, 1/f, Differences, f, Differences, Values of I, 1/f, Differences, f, Differences. Rows range from 18° 18' 30" to 28° 36' 6".

TABLE XIX. (6) — Values of 1/f and f corresponding to various values of I, to be used in computing H and R for the Tide K<sub>1</sub>.

Argument 1/f = {1 + (0.46407 \* k<sub>1</sub>)<sup>2</sup> + 0.92814k<sub>1</sub> Cos ν} 1/2 where k<sub>1</sub> = Sin ω Cos ε (1 - 3/4 Sin<sup>2</sup> ε)

Table with columns: Values of I, 1/f, Differences, f, Differences, Values of I, 1/f, Differences, f, Differences. Rows range from 18° 18' 30" to 28° 36' 6".

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TABLE XXI.—Values of  $2\nu''$  corresponding to  $I$ , to determine initial argument of Tide  $K_2$ .

$$\tan 2\nu'' = \frac{\sin 2\nu}{\cos 2\nu + 0.46407 \times k_2} \text{ where } k_2 = \frac{\sin^2 \omega (1 - \frac{3}{2} \sin^2 i)}{\sin^2 i}$$

$I$	$2\nu''$	Differences for $0^{\circ}1$ of $I$	$I$	$2\nu''$	Differences for $0^{\circ}1$ of $I$	$I$	$2\nu''$	Differences for $0^{\circ}1$ of $I$	$I$	$2\nu''$	Differences for $0^{\circ}1$ of $I$	$I$	$2\nu''$	Differences for $0^{\circ}1$ of $I$
18 18 30	0 000	0	20 4	13 963	0 265	22 5	17 422	0 072	24 6	17 463	0 078	26 7	0	0
18 4	2 810	1 738	5 14	228	2 46	6 17	494	0 088	8 17	299	0 086	9	13 331	3 19
5	4 548	0 983	6 14	474	2 40	8 17	621	0 082	9 17	204	0 095	27 0	13 012	3 48
6	5 531	0 907	7 14	714	2 27	9 17	673	0 082	25 0	17 105	0 113	2	12 305	3 59
7	6 438	0 758	8 14	941	2 16	23 0	17 720	0 085	1 16	992	0 117	3	11 922	4 09
8	7 196	0 674	9 15	157	2 10	1 17	755	0 082	3 16	875	0 128	4	11 513	4 23
9	7 870	0 632	1 15	561	1 94	2 17	787	0 083	4 16	611	0 142	5	11 090	4 70
19 0	8 502	0 549	2 15	750	1 89	3 17	810	0 082	5 16	469	0 157	6	10 620	4 91
1	9 051	0 528	3 15	929	1 79	4 17	826	0 082	6 16	312	0 162	7	10 129	5 29
2	9 579	0 488	4 16	097	1 68	5 17	838	0 084	8 15	978	0 184	8	9 600	5 83
3	10 067	0 454	5 16	261	1 49	6 16	834	0 084	9 15	794	0 189	9	9 017	6 09
4	10 521	0 438	6 16	410	1 45	7 16	822	0 082	26 0	15 605	0 207	2	8 408	7 20
5	10 959	0 399	7 16	555	1 36	8 16	691	0 082	1 15	398	0 213	3	7 688	7 80
6	11 358	0 388	8 16	691	1 36	9 16	802	0 084	2 15	185	0 213	4	6 908	9 01
7	11 746	0 364	9 16	817	1 26	10 16	817	0 082	3 14	959	0 226	5	6 007	1 066
8	12 110	0 346	10 16	939	1 22	11 17	742	0 082	4 14	720	0 239	6	5 354	1 300
9	12 456	0 336	11 17	048	1 09	12 17	653	0 082	5 14	475	0 245	7	4 841	1 483
20 0	12 792	0 310	12 17	153	1 05	13 17	563	0 082	6 14	270	0 256	8	4 366	1 666
1	13 102	0 303	13 17	250	0 97	14 17	597	0 082	7 14	175	0 268	9	3 931	1 859
2	13 405	0 286	14 17	338	0 88	15 17	536	0 082	8 14	107	0 276	10	3 541	2 052
3	13 691	0 272	15 17	422	0 84	16 17	469	0 082	9 14	63	0 283	11	3 191	2 255
4	13 963	0 267	16 17	463	0 81	17 17	403	0 082	10 14	27	0 287	12	2 881	2 468

$N.B.$ —In the above table  $2\nu''$  is positive when  $N$  is between  $0^{\circ}$  and  $180^{\circ}$ , and negative when  $N$  is between  $180^{\circ}$  and  $360^{\circ}$ ; thus it is necessary to observe what is the value of  $N$ , because  $I$  is always positive.

TABLE XX.—Values of  $\nu'$  corresponding to  $I$ , to determine initial argument of Tide  $K_1$ .

$$\tan \nu' = \frac{\sin \nu}{\cos \nu + 0.46407 \times k_1} \text{ where } k_1 = \frac{\sin \omega \cos \omega (1 - \frac{3}{2} \sin^2 i)}{\sin i \cos i}$$

$I$	$\nu'$	Differences for $0^{\circ}1$ of $I$	$I$	$\nu'$	Differences for $0^{\circ}1$ of $I$	$I$	$\nu'$	Differences for $0^{\circ}1$ of $I$	$I$	$\nu'$	Differences for $0^{\circ}1$ of $I$			
18 18 30	0 000	0	20 4	17 363	0 124	22 5	8 819	0 021	24 6	8 567	0 049	26 7	6 672	0 145
18 4	1 557	0 958	5 7	487	1 12	7 8	840	0 10	8 17	518	0 53	8	6 527	1 55
5	2 515	0 534	6 7	599	1 09	8 8	875	0 16	9 17	465	0 57	9	6 372	1 58
6	3 049	0 491	7 7	708	1 03	9 8	408	0 59	1 16	408	0 59	1	6 042	1 72
7	3 540	0 461	8 8	811	0 96	10 8	886	0 11	2 15	349	0 65	2	5 865	1 77
8	3 946	0 358	9 7	907	0 93	11 8	896	0 10	3 15	284	0 68	3	5 678	1 87
9	4 304	0 334	10 8	000	0 85	12 8	900	0 04	4 16	216	0 71	4	5 478	2 00
19 0	4 638	0 334	11 8	085	0 81	13 8	901	0 01	5 16	145	0 76	5	5 272	2 06
1	4 924	0 286	12 8	166	0 77	14 8	900	0 01	6 16	069	0 78	6	5 044	2 28
2	5 198	0 274	13 8	243	0 70	15 8	894	0 06	7 16	991	0 85	7	4 807	2 37
3	5 449	0 251	14 8	313	0 68	16 8	886	0 08	8 15	906	0 88	8	4 551	2 56
4	5 680	0 231	15 8	381	0 61	17 8	873	0 13	9 15	818	0 92	9	4 271	2 92
5	5 903	0 223	16 8	442	0 59	18 8	858	0 15	10 16	726	0 97	10	3 979	3 44
6	6 102	0 199	17 8	501	0 53	19 8	839	0 19	11 17	629	1 00	11	3 635	3 72
7	6 295	0 193	18 8	554	0 49	20 8	817	0 22	12 17	529	1 07	12	3 263	4 27
8	6 475	0 160	19 8	603	0 47	21 8	792	0 25	13 17	422	1 11	13	2 836	4 82
9	6 644	0 169	20 8	650	0 47	22 8	763	0 29	14 17	311	1 16	14	2 283	5 53
20 0	6 807	0 163	21 8	690	0 40	23 8	731	0 32	15 17	195	1 23	15	1 669	6 14
1	6 956	0 149	22 8	728	0 38	24 8	695	0 36	16 17	072	1 25	16	1 027	6 82
2	7 100	0 144	23 8	762	0 34	25 8	655	0 40	17 17	947	1 25	17	0 366	7 58
3	7 236	0 136	24 8	791	0 29	26 8	614	0 41	18 17	811	1 36	18	28 36 6	8 40
4	7 363	0 127	25 8	819	0 28	27 8	567	0 47	19 17	672	1 39	19	21 391	9 26

$N.B.$ —In the above table  $\nu'$  is positive when  $N$  is between  $0^{\circ}$  and  $180^{\circ}$ , and negative when  $N$  is between  $180^{\circ}$  and  $360^{\circ}$ ; thus it is necessary to observe what is the value of  $N$ , because  $I$  is always positive.

## CHAPTER VIII.

## TIDAL PREDICTION.

## 1.

*Harmonic Tide-predicting Machine.*

The harmonic tide-predicting machine is an instrument designed for the purpose of doing away with the great mass of computations which would be necessary to obtain the heights and times of high and low waters for each day in the year as published in the *Tide-tables for the Indian Ports*. The height of the tide at any instant being the sum of the ordinates of a considerable number of harmonic curves representing the various simple tides, it would be necessary to compute each of these ordinates for several hours each day about the times of high and low waters and add the results together: the machine makes the computations and the addition automatically and exhibits the result in the form of a curve from which the heights and times can at once be read off.

The machine under consideration was constructed for the Government of India for the prediction of the tides of India and the adjacent coasts, but owing to the delicacy of its mechanism it was deemed advisable not to expose it to the risks of transit to India, and it was therefore erected at the observatory of the India Stores Department, London.

The tidal constants or components used on the machine are those determined in the Office of the Tidal and Levelling Party at Poona from the records obtained from automatic self-registering tide-gauges in operation at the different ports. These constants are regularly transmitted to Mr. Roberts under whose direction the tidal predictions contained in the tide-tables are produced.

In the original design of 1879, the number of tidal components combined by the machine was twenty, *viz.* :—

				Numbered on Machine.
The mean lunar semi-diurnal tide, $M_2$	...	...	...	1
The mean solar semi-diurnal tide, $S_2$	...	...	...	2
Two lunar elliptic semi-diurnal tides, $N$ and $L$	...	...	...	5 and 10
Two lunar "evectional" semi-diurnal tides, $\nu$ and $\lambda$	...	...	...	9 „ 11
One lunar "variational" semi-diurnal tide, $\mu$	...	...	...	8
One lunar declinational diurnal tide, $O$	...	...	...	4
One solar declinational diurnal tide, $P$	...	...	...	6
One luni-solar declinational diurnal tide, $K_1$	...	...	...	3
One luni-solar declinational semi-diurnal tide, $K_2$	...	...	...	7
Two lunar declinational elliptic diurnal tides, $J$ and $Q$	...	...	...	13 and 12
One compound luni-solar quarter-diurnal tide, $MS$	...	...	...	14
One compound luni-solar semi-diurnal tide, $2SM$	...	...	...	15
One mean solar diurnal tide, $S_1$	...	...	...	20
Two mean lunar "over-tides" of the semi-diurnal tide, $M_4$ and $M_6$	...	...	...	18 and 19
One solar annual elliptic tide, $\eta$ or $S_a$	...	...	...	16
One solar semi-annual declinational tide, $2\eta$ or $S_{sa}$	...	...	...	17

In the spring of 1891 one new semi-diurnal and three new "compound" components were added to the machine and the larger solar elliptic semi-diurnal component ( $T$ ) substituted in the place of the smaller "evectional" semi-diurnal tide ( $\lambda$ ) which is of small value.

The new components are as follow :—

				Numbered on Machine.
One second-order lunar elliptic semi-diurnal tide, $2N$	...	...	...	21
One compound lunar quarter-diurnal tide, $M_2N$	...	...	...	22
Two compound lunar ter-diurnal tides, $2M_2K_1$ and $M_2K_1$	...	...	...	23 and 24
One larger solar elliptic semi-diurnal tide, $T$	...	...	...	11

These additions and the substitution raise the number of components now on the machine to twenty-four.

The machine, a front and a side view of which are given in Plate IX, consists of a plate of gun-metal of oval form measuring about 3 feet 8 inches wide by 3 feet deep, supported on two standards. Upon this plate, which supports the crank-axes of the different movements, are fitted all the guide pillars and bars of the parallel slides, hereafter described. At the back of the plate, and distant from it some 6 inches, are bolted two skeleton plates,  $P$ , (see Fig. 2, Plate IX and Fig. 1, Plate X) carrying the other ends of the crank-axes, which are provided with pointers,  $a$ , (see Plate X) for setting, and also with dials,  $b$ , divided into degrees, or to 360ths of the period of the tidal components. Between the plates are a horizontal centre main shaft,  $c$ , (see Plates IX and X) and four oblique shafts,  $d$ , (see Plate X) turning in the same time, the oblique shafts being driven through the main shaft, two from each end. The main shaft receives its motion from clock-work driving gear at the bottom of the machine through the approximately

vertical shafts, *e*, (see Plates IX and X) pinned together. Rivetted to the oblique shafts and the main driving shaft are the bevel wheels, *f*, (see Fig. 1, Plate X) which are geared with other bevel wheels, *g*, provided on their axes with endless screws, *h*, working into wheels, *i*, (see Figs. 1 and 2, Plate X) on the crank-axes of the several components. The clock-work driving gear also gives motion to the centre recording barrel, *j*, (see Fig. 3, Plate X) and through it to the receiving drum-barrel, *y*. The tracing point moves vertically up and down in the frame immediately in front of the recording barrel.

Perhaps the chief difficulty in the construction of the machine is the finding, within reasonable limits, of proportions which represent with sufficient accuracy the periods of the respective tidal components, in order that the machine may be used for a considerable period of prediction—say for twelve months' tides. Very great success has been attained in this respect in the present instrument. For instance, the error of the period of the chief component—the mean lunar semi-diurnal—relatively to the mean solar semi-diurnal, is inappreciable during a whole year's predictions, amounting to about 0.10 degree only in a period of fifty years. The greatest deviation from strict accuracy is 0.37 degree after a run representing twelve months. This is, however, one of the smaller components, and insensible in its effect. This part of the design may therefore be regarded as practically perfect.

A crank, *k*, (see Plate X, Fig. 2, and Plate XI), is fitted to the axis, *l*, of each component. A sliding piece, carrying a steel guiding pin, *m*, for setting, is fitted in each crank. The guiding pin is thrown out from the centre of the crank-axis by means of a fine cut screw of half millimetre pitch, and micrometer head, *n*. The requisite distance of the throw of the guiding pin is previously determined by the proper analysis of the tidal observations of the port for which the predictions are required. It may be here remarked that a year's tidal observations will yield fairly good constants, but a longer period of observations is very desirable, the general limit of the smaller Indian ports being five years, whilst at the more important ports the registration of tidal observations is continuous. A horizontal cross-head, *o*, (see Plate XI) carries at its centre a very light and well-balanced pulley, *p*, (see Plate X, Fig. 2, and Plate XI). The cross-head is fitted at one end with an adjustable steel rod guide, *q*, moving freely in two pillar guides, *G*, (see Plate XI), drilled out nearly their entire length to reduce the touching parts to a minimum. The opposite end of the cross-head carries a projecting fork guide, which travels with freedom on either side of a narrow, flat brass bar guide, *r*, supported on pillars. The steel rod guide, *q*, of the cross-head is balanced by an adjustable sliding weight, *W*, fitted in continuation of the projecting fork guide, so that the centre of gravity of the cross-head and guide is in a vertical through the centre of the axis of the pulley. [The cross-head thus balanced is counterpoised by a cord and weight passing over pulleys at some distance above it, in a vertical through its centre of gravity and the axis of the pulley as shewn in Fig. 1, Plate IX]. At the back of the cross-head are fitted two parallel steel jaws, *s*, (see Plate X, Fig. 2, and Plate XI), the lower one adjustable, in order that the distance between them can be regulated. Both the brass bar guide, *r*, and the steel rod guide, *q*, are divided to millimetres; the brass bar guide for approximate and the steel rod guide for the accurate adjustment of the throw of the crank-pin, for which purpose the upper pillar guide of the steel rod guide is furnished with a vernier. The flat brass bar guide is movable through a small range for perfect adjustment to zero. The head of the micrometer, *n*, is also divided, and may be used with the divisions of the brass bar guide. The cross-head, *o*, is movable on its steel rod guide, *q*, for the perfect adjustment of the pulley about the centre of motion of the crank-axis. The fine-toothed wheel, *i*, into which the endless screw, *h*, works as previously described, is fitted on a slotted cone, *u*, (see Fig. 2, Plate X) which can be clamped to the crank-axis by means of a screw-nut, *v*. This arrangement is necessary, because each of the components requires to be set in its proper position, previously determined by calculation, at the commencement before starting the machine. The setting dials, *b*, are toothed round their outer edges and movable round their centres by a pinion for setting.

A fine flexible wire fixed to a large screw-head, *S*, (see Fig. 1, Plate IX) below the date-dial, passes alternately under and over the pulleys of the lower and upper series of components, till leaving the

large pulley, it hangs vertically above the ink-recorder slide. The screw-head allows of the pen point of the ink-recorder being brought accurately to zero, when the components are each set to zero or brought to zero of their respective scales. A back screw to the screw-head prevents the latter from slipping when properly adjusted. It is necessary that this zero should be determined before the curves are run off, on account of the variation of the length of wire from change of temperature. The wire carries at its free end an ink-bottle fitted with a fine glass tracing point. The ink-recorder travels in a geometrical slide, and is suspended to give just sufficient pressure to ensure contact with the paper of recording barrel. The recording barrel is fitted with brass pins at equidistant intervals, to form the time indications on the paper by perforation. A vertical automatic ruling apparatus is available for ruling the vertical time lines, but on account of the recording paper being very thin, the resulting inked line is not always so perfect as desirable. In practice it has been found better to rule the time lines through the machine perforations by hand, a whole year's rulings only occupying about an hour and a half. An index for setting the recording barrel to time is fitted behind the framework near the upper axis of the barrel. The paper, which is continuous, and supplied from a reel, *w*, (see Fig. 3, Plate X) passes round two grooved rollers, *x*, at the back of the recording barrel, and is held in position whilst the pins enter the paper, and, after receiving the traced curves, is wound round the receiving barrel, *y*. The reel, on which the continuous paper is contained, is provided with a brake brush, which ensures a proper tension of the paper as it leaves the reel. The receiving barrel rests on toothed driving wheels, which are driven by the recording barrel, and by friction turns and slips to accommodate itself to receive the recorded paper. Motion is given to the whole system of wheel-work through the horizontal centre main shaft, *c*, from a clock-work driving gear at the bottom of the machine, the whole being originally driven by a weight of about one hundred-weight, and controlled by a fan. A warning bell sounds when the weight is nearly run down, and also when in winding, the operation is nearly completed. The length of the barrel round which the cord is wound is sufficient to give 15,000 turns of the main shaft. This corresponds to about three months' run of curves, and occupies about one hour to run off. A year's tides for any port occupy about four hours in running off.

In consequence of the height of the building in which the machine was placed not admitting of the full length of the cord being used, multiple pulleys had to be employed, thereby increasing the driving weight; the time occupied, however, was reduced to about two hours for a year's predictions. In 1891, when the components were augmented, advantage was taken of continuous water power, and a small water-motor, *M*, (see Fig. 1, Plate IX) was fitted for driving the machine with perfect success and regularity, the time occupied being about two hours, for a full year's predictions: the motor, *M*, has been omitted in Fig. 2 of Plate IX for clearness. The weight-driving gear is also available in case of failure from the water supply.

The setting of the machine for the prediction of any port, for which the tidal components are known, is as follows:—The dials, *b*, are first turned so that the value of  $\kappa$  found from the tidal reductions, is exactly under or above the highest or lowest point according as the component is situated on the upper or lower row of components. The cranks, *k*, are set vertically—the slotted cone, *u*, (see Fig. 2, Plate X) of the wheel, *i*, on the axle, *l*, having been first released—and the guide-pin, *m*, thrown out to its proper range according to the scale required to represent the half amplitude of the component. The scale on which the predictions are represented varies from a half-inch to the foot in the case of Bhavnagar to six inches (or half actual scale) to the foot for the Ceylon and adjacent ports. The width of the recording paper is twenty-two inches. The setting scale being in millimetres, to represent the curves on a scale of one inch to the foot for setting it is necessary to multiply the value in feet of each half-amplitude ( $\frac{1}{2}R$ ) by 25·4 or each amplitude (*R*) by 12·7, and in proportion for other scales. The proper position of the hands, *a*, having been previously determined by calculation for the time of starting, the hands are set and the slotted cones are tightened up. These positions are the values of  $V_0 + u$  and are generally found for noon of the day preceding the first day for which the predictions are required. The angles, *l*

are in this way automatically found on the machine. The recording barrel, which is twenty-four inches in circumference, is then set to the time for which the values of  $V_0 + u$  have been found, and the wheel-work set in motion.

The date-dial in the centre shows the progress of the record, which can be marked occasionally to facilitate the entry of the dates after the record has been removed from the machine. The date-dial containing only twenty-eight days for February, care should be taken to date the record one day back after March 1 in bissextile years, or to shift the dial hand back one day when it has arrived at March 1, by which means the dates will then correspond correctly to the days of the year. Noon, midnight, &c., are distinguished from the perforations of the other hours of the day by a few supplementary pins. Two speeds of travel can be given to the paper. These were originally one inch and one half-inch per hour, but subsequently these were reduced to one quarter-inch and one-eighth inch per hour, as these latter were found to be quite sufficient for the purposes of reading off. The pin perforations are one inch apart so that with the larger speed now fitted on the machine a day's tides occupy only six inches of paper. The extra pin perforations originally used to distinguish 6 hours, 12 hours and 18 hours of each day, now represent successive noons. A fixed vertical rod near the ink-recorder slide carries ruling-pens for the tracing of base-lines, such as dock-sills, river bars, or mean-tide levels. In practice it has been usual to use two horizontal lines only—one representing mean-tide level ( $R_0$  of the tidal reductions) and a lower one representing Indian Spring Low-water mark as defined in the tidal reductions. It is to the latter that the predictions in height are usually referred. If desired the paper can be ruled its entire width to represent feet, metres, &c., as it passes through the machine. An idea of the saving that is effected by the machine may be gathered from the fact that tide-curves computed by an expert calculator to include the same number of components as comprised in the machine, could not be worked out in less than five or six months for the year's tides at any port. These can be run off by the machine in about two hours, and then only require the heights and times to be read off.

The value of the machine is very great in any work where the whole tide-curve is of service, and is of great value in engineering works in which a fore-knowledge of the tides is necessary, such as in constructing the foundations of quay walls, embankments, dock-sills, &c., the whole time during which the work can be prosecuted being seen at a glance for every tide.

The machine as a whole is the design of Mr. Edward Roberts of the Nautical Almanac Office, while the improved parallel slide fitted to each tidal component is due to Lord Kelvin (Sir William Thomson), and the use of the fine flexible wire for summing the whole of the components is the suggestion of Mr. Beauchamp Tower. The machine was made by Messrs. A. Lége & Co., of London, by whom also the alterations and additions were carried out. As evidencing the makers' excellent workmanship, it may be mentioned that, when the machine was taken to pieces in 1891 for alteration, little or no wear was observable in the working parts, although the machine had been constantly in use for nearly twelve years.

## 2.

### *The Preparation of the Tide Tables for the Indian Ports.*

The tide-predicting machine, combining some twenty-four tidal components, gives results with great accuracy for all open coast stations. These comprise the bulk of the Indian ports. The preparation of the tables of high and low waters, from the traced curves of the machine, is most simply effected by obtaining the times of the highest and lowest points of the curves, and their measurements from the datum line for the heights according to the scale for which the machine has been set. For tidal stations situated, however, at some considerable distance from the mouths of rivers or in estuaries having a considerable shallow foreshore, the number of over-tides and compound shallow-water components

contained on the machine is not sufficient to represent, with the accuracy desired, the actual tidal curve. In addition to the above, the tides are greatly affected by the freshets in the rivers, which alter the normal times and heights very considerably through several months of the year.

In order therefore to give the best results obtainable, recourse has been had to a combination of the method pursued by the Hydrographic Office of the Admiralty, modified, however, to include the effects of the freshets, with the results for the diurnal tides obtainable by the tide-predictor as hereafter explained.

The ordinary method of reduction, pursued by the Hydrographic Office, is to refer the observed times and heights of high waters\*, extending over a considerable period, to the apparent times of transits of the Moon preceding the time of high water. The best transit to which to refer the observations can be determined from the values of  $\kappa$ , deduced from the harmonic analysis of the two chief tides of the port in question or of those of an adjacent port. The difference between the values of  $\kappa$  of the mean lunar semi-diurnal tide and that of the mean solar semi-diurnal tide, divided by twice the Moon's mean daily synodic motion will give the mean value of the retardation of the times of high water after the Moon's transit. For instance, if we take the values obtained for Bombay, we have

$$\frac{\kappa \text{ of } S_2 - \kappa \text{ of } M_2}{24^\circ \cdot 38} \text{ or } \frac{3^\circ \cdot 2 - 329^\circ \cdot 9}{24^\circ \cdot 38} = \frac{33^\circ \cdot 3}{24^\circ \cdot 38} = 1^{\text{d}} \cdot 37 \text{ or } 33^{\text{h}} \pm.$$

Having determined the Moon's transit to which the observations are to be referred, they are divided into twelve groups, *viz.*, all those tides depending on the Moon's transits which occur between 0<sup>h</sup> 0<sup>m</sup> and 1<sup>h</sup> 0<sup>m</sup> or 12<sup>h</sup> 0<sup>m</sup> and 13<sup>h</sup> 0<sup>m</sup> forming one group, all those high waters between 1<sup>h</sup> 0<sup>m</sup> and 2<sup>h</sup> 0<sup>m</sup> or 13<sup>h</sup> 0<sup>m</sup> and 14<sup>h</sup> 0<sup>m</sup> forming a second group and similarly through each of the twelve hours. The means of the Moon's transits and of the times and heights of high water depending on them are then taken. The results will give the mean times and mean heights of high water for values of the Moon's transit about 0<sup>h</sup> 30<sup>m</sup>, 1<sup>h</sup> 30<sup>m</sup>, 2<sup>h</sup> 30<sup>m</sup>, etc. If the means of the Moon's transit do not equal 30<sup>m</sup> exactly, they are made to do so, the times and heights depending on them being corrected accordingly. Having now the values for each hour of Moon's transit, *viz.*, at 0<sup>h</sup> 30<sup>m</sup>, 1<sup>h</sup> 30<sup>m</sup>, etc., the values for intermediate times of Moon's transit are obtained in the usual way by interpolation. It is usual to prepare a table for each 10<sup>m</sup> of Moon's transit, *i.e.*, five values are inserted between each of the twelve original quantities. The values of the heights are similarly treated. If the Indian riverain observations were treated as above, the results would include the mean effect due to the freshets. In order, however, to obtain the actual values due to the freshets which occur with fair regularity each year, a modification of the above method has been introduced, *viz.*, in place of a considerable period of observations (usually a year) being treated as a whole, each month is treated separately, so that twelve sets of values are obtained similar to the above for each year's observations. In order to obtain good values it is, however, necessary that the observations extending over some years should be thus treated, as the number of observations in any one month, depending on a certain hour of Moon's transit, is much too few to give a mean value fairly reliable. It may be here remarked that it is not necessary to find the time of the Moon's transit for the particular place in question, and in practice it has been the rule to refer the times and heights to the transits at Greenwich, which are given in the Nautical Almanac. In the predictions the Greenwich transits are again used, whereby a saving is effected both in the reductions of the observations and the actual predictions.

The next step in the work is the finding of the corrections due to the lunar and solar parallaxes, and the lunar and solar declinations. For this purpose recourse has been had to the following tables of the late Sir John Lubbock, published in "An Elementary Treatise† on the Tides. London, 1839."

\* The low waters have hitherto not received the same attention.

† In this treatise the successive transits of the Moon are denoted by the letters A, B, C, D, E and F:—F is supposed to denote the time of the transit of the Moon immediately preceding the time of high water at London Docks.



TABLE I.—Showing the correction for the Moon's Declination.

D's Transit B.	0° Dec.	3° Dec.	6° Dec.	9° Dec.	12° Dec.	15° Dec.	18° Dec.	21° Dec.	24° Dec.	27° Dec.	30° Dec.	D's Transit B.
h	m	m	m	m	m	m	m	m	m	m	m	h
0	- 1	- 1	0	0	0	0	+ 1	+ 1	+ 1	+ 1	+ 2	0
1	+ 2	+ 2	0	0	0	0	- 1	- 1	- 1	- 1	- 2	1
2	+ 1	+ 1	+ 1	+ 1	+ 1	0	- 1	- 1	- 2	- 3	- 4	2
3	+ 3	+ 3	+ 3	+ 2	+ 1	0	- 1	- 2	- 3	- 5	- 7	3
4	+ 3	+ 3	+ 3	+ 2	+ 1	0	- 1	- 3	- 5	- 7	- 10	4
5	+ 3	+ 3	+ 3	+ 2	+ 1	0	- 2	- 4	- 6	- 9	- 12	5
6	+ 2	+ 2	+ 2	+ 1	+ 1	0	- 1	- 2	- 4	- 4	- 5	6
7	- 2	- 2	- 2	- 1	- 1	0	+ 1	+ 2	+ 4	+ 4	+ 5	7
8	- 3	- 3	- 3	- 2	- 1	0	+ 2	+ 4	+ 6	+ 9	+ 12	8
9	- 3	- 3	- 3	- 2	- 1	0	+ 1	+ 3	+ 5	+ 7	+ 10	9
10	- 3	- 3	- 3	- 2	- 1	0	+ 1	+ 2	+ 3	+ 5	+ 7	10
11	- 2	- 2	- 1	- 1	- 1	0	+ 1	+ 1	+ 2	+ 3	+ 4	11

TABLE II.—Showing the correction for the Moon's Parallax.

D's Transit B.	H. P. 54'	H. P. 55'	H. P. 56'	H. P. 57'	H. P. 58'	H. P. 59'	H. P. 60'	H. P. 61'	D's Transit B.
h	m	m	m	m	m	m	m	m	h
0	+ 1	+ 1	+ 1	0	0	- 1	- 1	- 1	0
1	- 1	- 1	- 1	0	0	+ 1	+ 1	+ 1	1
2	- 3	- 2	- 1	0	+ 1	+ 2	+ 3	+ 4	2
3	- 5	- 3	- 1	0	+ 1	+ 3	+ 5	+ 7	3
4	- 7	- 5	- 2	0	+ 2	+ 4	+ 6	+ 8	4
5	- 9	- 6	- 3	0	+ 2	+ 5	+ 7	+ 9	5
6	- 4	- 2	- 1	0	+ 1	+ 2	+ 3	+ 4	6
7	+ 4	+ 2	+ 1	0	- 1	- 2	- 3	- 4	7
8	+ 9	+ 6	+ 3	0	- 2	- 5	- 7	- 9	8
9	+ 7	+ 5	+ 2	0	- 2	- 4	- 6	- 8	9
10	+ 5	+ 3	+ 1	0	- 1	- 3	- 5	- 7	10
11	+ 3	+ 2	+ 1	0	- 1	- 2	- 3	- 4	11

TABLE III.—Showing the correction for the Sun's Declination.

D's Transit B.	0° Dec.	3° Dec.	6° Dec.	9° Dec.	12° Dec.	15° Dec.	18° Dec.	21° Dec.	24° Dec.	D's Transit B.
h	m	m	m	m	m	m	m	m	m	h
0	0	0	0	0	0	0	0	0	0	0
1	0	0	0	0	0	0	0	0	+ 1	1
2	- 1	- 1	- 1	- 1	0	0	0	+ 1	+ 2	2
3	- 2	- 1	- 1	- 1	0	0	+ 1	+ 2	+ 4	3
4	- 3	- 2	- 1	- 2	0	0	+ 2	+ 3	+ 5	4
5	- 3	- 2	- 2	- 1	- 1	0	+ 1	+ 3	+ 5	5
6	- 1	- 1	- 1	- 1	0	0	+ 1	+ 1	+ 2	6
7	+ 1	+ 1	+ 1	+ 1	0	0	- 1	- 2	- 2	7
8	+ 3	+ 2	+ 2	+ 1	+ 1	0	- 2	- 3	- 5	8
9	+ 3	+ 2	+ 1	+ 2	0	0	- 2	- 3	- 5	9
10	+ 2	+ 1	+ 1	+ 1	0	0	- 1	- 2	- 4	10
11	+ 1	+ 1	+ 1	+ 1	0	0	0	- 1	- 2	11

TABLE IV.—Showing the correction for the Sun's Parallax.

D's Transit B.	Jan.	Feb.	March	April	May	June	D's Transit B.
	Dec.	Nov.	Oct.	Sept.	August	July	
	H. P.	H. P.	H. P.	H. P.	H. P.	H. P.	
	9''00	8''96	8''88	8''80	8''75	8''70	
h	m	n	m	m	m	m	h
0	0	0	0	0	0	0	0
1	0	0	0	0	0	0	1
2	-1	-1	0	0	0	0	2
3	-1	-1	0	0	+1	+1	3
4	-2	-2	0	0	+2	+2	4
5	-3	-2	-1	+1	+3	+3	5
6	-2	-1	-1	+1	+2	+2	6
7	+2	+1	+1	-1	-2	-2	7
8	+3	+2	+1	-1	-3	-3	8
9	+2	+2	0	0	-2	-2	9
10	+1	+1	0	0	-1	-1	10
11	+1	+1	0	0	0	0	11

TABLE V.—Showing the correction for the Moon's Declination.

D's Transit B.	0°	3°	6°	9°	12°	15°	18°	21°	24°	27°	30°	D's Transit B.
	Dec.	Dec.	Dec.	Dec.	Dec.	Dec.	Dec.	Dec.	Dec.	Dec.	Dec.	
h	Feet	Feet	Feet	Feet	Feet	Feet	Feet	Feet	Feet	Feet	Feet	h
0	+ '32	+ '31	+ '27	+ '21	+ '12	0	- '13	- '29	- '47	- '66	- '87	0
1	+ '32	+ '31	+ '27	+ '21	+ '12	0	- '13	- '29	- '47	- '66	- '87	1
2	+ '31	+ '30	+ '26	+ '20	+ '11	0	- '13	- '28	- '46	- '65	- '86	2
3	+ '30	+ '30	+ '26	+ '20	+ '10	0	- '13	- '28	- '45	- '63	- '83	3
4	+ '30	+ '29	+ '25	+ '19	+ '11	0	- '13	- '27	- '44	- '61	- '80	4
5	+ '30	+ '29	+ '25	+ '19	+ '11	0	- '13	- '27	- '44	- '61	- '79	5
6	+ '31	+ '30	+ '26	+ '20	+ '12	0	- '13	- '28	- '46	- '63	- '83	6
7	+ '31	+ '30	+ '26	+ '20	+ '12	0	- '13	- '28	- '46	- '63	- '83	7
8	+ '30	+ '29	+ '25	+ '19	+ '11	0	- '13	- '27	- '44	- '61	- '79	8
9	+ '30	+ '29	+ '25	+ '19	+ '11	0	- '13	- '27	- '44	- '61	- '80	9
10	+ '30	+ '30	+ '26	+ '20	+ '10	0	- '13	- '28	- '45	- '63	- '83	10
11	+ '31	+ '30	+ '26	+ '20	+ '11	0	- '13	- '28	- '46	- '65	- '86	11

TABLE VI.—Showing the correction for the Moon's Parallax.

D's Transit B.	H. P.	H. P.	H. P.	H. P.	H. P.	H. P.	H. P.	H. P.	D's Transit B.
	54'	55'	56'	57'	58'	59'	60'	61'	
h	Feet	Feet	Feet	Feet	Feet	Feet	Feet	Feet	h
0	- '66	- '45	- '23	0	+ '24	+ '49	+ '74	+ 1'00	0
1	- '66	- '45	- '23	0	+ '24	+ '49	+ '74	+ 1'00	1
2	- '65	- '44	- '23	0	+ '23	+ '47	+ '72	+ '98	2
3	- '63	- '43	- '22	0	+ '22	+ '46	+ '71	+ '96	3
4	- '61	- '42	- '21	0	+ '22	+ '45	+ '69	+ '94	4
5	- '63	- '43	- '22	0	+ '23	+ '46	+ '70	+ '96	5
6	- '65	- '45	- '23	0	+ '24	+ '48	+ '73	+ '99	6
7	- '65	- '45	- '23	0	+ '24	+ '48	+ '73	+ '99	7
8	- '63	- '43	- '22	0	+ '23	+ '46	+ '70	+ '96	8
9	- '61	- '42	- '21	0	+ '22	+ '45	+ '69	+ '94	9
10	- '63	- '43	- '22	0	+ '22	+ '46	+ '71	+ '96	10
11	- '65	- '44	- '23	0	+ '23	+ '47	+ '72	+ '98	11

TABLE VII.—Showing the correction for the Sun's Declination.

D's Transit B.	0° Dec.	3° Dec.	6° Dec.	9° Dec.	12° Dec.	15° Dec.	18° Dec.	21° Dec.	24° Dec.	D's Transit B.
h	Feet	Feet	Feet	Feet	Feet	Feet	Feet	Feet	Feet	h
0	+ '12	+ '11	+ '10	+ '08	+ '04	0	- '05	- '11	- '18	0
1	+ '12	+ '11	+ '10	+ '08	+ '04	0	- '05	- '11	- '18	1
2	+ '10	+ '09	+ '08	+ '06	+ '04	0	- '05	- '10	- '15	2
3	+ '07	+ '06	+ '05	+ '04	+ '02	0	- '03	- '06	- '10	3
4	+ '01	+ '01	+ '01	+ '01	- '00	0	- '01	- '01	- '02	4
5	- '06	- '06	- '05	- '04	- '02	0	+ '03	+ '05	+ '08	5
6	- '11	- '10	- '10	- '07	- '04	0	+ '05	+ '10	+ '15	6
7	- '11	- '10	- '10	- '07	- '04	0	+ '05	+ '10	+ '15	7
8	- '06	- '06	- '05	- '04	- '02	0	+ '03	+ '05	+ '08	8
9	+ '01	+ '01	+ '01	+ '01	+ '00	0	- '01	- '01	- '02	9
10	+ '07	+ '06	+ '05	+ '04	+ '02	0	- '03	- '05	- '10	10
11	+ '10	+ '09	+ '08	+ '06	+ '04	0	- '05	- '10	- '15	11

TABLE VIIa.—Showing the correction for the Sun's Parallax.

D's Transit B.	Jan. Dec.	Feb. Nov.	March Oct.	April Sept.	May August	June July	D's Transit B.
	H. P.	H. P.	H. P.	H. P.	H. P.	H. P.	
	9'00	8'96	8'88	8'80	8'75	8'70	
h	Feet	Feet	Feet	Feet	Feet	Feet	h
0	+ '09	+ '06	+ '03	- '03	- '05	- '08	0
1	+ '09	+ '06	+ '03	- '03	- '05	- '08	1
2	+ '07	+ '04	+ '02	- '02	- '04	- '07	2
3	+ '04	+ '03	+ '01	- '01	- '03	- '04	3
4	+ '01	+ '01	+ '01	- '01	- '01	- '01	4
5	- '04	- '03	- '01	+ '01	+ '02	+ '03	5
6	- '08	- '05	- '03	+ '03	+ '05	+ '07	6
7	- '08	- '05	- '03	+ '03	+ '05	+ '07	7
8	- '04	- '03	- '01	+ '01	+ '02	+ '03	8
9	+ '01	+ '01	+ '01	- '01	- '01	- '01	9
10	+ '04	+ '03	+ '01	- '01	- '03	- '04	10
11	+ '07	+ '04	+ '02	- '02	- '04	- '07	11

These tables are strictly for the London Docks, but can be used, without alteration for the semi-diurnal tides of any port, for the corrections for the times of high water unaltered, and for the heights by using corrections in proportion to the ranges of the semi-diurnal tides at London and the port in question. The corrections for the times of low water at the London Docks, have not been determined but have been assumed the same as for the high water, and have been so used in the prediction of the times of low water for the Indian riverain ports. The corrections for the heights of low waters will be of opposite sign to those for the high waters. The times of low water in the reductions are referred to the same Moon's transit as the *succeeding* high water, the low waters preceding the high waters by a shorter interval than that between the low water and the previous high water. In riverain ports at a considerable distance from the river's mouth, the high water succeeds the low water by a few hours only, the times being coincident at the place where the tidal flow ceases.

The following table exhibits the approximate interval after the Moon's transit to which the predictions are referred for the Indian riverain ports determined on this system :—

			Interval after Moon's transit to time of	
			Low water	High water
Dublat (Saugor Island) Hooghly River	...	...	29 <sup>h</sup>	35 <sup>h</sup>
Diamond Harbour	„	...	32	36
Kidderpore (Calcutta)	„	...	35	39
Chittagong	...	...	33	38
Elephant Point, Rangoon River	...	...	35	40
Rangoon	„	...	36	41
Amherst, Moulmein River	...	...	34	39
Moulmein	„	...	37	40

The corrections to the heights of high water and low water for the above ports, are obtained from those for London by multiplying them by the following factors, the values for London being taken as unity :—

			Factor for High water	Factor for Low water
Dublat (Saugor Island) Hooghly River	...	...	1·2	—1·2
Diamond Harbour	„	...	1·4	—1·0
Kidderpore (Calcutta)	„	...	1·2	—0·3
Chittagong	...	...	1·0	—0·5
Elephant Point, Rangoon River	...	...	1·6	—1·4
Rangoon	„	...	1·4	—0·9
Amherst, Moulmein River	...	...	1·8	—1·8
Moulmein	„	...	1·6	—1·2

The times of high water being now corrected as above explained, it has been usual to alter them slightly at the end of each month and at the beginning of the next, to smooth away the roughness in the flow of the numbers on account of the difference arising from the use of the slightly different values of the semi-menstrual curve used for successive months. The heights are similarly treated and the times and heights of the low waters also.

The times and heights now represent the tides depending on the semi-diurnal tides and corrected approximately for the effects of the freshets. The effects of the diurnal tides have now to be found.

The values of these components, *viz.*, those of S, K, O, P, J and Q, are determined in the usual way by the harmonic analysis of the tidal observations. These values being put on the tide-predictor, all the other components having been put to zero, the continuous curve for the whole year is run off. The value in height above or below mean-tide level is then found for each of the approximate times of high and low water. These values are combined with the corrected heights previously found. The resulting heights give the quantities published in the Tide Tables. It now only remains to correct the times similarly for the diurnal tides. The correction due to the diurnal tides will be *nil*, when the diurnal tide is at its maximum effect either above or below mean-tide level, *i.e.*, when it has no *variation*, and will be greatest when the variation is greatest. The difference between alternate values of the diurnal correction in height serves as a basis for obtaining the corrections in time. These alternate values are

already tabulated for the correction in height. The latest determination of the best values is found to be the division of the *difference* between alternate values of the diurnal correction in heights expressed in hundredths of a foot by 5, the resulting quotient representing minutes of time. For instance, if the difference between two consecutive corrections in height for diurnal tides is found to be 0·35 foot, then the correction in time to the intermediate high or low water is represented by 7 minutes.

For the high-water correction, if the differences are increasing *positively*, then the corrections to the time of high water is *positive*, or in other words, as the effect of the diurnal tide is to prolong the tidal flow, the time of high water will be retarded thereby. On the other hand, if the difference is increasing *negatively*, then the correction will be *negative*, or in other words the time of high water will be accelerated and *vice versá*. For the times of low water, the corrections will be the opposite, *i.e.*, if the differences are increasing *positively*, then the times will be accelerated, or the correction to the times will be *negative*, and on the other hand, if the differences are increasing *negatively*, then the times will be retarded, *i.e.*, the correction to the times will be *positive*. By using thus a common factor, the mean value only of the correction to the diurnal tides is obtained. The corrections thus formed will be slightly too large at the time of spring-tides as ordinarily understood, and too small at neap-tides, but the error introduced is probably small, and the correct values would create an amount of labour probably not recompensed by the extra labour involved.

The following are the tables actually used: they are practically the same in substance as Sir J. Lubbock's tables, but they are enlarged and re-arranged in a more convenient form:—

TABLE NO. 1.—Corrections to Times of High Water for Moon's Declination.

Declination	0 <sup>h</sup>			1 <sup>h</sup>			2 <sup>h</sup>			3 <sup>h</sup>			4 <sup>h</sup>			5 <sup>h</sup>		
	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>
0	-0.8	-0.3	+0.3	+0.8	+1.2	+1.6	+1.9	+2.2	+2.5	+2.8	+3.0	+3.1	+3.2	+3.3	+3.3	+3.2	+2.9	+2.5
1	0.8	0.3	0.3	0.8	1.2	1.6	1.9	2.2	2.4	2.7	2.9	3.0	3.1	3.2	3.2	3.1	2.8	2.4
2	0.8	0.3	0.3	0.8	1.1	1.5	1.8	2.1	2.3	2.6	2.8	2.9	3.0	3.1	3.1	3.0	2.7	2.3
3	0.8	0.3	0.3	0.8	1.1	1.5	1.8	2.0	2.2	2.4	2.6	2.8	2.9	3.0	3.0	2.9	2.6	2.2
4	-0.7	-0.3	+0.3	+0.7	+1.1	+1.4	+1.7	+1.9	+2.1	+2.3	+2.5	+2.6	+2.7	+2.8	+2.8	+2.7	+2.4	+2.1
5	0.7	0.3	0.3	0.7	1.0	1.4	1.6	1.8	2.0	2.1	2.4	2.5	2.6	2.7	2.7	2.6	2.3	2.0
6	0.6	0.2	0.2	0.6	1.0	1.3	1.5	1.7	1.8	1.9	2.2	2.4	2.5	2.6	2.6	2.5	2.2	1.8
7	0.6	0.2	0.2	0.6	0.9	1.2	1.4	1.6	1.7	1.8	2.0	2.3	2.3	2.4	2.4	2.3	2.1	1.7
8	-0.5	-0.2	+0.3	+0.5	+0.8	+1.1	+1.3	+1.4	+1.6	+1.7	+1.9	+2.1	+2.1	+2.2	+2.2	+2.1	+1.9	+1.6
9	0.4	0.2	0.2	0.4	0.7	1.0	1.1	1.3	1.4	1.6	1.7	1.9	1.9	2.0	2.0	1.9	1.7	1.4
10	0.4	0.2	0.2	0.4	0.6	0.8	1.0	1.1	1.3	1.4	1.5	1.6	1.6	1.7	1.7	1.6	1.5	1.3
11	0.3	0.1	0.1	0.3	0.5	0.7	0.8	0.9	1.1	1.1	1.2	1.3	1.3	1.4	1.4	1.3	1.2	1.1
12	-0.2	-0.1	+0.1	+0.2	+0.4	+0.6	+0.6	+0.7	+0.9	+0.9	+0.9	+1.0	+1.0	+1.1	+1.1	+1.0	+0.9	+0.9
13	0.2	0.1	0.1	0.2	0.3	0.4	0.4	0.5	0.6	0.6	0.6	0.7	0.7	0.8	0.8	0.7	0.6	0.6
14	0.1	0.1	0.1	0.1	0.1	0.2	0.2	0.2	0.3	0.3	0.3	0.4	0.4	0.4	0.4	0.4	0.3	0.3
15	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
16	+0.1	+0.1	-0.1	-0.1	-0.1	-0.2	-0.2	-0.3	-0.3	-0.3	-0.4	-0.4	-0.4	-0.5	-0.5	-0.5	-0.4	-0.4
17	0.2	0.1	0.1	0.2	0.2	0.4	0.4	0.5	0.6	0.7	0.8	0.8	0.9	1.0	1.0	1.0	0.9	0.8
18	0.3	0.2	0.2	0.3	0.4	0.6	0.6	0.8	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.6	1.5	1.2
19	0.4	0.2	0.2	0.4	0.5	0.8	0.8	1.1	1.3	1.5	1.7	1.8	1.9	2.1	2.2	2.2	2.0	1.7
20	+0.5	+0.3	-0.2	-0.5	-0.6	-1.0	-1.1	-1.4	-1.7	-1.9	-2.2	-2.3	-2.5	-2.7	-2.9	-2.9	-2.6	-2.3
21	0.6	0.3	0.3	0.6	0.8	1.3	1.4	1.7	2.1	2.4	2.7	2.9	3.1	3.4	3.6	3.6	3.2	2.7
22	0.7	0.3	0.3	0.7	0.9	1.6	1.7	2.0	2.5	2.8	3.2	3.5	3.8	4.1	4.3	4.3	3.9	3.2
23	0.8	0.3	0.3	0.8	1.1	1.8	2.0	2.4	2.9	3.3	3.7	4.1	4.5	4.8	5.1	5.1	4.6	3.7
24	+0.9	+0.4	-0.4	-0.9	-1.2	-2.1	-2.4	-2.8	-3.4	-3.8	-4.3	-4.7	-5.2	-5.6	-5.9	-5.9	-5.4	-4.3
25	1.0	0.4	0.4	1.0	1.4	2.3	2.7	3.2	3.9	4.3	4.9	5.3	6.0	6.4	6.8	6.8	6.2	4.9
26	1.2	0.5	0.5	1.2	1.6	2.6	3.0	3.6	4.4	4.9	5.5	6.0	6.8	7.2	7.7	7.7	7.0	5.5
27	1.3	0.5	0.5	1.3	1.8	2.8	3.3	4.1	4.9	5.5	6.2	6.7	7.6	8.1	8.6	8.6	7.8	6.2
28	+1.4	+0.5	-0.5	-1.4	-2.1	-3.0	-3.7	-4.5	-5.4	-6.1	-6.8	-7.5	-8.4	-9.0	-9.6	-9.6	-8.6	-6.8
29	1.6	0.6	0.6	1.6	2.3	3.3	4.0	4.9	5.9	6.7	7.5	8.3	9.2	10.0	10.6	10.6	9.5	7.5
30	1.7	0.6	0.6	1.7	2.6	3.5	4.3	5.4	6.4	7.3	8.1	9.1	10.0	11.0	11.7	11.7	10.5	8.1

Example.—Moon's Apparent Transit 3<sup>h</sup> 40<sup>m</sup> and Declination 25°; correction = - 5<sup>m</sup> 3.

Arguments—Moon's Declination and Apparent Transit.

6 <sup>h</sup>			7 <sup>h</sup>			8 <sup>h</sup>			9 <sup>h</sup>			10 <sup>h</sup>			11 <sup>h</sup>				Declination
0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	60 <sup>m</sup>	
+ 2.0	+ 0.9	- 0.9	- 2.0	- 2.5	- 2.9	- 3.2	- 3.3	- 3.3	- 3.2	- 3.1	- 3.0	- 2.8	- 2.5	- 2.2	- 1.9	- 1.6	- 1.2	- 0.8	0
1.9	0.9	0.9	1.9	2.4	2.8	3.1	3.2	3.2	3.1	3.0	2.9	2.7	2.4	2.2	1.9	1.6	1.2	0.8	1
1.8	0.9	0.9	1.8	2.3	2.7	3.0	3.1	3.1	3.0	2.9	2.8	2.6	2.3	2.1	1.8	1.5	1.1	0.8	2
1.8	0.8	0.8	1.8	2.2	2.6	2.9	3.0	3.0	2.9	2.8	2.6	2.4	2.2	2.0	1.8	1.5	1.1	0.8	3
+ 1.7	+ 0.8	- 0.8	- 1.7	- 2.1	- 2.4	- 2.7	- 2.8	- 2.8	- 2.7	- 2.6	- 2.5	- 2.3	- 2.1	- 1.9	- 1.7	- 1.4	- 1.1	- 0.7	4
1.6	0.8	0.8	1.6	2.0	2.3	2.6	2.7	2.7	2.6	2.5	2.4	2.1	2.0	1.8	1.6	1.4	1.0	0.7	5
1.5	0.7	0.7	1.5	1.8	2.2	2.5	2.6	2.6	2.5	2.4	2.2	1.9	1.8	1.7	1.5	1.3	1.0	0.6	6
1.4	0.7	0.7	1.4	1.7	2.1	2.3	2.4	2.4	2.3	2.3	2.0	1.8	1.7	1.6	1.4	1.2	0.9	0.6	7
+ 1.3	+ 0.6	- 0.6	- 1.3	- 1.6	- 1.9	- 2.1	- 2.2	- 2.2	- 2.1	- 2.1	- 1.9	- 1.7	- 1.6	- 1.4	- 1.3	- 1.1	- 0.8	- 0.5	8
1.1	0.5	0.5	1.1	1.4	1.7	1.9	2.0	2.0	1.9	1.9	1.7	1.6	1.4	1.3	1.1	1.0	0.7	0.4	9
1.0	0.5	0.5	1.0	1.3	1.5	1.6	1.7	1.7	1.6	1.6	1.5	1.4	1.3	1.1	1.0	0.8	0.6	0.4	10
0.8	0.4	0.4	0.8	1.1	1.2	1.3	1.4	1.4	1.3	1.3	1.2	1.1	1.1	0.9	0.8	0.7	0.5	0.3	11
+ 0.6	+ 0.3	- 0.3	- 0.6	- 0.9	- 0.9	- 1.0	- 1.1	- 1.1	- 1.0	- 1.0	- 0.9	- 0.9	- 0.9	- 0.7	- 0.6	- 0.6	- 0.4	- 0.2	12
0.4	0.2	0.2	0.4	0.6	0.6	0.7	0.8	0.8	0.7	0.7	0.6	0.6	0.6	0.5	0.4	0.4	0.3	0.2	13
0.2	0.1	0.1	0.2	0.3	0.3	0.4	0.4	0.4	0.4	0.4	0.3	0.3	0.3	0.2	0.2	0.2	0.1	0.1	14
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	15
- 0.2	- 0.1	+ 0.1	+ 0.2	+ 0.4	+ 0.4	+ 0.5	+ 0.5	+ 0.5	+ 0.4	+ 0.4	+ 0.4	+ 0.3	+ 0.3	+ 0.3	+ 0.2	+ 0.2	+ 0.1	+ 0.1	16
0.5	0.2	0.2	0.5	0.8	0.9	1.0	1.0	1.0	0.9	0.8	0.8	0.7	0.6	0.5	0.4	0.4	0.2	0.2	17
0.7	0.3	0.3	0.7	1.2	1.5	1.6	1.6	1.5	1.4	1.3	1.2	1.1	1.0	0.8	0.6	0.6	0.4	0.3	18
1.0	0.4	0.4	1.0	1.7	2.0	2.2	2.2	2.1	1.9	1.8	1.7	1.5	1.3	1.1	0.8	0.8	0.5	0.4	19
- 1.3	- 0.5	+ 0.5	+ 1.3	+ 2.2	+ 2.6	+ 2.9	+ 2.9	+ 2.7	+ 2.5	+ 2.3	+ 2.2	+ 1.9	+ 1.7	+ 1.4	+ 1.1	+ 1.0	+ 0.6	+ 0.5	20
1.6	0.6	0.6	1.6	2.7	3.2	3.6	3.6	3.4	3.1	2.9	2.7	2.4	2.1	1.7	1.4	1.3	0.8	0.6	21
1.9	0.7	0.7	1.9	3.2	3.9	4.3	4.3	4.1	3.8	3.5	3.2	2.8	2.5	2.0	1.7	1.6	0.9	0.7	22
2.3	0.8	0.8	2.3	3.7	4.6	5.1	5.1	4.8	4.5	4.1	3.7	3.3	2.9	2.4	2.0	1.8	1.1	0.8	23
- 2.6	- 0.9	+ 0.9	+ 2.6	+ 4.3	+ 5.4	+ 5.9	+ 5.9	+ 5.6	+ 5.2	+ 4.7	+ 4.3	+ 3.8	+ 3.4	+ 2.8	+ 2.4	+ 2.1	+ 1.2	+ 0.9	24
3.0	1.1	1.1	3.0	4.9	6.2	6.8	6.8	6.4	6.0	5.3	4.9	4.3	3.9	3.2	2.7	2.3	1.4	1.0	25
3.4	1.2	1.2	3.4	5.5	7.0	7.7	7.7	7.2	6.8	6.0	5.5	4.9	4.4	3.6	3.0	2.6	1.6	1.2	26
3.8	1.3	1.3	3.8	6.3	7.8	8.6	8.6	8.1	7.6	6.7	6.2	5.5	4.9	4.1	3.3	2.8	1.8	1.3	27
- 4.2	- 1.5	+ 1.5	+ 4.2	+ 6.8	+ 8.6	+ 9.6	+ 9.6	+ 9.0	+ 8.4	+ 7.5	+ 6.8	+ 6.1	+ 5.4	+ 4.5	+ 3.7	+ 3.0	+ 2.1	+ 1.4	28
4.6	1.6	1.6	4.6	7.5	9.5	10.6	10.6	10.0	9.2	8.3	7.5	6.7	5.9	4.9	4.0	3.2	2.3	1.6	29
5.0	1.8	1.8	5.0	8.1	10.5	11.7	11.7	11.0	10.0	9.1	8.1	7.3	6.4	5.4	4.3	3.5	2.6	1.7	30

Example.—Moon's Apparent Transit 3<sup>h</sup> 40<sup>m</sup> and Declination 25°; correction = - 5<sup>m</sup>.3.

TABLE No. 2.—Correction to Times of High Water. Arguments—

H. P.	0 <sup>h</sup>			1 <sup>h</sup>			2 <sup>h</sup>			3 <sup>h</sup>			4 <sup>h</sup>			5 <sup>h</sup>		
	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>
54 0	+ 1.0	+ 0.3	- 0.3	- 1.0	- 1.7	- 2.4	- 3.1	- 3.8	- 4.6	- 5.4	- 6.3	- 7.1	- 7.7	- 8.2	- 8.5	- 8.6	- 8.0	- 7.0
15	0.9	0.3	0.3	0.9	1.5	2.2	2.8	3.5	4.2	5.0	5.8	6.5	7.0	7.6	7.8	7.9	7.4	6.4
30	0.8	0.3	0.3	0.8	1.4	2.0	2.6	3.2	3.8	4.5	5.3	5.9	6.4	6.9	7.1	7.2	6.7	5.8
45	0.7	0.2	0.2	0.7	1.2	1.8	2.3	2.9	3.4	4.1	4.8	5.3	5.8	6.2	6.4	6.5	6.1	5.2
55 0	+ 0.6	+ 0.2	- 0.2	- 0.6	- 1.1	- 1.6	- 2.1	- 2.5	- 3.1	- 3.6	- 4.2	- 4.7	- 5.2	- 5.5	- 5.7	- 5.8	- 5.4	- 4.7
15	0.5	0.2	0.2	0.5	0.9	1.4	1.8	2.2	2.7	3.2	3.7	4.1	4.5	4.9	5.0	5.1	4.8	4.1
30	0.4	0.1	0.1	0.4	0.8	1.2	1.6	1.9	2.3	2.7	3.2	3.5	3.9	4.2	4.3	4.4	4.1	3.5
45	0.3	0.1	0.1	0.3	0.6	1.0	1.3	1.6	1.9	2.3	2.7	2.9	3.2	3.5	3.6	3.7	3.4	2.9
56 0	+ 0.2	+ 0.1	- 0.1	- 0.2	- 0.5	- 0.8	- 1.1	- 1.3	- 1.6	- 1.8	- 2.1	- 2.3	- 2.6	- 2.8	- 2.9	- 2.9	- 2.7	- 2.4
15	0.1	0.0	0.0	0.1	0.3	0.6	0.8	0.9	1.2	1.4	1.6	1.7	1.9	2.1	2.2	2.2	2.0	1.8
30	0.1	0.0	0.0	0.1	0.2	0.4	0.6	0.6	0.8	0.9	1.1	1.1	1.3	1.4	1.5	1.5	1.3	1.2
45	0.0	0.0	0.0	0.0	0.1	0.2	0.3	0.3	0.4	0.5	0.6	0.6	0.7	0.7	0.8	0.8	0.6	0.6
57 0	+ 0.0	+ 0.0	- 0.0	- 0.0	- 0.0	- 0.0	- 0.0	- 0.0	- 0.0	- 0.0	- 0.0	- 0.0	- 0.0	- 0.0	- 0.0	- 0.0	- 0.0	- 0.0
15	- 0.0	- 0.0	+ 0.0	+ 0.0	+ 0.1	+ 0.2	+ 0.2	+ 0.3	+ 0.4	+ 0.4	+ 0.5	+ 0.5	+ 0.6	+ 0.6	+ 0.6	+ 0.6	+ 0.5	+ 0.4
30	0.0	0.0	0.0	0.0	0.2	0.4	0.5	0.6	0.8	0.9	1.0	1.0	1.1	1.1	1.1	1.1	1.0	0.9
45	0.1	0.0	0.0	0.1	0.4	0.6	0.7	0.9	1.2	1.4	1.5	1.6	1.7	1.7	1.7	1.6	1.5	1.3
58 0	- 0.1	- 0.0	+ 0.0	+ 0.1	+ 0.5	+ 0.7	+ 1.0	+ 1.3	+ 1.6	+ 1.9	+ 2.0	+ 2.1	+ 2.2	+ 2.2	+ 2.2	+ 2.1	+ 2.0	+ 1.8
15	0.3	0.1	0.1	0.2	0.6	0.9	1.2	1.6	2.0	2.4	2.5	2.6	2.8	2.8	2.8	2.7	2.5	2.3
30	0.2	0.1	0.1	0.2	0.7	1.1	1.5	2.0	2.4	2.9	3.0	3.2	3.3	3.3	3.3	3.2	3.0	2.7
45	0.3	0.1	0.1	0.3	0.8	1.3	1.7	2.3	2.8	3.4	3.5	3.7	3.9	3.9	3.9	3.8	3.5	3.1
59 0	- 0.4	- 0.1	+ 0.1	+ 0.4	+ 1.0	+ 1.4	+ 2.0	+ 2.7	+ 3.3	+ 3.8	+ 4.1	+ 4.3	+ 4.4	+ 4.4	+ 4.4	+ 4.3	+ 4.0	+ 3.5
15	0.4	0.1	0.1	0.4	1.1	1.6	2.2	3.0	3.7	4.3	4.6	4.8	5.0	5.0	5.0	4.9	4.5	4.0
30	0.5	0.2	0.2	0.5	1.2	1.8	2.5	3.4	4.1	4.8	5.1	5.4	5.5	5.5	5.5	5.4	5.0	4.4
45	0.6	0.2	0.2	0.6	1.3	2.0	2.7	3.7	4.5	5.3	5.6	5.9	6.1	6.1	6.1	6.0	5.5	4.9
60 0	- 0.7	- 0.2	+ 0.2	+ 0.7	+ 1.4	+ 2.1	+ 3.0	+ 4.1	+ 5.0	+ 5.7	+ 6.2	+ 6.5	+ 6.6	+ 6.6	+ 6.6	+ 6.5	+ 6.0	+ 5.3
15	0.7	0.2	0.2	0.7	1.5	2.3	3.2	4.4	5.4	6.2	6.7	7.0	7.2	7.2	7.2	7.1	6.5	5.7
30	0.8	0.2	0.2	0.8	1.6	2.5	3.5	4.8	5.8	6.7	7.2	7.6	7.7	7.7	7.7	7.6	7.0	6.2
45	0.9	0.3	0.3	0.9	1.7	2.7	3.8	5.1	6.2	7.2	7.7	8.1	8.3	8.3	8.3	8.1	7.5	6.6
61 0	- 1.0	- 0.3	+ 0.3	+ 1.0	+ 1.8	+ 2.8	+ 4.1	+ 5.5	+ 6.7	+ 7.6	+ 8.3	+ 8.7	+ 8.8	+ 8.9	+ 8.8	+ 8.6	+ 8.0	+ 7.0
15	1.1	0.3	0.3	1.1	2.0	3.0	4.4	5.9	7.1	8.1	8.8	9.2	9.4	9.4	9.4	9.1	8.5	7.5

Example.—Moon's Apparent Transit 3<sup>h</sup> 0<sup>m</sup> and H. P. 59' 15"; correction = + 4<sup>m</sup> 3.



Moon's Horizontal Parallax and Apparent Transit.

6 <sup>h</sup>			7 <sup>h</sup>			8 <sup>h</sup>			9 <sup>h</sup>			10 <sup>h</sup>			11 <sup>h</sup>				H. P.
0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	60 <sup>m</sup>	
- 5'0	- 2'0	+ 2'0	+ 5'0	+ 7'0	+ 8'0	+ 8'6	+ 8'5	+ 8'2	+ 7'7	+ 7'1	+ 6'3	+ 5'4	+ 4'6	+ 3'8	+ 3'1	+ 2'4	+ 1'7	+ 1'0	54 0
4'6	1'8	1'8	4'6	6'4	7'4	7'9	7'8	7'6	7'0	6'5	5'8	5'0	4'2	3'5	2'8	2'2	1'5	0'9	15
4'2	1'7	1'7	4'2	5'8	6'7	7'2	7'1	6'9	6'4	5'9	5'3	4'5	3'8	3'2	2'6	2'0	1'4	0'8	30
3'8	1'5	1'5	3'8	5'2	6'1	6'5	6'4	6'2	5'8	5'3	4'8	4'1	3'4	2'9	2'3	1'8	1'2	0'7	45
- 3'4	- 1'3	+ 1'3	+ 3'4	+ 4'7	+ 5'4	+ 5'8	+ 5'7	+ 5'5	+ 5'2	+ 4'7	+ 4'2	+ 3'6	+ 3'1	+ 2'5	+ 2'1	+ 1'6	+ 1'1	+ 0'6	55 0
3'0	1'2	1'2	3'0	4'1	4'8	5'1	5'0	4'9	4'5	4'1	3'7	3'2	2'7	2'2	1'8	1'4	0'9	0'5	15
2'5	1'0	1'0	2'5	3'5	4'1	4'4	4'3	4'2	3'9	3'5	3'2	2'7	2'3	1'9	1'6	1'2	0'8	0'4	30
2'1	0'9	0'9	2'1	2'9	3'4	3'7	3'6	3'5	3'2	2'9	2'7	2'3	1'9	1'6	1'3	1'0	0'6	0'3	45
- 1'7	- 0'7	+ 0'7	+ 1'7	+ 2'4	+ 2'7	+ 2'9	+ 2'9	+ 2'8	+ 2'6	+ 2'3	+ 2'1	+ 1'8	+ 1'6	+ 1'3	+ 1'1	+ 0'8	+ 0'5	+ 0'2	56 0
1'3	0'5	0'5	1'3	1'8	2'0	2'2	2'2	2'1	1'9	1'7	1'6	1'4	1'2	0'9	0'8	0'6	0'3	0'1	15
0'8	0'4	0'4	0'8	1'2	1'3	1'5	1'5	1'4	1'3	1'1	1'1	0'9	0'8	0'6	0'6	0'4	0'2	0'1	30
0'4	0'2	0'2	0'4	0'6	0'6	0'8	0'8	0'7	0'7	0'6	0'6	0'5	0'4	0'3	0'3	0'2	0'1	0'0	45
- 0'0	- 0'0	+ 0'0	+ 0'0	+ 0'0	+ 0'0	+ 0'0	+ 0'0	+ 0'0	+ 0'0	+ 0'0	+ 0'0	+ 0'0	+ 0'0	+ 0'0	+ 0'0	+ 0'0	+ 0'0	+ 0'0	57 0
+ 0'3	+ 0'1	- 0'1	- 0'3	- 0'4	- 0'5	- 0'6	- 0'6	- 0'6	- 0'6	- 0'5	- 0'5	- 0'4	- 0'4	- 0'3	- 0'2	- 0'2	- 0'1	- 0'0	15
0'7	0'3	0'3	0'7	0'9	1'0	1'1	1'1	1'1	1'1	1'0	1'0	0'9	1'8	0'6	0'5	0'4	0'2	0'0	30
1'0	0'4	0'4	1'0	1'3	1'5	1'6	1'7	1'7	1'7	1'6	1'5	1'4	1'2	0'9	0'7	0'6	0'4	0'1	45
+ 1'3	+ 0'5	- 0'5	- 1'3	- 1'8	- 2'0	- 2'1	- 2'2	- 2'2	- 2'2	- 2'1	- 2'0	- 1'9	- 1'6	- 1'3	- 1'0	- 0'7	- 0'5	- 0'1	58 0
1'6	0'6	0'6	1'6	2'2	2'5	2'7	2'8	2'8	2'8	2'6	2'5	2'4	2'0	1'6	1'2	0'9	0'6	0'2	15
1'9	0'8	0'8	1'9	2'7	3'0	3'2	3'3	3'3	3'3	3'2	3'0	2'9	2'4	2'0	1'5	1'1	0'7	0'2	30
2'2	0'9	0'9	2'2	3'1	3'5	3'8	3'9	3'9	3'9	3'7	3'5	3'4	2'8	2'3	1'7	1'3	0'8	0'3	45
+ 2'5	+ 1'0	- 1'0	- 2'5	- 3'5	- 4'0	- 4'3	- 4'4	- 4'4	- 4'4	- 4'3	- 4'1	- 3'8	- 3'3	- 2'7	- 2'0	- 1'4	- 1'0	- 0'4	59 0
2'8	1'1	1'1	2'8	4'0	4'5	4'9	5'0	5'0	5'0	4'8	4'6	4'3	3'7	3'0	2'2	1'6	1'1	0'4	15
3'2	1'3	1'3	3'2	4'4	5'0	5'4	5'5	5'5	5'5	5'4	5'1	4'8	4'1	3'4	2'5	1'8	1'2	0'5	30
3'5	1'4	1'4	3'5	4'9	5'5	6'0	6'1	6'1	6'1	5'9	5'6	5'3	4'5	3'7	2'7	2'0	1'3	0'6	45
+ 3'8	+ 1'5	- 1'5	- 3'8	- 5'3	- 6'0	- 6'5	- 6'6	- 6'6	- 6'6	- 6'5	- 6'2	- 5'7	- 5'0	- 4'1	- 3'0	- 2'1	- 1'4	- 0'7	60 0
4'1	1'6	1'6	4'1	5'7	6'5	7'1	7'2	7'2	7'2	7'0	6'7	6'2	5'4	4'4	3'2	2'3	1'5	0'7	15
4'4	1'8	1'8	4'4	6'2	7'0	7'6	7'7	7'7	7'7	7'6	7'2	6'7	5'8	4'8	3'5	2'5	1'6	0'8	30
4'7	1'9	1'9	4'7	6'6	7'5	8'1	8'3	8'3	8'3	8'1	7'7	7'2	6'2	5'1	3'8	2'7	1'7	0'9	45
+ 5'0	+ 2'0	- 2'0	- 5'0	- 7'0	- 8'0	- 8'6	- 8'8	- 8'9	- 8'8	- 8'7	- 8'3	- 7'6	- 6'7	- 5'5	- 4'1	- 2'8	- 1'8	- 1'0	61 0
5'3	2'1	2'1	5'1	7'5	8'5	9'1	9'4	9'4	9'4	9'2	8'8	8'1	7'1	5'9	4'4	3'0	2'0	1'1	15

Example.—Moon's Apparent Transit 3<sup>h</sup> 0<sup>m</sup> and H. P. 59' 15"; correction = + 4<sup>m</sup>.3.

TABLES NOS. 3-4.—Corrections to Times of High Water for Sun's H. P., Declination, and

Date	0 <sup>h</sup>			1 <sup>h</sup>			2 <sup>h</sup>			3 <sup>h</sup>			4 <sup>h</sup>			5 <sup>h</sup>			
	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	
Jan.	1	+ 3.5	+ 3.8	+ 4.0	+ 4.3	+ 4.6	+ 4.9	+ 5.1	+ 5.4	+ 5.6	+ 5.9	+ 6.1	+ 6.3	+ 6.5	+ 6.6	+ 6.5	+ 6.2	+ 5.7	+ 5.2
	6	5.9	6.1	6.3	6.5	6.7	6.9	7.0	7.2	7.4	7.5	7.7	7.8	8.0	8.1	8.0	7.9	7.6	7.4
	11	8.1	8.2	8.4	8.5	8.6	8.7	8.8	8.9	9.0	9.1	9.2	9.3	9.4	9.5	9.5	9.4	9.3	9.2
	16	+10.0	+10.0	+10.2	+10.2	+10.3	+10.3	+10.4	+10.5	+10.5	+10.6	+10.7	+10.8	+10.8	+10.8	+10.8	+10.7	+10.7	+10.6
	21	11.7	11.7	11.7	11.7	11.7	11.7	11.7	11.8	11.8	11.8	11.8	11.9	11.9	11.9	11.9	11.9	11.8	11.8
	26	13.9	12.9	12.9	13.0	13.0	13.0	13.0	13.0	13.1	13.1	13.0	13.0	12.7	12.6	12.6	12.6	12.7	12.7
Feb.	31	+13.7	+13.8	+13.8	+13.9	+13.9	+14.0	+14.0	+14.0	+14.1	+14.1	+14.0	+13.7	+13.2	+13.0	+13.0	+13.1	+13.2	+13.3
	5	14.4	14.4	14.2	14.2	14.1	14.1	14.0	13.9	13.9	13.8	13.7	13.5	13.2	13.1	13.1	13.1	13.2	13.4
	10	14.8	14.6	14.4	14.2	14.0	13.8	13.7	13.6	13.4	13.3	13.1	13.0	12.9	12.8	12.8	12.9	13.0	13.3
	15	+14.8	+14.5	+14.3	+14.0	+13.7	+13.5	+13.3	+13.2	+13.0	+12.8	+12.6	+12.5	+12.3	+12.2	+12.2	+12.3	+12.5	+12.9
	20	14.4	14.1	13.7	13.4	13.1	12.8	12.6	12.4	12.2	12.0	11.8	11.6	11.4	11.3	11.3	11.4	11.7	12.1
	25	13.9	13.5	13.1	12.7	12.4	12.1	11.9	11.6	11.4	11.1	10.9	10.6	10.3	10.2	10.2	10.3	10.7	11.1
March	2	+13.0	+12.5	+12.1	+11.6	+11.3	+11.0	+10.8	+10.5	+10.2	+ 9.9	+ 9.6	+ 9.3	+ 9.0	+ 8.9	+ 8.9	+ 9.0	+ 9.4	+ 9.9
	7	11.9	11.4	11.0	10.5	10.2	9.9	9.7	9.4	9.1	8.8	8.5	8.2	7.9	7.8	7.8	7.9	8.3	8.8
	12	10.5	10.1	9.7	9.3	8.9	8.6	8.4	8.2	7.9	7.6	7.3	7.0	6.7	6.6	6.6	6.7	7.0	7.6
	17	+ 9.0	+ 8.7	+ 8.3	+ 8.0	+ 7.6	+ 7.3	+ 7.1	+ 6.9	+ 6.6	+ 6.3	+ 6.0	+ 5.8	+ 5.5	+ 5.4	+ 5.4	+ 5.5	+ 5.8	+ 6.4
	22	7.4	7.1	6.9	6.6	6.3	6.0	5.8	5.6	5.3	5.0	4.7	4.5	4.3	4.2	4.2	4.3	4.6	5.1
	27	5.8	5.5	5.3	5.0	4.8	4.6	4.4	4.2	4.0	3.8	3.6	3.4	3.2	3.1	3.1	3.2	3.4	3.7
April	1	+ 4.2	+ 4.0	+ 3.8	+ 3.6	+ 3.4	+ 3.3	+ 3.2	+ 3.0	+ 2.9	+ 2.7	+ 2.6	+ 2.4	+ 2.2	+ 2.1	+ 2.1	+ 2.2	+ 2.3	+ 2.5
	6	2.6	2.5	2.3	2.2	2.1	2.0	1.9	1.8	1.8	1.7	1.6	1.5	1.4	1.3	1.3	1.4	1.4	1.6
	11	1.1	1.0	1.0	0.9	0.9	0.9	0.8	0.8	0.8	0.8	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.8
	16	- 0.4	- 0.3	- 0.3	- 0.2	- 0.1	+ 0.0	+ 0.0	+ 0.0	+ 0.1	+ 0.1	+ 0.1	+ 0.1	+ 0.1	+ 0.1	+ 0.1	+ 0.1	+ 0.1	- 0.1
	21	1.6	1.5	1.3	1.2	1.0	- 0.8	- 0.7	- 0.6	- 0.5	- 0.5	- 0.4	- 0.4	- 0.3	- 0.3	- 0.3	- 0.4	- 0.5	0.7
	26	2.6	2.4	2.2	2.0	1.8	1.6	1.5	1.3	1.2	1.1	0.9	0.8	0.6	0.5	0.5	0.6	0.7	1.0
May	1	- 3.8	- 3.2	- 3.0	- 2.7	- 2.5	- 2.3	- 2.2	- 2.0	- 1.8	- 1.6	- 1.4	- 1.2	- 0.9	- 0.7	- 0.7	- 0.8	- 0.9	- 1.1
	6	4.1	3.8	3.4	3.1	2.8	2.6	2.4	2.2	1.9	1.7	1.4	1.2	0.8	0.6	0.6	0.7	0.8	1.1
	11	4.4	4.0	3.6	3.2	2.9	2.6	2.4	2.1	1.8	1.5	1.2	0.9	0.4	0.2	0.2	0.3	0.5	0.8
	16	- 4.5	- 4.1	- 3.7	- 3.3	- 2.9	- 2.6	- 2.3	- 2.0	- 1.6	- 1.2	- 0.8	- 0.4	+ 0.1	+ 0.3	+ 0.3	+ 0.1	- 0.1	- 0.5
	21	4.3	3.9	3.5	3.1	2.6	2.3	2.0	1.6	1.2	0.7	0.2	+ 0.3	0.8	1.0	1.0	0.8	+ 0.6	+ 0.1
	26	3.8	3.4	3.0	2.6	2.1	1.7	1.4	0.9	0.4	+ 0.2	+ 0.7	1.2	1.7	2.0	2.0	1.8	1.5	0.9
June	31	- 3.1	- 2.8	- 2.4	- 2.0	- 1.6	- 1.1	- 0.7	- 0.1	+ 0.4	+ 1.1	+ 1.7	+ 2.2	+ 2.7	+ 3.0	+ 3.0	+ 2.8	+ 2.4	+ 1.8
	5	2.5	2.0	1.6	1.1	0.7	0.2	+ 0.3	+ 1.0	1.5	2.3	2.9	3.5	4.0	4.3	4.3	4.1	3.6	2.0
	10	1.6	1.1	0.7	0.2	+ 0.3	+ 0.9	1.4	2.1	2.7	3.5	4.2	4.8	5.4	5.7	5.7	5.5	4.9	4.1
	15	- 0.7	- 0.3	+ 0.4	+ 0.9	+ 1.5	+ 2.1	+ 2.8	+ 3.5	+ 4.2	+ 5.1	+ 5.8	+ 6.3	+ 6.9	+ 7.1	+ 7.1	+ 6.9	+ 6.2	+ 5.2
	20	- 0.3	+ 0.9	1.5	2.1	2.8	3.5	4.3	5.0	5.8	6.7	7.4	7.9	8.4	8.6	8.6	8.3	7.5	6.4
	25	1.3	1.9	2.7	3.3	4.0	4.7	5.5	6.2	7.0	7.9	8.6	9.1	9.6	9.8	9.8	9.5	8.7	7.6
July	30	+ 3.1	+ 2.9	+ 2.7	+ 2.4	+ 2.1	+ 1.8	+ 1.6	+ 1.3	+ 1.0	+ 0.7	+ 0.2	+ 0.7	+ 1.2	+ 1.7	+ 2.0	+ 1.8	+ 1.5	0.9
	5	3.1	3.8	4.6	5.3	6.0	6.6	7.4	8.1	8.9	9.7	10.4	10.9	11.4	11.5	11.5	11.3	10.5	9.4

Example.—January 20th and Moon's Apparent Transit 5<sup>h</sup> 40<sup>m</sup>; correction = + 12<sup>m</sup>.7.

Equation of Time (Apparent to Mean). Arguments—Day of Year and Moon's Apparent Transit.

6 <sup>h</sup>			7 <sup>h</sup>			8 <sup>h</sup>			9 <sup>h</sup>			10 <sup>h</sup>			11 <sup>h</sup>				Date
0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	60 <sup>m</sup>	
<sup>m</sup> + 4'6	<sup>m</sup> + 4'2	<sup>m</sup> + 3'6	<sup>m</sup> + 3'2	<sup>m</sup> + 2'6	<sup>m</sup> + 2'1	<sup>m</sup> + 1'6	<sup>m</sup> + 1'3	<sup>m</sup> + 1'2	<sup>m</sup> + 1'3	<sup>m</sup> + 1'5	<sup>m</sup> + 1'7	<sup>m</sup> + 1'9	<sup>m</sup> + 2'2	<sup>m</sup> + 2'4	<sup>m</sup> + 2'7	<sup>m</sup> + 2'9	<sup>m</sup> + 3'2	<sup>m</sup> + 3'5	Jan. 1
6'9	6'5	5'9	5'5	5'0	4'8	4'5	4'3	4'3	4'4	4'6	4'7	4'9	5'0	5'2	5'4	5'5	5'7	5'9	6
8'9	8'5	8'1	7'7	7'4	7'3	7'2	7'1	7'1	7'2	7'3	7'4	7'5	7'6	7'7	7'8	7'9	8'0	8'1	11
+10'5	+10'2	+10'0	+9'7	+9'6	+9'5	+9'5	+9'4	+9'4	+9'4	+9'4	+9'5	+9'6	+9'7	+9'7	+9'8	+9'9	+9'9	+10'0	16
11'8	11'7	11'7	11'6	11'6	11'6	11'5	11'5	11'5	11'5	11'5	11'6	11'6	11'6	11'6	11'7	11'7	11'7	11'7	21
12'8	12'8	13'0	13'0	13'1	13'2	13'2	13'2	13'2	13'1	13'0	12'8	12'7	12'7	12'7	12'8	12'8	12'8	12'8	26
+13'4	+13'6	+14'0	+14'2	+14'3	+14'4	+14'5	+14'6	+14'6	+14'3	+13'9	+13'6	+13'5	+13'5	+13'6	+13'6	+13'6	+13'7	+13'7	31
13'7	14'0	14'6	14'9	15'2	15'4	15'5	15'6	15'6	15'4	15'2	15'0	14'9	14'8	14'7	14'6	14'6	14'5	14'4	Feb. 5
13'7	14'2	14'8	15'3	15'7	16'0	16'1	16'2	16'2	16'1	16'0	15'9	15'7	15'6	15'4	15'3	15'2	15'0	14'8	10
+13'3	+14'0	+14'8	+15'5	+15'9	+16'3	+16'5	+16'6	+16'6	+16'5	+16'3	+16'2	+16'0	+15'8	+15'6	+15'5	+15'3	+15'1	+14'8	15
12'6	13'4	14'4	15'2	15'7	16'1	16'4	16'5	16'5	16'4	16'2	16'0	15'8	15'6	15'4	15'2	15'0	14'7	14'4	20
11'8	12'7	13'9	14'8	15'5	15'9	16'3	16'4	16'4	16'3	16'0	15'7	15'5	15'2	15'0	14'7	14'5	14'2	13'9	25
+10'6	+11'6	+13'0	+14'0	+14'7	+15'2	+15'6	+15'7	+15'7	+15'6	+15'3	+15'0	+14'7	+14'4	+14'1	+13'8	+13'6	+13'3	+13'0	Mar. 2
9'6	10'5	11'9	12'8	13'6	14'1	14'5	14'6	14'6	14'5	14'2	13'9	13'6	13'3	13'0	12'7	12'5	12'2	11'9	7
8'3	9'2	10'6	11'5	12'2	12'8	13'1	13'2	13'2	13'1	12'8	12'5	12'2	11'9	11'6	11'4	11'2	10'9	10'5	12
+7'0	+7'9	+9'1	+10'0	+10'6	+11'2	+11'5	+11'6	+11'6	+11'5	+11'2	+11'0	+10'7	+10'4	+10'1	+9'9	+9'7	+9'4	+9'0	17
5'7	6'5	7'5	8'3	8'9	9'4	9'7	9'8	9'8	9'7	9'5	9'3	9'0	8'7	8'4	8'2	8'0	7'7	7'4	22
4'2	4'9	5'9	6'6	7'1	7'4	7'6	7'7	7'7	7'6	7'4	7'2	7'0	6'8	6'6	6'4	6'2	6'0	5'8	27
+2'9	+3'5	+4'3	+4'9	+5'3	+5'5	+5'6	+5'7	+5'7	+5'6	+5'4	+5'2	+5'1	+4'9	+4'8	+4'6	+4'5	+4'4	+4'2	Ap. 1
1'8	2'1	2'7	3'0	3'2	3'4	3'4	3'5	3'5	3'4	3'3	3'2	3'1	3'0	3'0	2'9	2'8	2'7	2'6	6
0'8	0'9	1'1	1'2	1'2	1'3	1'3	1'3	1'3	1'3	1'3	1'3	1'2	1'2	1'2	1'2	1'1	1'1	1'1	11
-0'1	-0'2	-0'4	-0'5	-0'5	-0'6	-0'7	-0'7	-0'7	-0'7	-0'7	-0'7	-0'7	-0'6	-0'6	-0'6	-0'5	-0'4	-0'4	16
0'9	1'2	1'6	1'9	2'1	2'3	2'4	2'5	2'5	2'5	2'4	2'4	2'3	2'3	2'2	2'1	2'0	1'8	1'6	21
1'2	1'9	2'7	3'4	3'6	3'9	4'0	4'1	4'1	4'0	3'8	3'7	3'5	3'4	3'3	3'1	3'0	2'8	2'6	26
-1'5	-2'4	-3'8	-4'7	-5'1	-5'3	-5'4	-5'5	-5'5	-5'3	-5'0	-4'8	-4'6	-4'4	-4'2	-4'0	-3'9	-3'7	-3'5	May 1
1'6	2'7	4'5	5'6	6'1	6'4	6'5	6'6	6'6	6'4	6'0	5'8	5'5	5'3	5'0	4'8	4'6	4'4	4'1	6
1'4	2'8	4'8	6'2	6'8	7'1	7'3	7'4	7'4	7'2	6'7	6'4	6'1	5'8	5'5	5'2	5'0	4'7	4'4	11
-1'2	-2'7	-5'1	-6'6	-7'3	-7'7	-7'9	-8'1	-8'1	-7'9	-7'4	-7'0	-6'6	-6'2	-5'8	-5'5	-5'2	-4'9	-4'5	16
0'8	2'4	5'0	6'6	7'5	8'0	8'2	8'4	8'4	8'2	7'7	7'2	6'7	6'2	5'8	5'4	5'1	4'8	4'3	21
0'1	1'8	4'6	6'3	7'3	7'9	8'2	8'4	8'4	8'1	7'6	7'1	6'6	6'0	5'5	5'0	4'7	4'3	3'8	26
+0'7	-1'2	-4'0	-5'9	-7'0	-7'6	-8'0	-8'2	-8'2	-7'9	-7'4	-6'9	-6'3	-5'6	-5'1	-4'5	-4'1	-3'6	-3'2	31
1'7	0'3	3'3	5'3	6'5	7'2	7'7	7'9	7'9	7'6	7'1	6'5	5'9	5'1	4'6	3'9	3'4	2'9	2'5	June 5
2'8	+0'7	2'5	4'6	5'9	6'7	7'3	7'5	7'5	7'2	6'6	6'0	5'3	4'5	3'9	3'2	2'7	2'1	1'6	10
+3'8	+1'7	-1'5	-3'6	-5'0	-6'0	-6'7	-6'9	-6'9	-6'7	-6'1	-5'6	-4'9	-4'0	-3'3	-2'6	-1'9	-1'3	-0'7	15
4'9	2'8	0'4	2'5	4'0	5'1	5'9	6'2	6'2	6'0	5'5	5'0	4'3	3'4	2'6	1'9	1'1	0'4	+0'3	20
6'1	3'9	+0'7	1'5	3'0	4'1	4'9	5'2	5'2	5'0	4'5	4'0	3'3	2'4	1'6	0'9	0'1	+0'6	1'3	25
+7'1	+4'9	+1'7	-0'5	-2'1	-3'2	-4'0	-4'3	-4'3	-4'1	-3'6	-3'1	-2'4	-1'5	-0'7	+0'0	+0'8	+1'5	+2'2	30
7'9	5'8	2'6	+0'5	1'0	2'1	2'9	3'1	3'1	3'0	2'5	2'0	1'3	0'5	+0'3	1'0	1'8	2'4	3'1	July 5

Example.—January 26th and Moon's Apparent Transit 5<sup>h</sup> 40<sup>m</sup>; correction = + 12<sup>m</sup>.7.

TABLES Nos. 3-4.—Corrections to Times of High Water for Sun's H. P., Declination, and

Date	0 <sup>h</sup>			1 <sup>h</sup>			2 <sup>h</sup>			3 <sup>h</sup>			4 <sup>h</sup>			5 <sup>h</sup>			
	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	
July	5	+ 3'1	+ 3'8	+ 4'6	+ 5'3	+ 6'0	+ 6'6	+ 7'4	+ 8'1	+ 8'9	+ 9'7	+ 10'4	+ 11'4	+ 11'5	+ 11'5	+ 11'3	+ 10'5	+ 9'4	
	10	4'0	4'6	5'4	6'0	6'7	7'3	8'1	8'7	9'3	10'3	11'0	11'4	11'9	12'0	12'0	11'8	11'1	10'0
	15	4'6	5'3	5'9	6'6	7'2	7'8	8'5	9'1	9'8	10'6	11'2	11'6	12'1	12'1	12'1	12'0	11'3	10'3
	20	+ 5'1	+ 5'7	+ 6'3	+ 6'9	+ 7'5	+ 8'1	+ 8'7	+ 9'2	+ 9'9	+ 10'6	+ 11'1	+ 11'5	+ 12'0	+ 12'0	+ 12'0	+ 11'9	+ 11'2	+ 10'3
	25	5'4	6'0	6'4	7'0	7'5	8'0	8'4	8'9	9'5	10'1	10'5	10'9	11'4	11'6	11'6	11'4	10'8	10'1
	30	5'4	5'9	6'3	6'8	7'2	7'5	7'8	8'2	8'7	9'2	9'6	10'0	10'5	10'8	10'8	10'6	10'1	9'5
Aug.	4	+ 5'1	+ 5'6	+ 6'0	+ 6'5	+ 6'8	+ 7'1	+ 7'3	+ 7'7	+ 8'1	+ 8'5	+ 8'8	+ 9'2	+ 9'7	+ 10'0	+ 10'0	+ 9'8	+ 9'4	+ 9'0
	9	4'6	5'0	5'4	5'8	6'1	6'4	6'6	6'9	7'2	7'5	7'8	8'1	8'6	8'8	8'8	8'7	8'5	8'2
	14	3'9	4'3	4'5	4'9	5'2	5'4	5'6	5'8	6'1	6'3	6'6	6'8	7'2	7'4	7'4	7'3	7'1	6'9
	19	+ 3'0	+ 3'3	+ 3'5	+ 3'8	+ 4'0	+ 4'2	+ 4'3	+ 4'5	+ 4'7	+ 4'9	+ 5'1	+ 5'3	+ 5'6	+ 5'8	+ 5'8	+ 5'7	+ 5'6	+ 5'4
	24	1'9	2'1	2'3	2'5	2'7	2'8	2'9	3'1	3'2	3'4	3'5	3'7	3'9	4'0	4'0	3'9	3'8	3'6
	29	0'5	0'6	0'8	0'9	1'0	1'1	1'2	1'3	1'4	1'5	1'6	1'7	1'8	1'9	1'9	1'8	1'6	1'4
Sept.	3	- 0'9	- 0'8	- 0'8	- 0'7	- 0'6	- 0'6	- 0'5	- 0'4	- 0'4	- 0'3	- 0'3	- 0'2	- 0'2	- 0'1	- 0'1	- 0'2	- 0'4	- 0'4
	8	2'5	2'5	2'5	2'5	2'4	2'4	2'4	2'4	2'4	2'4	2'3	2'3	2'3	2'3	2'3	2'3	2'3	2'4
	13	4'1	4'2	4'2	4'3	4'3	4'3	4'3	4'4	4'4	4'4	4'5	4'5	4'5	4'6	4'6	4'5	4'5	4'4
	18	- 5'8	- 5'9	- 6'1	- 6'2	- 6'3	- 6'3	- 6'4	- 6'4	- 6'5	- 6'6	- 6'7	- 6'7	- 6'8	- 6'9	- 6'9	- 6'8	- 6'7	- 6'5
	23	7'5	7'6	7'8	7'9	8'1	8'2	8'3	8'4	8'5	8'6	8'8	8'8	9'0	9'1	9'1	9'0	8'8	8'5
	28	9'1	9'3	9'5	9'7	9'9	10'0	10'2	10'3	10'5	10'6	10'8	10'9	11'1	11'2	11'2	11'1	10'8	10'5
Oct.	3	- 10'7	- 10'9	- 11'1	- 11'3	- 11'5	- 11'7	- 11'8	- 12'0	- 12'2	- 12'3	- 12'5	- 12'7	- 12'9	- 13'0	- 13'0	- 12'9	- 12'5	- 12'2
	8	12'2	12'4	12'6	12'8	13'1	13'2	13'3	13'6	13'8	13'9	14'1	14'3	14'5	14'6	14'6	14'5	14'1	13'8
	13	13'4	13'6	13'8	14'0	14'3	14'4	14'5	14'8	15'0	15'1	15'3	15'5	15'7	15'8	15'8	15'7	15'3	15'0
	18	- 14'5	- 14'7	- 14'9	- 15'1	- 15'4	- 15'5	- 15'6	- 15'9	- 16'1	- 16'2	- 16'4	- 16'6	- 16'8	- 16'9	- 16'9	- 16'8	- 16'4	- 16'1
	23	15'3	15'5	15'7	15'9	16'1	16'3	16'4	16'6	16'8	16'9	17'1	17'3	17'5	17'6	17'6	17'5	17'1	16'8
	28	15'8	16'0	16'2	16'4	16'6	16'7	16'9	17'0	17'2	17'3	17'5	17'6	17'8	17'9	17'9	17'8	17'5	17'2
Nov.	2	- 16'0	- 16'2	- 16'4	- 16'6	- 16'7	- 16'8	- 16'9	- 17'0	- 17'1	- 17'2	- 17'4	- 17'4	- 17'6	- 17'7	- 17'7	- 17'6	- 17'4	- 17'1
	7	16'0	16'1	16'3	16'4	16'5	16'5	16'6	16'6	16'7	16'8	16'9	16'9	17'0	17'1	17'1	17'0	16'9	16'7
	12	15'6	15'7	15'7	15'8	15'8	15'8	15'9	15'9	15'9	15'9	15'9	15'9	15'9	16'0	16'0	16'0	16'0	15'9
	17	- 14'9	- 14'8	- 14'8	- 14'7	- 14'7	- 14'7	- 14'7	- 14'6	- 14'6	- 14'6	- 14'6	- 14'6	- 14'5	- 14'5	- 14'5	- 14'5	- 14'6	- 14'6
	22	13'9	13'8	13'6	13'5	13'4	13'4	13'3	13'2	13'1	13'0	12'9	12'9	12'8	12'7	12'7	12'8	12'9	13'1
	27	12'4	12'2	12'0	11'8	11'7	11'6	11'4	11'3	11'1	11'0	10'8	10'7	10'6	10'5	10'5	10'6	10'8	11'1
Dec.	2	- 10'7	- 10'5	- 10'1	- 9'9	- 9'7	- 9'5	- 9'3	- 9'1	- 8'9	- 8'8	- 8'6	- 8'4	- 8'3	- 8'2	- 8'2	- 8'3	- 8'5	- 8'9
	7	8'8	8'5	8'1	7'8	7'5	7'2	7'0	6'8	6'6	6'4	6'2	6'0	5'8	5'7	5'7	5'8	6'1	6'3
	12	6'5	6'2	5'8	5'5	5'2	4'9	4'7	4'4	4'1	3'8	3'5	3'2	3'0	2'9	2'9	3'1	3'5	3'9
	17	- 4'1	- 3'8	- 3'4	- 3'1	- 2'8	- 2'5	- 2'3	- 2'0	- 1'6	- 1'2	- 0'9	- 0'6	- 0'4	- 0'3	- 0'3	- 0'5	- 0'9	- 1'4
	22	1'5	1'2	1'0	0'7	0'4	0'1	+ 0'2	+ 0'6	+ 1'0	+ 1'4	+ 1'7	+ 2'0	+ 2'2	+ 2'3	+ 2'3	+ 2'0	+ 1'6	+ 1'1
	27	+ 1'0	+ 1'3	+ 1'5	+ 1'8	+ 2'1	+ 2'4	2'7	3'1	3'5	3'9	4'2	4'5	4'7	4'8	4'8	4'5	4'1	3'6
32	+ 3'4	+ 3'7	+ 3'9	+ 4'2	+ 4'5	+ 4'7	+ 4'9	+ 5'3	+ 5'5	+ 5'9	+ 6'2	+ 6'5	+ 6'6	+ 6'7	+ 6'7	+ 6'5	+ 6'1	+ 5'7	

Example.—January 26th and Moon's Apparent Transit 5<sup>h</sup> 40<sup>m</sup>; correction = + 12<sup>m</sup>.7.

Equation of Time (Apparent to Mean). Arguments—Day of Year and Moon's Apparent Transit.

6 <sup>h</sup>			7 <sup>h</sup>			8 <sup>h</sup>			9 <sup>h</sup>			10 <sup>h</sup>			11 <sup>h</sup>				Date
0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	0 <sup>m</sup>	20 <sup>m</sup>	40 <sup>m</sup>	60 <sup>m</sup>	
+ 7 <sup>9</sup>	+ 5 <sup>8</sup>	+ 2 <sup>6</sup>	+ 0 <sup>5</sup>	- 1 <sup>1</sup>	- 2 <sup>1</sup>	- 2 <sup>9</sup>	- 3 <sup>1</sup>	- 3 <sup>1</sup>	- 3 <sup>0</sup>	- 2 <sup>5</sup>	- 2 <sup>5</sup>	- 1 <sup>3</sup>	- 0 <sup>5</sup>	+ 0 <sup>3</sup>	+ 1 <sup>0</sup>	+ 1 <sup>8</sup>	+ 2 <sup>4</sup>	+ 3 <sup>1</sup>	July 5
8 <sup>6</sup>	6 <sup>5</sup>	3 <sup>5</sup>	1 <sup>4</sup>	0 <sup>0</sup>	1 <sup>1</sup>	1 <sup>8</sup>	2 <sup>0</sup>	2 <sup>0</sup>	1 <sup>9</sup>	1 <sup>4</sup>	1 <sup>0</sup>	0 <sup>3</sup>	+ 0 <sup>5</sup>	1 <sup>3</sup>	1 <sup>9</sup>	2 <sup>7</sup>	3 <sup>3</sup>	4 <sup>0</sup>	10
9 <sup>0</sup>	7 <sup>0</sup>	4 <sup>2</sup>	2 <sup>2</sup>	+ 0 <sup>9</sup>	0 <sup>1</sup>	0 <sup>8</sup>	0 <sup>9</sup>	0 <sup>9</sup>	0 <sup>9</sup>	0 <sup>4</sup>	0 <sup>0</sup>	+ 0 <sup>6</sup>	1 <sup>4</sup>	2 <sup>1</sup>	2 <sup>7</sup>	3 <sup>4</sup>	4 <sup>0</sup>	4 <sup>6</sup>	15
+ 9 <sup>1</sup>	+ 7 <sup>3</sup>	+ 4 <sup>7</sup>	+ 2 <sup>9</sup>	+ 1 <sup>7</sup>	+ 0 <sup>8</sup>	+ 0 <sup>1</sup>	0 <sup>0</sup>	0 <sup>0</sup>	0 <sup>0</sup>	+ 0 <sup>5</sup>	+ 0 <sup>9</sup>	+ 1 <sup>4</sup>	+ 2 <sup>1</sup>	+ 2 <sup>8</sup>	+ 3 <sup>3</sup>	+ 3 <sup>9</sup>	+ 4 <sup>5</sup>	+ 5 <sup>1</sup>	20
9 <sup>0</sup>	7 <sup>4</sup>	5 <sup>0</sup>	3 <sup>4</sup>	2 <sup>3</sup>	1 <sup>6</sup>	1 <sup>0</sup>	+ 0 <sup>8</sup>	+ 0 <sup>8</sup>	+ 1 <sup>0</sup>	1 <sup>5</sup>	1 <sup>9</sup>	2 <sup>3</sup>	2 <sup>9</sup>	3 <sup>5</sup>	4 <sup>0</sup>	4 <sup>4</sup>	4 <sup>9</sup>	5 <sup>4</sup>	25
8 <sup>7</sup>	7 <sup>2</sup>	5 <sup>0</sup>	3 <sup>5</sup>	2 <sup>7</sup>	2 <sup>1</sup>	1 <sup>6</sup>	1 <sup>4</sup>	1 <sup>4</sup>	1 <sup>7</sup>	2 <sup>2</sup>	2 <sup>6</sup>	3 <sup>0</sup>	3 <sup>5</sup>	4 <sup>0</sup>	4 <sup>4</sup>	4 <sup>7</sup>	5 <sup>0</sup>	5 <sup>4</sup>	30
+ 8 <sup>3</sup>	+ 6 <sup>9</sup>	+ 4 <sup>7</sup>	+ 3 <sup>3</sup>	+ 2 <sup>6</sup>	+ 2 <sup>2</sup>	+ 1 <sup>8</sup>	+ 1 <sup>6</sup>	+ 1 <sup>6</sup>	+ 1 <sup>9</sup>	+ 2 <sup>4</sup>	+ 2 <sup>8</sup>	+ 3 <sup>1</sup>	+ 3 <sup>5</sup>	+ 3 <sup>9</sup>	+ 4 <sup>3</sup>	+ 4 <sup>5</sup>	+ 4 <sup>8</sup>	+ 5 <sup>1</sup>	Aug. 4
7 <sup>6</sup>	6 <sup>2</sup>	4 <sup>2</sup>	2 <sup>8</sup>	2 <sup>2</sup>	1 <sup>9</sup>	1 <sup>7</sup>	1 <sup>6</sup>	1 <sup>6</sup>	1 <sup>8</sup>	2 <sup>3</sup>	2 <sup>6</sup>	2 <sup>9</sup>	3 <sup>2</sup>	3 <sup>5</sup>	3 <sup>8</sup>	4 <sup>0</sup>	4 <sup>3</sup>	4 <sup>6</sup>	9
6 <sup>4</sup>	5 <sup>3</sup>	3 <sup>5</sup>	2 <sup>4</sup>	1 <sup>9</sup>	1 <sup>7</sup>	1 <sup>5</sup>	1 <sup>4</sup>	1 <sup>4</sup>	1 <sup>6</sup>	2 <sup>0</sup>	2 <sup>2</sup>	2 <sup>5</sup>	2 <sup>7</sup>	3 <sup>0</sup>	3 <sup>2</sup>	3 <sup>4</sup>	3 <sup>6</sup>	3 <sup>9</sup>	14
+ 5 <sup>0</sup>	+ 4 <sup>1</sup>	+ 2 <sup>7</sup>	+ 1 <sup>8</sup>	+ 1 <sup>4</sup>	+ 1 <sup>2</sup>	+ 1 <sup>1</sup>	+ 1 <sup>0</sup>	+ 1 <sup>0</sup>	+ 1 <sup>2</sup>	+ 1 <sup>5</sup>	+ 1 <sup>7</sup>	+ 1 <sup>9</sup>	+ 2 <sup>1</sup>	+ 2 <sup>3</sup>	+ 2 <sup>5</sup>	+ 2 <sup>6</sup>	+ 2 <sup>8</sup>	+ 3 <sup>0</sup>	19
3 <sup>3</sup>	2 <sup>7</sup>	1 <sup>7</sup>	1 <sup>1</sup>	0 <sup>8</sup>	0 <sup>6</sup>	0 <sup>5</sup>	0 <sup>4</sup>	0 <sup>4</sup>	0 <sup>5</sup>	0 <sup>7</sup>	0 <sup>9</sup>	1 <sup>0</sup>	1 <sup>2</sup>	1 <sup>3</sup>	1 <sup>5</sup>	1 <sup>6</sup>	1 <sup>7</sup>	1 <sup>9</sup>	24
1 <sup>2</sup>	0 <sup>9</sup>	0 <sup>5</sup>	0 <sup>2</sup>	0 <sup>0</sup>	- 0 <sup>2</sup>	- 0 <sup>4</sup>	- 0 <sup>5</sup>	- 0 <sup>5</sup>	- 0 <sup>4</sup>	- 0 <sup>3</sup>	- 0 <sup>2</sup>	- 0 <sup>1</sup>	0 <sup>0</sup>	0 <sup>1</sup>	0 <sup>2</sup>	0 <sup>3</sup>	0 <sup>4</sup>	0 <sup>5</sup>	29
- 0 <sup>5</sup>	- 0 <sup>7</sup>	- 0 <sup>9</sup>	- 1 <sup>1</sup>	- 1 <sup>2</sup>	- 1 <sup>2</sup>	- 1 <sup>4</sup>	- 1 <sup>5</sup>	- 1 <sup>5</sup>	- 1 <sup>4</sup>	- 1 <sup>4</sup>	- 1 <sup>3</sup>	- 1 <sup>3</sup>	- 1 <sup>2</sup>	- 1 <sup>2</sup>	- 1 <sup>1</sup>	- 1 <sup>0</sup>	- 1 <sup>0</sup>	- 0 <sup>9</sup>	Sep. 3
2 <sup>4</sup>	2 <sup>5</sup>	2 <sup>5</sup>	2 <sup>6</sup>	2 <sup>6</sup>	2 <sup>7</sup>	2 <sup>7</sup>	2 <sup>7</sup>	2 <sup>7</sup>	2 <sup>7</sup>	2 <sup>7</sup>	2 <sup>7</sup>	2 <sup>7</sup>	2 <sup>6</sup>	2 <sup>6</sup>	2 <sup>6</sup>	2 <sup>6</sup>	2 <sup>6</sup>	2 <sup>5</sup>	8
4 <sup>3</sup>	4 <sup>2</sup>	4 <sup>2</sup>	4 <sup>1</sup>	4 <sup>0</sup>	3 <sup>9</sup>	3 <sup>9</sup>	3 <sup>8</sup>	3 <sup>8</sup>	3 <sup>9</sup>	3 <sup>9</sup>	3 <sup>9</sup>	4 <sup>0</sup>	4 <sup>0</sup>	4 <sup>0</sup>	4 <sup>1</sup>	4 <sup>1</sup>	4 <sup>1</sup>	4 <sup>1</sup>	13
- 6 <sup>3</sup>	- 6 <sup>1</sup>	- 5 <sup>9</sup>	- 5 <sup>7</sup>	- 5 <sup>5</sup>	- 5 <sup>3</sup>	- 5 <sup>2</sup>	- 5 <sup>1</sup>	- 5 <sup>1</sup>	- 5 <sup>2</sup>	- 5 <sup>3</sup>	- 5 <sup>3</sup>	- 5 <sup>4</sup>	- 5 <sup>5</sup>	- 5 <sup>6</sup>	- 5 <sup>6</sup>	- 5 <sup>7</sup>	- 5 <sup>7</sup>	- 5 <sup>8</sup>	18
8 <sup>2</sup>	7 <sup>9</sup>	7 <sup>5</sup>	7 <sup>2</sup>	6 <sup>9</sup>	6 <sup>6</sup>	6 <sup>4</sup>	6 <sup>3</sup>	6 <sup>3</sup>	6 <sup>4</sup>	6 <sup>6</sup>	6 <sup>6</sup>	6 <sup>8</sup>	6 <sup>9</sup>	7 <sup>0</sup>	7 <sup>1</sup>	7 <sup>2</sup>	7 <sup>3</sup>	7 <sup>5</sup>	23
10 <sup>1</sup>	9 <sup>7</sup>	9 <sup>1</sup>	8 <sup>7</sup>	8 <sup>3</sup>	8 <sup>0</sup>	7 <sup>7</sup>	7 <sup>6</sup>	7 <sup>6</sup>	7 <sup>7</sup>	7 <sup>9</sup>	8 <sup>0</sup>	8 <sup>2</sup>	8 <sup>3</sup>	8 <sup>5</sup>	8 <sup>6</sup>	8 <sup>8</sup>	8 <sup>9</sup>	9 <sup>1</sup>	28
- 11 <sup>8</sup>	- 11 <sup>3</sup>	- 10 <sup>7</sup>	- 10 <sup>2</sup>	- 9 <sup>8</sup>	- 9 <sup>5</sup>	- 9 <sup>1</sup>	- 9 <sup>0</sup>	- 9 <sup>0</sup>	- 9 <sup>1</sup>	- 9 <sup>3</sup>	- 9 <sup>5</sup>	- 9 <sup>7</sup>	- 9 <sup>8</sup>	- 10 <sup>0</sup>	- 10 <sup>2</sup>	- 10 <sup>3</sup>	- 10 <sup>5</sup>	- 10 <sup>7</sup>	Oct. 3
13 <sup>3</sup>	12 <sup>8</sup>	12 <sup>2</sup>	11 <sup>7</sup>	11 <sup>2</sup>	10 <sup>9</sup>	10 <sup>5</sup>	10 <sup>4</sup>	10 <sup>4</sup>	10 <sup>5</sup>	10 <sup>7</sup>	10 <sup>9</sup>	11 <sup>1</sup>	11 <sup>2</sup>	11 <sup>4</sup>	11 <sup>7</sup>	11 <sup>8</sup>	11 <sup>9</sup>	12 <sup>2</sup>	8
14 <sup>5</sup>	14 <sup>0</sup>	13 <sup>4</sup>	12 <sup>9</sup>	12 <sup>4</sup>	12 <sup>1</sup>	11 <sup>7</sup>	11 <sup>6</sup>	11 <sup>6</sup>	11 <sup>7</sup>	11 <sup>9</sup>	12 <sup>2</sup>	12 <sup>3</sup>	12 <sup>4</sup>	12 <sup>6</sup>	12 <sup>9</sup>	13 <sup>0</sup>	13 <sup>1</sup>	13 <sup>4</sup>	13
- 15 <sup>6</sup>	- 15 <sup>1</sup>	- 14 <sup>5</sup>	- 14 <sup>0</sup>	- 13 <sup>5</sup>	- 13 <sup>2</sup>	- 12 <sup>8</sup>	- 12 <sup>7</sup>	- 12 <sup>7</sup>	- 12 <sup>8</sup>	- 13 <sup>0</sup>	- 13 <sup>2</sup>	- 13 <sup>4</sup>	- 13 <sup>5</sup>	- 13 <sup>7</sup>	- 14 <sup>0</sup>	- 14 <sup>1</sup>	- 14 <sup>2</sup>	- 14 <sup>5</sup>	18
16 <sup>3</sup>	15 <sup>9</sup>	15 <sup>3</sup>	14 <sup>9</sup>	14 <sup>4</sup>	14 <sup>1</sup>	13 <sup>7</sup>	13 <sup>6</sup>	13 <sup>6</sup>	13 <sup>7</sup>	13 <sup>9</sup>	14 <sup>1</sup>	14 <sup>3</sup>	14 <sup>4</sup>	14 <sup>6</sup>	14 <sup>8</sup>	14 <sup>9</sup>	15 <sup>1</sup>	15 <sup>5</sup>	23
16 <sup>8</sup>	16 <sup>4</sup>	15 <sup>8</sup>	15 <sup>4</sup>	15 <sup>0</sup>	14 <sup>7</sup>	14 <sup>4</sup>	14 <sup>3</sup>	14 <sup>3</sup>	14 <sup>4</sup>	14 <sup>6</sup>	14 <sup>7</sup>	14 <sup>9</sup>	15 <sup>0</sup>	15 <sup>2</sup>	15 <sup>3</sup>	15 <sup>5</sup>	15 <sup>6</sup>	15 <sup>8</sup>	28
- 16 <sup>8</sup>	- 16 <sup>5</sup>	- 16 <sup>1</sup>	- 15 <sup>8</sup>	- 15 <sup>5</sup>	- 15 <sup>2</sup>	- 15 <sup>0</sup>	- 14 <sup>9</sup>	- 14 <sup>9</sup>	- 15 <sup>0</sup>	- 15 <sup>2</sup>	- 15 <sup>2</sup>	- 15 <sup>4</sup>	- 15 <sup>5</sup>	- 15 <sup>6</sup>	- 15 <sup>7</sup>	- 15 <sup>8</sup>	- 15 <sup>9</sup>	- 16 <sup>0</sup>	Nov. 2
16 <sup>5</sup>	16 <sup>3</sup>	16 <sup>1</sup>	15 <sup>9</sup>	15 <sup>7</sup>	15 <sup>5</sup>	15 <sup>4</sup>	15 <sup>3</sup>	15 <sup>3</sup>	15 <sup>4</sup>	15 <sup>5</sup>	15 <sup>5</sup>	15 <sup>6</sup>	15 <sup>7</sup>	15 <sup>8</sup>	15 <sup>8</sup>	15 <sup>9</sup>	15 <sup>9</sup>	16 <sup>0</sup>	7
15 <sup>8</sup>	15 <sup>8</sup>	15 <sup>6</sup>	15 <sup>6</sup>	15 <sup>5</sup>	15 <sup>4</sup>	15 <sup>4</sup>	15 <sup>4</sup>	15 <sup>4</sup>	15 <sup>5</sup>	15 <sup>5</sup>	15 <sup>5</sup>	15 <sup>5</sup>	15 <sup>5</sup>	15 <sup>5</sup>	15 <sup>5</sup>	15 <sup>5</sup>	15 <sup>6</sup>	15 <sup>6</sup>	12
- 14 <sup>7</sup>	- 14 <sup>8</sup>	- 14 <sup>8</sup>	- 14 <sup>9</sup>	- 15 <sup>0</sup>	- 15 <sup>0</sup>	- 15 <sup>1</sup>	- 15 <sup>1</sup>	- 15 <sup>1</sup>	- 15 <sup>1</sup>	- 15 <sup>0</sup>	- 15 <sup>0</sup>	- 15 <sup>0</sup>	- 15 <sup>0</sup>	- 14 <sup>9</sup>	- 14 <sup>9</sup>	- 14 <sup>9</sup>	- 14 <sup>9</sup>	- 14 <sup>9</sup>	17
13 <sup>4</sup>	13 <sup>6</sup>	13 <sup>8</sup>	14 <sup>0</sup>	14 <sup>3</sup>	14 <sup>5</sup>	14 <sup>6</sup>	14 <sup>7</sup>	14 <sup>7</sup>	14 <sup>6</sup>	14 <sup>5</sup>	14 <sup>5</sup>	14 <sup>4</sup>	14 <sup>3</sup>	14 <sup>2</sup>	14 <sup>1</sup>	14 <sup>0</sup>	14 <sup>0</sup>	13 <sup>9</sup>	22
11 <sup>5</sup>	11 <sup>8</sup>	12 <sup>4</sup>	12 <sup>7</sup>	13 <sup>1</sup>	13 <sup>4</sup>	13 <sup>6</sup>	13 <sup>7</sup>	13 <sup>7</sup>	13 <sup>6</sup>	13 <sup>5</sup>	13 <sup>4</sup>	13 <sup>2</sup>	13 <sup>1</sup>	12 <sup>9</sup>	12 <sup>8</sup>	12 <sup>6</sup>	12 <sup>5</sup>	12 <sup>4</sup>	27
- 9 <sup>3</sup>	- 9 <sup>9</sup>	- 10 <sup>7</sup>	- 11 <sup>3</sup>	- 11 <sup>7</sup>	- 12 <sup>1</sup>	- 12 <sup>3</sup>	- 12 <sup>4</sup>	- 12 <sup>4</sup>	- 12 <sup>3</sup>	- 12 <sup>2</sup>	- 12 <sup>0</sup>	- 11 <sup>8</sup>	- 11 <sup>7</sup>	- 11 <sup>5</sup>	- 11 <sup>3</sup>	- 11 <sup>1</sup>	- 10 <sup>9</sup>	- 10 <sup>7</sup>	Dec. 2
7 <sup>0</sup>	7 <sup>8</sup>	8 <sup>8</sup>	9 <sup>6</sup>	10 <sup>1</sup>	10 <sup>5</sup>	10 <sup>8</sup>	10 <sup>9</sup>	10 <sup>9</sup>	10 <sup>8</sup>	10 <sup>6</sup>	10 <sup>4</sup>	10 <sup>2</sup>	10 <sup>0</sup>	9 <sup>8</sup>	9 <sup>6</sup>	9 <sup>4</sup>	9 <sup>1</sup>	8 <sup>8</sup>	7
4 <sup>6</sup>	5 <sup>4</sup>	6 <sup>6</sup>	7 <sup>4</sup>	8 <sup>1</sup>	8 <sup>5</sup>	8 <sup>9</sup>	9 <sup>1</sup>	9 <sup>1</sup>	9 <sup>0</sup>	8 <sup>8</sup>	8 <sup>5</sup>	8 <sup>2</sup>	7 <sup>9</sup>	7 <sup>6</sup>	7 <sup>3</sup>	7 <sup>1</sup>	6 <sup>8</sup>	6 <sup>5</sup>	12
- 2 <sup>1</sup>	- 3 <sup>0</sup>	- 4 <sup>2</sup>	- 5 <sup>1</sup>	- 5 <sup>8</sup>	- 6 <sup>3</sup>	- 6 <sup>7</sup>	- 6 <sup>9</sup>	- 6 <sup>9</sup>	- 6 <sup>8</sup>	- 6 <sup>6</sup>	- 6 <sup>3</sup>	- 6 <sup>0</sup>	- 5 <sup>6</sup>	- 5 <sup>2</sup>	- 4 <sup>9</sup>	- 4 <sup>7</sup>	- 4 <sup>4</sup>	- 4 <sup>1</sup>	17
+ 0 <sup>4</sup>	+ 0 <sup>5</sup>	+ 1 <sup>7</sup>	+ 2 <sup>6</sup>	+ 3 <sup>3</sup>	+ 3 <sup>8</sup>	+ 4 <sup>2</sup>	+ 4 <sup>5</sup>	+ 4 <sup>5</sup>	+ 4 <sup>4</sup>	+ 4 <sup>2</sup>	+ 3 <sup>9</sup>	+ 3 <sup>6</sup>	+ 3 <sup>2</sup>	+ 2 <sup>8</sup>	+ 2 <sup>4</sup>	+ 2 <sup>1</sup>	+ 1 <sup>8</sup>	+ 1 <sup>5</sup>	22
2 <sup>9</sup>	+ 2 <sup>0</sup>	+ 0 <sup>8</sup>	0 <sup>1</sup>	0 <sup>8</sup>	1 <sup>3</sup>	1 <sup>7</sup>	2 <sup>0</sup>	2 <sup>0</sup>	1 <sup>9</sup>	1 <sup>7</sup>	1 <sup>4</sup>	1 <sup>1</sup>	0 <sup>7</sup>	0 <sup>3</sup>	+ 0 <sup>1</sup>	+ 0 <sup>4</sup>	+ 0 <sup>7</sup>	+ 1 <sup>0</sup>	27
+ 5 <sup>1</sup>	+ 4 <sup>3</sup>	+ 3 <sup>3</sup>	+ 2 <sup>5</sup>	+ 1 <sup>9</sup>	+ 1 <sup>5</sup>	+ 1 <sup>1</sup>	+ 0 <sup>9</sup>	+ 0 <sup>9</sup>	+ 1 <sup>0</sup>	+ 1 <sup>2</sup>	+ 1 <sup>4</sup>	+ 1 <sup>7</sup>	+ 2 <sup>0</sup>	+ 2 <sup>3</sup>	+ 2 <sup>7</sup>	+ 2 <sup>9</sup>	+ 3 <sup>1</sup>	+ 3 <sup>4</sup>	32

Example.—January 26th and Moon's Apparent Transit 5<sup>h</sup> 40<sup>m</sup>; correction = + 12<sup>m</sup>.7.

TABLE No. 5.—Correction for Moon's Declination for London Heights. Applicable to Moon's Transit B. (or 4th previous).

Declina- tion	0 <sup>h</sup> 0 <sup>m</sup>	0 <sup>h</sup> 10 <sup>m</sup>	0 <sup>h</sup> 20 <sup>m</sup>	0 <sup>h</sup> 30 <sup>m</sup>	0 <sup>h</sup> 40 <sup>m</sup>	0 <sup>h</sup> 50 <sup>m</sup>	0 <sup>h</sup> 0 <sup>m</sup>	0 <sup>h</sup> 10 <sup>m</sup>	0 <sup>h</sup> 20 <sup>m</sup>	0 <sup>h</sup> 30 <sup>m</sup>	0 <sup>h</sup> 40 <sup>m</sup>	0 <sup>h</sup> 50 <sup>m</sup>	0 <sup>h</sup> 0 <sup>m</sup>	0 <sup>h</sup> 10 <sup>m</sup>	0 <sup>h</sup> 20 <sup>m</sup>	0 <sup>h</sup> 30 <sup>m</sup>	0 <sup>h</sup> 40 <sup>m</sup>	0 <sup>h</sup> 50 <sup>m</sup>	0 <sup>h</sup> 0 <sup>m</sup>	0 <sup>h</sup> 10 <sup>m</sup>	0 <sup>h</sup> 20 <sup>m</sup>	0 <sup>h</sup> 30 <sup>m</sup>	0 <sup>h</sup> 40 <sup>m</sup>	0 <sup>h</sup> 50 <sup>m</sup>	0 <sup>h</sup> 0 <sup>m</sup>	0 <sup>h</sup> 10 <sup>m</sup>	0 <sup>h</sup> 20 <sup>m</sup>	0 <sup>h</sup> 30 <sup>m</sup>	0 <sup>h</sup> 40 <sup>m</sup>	0 <sup>h</sup> 50 <sup>m</sup>	Declina- tion
0	.32	.32	.31	.31	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	0
1	.32	.32	.31	.31	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	1
2	.31	.31	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	2
3	.31	.31	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	3
4	.30	.30	.30	.30	.29	.29	.29	.29	.29	.29	.29	.29	.29	.29	.29	.29	.29	.29	.29	.29	.29	.29	.29	.29	.29	.29	.29	.29	.29	.29	4
5	.29	.29	.29	.29	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	5
6	.27	.27	.27	.27	.26	.26	.26	.26	.26	.26	.26	.26	.26	.26	.26	.26	.26	.26	.26	.26	.26	.26	.26	.26	.26	.26	.26	.26	.26	.26	6
7	.25	.25	.25	.25	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	.24	7
8	.23	.23	.23	.23	.22	.22	.22	.22	.22	.22	.22	.22	.22	.22	.22	.22	.22	.22	.22	.22	.22	.22	.22	.22	.22	.22	.22	.22	.22	.22	8
9	.21	.21	.21	.21	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	9
10	.18	.18	.18	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17	10
11	.15	.15	.15	.14	.14	.14	.14	.14	.14	.14	.14	.14	.14	.14	.14	.14	.14	.14	.14	.14	.14	.14	.14	.14	.14	.14	.14	.14	.14	.14	11
12	.12	.12	.12	.11	.11	.11	.11	.11	.11	.11	.11	.11	.11	.11	.11	.11	.11	.11	.11	.11	.11	.11	.11	.11	.11	.11	.11	.11	.11	.11	12
13	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	13
14	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	14
15	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	15
16	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	16
17	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	17
18	.13	.13	.13	.13	.13	.13	.13	.13	.13	.13	.13	.13	.13	.13	.13	.13	.13	.13	.13	.13	.13	.13	.13	.13	.13	.13	.13	.13	.13	.13	18
19	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	.18	19
20	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	.23	20
21	.29	.29	.29	.29	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	.28	21
22	.35	.35	.35	.35	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34	22
23	.41	.41	.41	.41	.40	.40	.40	.40	.40	.40	.40	.40	.40	.40	.40	.40	.40	.40	.40	.40	.40	.40	.40	.40	.40	.40	.40	.40	.40	.40	23
24	.47	.47	.47	.47	.46	.46	.46	.46	.46	.46	.46	.46	.46	.46	.46	.46	.46	.46	.46	.46	.46	.46	.46	.46	.46	.46	.46	.46	.46	.46	24
25	.53	.53	.53	.53	.52	.52	.52	.52	.52	.52	.52	.52	.52	.52	.52	.52	.52	.52	.52	.52	.52	.52	.52	.52	.52	.52	.52	.52	.52	.52	25
26	.59	.59	.59	.59	.58	.58	.58	.58	.58	.58	.58	.58	.58	.58	.58	.58	.58	.58	.58	.58	.58	.58	.58	.58	.58	.58	.58	.58	.58	.58	26
27	.66	.66	.66	.66	.65	.65	.65	.65	.65	.65	.65	.65	.65	.65	.65	.65	.65	.65	.65	.65	.65	.65	.65	.65	.65	.65	.65	.65	.65	.65	27
28	.73	.73	.73	.73	.72	.72	.72	.72	.72	.72	.72	.72	.72	.72	.72	.72	.72	.72	.72	.72	.72	.72	.72	.72	.72	.72	.72	.72	.72	.72	28
29	.80	.80	.80	.80	.79	.79	.79	.79	.79	.79	.79	.79	.79	.79	.79	.79	.79	.79	.79	.79	.79	.79	.79	.79	.79	.79	.79	.79	.79	.79	29
30	.87	.87	.87	.87	.86	.86	.86	.86	.86	.86	.86	.86	.86	.86	.86	.86	.86	.86	.86	.86	.86	.86	.86	.86	.86	.86	.86	.86	.86	.86	30

Example.—Moon's Apparent Transit 2<sup>h</sup> 50<sup>m</sup> and Declination 25°; correction = - 0.52 feet.

TABLE No. 6.—Correction for Moon's H. P. for London Heights. Applicable to Moon's Transit B. (or 4th previous).

H. P.	0 <sup>h</sup> 0 <sup>m</sup>	1 <sup>h</sup> 0 <sup>m</sup>	1 <sup>h</sup> 30 <sup>m</sup>	2 <sup>h</sup> 0 <sup>m</sup>	2 <sup>h</sup> 30 <sup>m</sup>	3 <sup>h</sup> 0 <sup>m</sup>	3 <sup>h</sup> 30 <sup>m</sup>	4 <sup>h</sup> 0 <sup>m</sup>	4 <sup>h</sup> 30 <sup>m</sup>	5 <sup>h</sup> 0 <sup>m</sup>	5 <sup>h</sup> 30 <sup>m</sup>	6 <sup>h</sup> 0 <sup>m</sup>	6 <sup>h</sup> 30 <sup>m</sup>	7 <sup>h</sup> 0 <sup>m</sup>	7 <sup>h</sup> 30 <sup>m</sup>	8 <sup>h</sup> 0 <sup>m</sup>	8 <sup>h</sup> 30 <sup>m</sup>	9 <sup>h</sup> 0 <sup>m</sup>	9 <sup>h</sup> 30 <sup>m</sup>	10 <sup>h</sup> 0 <sup>m</sup>	10 <sup>h</sup> 30 <sup>m</sup>	11 <sup>h</sup> 0 <sup>m</sup>	11 <sup>h</sup> 30 <sup>m</sup>	H. P.	
53 0	-70	-70	-69	-69	-68	-67	-66	-65	-64	-63	-62	-61	-60	-59	-58	-57	-56	-55	-54	-53	-52	-51	-50	-49	53 50
54 0	-60	-60	-60	-60	-59	-58	-57	-56	-55	-54	-53	-52	-51	-50	-49	-48	-47	-46	-45	-44	-43	-42	-41	-40	54 10
10	-62	-62	-61	-61	-60	-59	-58	-57	-56	-55	-54	-53	-52	-51	-50	-49	-48	-47	-46	-45	-44	-43	-42	-41	55 0
20	-59	-59	-58	-58	-57	-56	-55	-54	-53	-52	-51	-50	-49	-48	-47	-46	-45	-44	-43	-42	-41	-40	-39	-38	55 10
30	-56	-56	-55	-55	-54	-53	-52	-51	-50	-49	-48	-47	-46	-45	-44	-43	-42	-41	-40	-39	-38	-37	-36	-35	56 0
40	-53	-53	-52	-52	-51	-50	-49	-48	-47	-46	-45	-44	-43	-42	-41	-40	-39	-38	-37	-36	-35	-34	-33	-32	56 10
50	-49	-49	-48	-48	-47	-46	-45	-44	-43	-42	-41	-40	-39	-38	-37	-36	-35	-34	-33	-32	-31	-30	-29	-28	57 0
30	-35	-35	-35	-35	-34	-34	-33	-33	-32	-31	-30	-29	-28	-27	-27	-26	-25	-24	-23	-22	-21	-20	-19	-18	57 10
40	-31	-31	-31	-31	-30	-30	-29	-29	-28	-27	-26	-25	-24	-23	-22	-21	-20	-19	-18	-17	-16	-15	-14	-13	58 0
50	-27	-27	-27	-27	-26	-26	-25	-25	-24	-23	-22	-21	-20	-19	-18	-17	-16	-15	-14	-13	-12	-11	-10	-9	58 10
30	-23	-23	-23	-23	-22	-22	-21	-21	-20	-19	-18	-17	-16	-15	-14	-13	-12	-11	-10	-9	-8	-7	-6	-5	59 0
40	-20	-20	-20	-20	-19	-19	-18	-18	-17	-16	-15	-14	-13	-12	-11	-10	-9	-8	-7	-6	-5	-4	-3	-2	59 10
50	-16	-16	-16	-16	-15	-15	-14	-14	-13	-12	-11	-10	-9	-8	-7	-6	-5	-4	-3	-2	-1	0	1	2	59 20
30	-12	-12	-12	-12	-11	-11	-10	-10	-9	-8	-7	-6	-5	-4	-3	-2	-1	0	1	2	3	4	5	6	59 30
40	-08	-08	-08	-08	-07	-07	-06	-06	-05	-04	-04	-03	-02	-01	0	1	2	3	4	5	6	7	8	9	59 40
50	-04	-04	-04	-04	-03	-03	-02	-02	-01	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	59 50
30	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	59 59
40	04	04	04	04	04	04	04	04	04	04	04	04	04	04	04	04	04	04	04	04	04	04	04	04	59 59
50	08	08	08	08	08	08	08	08	08	08	08	08	08	08	08	08	08	08	08	08	08	08	08	08	59 59
30	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	59 59
40	16	16	16	16	16	16	16	16	16	16	16	16	16	16	16	16	16	16	16	16	16	16	16	16	59 59
50	20	20	20	20	20	20	20	20	20	20	20	20	20	20	20	20	20	20	20	20	20	20	20	20	59 59
30	24	24	24	24	24	24	24	24	24	24	24	24	24	24	24	24	24	24	24	24	24	24	24	24	59 59
40	28	28	28	28	27	27	26	26	25	24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	59 59
50	32	32	32	32	31	31	30	30	29	28	27	26	25	24	23	22	21	20	19	18	17	16	15	14	59 59
30	36	36	36	36	35	35	34	34	33	32	31	30	29	28	27	26	25	24	23	22	21	20	19	18	59 59
40	40	40	40	40	39	39	38	38	37	36	35	34	33	32	31	30	29	28	27	26	25	24	23	22	59 59
50	44	44	44	44	43	43	42	42	41	40	39	38	37	36	35	34	33	32	31	30	29	28	27	26	59 59
30	48	48	48	47	47	46	45	44	43	42	41	40	39	38	37	36	35	34	33	32	31	30	29	28	59 59
40	52	52	52	51	51	50	49	48	47	46	45	44	43	42	41	40	39	38	37	36	35	34	33	32	59 59
50	56	56	56	55	55	54	53	52	51	50	49	48	47	46	45	44	43	42	41	40	39	38	37	36	59 59
30	60	60	60	60	60	60	60	60	60	60	60	60	60	60	60	60	60	60	60	60	60	60	60	60	59 59
40	64	64	64	63	63	62	61	60	59	58	57	56	55	54	53	52	51	50	49	48	47	46	45	44	59 59
50	68	68	68	67	67	66	65	64	63	62	61	60	59	58	57	56	55	54	53	52	51	50	49	48	59 59
30	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	59 59
40	76	76	76	76	76	76	76	76	76	76	76	76	76	76	76	76	76	76	76	76	76	76	76	76	59 59
50	80	80	80	80	80	80	80	80	80	80	80	80	80	80	80	80	80	80	80	80	80	80	80	80	59 59
30	84	84	84	84	84	84	84	84	84	84	84	84	84	84	84	84	84	84	84	84	84	84	84	84	59 59
40	88	88	88	88	88	88	88	88	88	88	88	88	88	88	88	88	88	88	88	88	88	88	88	88	59 59
50	92	92	92	92	92	92	92	92	92	92	92	92	92	92	92	92	92	92	92	92	92	92	92	92	59 59
30	96	96	96	96	96	96	96	96	96	96	96	96	96	96	96	96	96	96	96	96	96	96	96	96	59 59
40	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	59 59
50	104	104	104	104	104	104	104	104	104	104	104	104	104	104	104	104	104	104	104	104	104	104	104	104	59 59
30	108	108	108	108	108	108	108	108	108	108	108	108	108	108	108	108	108	108	108	108	108	108	108	108	59 59
40	112	112	112	112	112	112	112	112	112	112	112	112	112	112	112	112	112	112	112	112	112	112	112	112	59 59
50	116	116	116	116	116	116	116	116	116	116	116	116	116	116	116	116	116	116	116	116	116	116	116	116	59 59

Example.—Moon's apparent Transit 6<sup>h</sup> 30<sup>m</sup> and H. P. 58' 10"; correction = + 0.28 feet.

TABLE NO. 7.—Correction for Sun's H. P. and Declination combined for London Heights.  
Applicable to Moon's Transit B (or 4th previous).

Date	0 <sup>h</sup> 0 <sup>m</sup>	1 <sup>h</sup> 0 <sup>m</sup>	2 <sup>h</sup> 0 <sup>m</sup>	3 <sup>h</sup> 0 <sup>m</sup>	4 <sup>h</sup> 0 <sup>m</sup>	5 <sup>h</sup> 30 <sup>m</sup>	6 <sup>h</sup> 0 <sup>m</sup>	7 <sup>h</sup> 0 <sup>m</sup>	7 <sup>h</sup> 30 <sup>m</sup>	8 <sup>h</sup> 0 <sup>m</sup>	8 <sup>h</sup> 30 <sup>m</sup>	9 <sup>h</sup> 0 <sup>m</sup>	10 <sup>h</sup> 0 <sup>m</sup>	11 <sup>h</sup> 0 <sup>m</sup>	11 <sup>h</sup> 30 <sup>m</sup>	Date
	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	
Jan. 1	-.06	-.06	-.06	-.05	-.04	-.03	-.03	-.02	-.01	-.01	-.01	-.01	-.02	-.04	-.05	Jan. 1
11	.04	.04	.04	.03	.02	.01	.01	.01	.01	.01	.01	.01	.02	.03	.04	11
21	.00	.00	.01	.01	.01	.00	.00	.00	.00	.00	.00	.00	.00	.01	.01	21
31	+.06	+.06	+.06	+.05	+.04	+.03	+.03	+.02	+.01	+.01	+.01	+.01	+.02	+.03	+.04	31
Feb. 10	.00	.00	.00	.03	.03	.02	.02	.01	.01	.01	.01	.01	.02	.03	.04	Feb. 10
20	.12	.12	.12	.11	.10	.09	.08	.07	.06	.05	.04	.03	.02	.01	.01	20
Mar. 2	.15	.15	.14	.13	.12	.11	.10	.09	.08	.07	.06	.05	.04	.03	.02	Mar. 2
12	.14	.14	.14	.13	.12	.11	.10	.09	.08	.07	.06	.05	.04	.03	.02	12
22	.13	.13	.13	.12	.11	.10	.09	.08	.07	.06	.05	.04	.03	.02	.01	22
Apr. 1	.10	.10	.10	.09	.08	.07	.06	.05	.04	.03	.02	.01	.01	.01	.01	Apr. 1
11	.07	.07	.07	.06	.05	.04	.03	.02	.01	.01	.01	.01	.01	.01	.01	11
21	.03	.03	.02	.02	.01	.01	.00	.00	.00	.00	.00	.00	.00	.01	.02	21
May 1	-.04	-.04	-.04	-.03	-.02	-.02	-.01	-.01	-.01	-.01	-.01	-.01	-.02	-.03	-.04	May 1
11	.09	.09	.09	.08	.07	.06	.05	.04	.03	.02	.01	.01	.02	.03	.04	11
21	.15	.15	.14	.13	.12	.11	.10	.09	.08	.07	.06	.05	.04	.03	.02	21
31	.19	.19	.18	.16	.15	.14	.13	.12	.11	.10	.09	.08	.07	.06	.05	31
June 10	.22	.22	.21	.19	.18	.16	.15	.14	.13	.12	.11	.10	.09	.08	.07	June 10
20	.24	.24	.23	.21	.20	.18	.17	.16	.15	.14	.13	.12	.11	.10	.09	20
30	.24	.24	.23	.21	.20	.18	.17	.16	.15	.14	.13	.12	.11	.10	.09	30
July 10	.21	.21	.20	.18	.17	.15	.14	.13	.12	.11	.10	.09	.08	.07	.06	July 10
20	.17	.17	.16	.15	.14	.12	.11	.10	.09	.08	.07	.06	.05	.04	.03	20
30	.12	.12	.11	.10	.09	.08	.07	.06	.05	.04	.03	.02	.01	.01	.01	30
Aug. 9	.06	.06	.05	.04	.03	.02	.01	.01	.01	.01	.01	.01	.01	.01	.01	Aug. 9
19	.01	.01	.01	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	19
29	+.04	+.04	+.04	+.03	+.02	+.02	+.01	+.01	+.01	+.01	+.01	+.01	+.02	+.03	+.04	29
Sept. 8	.07	.07	.07	.06	.05	.04	.03	.02	.01	.01	.01	.01	.02	.03	.04	Sept. 8
18	.09	.09	.09	.08	.07	.06	.05	.04	.03	.02	.01	.01	.02	.03	.04	18
28	.11	.11	.10	.09	.08	.07	.06	.05	.04	.03	.02	.01	.01	.01	.01	28
Oct. 8	.12	.12	.12	.11	.10	.09	.08	.07	.06	.05	.04	.03	.02	.01	.01	Oct. 8
18	.10	.10	.10	.09	.08	.07	.06	.05	.04	.03	.02	.01	.01	.01	.01	18
28	.08	.08	.08	.07	.06	.05	.04	.03	.02	.01	.01	.01	.01	.01	.01	28
Nov. 7	.04	.04	.04	.03	.02	.02	.01	.01	.01	.01	.01	.01	.01	.01	.01	Nov. 7
17	.00	.00	.00	.01	.01	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	17
27	-.02	-.02	-.02	-.03	-.03	-.02	-.01	-.01	-.01	-.01	-.01	-.01	-.02	-.03	-.04	27
Dec. 7	.05	.05	.05	.04	.03	.02	.02	.01	.01	.01	.01	.01	.02	.03	.04	Dec. 7
17	.09	.09	.09	.08	.07	.06	.05	.04	.03	.02	.01	.01	.02	.03	.04	17
27	.09	.09	.09	.08	.07	.06	.05	.04	.03	.02	.01	.01	.02	.03	.04	27
37	.05	.05	.05	.04	.03	.02	.02	.01	.01	.01	.01	.01	.02	.03	.04	37

Example.—June 30th and Moon's Apparent Transit 7<sup>h</sup> 30<sup>m</sup>; correction — + 0.10 feet.



DUBLAT.  
Deduced from the Observations 1881-84 (June 17th to Sept. 16th omitted from each year).

LOW WATER Approximate Interval = 20 <sup>m</sup> (neglecting Longitude)			HIGH WATER Approximate Interval = 35 <sup>m</sup> (neglecting Longitude)			LOW WATER Factor = - 1.2			HIGH WATER Factor = + 1.2			
Moons' App't. Transit at Greenwich	Time	h m diff.	Moons' App't. Transit at Greenwich	Time	h m diff.	Moons' App't. Transit at Greenwich	Time	h m diff.	Moons' App't. Transit at Greenwich	Time	h m diff.	
0	4 53 +	7	0	10 36 +	7	0	4 12 +	20	0	7 46	0	11 19 +
10	5 0	10	10	10 43	7	10	4 32	20	10	7 45	10	11 24
20	5 6	19	20	10 50	7	20	4 52	20	20	7 45	20	11 28
30	5 13	7	30	10 57	7	30	5 12	19	30	7 45	30	11 30
40	5 20	19	40	11 4	7	40	5 31	19	40	7 47	40	11 27
50	5 26	6	50	11 35	19	50	5 49	18	50	7 50	50	11 21
1	5 33	7	1	11 53	18	1	6 7	18	1	7 55	1	11 11
10	5 40	7	10	11 25	7	10	6 24	17	10	7 50	10	10 99
20	5 46	6	20	11 32	7	20	6 40	16	20	7 56	20	10 86
30	5 53	7	30	11 39	7	30	6 54	14	30	7 74	30	10 71
40	6 0	7	40	11 46	7	40	7 8	14	40	7 82	40	10 53
50	6 6	6	50	11 54	8	50	7 21	13	50	7 91	50	10 34
2	6 13	7	2	0 1	7	2	7 33	12	2	8 00	2	10 13
10	6 20	7	10	0 8	7	10	7 44	11	10	8 10	10	9 91
20	6 26	6	20	0 16	8	20	7 55	10	20	8 21	20	9 70
30	6 33	7	30	0 23	7	30	8 5	9	30	8 32	30	9 51
40	6 40	7	40	0 30	7	40	8 14	9	40	8 44	40	9 33
50	6 46	6	50	0 38	8	50	8 23	9	50	8 56	50	9 17
3	6 53	7	3	0 45	7	3	8 31	8	3	8 68	3	9 02
10	7 0	7	10	0 53	8	10	8 39	8	10	8 81	10	8 87
20	7 6	6	20	1 0	8	20	8 47	7	20	8 95	20	8 73
30	7 13	7	30	1 8	8	30	8 54	7	30	9 09	30	8 59
40	7 20	7	40	1 16	8	40	9 1	8	40	9 24	40	8 45
50	7 27	8	50	1 24	8	50	9 9	8	50	9 39	50	8 32
4	7 35	8	4	1 32	8	4	9 16	7	4	9 55	4	8 19
10	7 43	8	10	1 41	9	10	9 23	6	10	9 71	10	8 07
20	7 51	8	20	1 50	9	20	9 29	6	20	9 87	20	7 96
30	8 0	9	30	1 59	9	30	9 36	7	30	10 03	30	7 86
40	8 10	10	40	2 9	10	40	9 43	6	40	10 19	40	7 78
50	8 20	10	50	2 21	12	50	9 49	6	50	10 34	50	7 71
5	8 31	11	5	2 34	13	5	9 56	7	5	10 49	5	7 66
10	8 43	12	10	2 48	14	10	10 3	7	10	10 63	10	7 61
20	8 56	13	20	3 3	15	20	10 9	6	20	10 77	20	7 57
30	9 9	13	30	3 19	16	30	10 16	7	30	10 90	30	7 54
40	9 24	15	40	3 36	17	40	10 23	7	40	11 02	40	7 51
50	9 41	17	50	3 54	18	50	10 29	6	50	11 12	50	7 48
6	10 0	19	6	4 12	18	6	10 36	7	6	11 10	6	7 46

Note. — Time Correction for Freshets = - 10<sup>m</sup> maximum August 15th (to be applied from June 17th to September 16th).  
Note. — 4.83 feet for Kedge gauge.

DIAMOND HARBOUR.  
Deduced from the Observations 1881-84 (June 17th to September 16th omitted from each year).

LOW WATER Approximate Interval = 32 <sup>m</sup> (neglecting Longitude)				HIGH WATER Approximate Interval = 30 <sup>m</sup> (neglecting Longitude)				LOW WATER Factor = -1.0				HIGH WATER Factor = +1.4			
Time		Time		Time		Time		Height		Height		Height		Height	
Moons Appt. Greenwich	h m	h m	diff.	Moons Appt. Greenwich	h m	h m	diff.	Moons Appt. Greenwich	h m	h m	diff.	Moons Appt. Greenwich	h m	h m	diff.
0	8 7	6	0 31	0	10	0 14	6	0	1 60	0	1 60	0	0	10	16 83
10	8 11	7	0 48	10	0 20	7	10	1 60	0	1 60	0	0	10	16 82	- 1
20	8 20	6	1 6	20	0 27	7	20	1 60	0	1 60	0	0	20	16 80	2
30	8 26	6	1 25	30	0 34	7	30	1 61	+	1 61	+	0	30	16 74	0
40	8 33	6	1 45	40	0 41	7	40	1 63	2	1 63	2	4	40	16 72	4
50	8 39	6	2 6	50	0 48	7	50	1 67	4	1 67	4	5	50	16 67	9
1	8 45	6	2 26	1	0 55	7	1	1 72	5	1 72	5	7	1	16 61	6
10	8 51	6	2 46	10	1 2	7	10	1 77	5	1 77	5	10	16 54	7	10
20	8 57	6	3 6	20	1 10	8	20	1 83	6	1 83	6	20	16 46	8	20
30	9 3	6	3 26	30	1 17	7	30	1 89	6	1 89	6	30	16 36	10	30
40	9 9	6	3 45	40	1 25	8	40	1 96	7	1 96	7	40	16 25	11	40
50	9 15	6	4 2	50	1 32	7	50	2 03	7	2 03	7	50	16 13	12	50
2	9 21	6	4 18	2	1 40	8	2	2 10	7	2 10	7	2	16 00	13	2
10	9 27	6	4 33	10	1 48	8	10	2 18	8	2 18	8	10	15 86	14	10
20	9 33	6	4 48	20	1 56	8	20	2 26	8	2 26	8	20	15 71	15	20
30	9 39	6	5 2	30	2 4	8	30	2 34	8	2 34	8	30	15 55	16	30
40	9 45	6	5 15	40	2 12	8	40	2 42	8	2 42	8	40	15 38	17	40
50	9 51	6	5 27	50	2 21	9	50	2 50	8	2 50	8	50	15 21	17	50
3	9 57	6	5 37	3	2 29	8	3	2 59	9	2 59	9	3	15 04	17	9
10	10 3	6	5 47	10	2 38	9	10	2 68	9	2 68	9	10	14 86	18	10
20	10 9	6	5 57	20	2 46	8	20	2 77	9	2 77	9	20	14 68	18	20
30	10 15	6	6 6	30	2 55	9	30	2 87	10	2 87	10	30	14 50	18	30
40	10 21	6	6 16	40	3 4	9	40	2 97	10	2 97	10	40	14 32	18	40
50	10 27	6	6 25	50	3 13	9	50	3 07	10	3 07	10	50	14 13	19	50
4	10 33	7	6 34	4	3 22	9	4	3 18	11	3 18	11	4	13 95	19	4
10	10 40	7	6 43	10	3 31	9	10	3 29	11	3 29	11	10	13 76	19	10
20	10 46	7	6 52	20	3 41	10	20	3 40	11	3 40	11	20	13 58	18	20
30	10 53	8	7 0	30	3 51	10	30	3 51	11	3 51	11	30	13 40	18	30
40	11 1	8	7 8	40	4 2	11	40	3 63	12	3 63	12	40	13 21	19	40
50	11 9	8	7 16	50	4 14	12	50	3 76	13	3 76	13	50	13 03	18	50
5	11 17	8	7 24	5	4 26	12	5	3 89	13	3 89	13	5	12 86	17	11
10	11 25	10	7 31	10	4 39	13	10	4 02	13	4 02	13	10	12 70	16	10
20	11 35	11	7 39	20	4 53	14	20	4 14	12	4 14	12	20	12 56	14	20
30	11 46	14	7 46	30	5 8	15	30	4 24	10	4 24	10	30	12 43	13	30
40	0 0	15	7 53	40	5 25	17	40	4 33	9	4 33	9	40	12 30	9	40
50	0 15	16	8 0	50	5 43	18	50	4 41	8	4 41	8	50	12 28	6	50
6	0 31	13	8 7	6	6 1	18	6	4 49	8	4 49	8	6	12 25	3	12

Note.—Referred to Kildare Dock Still.

Note.—Greenwich Mean Time.

KIDDERPORE.

Deduced from the Observations 1881-84, omitting those from June 17th to September 16th.

CHAP. VIII.]

LOW WATER Approximate Interval = 35 <sup>b</sup>				HIGH WATER Approximate Interval = 39 <sup>b</sup>				LOW WATER Factor = - 0.3				HIGH WATER Factor = + 1.2																	
Moon's Appt. Transit at Greenwich		Time		Moon's Appt. Transit at Greenwich		Time		Moon's Appt. Transit at Greenwich		Height		Moon's Appt. Transit at Greenwich		Height															
h	m	h	m	diff.	h	m	h	m	diff.	h	m	feet	diff.	h	m	feet	diff.	h	m	feet	diff.								
0	0	11	10		6	0	3	33		0	0	4	74		6	0	5	72		0	0	16	20		6	0	12	01	
		10	11	17	+	7				10	2	50	+	6						10	16	19	-	1		10	12	00	
		20	11	23		6		20	4	6	17				20	2	57		20	16	17		2		20	12	00	0	
		30	11	30		7		30	4	25	19				30	3	4		30	16	13		4		30	12	02	+	2
		40	11	37		7		40	4	45	20				40	3	11		40	16	09		4		40	12	08	6	
		50	11	43		6		50	5	6	21				50	3	18		50	16	05		4		50	12	17	9	
1	0	11	49		6	7	0	5	28	22				1	0	3	25		7	0	16	00	5	7	0	12	28	11	
		10	11	55		6	10	5	50	22				1	0	3	32		7	0	15	94	6	7	0	10	12	40	12
		20	0	1		6	20	6	11	21				2	0	3	40		8	0	15	87	7	20	12	54	14		
		30	0	7		6	30	6	31	20				3	0	3	47		7	0	15	78	9	30	12	69	15		
		40	0	13		6	40	6	50	19				4	0	3	55		8	0	15	69	9	40	12	85	16		
		50	0	19		6	50	7	7	17				5	0	3	47		7	0	15	59	10	50	13	01	16		
		0	0	25		6	8	0	7	22	15			2	0	3	10		8	0	15	47	12	8	0	13	18	17	
		10	0	31		6	10	7	37	15				2	0	3	18		8	0	15	35	12	10	10	13	36	18	
		20	0	36		5	20	7	51	14				2	0	3	26		8	0	15	22	13	20	10	13	54	18	
		30	0	42		6	30	8	4	13				3	0	3	34		8	0	15	08	14	30	10	13	72	18	
		40	0	48		6	40	8	17	13				4	0	3	42		8	0	14	93	15	40	10	13	91	19	
		50	0	53		6	50	8	29	12				5	0	3	51		9	0	14	78	15	50	10	14	09	18	
		0	0	59		6	9	0	8	40	11			3	0	3	59		8	0	14	62	16	9	0	14	27	18	
		10	1	5		6	10	8	50	10				3	0	3	8		9	0	14	46	16	10	10	14	45	18	
		20	1	10		5	20	9	0	10				2	0	3	17		9	0	14	29	17	20	10	14	62	17	
		30	1	16		6	30	9	10	10				3	0	3	26		9	0	14	12	17	30	10	14	79	17	
		40	1	22		6	40	9	20	10				4	0	3	35		9	0	13	94	18	40	10	14	95	16	
		50	1	27		5	50	9	29	9				5	0	3	44		9	0	13	76	18	50	10	15	11	16	
		0	1	33		6	10	9	38	9				4	0	3	54		10	0	13	58	18	10	10	15	27	16	
		10	1	39		6	10	9	47	9				4	0	3	6		10	0	13	40	18	10	10	15	42	15	
		20	1	45		6	20	9	55	8				3	0	3	15		11	0	13	23	17	20	10	15	56	14	
		30	1	52		7	30	10	3	8				4	0	3	26		11	0	13	06	17	30	10	15	68	12	
		40	2	0		8	40	10	11	8				4	0	3	37		11	0	12	89	17	40	10	15	79	11	
		50	2	8		8	50	10	19	8				5	0	3	49		12	0	12	73	16	50	10	15	89	10	
		0	2	17		9	11	0	10	26	7			5	0	3	7		13	0	12	57	16	11	0	15	98	9	
		10	2	26		9	10	10	34	8				5	0	3	15		13	0	12	42	15	10	10	16	06	8	
		20	2	37		11	20	10	41	7				4	0	3	29		14	0	12	30	13	20	10	16	12	6	
		30	2	49		12	30	10	48	7				4	0	3	45		16	0	12	20	10	30	10	16	17	5	
		40	3	2		13	40	10	55	7				3	0	3	8		17	0	12	12	8	40	10	16	20	3	
		50	3	17		15	50	11	3	8				3	0	3	20		18	0	12	06	6	50	10	16	20	0	
		6	3	33		16	12	0	11	10	7			3	0	3	39		19	0	12	01	5	12	0	16	20	0	

Note.—Calcutta Mean Time.

TIDAL PREDICTION.

ELEPHANT POINT.—(NEW SITE).  
Deduced from the Observations 1884, January to June\* (—3.90 feet).

Low WATER Approximate Interval = 35 <sup>a</sup>				High WATER Approximate Interval = 40 <sup>b</sup>				Low WATER Factor = -1.4				High WATER Factor = +1.6													
Time		Moon's Appt.		Time		Moon's Appt.		Height		Moon's Appt.		Height		Moon's Appt.		Height									
A	M	h	m	A	M	h	m	feet	diff.	A	M	h	m	feet	diff.	A	M								
0	11	21	7	6	0	4	36	+ 18	7	0	10	39	+ 19	0	3	00	- 1	0	21	12	0	15	09	- 2	
10	11	30	7	10	4	54	18	18	6	10	10	58	18	10	2	09	1	10	21	12	2	15	07	0	
20	11	37	7	20	5	13	18	18	6	20	11	16	18	20	2	08	0	20	21	10	3	15	07	2	
30	11	44	6	30	5	30	18	18	7	30	11	34	17	30	2	08	1	30	21	07	4	15	09	8	
40	11	50	6	40	5	48	17	17	7	40	11	51	16	40	2	09	1	40	21	03	6	16	07	14	
50	11	57	6	50	6	5	17	15	8	50	0	7	15	50	3	00	2	50	20	07	7	16	21	20	
1	0	3	6	7	0	6	22	17	7	1	0	5	11	1	0	3	02	7	0	20	00	8	16	41	21
10	0	9	7	10	6	39	16	16	7	10	0	37	14	10	3	05	3	10	20	82	8	16	02	21	
20	0	16	6	20	6	55	15	15	8	20	0	51	13	20	3	08	4	20	7	02	20	16	83	22	
30	0	23	6	30	7	10	15	14	8	30	1	4	12	30	3	12	5	30	20	65	9	17	05	23	
40	0	28	6	40	7	25	14	14	7	40	0	16	11	40	3	17	6	40	20	55	10	17	28	24	
50	0	34	6	50	7	39	13	13	8	50	1	27	10	50	3	23	6	50	20	45	11	17	52	24	
2	0	40	6	8	0	7	52	13	8	8	0	1	37	2	0	2	9	8	0	34	12	17	76	25	
10	0	46	6	10	8	5	12	12	9	10	1	47	9	10	3	37	9	10	20	22	12	18	01	25	
20	0	51	6	20	8	17	12	12	9	20	2	6	13	20	4	35	20	20	10	10	13	18	25	24	
30	0	58	6	30	8	29	11	11	9	30	2	5	8	30	3	57	11	30	19	10	13	19	25	24	
40	1	4	6	40	8	40	11	11	8	40	2	13	8	40	3	70	13	40	19	84	13	18	49	23	
50	1	10	6	50	8	51	11	11	8	50	2	21	8	50	3	84	14	50	19	69	15	18	72	21	
3	0	1	6	9	0	9	10	10	9	9	0	2	9	3	0	4	00	16	9	0	53	16	19	15	20
10	1	23	7	10	9	10	10	10	9	10	2	29	7	10	4	17	17	0	4	78	19	19	35	20	
20	1	30	7	20	9	20	10	10	9	20	2	36	8	20	4	17	18	20	4	59	18	19	35	19	
30	1	37	7	30	9	29	9	9	9	30	2	44	8	20	4	35	20	20	4	41	18	19	35	19	
40	1	45	8	40	9	38	9	9	9	40	2	51	7	30	4	55	21	30	10	00	10	19	35	19	
50	1	53	8	50	9	46	8	8	8	50	2	58	7	40	4	76	22	40	18	80	20	19	35	19	
4	0	2	1	10	0	9	54	8	8	4	0	7	44	7	50	4	98	22	50	18	59	21	20	06	16
10	2	10	9	10	0	10	2	2	8	10	0	3	12	4	0	5	22	24	0	18	36	23	20	21	15
20	2	20	10	20	0	10	2	2	7	20	3	18	6	10	5	46	24	10	3	68	12	18	13	15	14
30	2	30	10	30	0	10	9	9	7	20	3	25	7	20	5	69	23	20	3	57	11	18	13	13	
40	2	41	11	40	0	10	17	8	8	30	3	31	6	30	5	92	23	30	3	47	10	17	90	11	
50	2	53	12	50	0	10	25	7	7	40	3	37	6	40	6	16	24	40	3	38	8	17	43	10	
5	0	3	5	11	0	10	32	8	8	50	3	44	7	50	6	39	23	50	3	30	7	17	18	9	
10	3	17	12	10	0	10	40	7	7	5	0	3	50	6	6	61	22	11	0	3	23	6	16	88	9
20	3	31	14	20	0	10	47	8	8	10	3	56	6	10	6	82	21	10	3	12	5	16	68	7	
30	3	46	15	30	0	10	55	7	7	20	4	3	7	20	7	02	20	20	3	17	5	16	47	6	
40	4	2	16	40	0	11	3	7	30	30	4	9	6	30	7	20	18	30	3	08	4	16	30	5	
50	4	4	17	50	0	11	9	7	40	40	4	16	7	40	7	36	16	40	3	05	3	16	16	3	
6	0	4	19	6	0	11	16	7	50	10	20	18	6	50	7	49	13	50	3	02	2	16	05	2	
6	0	4	36	17	13	0	11	23	7	12	0	29	7	6	0	7	58	9	12	0	3	00	15	09	1

\* Moon Observations Accurately

RANGOON.  
Deduced from the Observations 1880-84 (Dry Season only).

LOW WATER Approximate Interval = 36 <sup>s</sup>				HIGH WATER Approximate Interval = 41 <sup>s</sup>				LOW WATER Factor = -0.9				HIGH WATER Factor = +1.4							
Moon's Appt.	Time	Greenwich	Moon's Appt.	Time	Greenwich	Moon's Appt.	Time	Greenwich	Moon's Appt.	Time	Greenwich	Moon's Appt.	Time	Greenwich	Moon's Appt.	Time	Greenwich	Height	diff.
h 0	0 39	10	h 6	5 37	10	h 6	11 29	10	h 6	2 16	10	h 6	4 85	10	h 6	18 50	10	14 10	- 1
0	0 46	20	0	5 55	20	0	11 49	20	0	2 15	20	0	4 90	20	0	18 50	20	14 09	+ 1
20	0 52	30	20	6 13	30	20	0 8	30	20	2 14	30	20	4 93	30	20	18 49	30	14 10	+
30	0 59	40	30	6 31	40	30	0 26	40	30	2 14	40	30	4 94	40	30	18 46	40	14 14	4
40	1 6	50	40	6 49	50	40	0 43	50	40	2 14	50	40	4 89	50	40	18 43	50	14 23	9
50	1 12	6	50	7 7	6	50	0 59	6	50	2 14	6	50	4 81	6	50	18 40	6	14 36	13
1	0 19	7	1	7 25	7	1	1 14	7	1	2 14	7	1	4 68	7	1	18 36	7	14 53	17
10	1 26	7	10	7 43	7	10	1 29	7	10	2 15	7	10	4 54	7	10	18 31	7	14 71	18
20	1 32	6	20	8 0	6	20	1 43	6	20	2 16	6	20	4 40	6	20	18 25	6	14 90	19
30	1 39	7	30	8 17	7	30	1 56	7	30	2 18	7	30	4 25	7	30	18 18	7	15 10	20
40	1 45	6	40	8 33	6	40	2 8	6	40	2 21	6	40	4 09	6	40	18 10	6	15 30	20
50	1 52	7	50	8 48	7	50	2 19	7	50	2 25	7	50	3 93	7	50	18 02	7	15 50	20
2	0 1 58	6	2	9 1	6	2	0 29	6	2	2 30	6	2	3 77	6	2	17 93	6	15 70	20
10	2 4	6	10	9 14	6	10	0 39	6	10	2 35	6	10	3 61	6	10	17 83	6	15 91	21
20	2 10	6	20	9 27	6	20	0 48	6	20	2 40	6	20	3 45	6	20	17 72	6	16 12	21
30	2 16	6	30	9 39	6	30	0 57	6	30	2 46	6	30	3 50	6	30	17 61	6	16 32	20
40	2 22	6	40	9 51	6	40	1 6	6	40	2 53	6	40	3 57	6	40	17 48	6	16 50	18
50	2 28	6	50	10 3	6	50	1 12	6	50	2 60	6	50	3 05	6	50	17 34	6	16 68	18
3	0 2 34	6	3	10 14	6	3	0 22	6	3	2 68	6	3	2 93	6	3	17 19	6	16 85	17
10	2 41	7	10	10 24	6	10	0 30	7	10	2 77	6	10	2 83	7	10	17 04	7	17 01	16
20	2 47	6	20	10 34	6	20	0 37	6	20	2 86	6	20	2 73	6	20	16 88	6	17 16	15
30	2 54	7	30	10 44	6	30	0 44	7	30	2 96	6	30	2 64	7	30	16 70	7	17 31	15
40	3 1	7	40	10 53	6	40	0 51	7	40	3 07	6	40	2 56	7	40	16 53	7	17 45	14
50	3 8	7	50	11 2	6	50	1 0	7	50	3 19	6	50	2 50	7	50	16 33	7	17 58	13
4	0 3 15	7	4	11 10	6	4	0 5	7	4	3 32	6	4	2 46	7	4	16 14	7	17 70	12
10	3 23	8	10	11 18	6	10	0 11	8	10	3 45	6	10	2 42	8	10	15 05	8	17 81	11
20	3 31	8	20	11 26	6	20	0 2	8	20	3 58	6	20	2 38	8	20	15 05	8	17 93	11
30	3 40	9	30	11 34	6	30	0 13	9	30	3 72	6	30	2 34	9	30	15 05	9	18 02	10
40	3 50	10	40	11 42	6	40	0 25	10	40	3 87	6	40	2 31	10	40	15 11	10	18 11	9
50	4 0	10	50	11 50	6	50	0 37	10	50	4 02	6	50	2 28	10	50	15 12	10	18 19	8
5	0 4 11	11	5	11 57	6	5	0 50	11	5	4 16	6	5	2 25	11	5	14 89	11	18 26	7
10	4 23	12	10	12 0	6	10	1 0	12	10	4 30	6	10	2 23	12	10	14 69	12	18 32	6
20	4 35	12	20	12 11	6	20	0 11	12	20	4 43	6	20	2 21	12	20	14 51	12	18 37	5
30	4 48	13	30	12 18	6	30	0 18	13	30	4 56	6	30	2 20	13	30	14 34	13	18 43	5
40	5 3	15	40	12 25	6	40	0 25	15	40	5 11	6	40	2 18	15	40	14 22	15	18 46	4
50	5 19	16	50	12 32	6	50	0 32	16	50	5 25	6	50	2 17	16	50	14 14	16	18 49	3
6	0 5 37	18	6	12 39	6	6	0 39	18	6	5 38	6	6	2 16	18	6	14 10	18	18 50	1

AMHERST.  
 Deduced from the Observations 1880-84 (Dry Season only), -4.61 feet.

LOW WATER Approximate Interval = 34 <sup>h</sup>				HIGH WATER Approximate Interval = 30 <sup>h</sup>				LOW WATER Factor = -1.8				HIGH WATER Factor = +1.8					
h	m	diff.	Time	h	m	diff.	Time	h	m	diff.	Height	h	m	diff.	Height		
Moon's Appt.	Greenwich			Moon's Appt.	Greenwich			Moon's Appt.	Greenwich		feet	Moon's Appt.	Greenwich		feet		
0	0	9.41	+	6	0	3.17	+18	6	0	9.28	+19	0	0	18.41	0	0	18.94
10	0	9.49	7	10	0	3.35	17	10	0	9.47	19	10	0	18.41	0	0	18.94
20	0	9.56	7	20	0	3.53	17	20	0	10.5	18	20	0	18.39	0	0	18.93
30	0	10.3	7	30	0	4.9	17	30	0	10.22	17	30	0	18.35	0	0	18.95
40	0	10.10	7	40	0	4.26	17	40	0	10.39	17	40	0	18.31	0	0	18.92
50	0	10.17	7	50	0	4.43	17	50	0	10.55	16	50	0	18.26	0	0	18.88
1	0	10.24	7	7	0	5.0	17	7	0	11.10	15	7	0	18.21	0	0	18.83
10	0	10.31	7	10	0	5.17	17	10	0	11.24	14	10	0	18.15	0	0	18.78
20	0	10.37	6	20	0	5.33	16	20	0	11.38	14	20	0	18.07	0	0	18.70
30	0	10.44	7	30	0	5.47	14	30	0	11.51	13	30	0	17.98	0	0	18.52
40	0	10.51	7	40	0	6.1	14	40	0	12.11	11	40	0	17.89	0	0	18.43
50	0	10.58	7	50	0	6.14	13	50	0	12.31	11	50	0	17.79	0	0	18.34
2	0	11.5	7	8	0	6.26	12	8	0	12.40	10	8	0	17.68	0	0	18.25
10	0	11.12	7	10	0	6.37	11	10	0	12.48	9	10	0	17.56	0	0	18.16
20	0	11.19	7	20	0	6.48	11	20	0	12.56	8	20	0	17.42	0	0	18.07
30	0	11.26	7	30	0	6.59	11	30	0	13.1	8	30	0	17.27	0	0	17.98
40	0	11.33	7	40	0	7.9	10	40	0	13.24	7	40	0	17.11	0	0	17.89
50	0	11.41	8	50	0	7.19	10	50	0	13.37	6	50	0	16.93	0	0	17.80
3	0	11.48	7	9	0	7.28	9	9	0	13.50	5	9	0	16.73	0	0	17.71
10	0	11.56	8	10	0	7.37	8	10	0	14.1	4	10	0	16.53	0	0	17.62
20	0	12.3	8	20	0	7.45	8	20	0	14.24	3	20	0	16.32	0	0	17.53
30	0	12.11	8	30	0	7.53	8	30	0	14.37	2	30	0	16.10	0	0	17.44
40	0	12.19	8	40	0	8.1	8	40	0	14.50	1	40	0	15.88	0	0	17.35
50	0	12.27	8	50	0	8.8	7	50	0	14.63	0	50	0	15.66	0	0	17.26
4	0	12.36	9	10	0	8.16	8	4	0	14.76	0	4	0	15.44	0	0	17.17
10	0	12.45	9	10	0	8.23	7	10	0	14.89	0	10	0	15.22	0	0	17.08
20	0	12.55	10	20	0	8.31	8	20	0	15.02	0	20	0	15.00	0	0	17.00
30	0	13.1	11	30	0	8.38	7	30	0	15.15	0	30	0	14.78	0	0	16.91
40	0	13.17	11	40	0	8.45	7	40	0	15.28	0	40	0	14.56	0	0	16.82
50	0	13.24	12	50	0	8.53	8	50	0	15.41	0	50	0	14.34	0	0	16.73
5	0	13.41	13	11	0	9.0	7	5	0	15.54	0	5	0	14.12	0	0	16.64
10	0	13.54	13	10	0	9.7	7	10	0	15.67	0	10	0	13.90	0	0	16.55
20	0	13.8	14	20	0	9.14	7	20	0	15.80	0	20	0	13.68	0	0	16.46
30	0	13.23	15	30	0	9.21	7	30	0	15.93	0	30	0	13.46	0	0	16.37
40	0	13.40	17	40	0	9.28	7	40	0	16.06	0	40	0	13.24	0	0	16.28
50	0	13.58	18	50	0	9.35	7	50	0	16.19	0	50	0	13.02	0	0	16.19
6	0	13.17	19	12	0	9.42	7	6	0	16.32	0	6	0	12.80	0	0	16.10

MOULMEIN. Deduced from the Observations 1880-84 (—0.96 applied to observation for chart datum. Dry Season only).

LOW WATER Approximate Interval = 37 <sup>h</sup>				HIGH WATER Approximate Interval = 40 <sup>h</sup>				LOW WATER Factor = -0.2				HIGH WATER Factor = +1.6				
Moons' Appl.	Transit at Greenwich	Time	diff.	Moons' Appl.	Transit at Greenwich	Time	diff.	Moons' Appl.	Transit at Greenwich	Height	diff.	Moons' Appl.	Transit at Greenwich	Height	diff.	
0	h m	0 47	6	0	h m	4 28	7	0	h m	2 79	1	0	h m	14 55	0	
10	0 53	+	10	10	4 35	+	6	10	2 80	+	1	10	2 22	-	2	
20	1 0	7	20	20	4 41	18	20	11 11	20	2 81	1	20	2 21	1	20	
30	1 7	7	30	30	4 48	17	30	11 28	30	2 82	1	30	2 19	2	30	
40	1 14	7	40	40	4 55	19	40	11 45	40	2 83	1	40	2 18	1	40	
50	1 21	7	50	50	5 2	18	50	0 16	50	2 83	0	50	2 16	2	50	
1	0 1 28	7	7	0 5 9	7	19	1	0 0 17	16	1	0	7	0 2 15	1	1	
10	1 35	7	10	5 16	7	19	10	0 32	15	10	2 82	0	10	2 15	0	
20	1 41	6	20	5 23	7	18	20	0 47	15	20	2 81	1	20	2 14	1	
30	1 48	7	30	5 30	7	17	30	1 14	14	30	2 80	1	30	2 13	1	
40	1 55	7	40	5 37	7	16	40	1 13	12	40	2 79	1	40	2 13	0	
50	2 2	7	50	5 45	8	15	50	1 24	11	50	2 78	1	50	2 13	0	
2	0 2 9	7	8	5 52	7	14	2	0 1 35	11	2	0	8	0 2 13	0	2	
10	2 16	7	10	6 0	8	14	10	1 45	10	10	2 75	1	10	2 14	1	
20	2 22	6	20	6 7	7	13	20	1 54	9	20	2 73	2	20	2 15	1	
30	2 29	7	30	6 15	8	12	30	2 1	8	30	2 71	2	30	2 17	2	
40	2 36	7	40	6 23	8	11	40	2 11	8	40	2 69	2	40	2 20	3	
50	2 43	7	50	6 32	9	11	50	2 19	8	50	2 67	2	50	2 23	3	
3	0 2 50	7	9	6 40	8	10	3	0 2 27	8	3	0	9	0 2 27	4	3	
10	2 57	7	10	6 49	9	10	10	2 35	8	10	2 61	3	10	2 31	4	
20	3 4	7	20	6 58	9	9	20	2 42	7	20	2 59	2	20	2 35	4	
30	3 11	7	30	7 7	9	9	30	2 49	7	30	2 56	3	30	2 39	4	
40	3 18	7	40	7 17	10	8	40	2 56	7	40	2 53	3	40	2 43	4	
50	3 26	8	50	7 27	10	8	50	3 2	6	50	2 51	2	50	2 47	4	
4	0 3 33	8	10	7 37	10	8	4	0 3 9	7	4	0	3	0 2 48	3	4	
10	3 41	8	10	7 48	11	8	10	3 16	7	10	2 46	2	10	2 55	4	
20	3 49	8	20	7 59	11	7	20	3 22	6	20	2 43	3	20	2 59	4	
30	3 57	8	30	8 11	12	7	30	3 29	7	30	2 41	2	30	2 62	3	
40	4 6	9	40	8 24	13	6	40	3 36	7	40	2 39	2	40	2 65	3	
50	4 15	9	50	8 38	14	6	50	3 42	6	50	2 37	2	50	2 67	2	
5	0 4 25	10	11	8 53	15	5	11	0 3 49	7	5	0	2 35	2	11	0 2 70	3
10	4 35	10	10	9 8	15	4	10	3 55	6	10	2 33	2	10	2 72	2	
20	4 46	11	20	9 24	16	3	20	4 2	7	20	2 31	2	20	2 74	1	
30	4 59	13	30	9 40	16	2	30	4 8	6	30	2 29	2	30	2 75	1	
40	5 13	14	40	9 57	17	1	40	4 15	7	40	2 27	2	40	2 77	2	
50	5 29	16	50	10 15	18	0	50	4 21	6	50	2 26	1	50	2 78	1	
6	0 5 46	17	12	10 34	19	0	12	0 4 28	7	6	0	2 24	2	12	0 2 79	1

DUBLAT.  
Freshets Correction (High Water Heights). Arguments—Date and Approximate Apparent Time of Moon's Transit.

Moon's Transit	h	m	sec	h	m	sec	h	m	sec	h	m	sec	h	m	sec	h	m	sec	h	m	sec	h	m	sec							
June 16	0	0	0	1	0	0	2	0	3	0	4	0	5	0	6	0	7	0	8	0	9	0	10	0	11	0	12	0			
19	+14			+16			+17		+18		+19		+19		+19		+19		+19		+19		+19		+12		+13		+14		
22	29			31			34		36		38		38		38		38		38		38		38		23		24		26	29	
25	42			45			48		50		52		52		52		52		52		52		52		31		31		35	38	42
28	55			60			65		70		73		73		73		73		73		73		73		42		42		45	49	53
July 1	+67			+74			+80		+86		+89		+86		+86		+86		+86		+86		+86		+51		+51		+54	+61	+67
4	81			88			95		101		108		101		101		95		88		81		75		61		64		68	72	81
7	93			101			109		117		125		117		117		109		93		86		82		74		74		78	82	93
10	106			115			123		131		138		131		131		123		106		97		93		84		84		88	93	106
13	116			127			136		146		152		146		146		136		116		107		93		93		93		98	103	116
16	127			138			148		156		166		160		160		148		127		116		103		103		103		107	112	127
19	136			148			159		171		182		171		171		159		136		127		114		114		114		118	120	136
22	145			158			169		182		194		182		182		169		145		136		122		122		122		128	133	145
25	152			166			178		191		204		191		191		178		152		140		134		134		134		138	140	152
28	159			174			186		200		213		200		200		186		159		146		140		140		140		142	146	159
31	165			179			192		207		221		207		207		192		165		153		145		145		145		148	153	165
Aug. 3	170			185			199		214		228		214		214		199		170		157		150		150		150		153	157	170
6	174			189			203		218		233		218		218		203		174		160		153		153		153		156	160	174
9	177			193			208		223		238		223		223		208		177		163		156		156		156		159	163	177
12	179			195			211		225		240		225		225		211		179		165		157		157		157		161	165	179
15	179			195			211		225		240		225		225		211		179		165		157		157		157		165	169	179
18	177			193			208		223		238		223		223		208		177		163		156		156		156		160	163	177
21	170			185			199		214		228		214		214		199		170		157		150		150		150		153	157	170
24	159			174			186		200		213		200		200		186		159		146		140		140		140		146	159	
27	145			158			169		182		194		182		182		169		145		133		128		128		128		133	145	
30	127			138			148		160		170		160		160		148		127		116		112		112		112		116	127	
Sept. 2	106			115			123		133		141		133		133		123		106		97		93		93		93		97	106	
5	81			88			95		101		108		101		101		95		81		75		72		72		72		75	81	
8	55			60			65		70		73		70		70		65		55		51		49		49		49		51	55	
11	20			26			31		36		38		36		36		31		20		26		25		25		25		26	29	
14	00			04			08		11		13		11		11		08		00		00		00		00		00		00	00	

Correction for time = — Correction for height. Example—August 15 and 31, 1860. — 2.40 feet and — 16in.









**KIDDERPORE.**  
**Freshets Correction (High Water Times). Arguments—Date and Approximate Apparent Time of Moon's Transit.**

Moon's Transit	0 0	0 30	1 0	1 30	2 0	2 30	3 0	3 30	4 0	4 30	5 0	5 30	6 0	6 30	7 0	7 30	8 0	8 30	9 0	9 30	10 0	10 30	11 0	11 30	12 0
June 16	m	m	m	m	m	m	m	m	m	m	m	m	m	m	m	m	m	m	m	m	m	m	m	m	m
19	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25
22	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27
25	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28
28	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29
July 1	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
4	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	1
10	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	1	2
13	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	1	2	3
16	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	1	2	3	4
19	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	1	2	3	4	5
22	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	1	2	3	4	5	6
25	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	1	2	3	4	5	6	7
28	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	1	2	3	4	5	6	7	8
Aug. 3	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	1	2	3	4	5	6	7	8	9
6	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	1	2	3	4	5	6	7	8	9	10
9	18	19	20	21	22	23	24	25	26	27	28	29	30	31	1	2	3	4	5	6	7	8	9	10	11
12	19	20	21	22	23	24	25	26	27	28	29	30	31	1	2	3	4	5	6	7	8	9	10	11	12
15	20	21	22	23	24	25	26	27	28	29	30	31	1	2	3	4	5	6	7	8	9	10	11	12	13
18	21	22	23	24	25	26	27	28	29	30	31	1	2	3	4	5	6	7	8	9	10	11	12	13	14
21	22	23	24	25	26	27	28	29	30	31	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
24	23	24	25	26	27	28	29	30	31	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
27	24	25	26	27	28	29	30	31	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
30	25	26	27	28	29	30	31	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Sept. 2	26	27	28	29	30	31	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
5	27	28	29	30	31	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
8	28	29	30	31	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
11	29	30	31	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22
14	30	31	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23



KIDDERPORE. Freshets Correction (High Water Heights). Argument—Date and Approximate Apparent Time of Moon's Transit.

Table with columns for Moon's Transit (Date and Time) and rows for Freshets Correction (High Water Heights) in feet. The table is organized by month: June 16, July 1, Aug. 8, and Sept. 5. Each row contains 12 columns of data representing different times of day (e.g., 19, 22, 25, 28, July 1, 4, 7, 10, 18, 16, 19, 22, 25, 28, Aug. 8, 15, 18, 21, 24, 27, 30, Sept. 5, 8, 11, 14).







### ELEPHANT POINT. Corrections to Times of Low Water (Freshets Period).

Moon's Transit	h	m	h	m	h	m	h	m	h	m	h	m	h	m	h	m	h	m	h	m	h	m	h	m	h	m	h	m	h	m	h	m	h	m	h	m																
	0	0	0	30	1	0	1	30	2	0	2	30	3	0	3	30	4	0	4	30	5	0	5	30	6	0	6	30	7	0	7	30	8	0	8	30	9	0	9	30	10	0	10	30	11	0	11	30	12	0		
June 16	m	o	m	o	m	o	m	o	m	o	m	o	m	o	m	o	m	o	m	o	m	o	m	o	m	o	m	o	m	o	m	o	m	o	m	o	m	o	m	o	m	o	m	o	m	o	m	o	m	o		
19	-	1	-	1	-	1	-	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	1	2	2	3	3	4	4	5	5	6	6	7	7	8	7	7	7	6	5	5	4	4	3	3	2	2	1	1	1
22		2		2		2		1	1		1		1		1		1		1		1		2		2		3		3		3		3		3		3		3		3		3		3		3		2	2	2	
25		3		3		2		2		1		1		1		1		2		2		2		2		3		4		4		5		5		5		5		4		4		4		3		3		3		3
28		4		4		3		2		2		2		2		2		2		2		3		4		4		5		6		7		7		8		7		7		6		5		5		4		4		4
July 1		5		5		4		3		2		2		2		2		2		3		4		4		6		7		7		9		9		10		9		8		7		7		6		6		5		
4		6		5		5		4		3		2		2		3		3		4		4		5		7		8		9		10		10		11		10		10		9		8		7		7		6		
7		7		6		5		4		3		3		3		3		4		4		5		6		8		10		11		12		12		13		12		12		11		10		9		8		7		
10		8		7		6		5		4		3		3		4		4		5		6		7		9		11		12		14		14		15		14		13		12		11		10		9		8		
13		9		8		7		5		4		3		3		4		5		6		7		8		10		12		13		15		15		16		15		14		13		12		11		10		9		
16		10		9		7		6		4		4		4		4		5		6		7		9		11		13		14		17		17		18		17		16		14		13		12		11		10		
19		11		9		8		6		5		4		5		5		6		6		8		9		12		14		15		18		18		19		18		17		15		14		12		12		11		
22		11		10		8		6		5		4		5		5		6		7		8		10		12		15		17		19		19		20		19		18		17		15		13		12		11		
25		12		10		9		7		5		4		5		5		6		7		9		10		14		16		17		20		20		21		20		19		17		16		14		14		12		
28		12		11		9		7		5		4		5		6		7		8		9		11		14		17		18		21		21		22		21		20		18		17		15		14		12		
31		13		11		9		7		6		5		6		6		7		8		10		11		15		18		19		22		22		23		22		21		19		18		15		15		13		
Aug. 3		13		11		10		8		6		5		6		6		8		8		10		11		15		18		19		22		22		24		22		21		19		18		16		15		13		
6		14		12		10		8		6		5		6		6		8		8		10		12		15		18		20		23		23		24		23		22		20		18		16		15		14		
9		14		12		10		8		6		5		6		7		8		8		10		12		15		18		20		23		23		25		23		22		20		18		16		15		14		
12		14		12		10		8		6		5		6		7		8		9		11		13		16		19		21		23		24		25		24		23		21		19		17		16		14		
15		14		12		10		8		6		5		6		7		8		9		11		13		16		19		21		23		24		25		24		23		21		19		17		16		14		
18		14		12		10		8		6		5		6		6		8		8		10		13		15		18		20		22		23		25		23		22		20		18		16		15		14		
21		13		11		10		8		6		5		6		6		8		8		9		12		15		18		19		21		22		24		22		21		19		18		16		15		13		
24		12		11		9		7		5		4		5		6		7		8		8		11		14		17		18		20		21		22		21		20		18		17		15		14		12		
27		11		10		8		6		5		4		5		5		6		7		7		10		12		15		17		18		19		20		19		18		17		15		13		12		11		
30		10		9		7		6		4		4		4		4		6		6		7		9		11		13		14		16		17		18		17		16		14		13		12		11		10		
Sept. 2		8		7		6		5		4		3		4		4		5		5		5		8		9		11		12		13		14		15		14		13		12		11		10		9		8		
5		6		5		5		4		3		2		3		3		4		4		4		6		7		8		9		10		10		11		10		10		9		8		7		7		6		
8		4		4		3		2		2		2		2		2		2		2		2		2		3		4		4		5		6		7		7		8		7		7		6		5		4		4
11		2		2		2		1		1		1		1		1		1		1		1		1		1		1		1		2		2		3		3		3		3		3		3		2		2		2
14		c		o		o		o		o		o		o		o		o		o		o		o		o		o		o		o		o		o		o		o		o		o		o		o		o		o









RANGOON.  
Corrections to Heights of High Water (Freshets Period).

Table with columns for Moon's Transit (h m s), June 10, 11, 12, 13, 14, 15, 16, 17, 18, 19, 20, 21, 22, 23, 24, 25, 26, 27, 28, 29, 30, and Sept. 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12. Each column contains a correction value in feet and inches (e.g., +1' 17", +0' 31").













**MOULMEIN.**  
Corrections to Times of High Water (Freshets Period).

Moon's Tribut	Corrections to Times of High Water (Freshets Period)											
	h m	a m	b m	h m	a m	b m	h m	a m	b m	h m	a m	b m
June 16	0 0	0 0	0 0	1 0	1 0	1 0	2 0	2 0	2 0	3 0	3 0	4 0
	0	0	0	0	0	0	0	0	0	0	0	0
June 19	1 1	1 1	1 1	1 1	1 1	1 1	2 1	2 1	2 1	3 1	3 1	4 1
	2	2	2	2	2	2	3	3	3	4	4	5
June 22	2 2	2 2	2 2	2 2	2 2	2 2	3 2	3 2	3 2	4 2	4 2	5 2
	5	5	5	5	5	5	6	6	6	7	7	8
June 25	3 3	3 3	3 3	3 3	3 3	3 3	4 3	4 3	4 3	5 3	5 3	6 3
	7	7	7	7	7	7	8	8	8	9	9	10
June 28	3 3	3 3	3 3	3 3	3 3	3 3	4 3	4 3	4 3	5 3	5 3	6 3
	9	9	9	9	9	9	10	10	10	11	11	12
July 1	4 4	4 4	4 4	4 4	4 4	4 4	5 4	5 4	5 4	6 4	6 4	7 4
	11	11	11	11	11	11	12	12	12	13	13	14
July 4	4 4	4 4	4 4	4 4	4 4	4 4	5 4	5 4	5 4	6 4	6 4	7 4
	14	14	14	14	14	14	15	15	15	16	16	17
July 7	4 4	4 4	4 4	4 4	4 4	4 4	5 4	5 4	5 4	6 4	6 4	7 4
	16	16	16	16	16	16	17	17	17	18	18	19
July 10	4 4	4 4	4 4	4 4	4 4	4 4	5 4	5 4	5 4	6 4	6 4	7 4
	18	18	18	18	18	18	19	19	19	20	20	21
July 13	4 4	4 4	4 4	4 4	4 4	4 4	5 4	5 4	5 4	6 4	6 4	7 4
	20	20	20	20	20	20	21	21	21	22	22	23
July 16	4 4	4 4	4 4	4 4	4 4	4 4	5 4	5 4	5 4	6 4	6 4	7 4
	21	21	21	21	21	21	22	22	22	23	23	24
July 19	4 4	4 4	4 4	4 4	4 4	4 4	5 4	5 4	5 4	6 4	6 4	7 4
	23	23	23	23	23	23	24	24	24	25	25	26
July 22	4 4	4 4	4 4	4 4	4 4	4 4	5 4	5 4	5 4	6 4	6 4	7 4
	24	24	24	24	24	24	25	25	25	26	26	27
July 25	4 4	4 4	4 4	4 4	4 4	4 4	5 4	5 4	5 4	6 4	6 4	7 4
	26	26	26	26	26	26	27	27	27	28	28	29
July 28	4 4	4 4	4 4	4 4	4 4	4 4	5 4	5 4	5 4	6 4	6 4	7 4
	27	27	27	27	27	27	28	28	28	29	29	30
Aug. 3	4 4	4 4	4 4	4 4	4 4	4 4	5 4	5 4	5 4	6 4	6 4	7 4
	28	28	28	28	28	28	29	29	29	30	30	31
Aug. 6	4 4	4 4	4 4	4 4	4 4	4 4	5 4	5 4	5 4	6 4	6 4	7 4
	29	29	29	29	29	29	30	30	30	31	31	32
Aug. 9	4 4	4 4	4 4	4 4	4 4	4 4	5 4	5 4	5 4	6 4	6 4	7 4
	30	30	30	30	30	30	31	31	31	32	32	33
Aug. 12	4 4	4 4	4 4	4 4	4 4	4 4	5 4	5 4	5 4	6 4	6 4	7 4
	30	30	30	30	30	30	31	31	31	32	32	33
Aug. 15	4 4	4 4	4 4	4 4	4 4	4 4	5 4	5 4	5 4	6 4	6 4	7 4
	30	30	30	30	30	30	31	31	31	32	32	33
Aug. 18	4 4	4 4	4 4	4 4	4 4	4 4	5 4	5 4	5 4	6 4	6 4	7 4
	30	30	30	30	30	30	31	31	31	32	32	33
Aug. 21	4 4	4 4	4 4	4 4	4 4	4 4	5 4	5 4	5 4	6 4	6 4	7 4
	30	30	30	30	30	30	31	31	31	32	32	33
Aug. 24	4 4	4 4	4 4	4 4	4 4	4 4	5 4	5 4	5 4	6 4	6 4	7 4
	30	30	30	30	30	30	31	31	31	32	32	33
Aug. 27	4 4	4 4	4 4	4 4	4 4	4 4	5 4	5 4	5 4	6 4	6 4	7 4
	30	30	30	30	30	30	31	31	31	32	32	33
Sept. 2	4 4	4 4	4 4	4 4	4 4	4 4	5 4	5 4	5 4	6 4	6 4	7 4
	30	30	30	30	30	30	31	31	31	32	32	33
Sept. 5	4 4	4 4	4 4	4 4	4 4	4 4	5 4	5 4	5 4	6 4	6 4	7 4
	30	30	30	30	30	30	31	31	31	32	32	33
Sept. 8	4 4	4 4	4 4	4 4	4 4	4 4	5 4	5 4	5 4	6 4	6 4	7 4
	30	30	30	30	30	30	31	31	31	32	32	33
Sept. 11	4 4	4 4	4 4	4 4	4 4	4 4	5 4	5 4	5 4	6 4	6 4	7 4
	30	30	30	30	30	30	31	31	31	32	32	33
Sept. 14	4 4	4 4	4 4	4 4	4 4	4 4	5 4	5 4	5 4	6 4	6 4	7 4
	30	30	30	30	30	30	31	31	31	32	32	33



Moulmein. Corrections to Heights of High Water (Freshets Period).

Table with columns for Moon's Transit, Date/Time, and 12 columns of 'feet' values with associated corrections. Rows include dates from June 19 to August 14, 1882.







**TIDAL OBSERVATIONS**

**PART II.**

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**HISTORY AND DESCRIPTION OF THE OBSERVATORIES,**

**RESULTS OF THE OBSERVATIONS,**

**AND**

**VALUES OF THE TIDAL CONSTANTS,**

**UP TO**

**1892.**

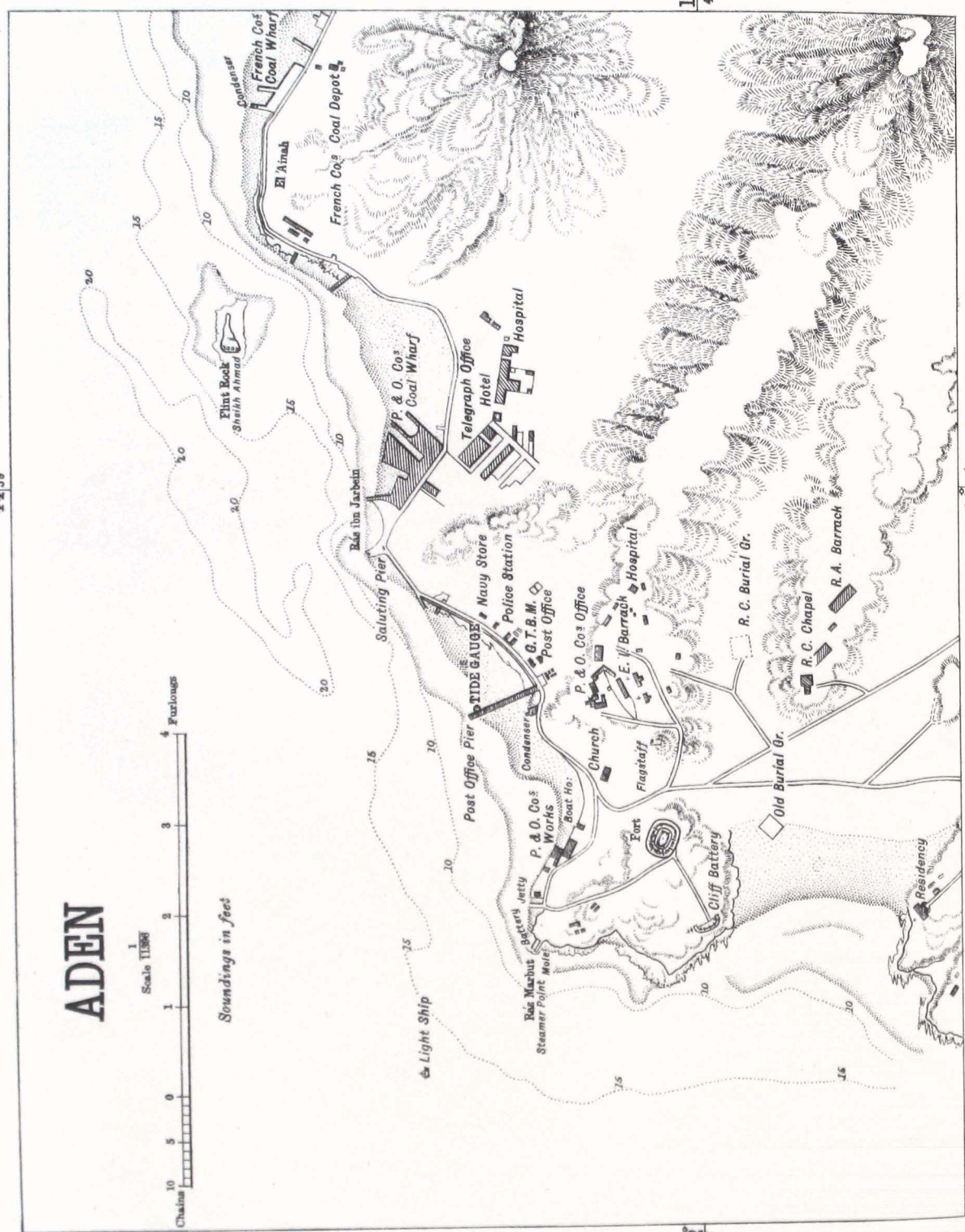
44 56

# ADEN

Scale 1:11300



*Soundings in feet*



12 47

12 47

44 59

## A D E N .

*(Tidal Observatory, Lat. 12° 47' N., Long. 44° 59' E.)*

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The tidal observatory at Aden, on the south coast of Arabia, is one of the permanent observatories, and is situated in the angle formed by the T-head of the end of the Post Office pier, in the position shown in the accompanying chart. It is a wooden structure built on piles driven eight or nine feet into the bed of the sea. The cylinder is circular and of wrought iron, about twenty-two inches in internal diameter and sixteen feet long, closed at the bottom and resting on the bed of the sea, there being never less than three feet of water above the bottom even at the lowest tides.

The working scale of the tide-gauge is one-half.

Registrations were commenced on the 3rd March, 1879, and were very satisfactory up to the 17th March, 1890. From the latter date to the 31st May, 1890, when a new gauge was set up, the observations were rendered untrustworthy through the negligence of the clerk. With this exception, the observations have proved satisfactory. When the gauge was originally set up there was a short communication pipe, having two bends, and a "rose" at its end, attached to the cylinder near the bottom. The rose was fifteen inches above the bed of the sea. At the inspection in August, 1886, this arrangement was found to have disappeared without entailing any bad consequences; and it has not been necessary to renew it. Prior to the commencement of these registrations a small gauge was at work for a considerable time, but its registrations were found to be useless.

A peculiarity of the Aden tides is, that at the times of the moon's quarters there is frequently only one high and one low water in the twenty-four hours.

The disturbances of the surface of the ocean, caused by the Krakatoa volcanic eruptions, were recorded at this the most remote Indian Tidal Station by the self-registering tide-gauge on the 27th August, 1883.

Barometrical and anemometrical observations were carried on simultaneously with the tidal observations. The barometer was placed in the observatory, but as that site was not suitable for the anemometer, the latter instrument was placed on the Flag-staff hill, about a quarter of a mile inland.

The bench-mark of reference is a large stone in the north-east corner of the Post Office verandah pavement, having its face flush with the pavement, and the letters <sup>G.T.S.</sup>  $\square$ A engraved on it. It is 13·489 feet above the zero of the gauge.  
B.M.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = VII<sup>h</sup> 54<sup>m</sup>.

The highest high water recorded was 10·1 feet above the zero of the gauge, and occurred in April, 1879.

The lowest low water recorded was 0·1 of a foot above the zero of the gauge, and occurred in November, 1879.

In 1879-80 the mean range of largest ordinary springs was found to be 6·7 feet.

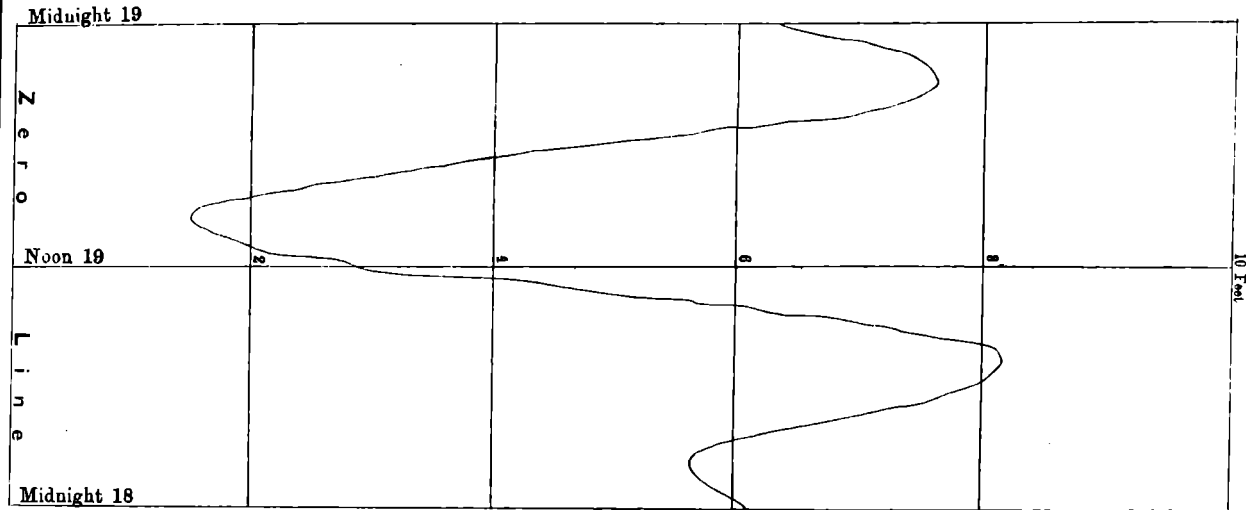
The height of mean-sea-level above the zero of the gauge had the following values :—

1879-80	...	...	...	5·768 feet.
1880-81	...	...	...	5·784 „
1881-82	...	...	...	5·814 „
1882-83	...	...	...	5·754 „
1883-84	...	...	...	5·800 „
1884-85	...	...	...	5·849 „
1885-86	...	...	...	5·883 „
1886-87	...	...	...	5·902 „
1887-88	...	...	...	5·822 „
1888-89	...	...	...	5·857 „
1889-90	...	...	...	5·835 „
1890-91	...	...	...	5·780 „
1891-92	...	...	...	5·845 „

# TIDAL CURVES

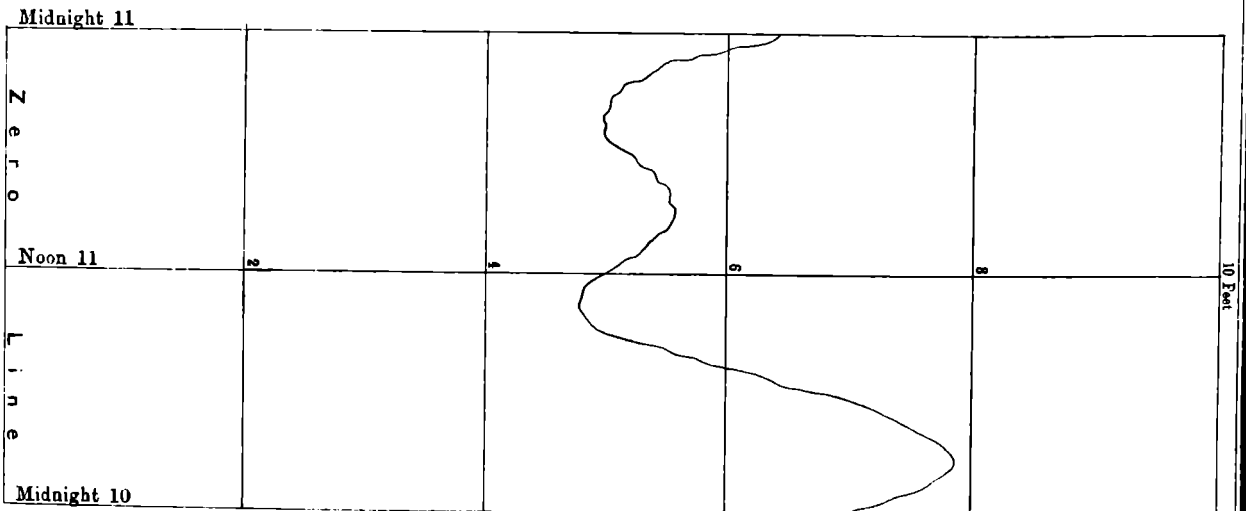
at  
ADEN

Spring Tide — 19th December 1888



Full Moon — 18th December 1888

Neap Tide — 11th December 1888



First Quarter — 10th December 1888

*Photostereographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun June 1899.*

*Values of H's at Aden.*

TIDE	H						TIDE
	1879-80	1880-81	1881-82	1882-83	1883-84	1884-85	
	Feet	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0.073	0.117	0.093	0.077	0.094	0.074	S <sub>1</sub>
S <sub>2</sub>	.693	.693	.704	.699	.702	.700	S <sub>2</sub>
S <sub>4</sub>	.006	.005	.006	.005	.004	.004	S <sub>4</sub>
S <sub>6</sub>	.005	.004	.004	.004	.006	.006	S <sub>6</sub>
S <sub>8</sub>	.001	.001	.001	.001	.001	.001	S <sub>8</sub>
M <sub>1</sub>	.033	.052	.053	.048	.066	.084	M <sub>1</sub>
M <sub>2</sub>	1.578	1.558	1.569	1.567	1.588	1.581	M <sub>2</sub>
M <sub>3</sub>	0.019	0.020	0.018	0.016	0.019	0.014	M <sub>3</sub>
M <sub>4</sub>	.011	.006	.007	.003	.004	.003	M <sub>4</sub>
M <sub>6</sub>	.006	.004	.004	.007	.006	.005	M <sub>6</sub>
M <sub>8</sub>	.003	.001	.004	.002	.003	.001	M <sub>8</sub>
O	.657	.658	.646	.651	.660	.670	O
K <sub>1</sub>	1.295	1.297	1.299	1.305	1.312	1.303	K <sub>1</sub>
K <sub>2</sub>	0.218	0.197	0.188	0.202	0.215	0.206	K <sub>2</sub>
P	.389	.375	.389	.399	.384	.399	P
J	.118	.110	.083	.100	.131	.099	J
Q	.174	.157	.134	.139	.158	.144	Q
L	.023	.063	.033	.065	.028	.047	L
N	.443	.436	.421	.409	.423	.434	N
λ	.018	.020	.038	.026	.015	.037	λ
ν	.157	.132	.059	.048	.139	.156	ν
μ	.086	.082	.072	.058	.081	.083	μ
R	...	.006	...	.003	...	.019	R
T	...	.057	...	.042	...	.081	T
MS	.007	.020	.009	.011	.012	.014	MS
2SM	.022	.021	.021	.026	.022	.021	2SM
2N	.084	.101	.079	.058	.087	.107	2N
M <sub>2</sub> N	.035	.020	.077	.037	.044	.036	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	.031	.027	.011	.023	.034	.033	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	.009	.006	.009	.011	.007	.006	2M <sub>2</sub> K <sub>1</sub>
Mm	.035	.076	.025	.033	.015	.039	Mm
Mf	.052	.039	.045	.044	.065	.012	Mf
MSf	.014	.015	.016	.010	.012	.019	MSf
Sa	.404	.402	.353	.399	.363	.367	Sa
Ssa	.110	.109	.093	.069	.114	.102	Ssa

## TIDAL OBSERVATIONS.

*Values of H's at Aden—(Continued).*

TIDE	H							TIDE
	1885-86	1886-87	1887-88	1888-89	1889-90	1890-91	1891-92	
	Feet	Feet	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0·077	0·070	0·095	0·090	0·101	0·080	0·101	S <sub>1</sub>
S <sub>2</sub>	·692	·700	·700	·706	·682	·652	·656	S <sub>2</sub>
S <sub>4</sub>	·005	·004	·005	·004	·002	·006	·006	S <sub>4</sub>
S <sub>6</sub>	·005	·006	·006	·006	·008	·006	·005	S <sub>6</sub>
S <sub>8</sub>	·002	·001	·002	·001	·001	·002	·000	S <sub>8</sub>
M <sub>1</sub>	·015	·036	·030	·035	·034	·079	·050	M <sub>1</sub>
M <sub>2</sub>	1·573	1·570	1·594	1·579	1·566	1·564	1·576	M <sub>2</sub>
M <sub>3</sub>	0·021	0·019	0·018	0·021	0·019	0·019	0·017	M <sub>3</sub>
M <sub>4</sub>	·008	·006	·008	·004	·004	·008	·005	M <sub>4</sub>
M <sub>6</sub>	·003	·005	·006	·006	·002	·006	·002	M <sub>6</sub>
M <sub>8</sub>	·002	·003	·001	·002	·004	·003	·001	M <sub>8</sub>
O	·669	·666	·666	·660	·654	·642	·652	O
K <sub>1</sub>	1·307	1·301	1·307	1·306	1·311	1·289	1·309	K <sub>1</sub>
K <sub>2</sub>	0·195	0·213	0·206	0·194	0·206	0·233	0·192	K <sub>2</sub>
P	·409	·391	·388	·401	·413	·343	·373	P
J	·067	·087	·119	·102	·083	·143	·135	J
Q	·136	·147	·169	·162	·145	·177	·155	Q
L	·034	·048	·026	·045	·025	·026	·059	L
N	·444	·428	·446	·452	·426	·451	·411	N
λ	·033	...	...	...	...	...	...	λ
ν	·090	·007	·098	·158	·128	·065	·061	ν
μ	·080	·056	·074	·075	·101	·064	·080	μ
R	...	...	...	...	...	...	...	R
T	...	·027	·035	·088	·067	·008	·055	T
MS	·006	·011	·009	·017	·014	·013	·016	MS
2SM	·019	·024	·020	·018	·025	·037	·024	2SM
2N	·091	·067	·088	·089	·095	·080	·074	2N
M <sub>2</sub> N	·065	·031	·034	·043	·056	·028	·024	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	·011	·021	·033	·027	·009	·028	·032	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	·003	·001	·006	·007	·012	·014	·008	2M <sub>2</sub> K <sub>1</sub>
Mm	·016	·037	·050	·055	·029	·018	·031	Mm
Mf	·038	·065	·028	·046	·043	·045	·047	Mf
MSf	·013	·015	·018	·010	·024	·002	·014	MSf
Sa	·448	·403	·416	·296	·381	·424	·346	Sa
Ssa	·183	·166	·152	·116	·083	·161	·141	Ssa

*Values of  $\kappa$ 's at Aden.*

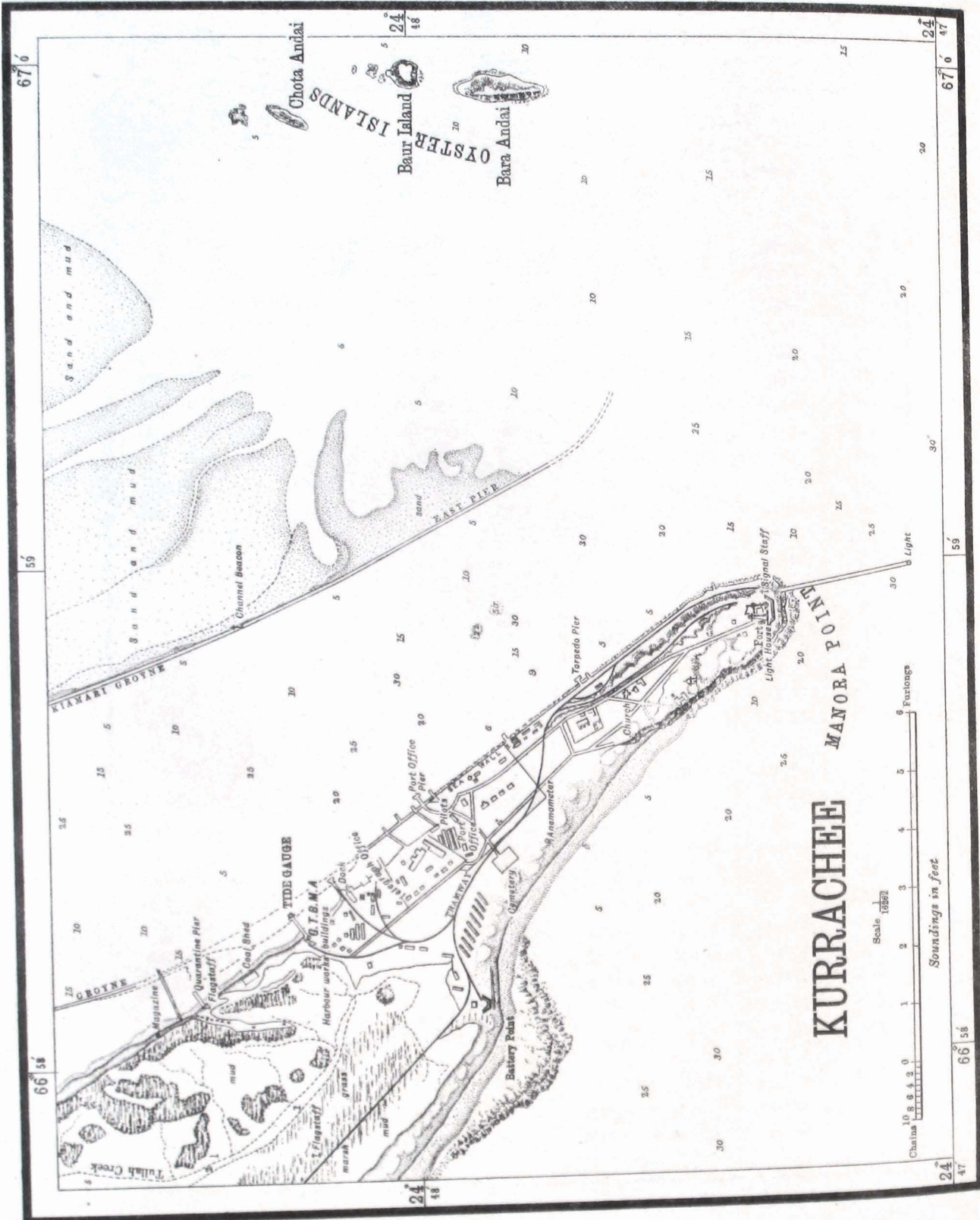
TIDE	$\kappa$						TIDE
	1879-80	1880-81	1881-82	1882-83	1883-84	1884-85	
	°	°	°	°	°	°	
S <sub>1</sub>	167.95	151.17	161.49	165.96	165.00	173.69	S <sub>1</sub>
S <sub>2</sub>	248.43	251.51	246.32	247.25	244.77	244.76	S <sub>2</sub>
S <sub>4</sub>	263.00	256.55	274.76	289.80	244.06	6.95	S <sub>4</sub>
S <sub>6</sub>	217.78	190.71	209.58	185.44	185.01	188.43	S <sub>6</sub>
S <sub>8</sub>	212.01	238.00	325.01	260.54	221.63	265.60	S <sub>8</sub>
M <sub>1</sub>	29.53	12.18	355.47	44.91	30.54	35.62	M <sub>1</sub>
M <sub>2</sub>	228.41	232.03	227.53	227.33	224.80	224.98	M <sub>2</sub>
M <sub>3</sub>	219.59	214.88	201.36	201.77	204.92	212.12	M <sub>3</sub>
M <sub>4</sub>	322.03	333.52	317.91	280.95	346.08	325.77	M <sub>4</sub>
M <sub>6</sub>	343.05	279.82	25.74	355.00	358.12	317.12	M <sub>6</sub>
M <sub>8</sub>	87.29	48.55	332.61	65.39	146.48	84.26	M <sub>8</sub>
O	38.44	39.87	37.94	37.54	37.56	37.04	O
K <sub>1</sub>	36.34	38.10	35.58	35.80	34.47	34.24	K <sub>1</sub>
K <sub>2</sub>	245.03	243.79	242.11	246.15	233.71	233.53	K <sub>2</sub>
P	31.19	35.47	33.45	31.44	30.81	31.75	P
J	48.56	70.31	53.24	35.32	39.41	57.30	J
Q	39.64	37.98	41.55	47.91	39.63	29.14	Q
L	259.45	230.25	209.23	222.81	194.11	223.65	L
N	222.92	229.98	223.71	222.03	217.27	217.09	N
$\lambda$	122.72	301.16	210.44	155.15	135.12	258.74	$\lambda$
$\nu$	241.49	200.36	169.87	292.80	254.24	213.74	$\nu$
$\mu$	191.74	203.97	182.34	204.45	193.20	192.91	$\mu$
R	...	63.81	...	355.89	...	242.44	R
T	...	286.13	...	194.49	...	275.15	T
MS	136.41	166.88	166.20	167.05	138.22	131.37	MS
2SM	106.46	100.58	113.80	113.66	106.56	107.69	2SM
2N	195.92	195.96	203.92	180.93	188.17	176.75	2N
M <sub>2</sub> N	55.99	335.56	19.90	59.03	71.77	334.74	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	339.10	57.39	125.52	285.53	337.56	43.14	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	64.28	43.88	6.97	344.82	308.51	282.26	2M <sub>2</sub> K <sub>1</sub>
Mm	4.62	347.81	324.13	17.90	57.50	53.33	Mm
Mf	14.44	30.38	25.83	53.22	15.75	35.75	Mf
MSf	40.02	295.48	98.32	209.21	231.08	264.87	MSf
Sa	2.72	358.03	1.62	346.98	346.01	356.05	Sa
Ssa	94.16	160.57	150.93	98.61	122.51	158.75	Ssa



## TIDAL OBSERVATIONS.

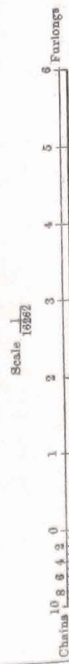
*Values of  $\kappa$ 's at Aden—(Continued).*

TIDE	$\kappa$							TIDE
	1885-86	1886-87	1887-88	1888-89	1889-90	1890-91	1891-92	
	°	°	°	°	°	°	°	
S <sub>1</sub>	162.20	170.58	169.20	173.82	173.08	181.51	169.91	S <sub>1</sub>
S <sub>2</sub>	245.33	246.98	245.89	244.89	243.39	242.60	244.36	S <sub>2</sub>
S <sub>4</sub>	323.62	318.24	326.63	311.50	281.31	278.26	245.56	S <sub>4</sub>
S <sub>6</sub>	220.86	214.19	208.86	194.28	201.40	193.57	193.17	S <sub>6</sub>
S <sub>8</sub>	334.98	340.02	341.57	50.19	323.13	135.00	161.57	S <sub>8</sub>
M <sub>1</sub>	58.21	97.46	66.27	357.75	267.29	52.96	36.20	M <sub>1</sub>
M <sub>2</sub>	225.76	226.71	225.89	225.54	223.58	224.68	225.79	M <sub>2</sub>
M <sub>3</sub>	225.63	219.24	218.63	209.11	181.48	209.19	202.52	M <sub>3</sub>
M <sub>4</sub>	338.84	331.95	340.35	309.55	308.40	238.87	320.25	M <sub>4</sub>
M <sub>6</sub>	14.06	350.46	8.62	326.07	300.79	319.64	33.44	M <sub>6</sub>
M <sub>8</sub>	20.82	114.46	123.57	39.02	51.28	210.47	244.04	M <sub>8</sub>
O	36.93	36.75	36.55	36.74	35.36	35.81	36.61	O
K <sub>1</sub>	35.00	35.62	34.88	34.62	33.63	34.00	33.88	K <sub>1</sub>
K <sub>2</sub>	245.84	244.04	237.64	238.38	238.53	235.93	235.26	K <sub>2</sub>
P	31.64	31.11	32.15	32.39	29.95	25.44	30.20	P
J	44.53	28.15	44.93	68.78	50.81	21.29	41.48	J
Q	34.55	43.04	35.86	32.10	39.91	52.92	43.56	Q
L	196.90	229.34	185.24	232.68	228.88	315.91	193.27	L
N	219.56	221.25	219.07	220.86	219.17	223.48	218.76	N
$\lambda$	200.60	...	...	...	...	...	...	$\lambda$
$\nu$	179.76	235.17	274.84	232.09	192.56	154.97	281.89	$\nu$
$\mu$	180.00	194.49	191.68	193.98	177.12	188.56	196.24	$\mu$
R	...	...	...	...	...	...	...	R
T	...	173.99	321.19	268.47	222.90	108.51	309.50	T
MS	173.08	146.30	129.14	142.32	149.12	143.26	179.83	MS
2SM	109.08	109.23	99.75	115.14	92.14	72.86	96.77	2SM
2N	198.94	193.88	195.68	178.28	197.27	194.69	194.28	2N
M <sub>2</sub> N	37.16	50.28	87.31	341.48	55.03	102.66	94.59	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	135.73	267.85	336.41	47.81	138.27	279.43	340.12	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	321.94	105.73	73.31	13.02	5.96	344.11	338.15	2M <sub>2</sub> K <sub>1</sub>
Mm	1.28	70.41	29.60	11.99	354.74	29.95	6.36	Mm
Mf	14.40	10.07	342.31	19.01	12.45	341.79	351.57	Mf
MSf	189.36	110.27	84.87	90.82	222.95	186.11	295.77	MSf
Sa	3.41	11.16	345.29	357.53	355.76	355.07	352.31	Sa
Ssa	144.18	146.86	144.10	130.16	117.96	105.97	97.08	Ssa



# KURRACHEE

## MANORA POINT



Soundings in feet

## KURRACHEE.

(*Tidal Observatory, Lat. 24° 48' N., Long. 66° 58' E.*)

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The tidal observatory at Kurrachee on the coast of Sind is one of the permanent observatories, and is situated alongside the end of the 'Tipping pier' on the Manora side of the Harbour, in the position shown on the accompanying chart. It is a substantial, isolated wooden structure, built on piles driven from eight to twelve feet into the ground. The cylinder is an iron screw pile of about two feet four inches internal diameter and seventeen feet six inches long, driven about two feet into the ground, and firmly braced to the observatory joists; the intention being that there should be about one foot of the cylinder above the highest tides, and about four feet of water within it at the lowest tides. The communication is by a hole one inch in diameter, drilled through the cylinder at a depth of fifteen feet eight inches below the top flange.

The working scale of the tide-gauge is one-third.

Registrations were commenced on the 1st January, 1881, and have been highly satisfactory, though occasionally the curves have slight imperfections due to shell fish blocking the communication; and in 1892 silt accumulated to such an extent that extreme high and low tides were not properly indicated, owing to the float at extreme low water and the counterpoise at extreme high water resting on the accumulation, which was removed in January, 1893. Prior to the commencement of these registrations, a small self-registering tide-gauge was at work between 1868 and 1880 in connection with the Kurrachee Harbour Works, and its observations have been utilised together with those of the larger instrument. The disturbances of the surface of the ocean, caused by the Krakatoa volcanic eruptions, were recorded at this tidal station by the self-registering tide-gauge on the 27th August, 1883.

Barometrical and anemometrical observations were carried on simultaneously with the tidal observations.

The barometer was placed in the observatory, and the anemometer fixed to the exterior of the same building but its use was discontinued as that site was found to be inferior to that of the Port-Trust Anemometer on a neighbouring hillock, and the observations of the latter instrument have been accepted since December, 1881.

The bench-mark of reference is a stone, about half a furlong S.W. of the observatory, marked <sup>G.T.S.</sup>  $\square \Delta$  .  
It is 16·139 feet above the zero of the gauge. <sub>B.M.</sub>

The establishment of the Port, calculated according to the method employed by the Marine Survey of India =  $X^h 19^m$ .

The highest high water recorded was 13·4 feet above the zero of the gauge and occurred in June, 1885.

The lowest low water recorded was 0·4 foot above the zero of the gauge and occurred in November, 1879.

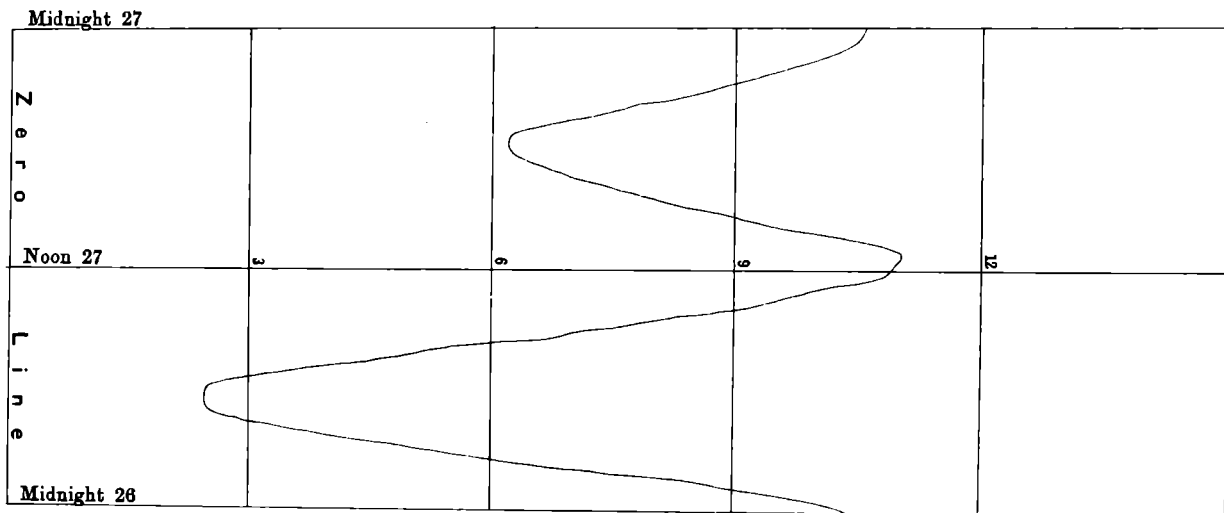
In 1890 the mean range of largest ordinary springs was found to be 9·3 feet.

The height of mean-sea-level above the zero of the gauge had the following values:—

<i>By small gauge.</i>				<i>By large gauge.</i>			
1868-69	...	...	7·149 feet.	1881-82	...	...	7·179 feet.
1869-70	...	...	·291 „	1882-83	...	...	·060 „
1870-71	...	...	·264 „	1883-84	...	...	·192 „
1871-72	...	...	·107 „	1884-85	...	...	·198 „
1872-73	...	...	·051 „	1885-86	...	...	·206 „
1873-74	...	...	·079 „	1886-87	...	...	·225 „
1874-75	...	...	·152 „	1887-88	...	...	·152 „
1875-76	...	...	·153 „	1888-89	...	...	·133 „
1876-77	...	...	·134 „	1889-90	...	...	·155 „
1877-78	...	...	·207 „	1890-91	...	...	·143 „
1878-79	...	...	·331 „	1891-92	...	...	·114 „
1879-80	...	...	·308 „				
1880-81	...	...	·267 „				

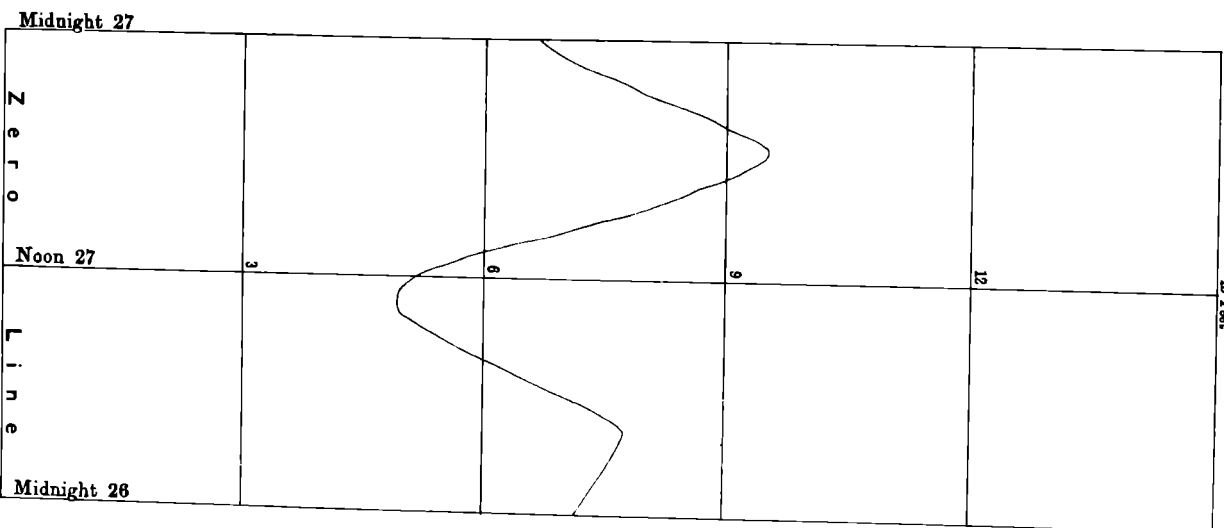
TIDAL CURVES  
at  
KURRACHEE

Spring Tide — 27th April 1891



Full Moon — 24th April 1891

Neap Tide — 17th April 1891



First Quarter — 16th April 1891

*Photoincographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun, July 1899.*

*Values of H's at Kurrachee.*

TIDE	H						TIDE
	1868-69	1869-70	1870-71	1871-72	1872-73	1873-74	
	Feet	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0·072	0·071	0·075	0·083	0·108	0·083	S <sub>1</sub>
S <sub>2</sub>	·932	·943	·923	·951	·952	·943	S <sub>2</sub>
S <sub>4</sub>	...	...	·014	·013	·008	·010	S <sub>4</sub>
S <sub>6</sub>	...	...	...	·004	·012	·004	S <sub>6</sub>
S <sub>8</sub>	...	...	...	...	...	·000	S <sub>8</sub>
M <sub>1</sub>	·013	...	·030	·063	·040	·038	M <sub>1</sub>
M <sub>2</sub>	2·511	2·447	2·450	2·492	2·476	2·471	M <sub>2</sub>
M <sub>3</sub>	0·042	0·037	0·048	0·048	0·037	0·030	M <sub>3</sub>
M <sub>4</sub>	·016	·027	·024	·029	·020	·022	M <sub>4</sub>
M <sub>6</sub>	·040	·046	·044	·045	·046	·048	M <sub>6</sub>
M <sub>8</sub>	...	...	...	·006	·006	·003	M <sub>8</sub>
O	·662	·645	·629	·636	·632	·645	O
K <sub>1</sub>	1·278	1·257	1·255	1·279	1·275	1·269	K <sub>1</sub>
K <sub>2</sub>	0·299	0·273	0·260	0·293	0·292	0·274	K <sub>2</sub>
P	·376	·385	·375	·360	·368	·393	P
J	·091	·046	·070	·107	·104	·059	J
Q	·129	·120	·138	·146	·129	·119	Q
L	·079	·047	·089	·043	·137	·084	L
N	·604	·587	·572	·650	·605	·587	N
λ	·059	·037	·043	·084	·076	·041	λ
ν	·190	·081	·080	·143	·191	·116	ν
μ	·066	·032	·070	·062	·055	·055	μ
R	...	·035	...	·027	...	·021	R
T	...	·111	...	·058	...	·012	T
MS	·017	·024	·031	·020	...	·023	MS
2SM	...	...	...	...	...	·007	2SM
2N	...	...	...	...	...	...	2N
M <sub>2</sub> N	...	...	...	...	...	...	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	...	...	...	...	...	...	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	...	...	...	...	...	...	2M <sub>2</sub> K <sub>1</sub>
Mm	·069	·040	·031	...	...	·055	Mm
Mf	·053	·078	·037	...	...	·012	Mf
MSf	·009	·074	·057	...	...	·042	MSf
Sa	·115	·179	·162	...	...	·250	Sa
Ssa	·198	·059	·062	...	...	·211	Ssa

## TIDAL OBSERVATIONS.

*Values of H's at Kurrachee—(Continued).*

TIDE	H						TIDE
	1874-75	1875-76	1876-77	1877-78	1878-79	1879-80	
	Feet	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0.076	0.079	0.087	0.088	0.044	0.086	S <sub>1</sub>
S <sub>2</sub>	.949	.953	.936	.961	.922	.957	S <sub>2</sub>
S <sub>4</sub>	.008	.008	.012	.010	.009	.008	S <sub>4</sub>
S <sub>6</sub>	.007	.009	.006	.005	.008	.006	S <sub>6</sub>
S <sub>8</sub>	.003	.002	.001	.002	.001	.002	S <sub>8</sub>
M <sub>1</sub>	.055	.081	.015	.013	.035	.060	M <sub>1</sub>
M <sub>2</sub>	2.517	2.550	2.474	2.468	2.521	2.555	M <sub>2</sub>
M <sub>3</sub>	0.026	0.037	0.037	0.055	0.048	0.042	M <sub>3</sub>
M <sub>4</sub>	.020	.025	.019	.024	.031	.027	M <sub>4</sub>
M <sub>6</sub>	.056	.055	.049	.053	.051	.055	M <sub>6</sub>
M <sub>8</sub>	.006	.006	.006	.006	.004	.003	M <sub>8</sub>
O	.647	.649	.646	.654	.677	.654	O
K <sub>1</sub>	1.292	1.296	1.263	1.278	1.314	1.301	K <sub>1</sub>
K <sub>3</sub>	0.247	0.261	0.276	0.260	0.240	0.284	K <sub>3</sub>
P	.386	.367	.368	.423	.440	.396	P
J	.088	.104	.077	.025	.084	.102	J
Q	.123	.136	.124	.110	.150	.154	Q
L	.088	.042	.085	.099	.054	.066	L
N	.560	.602	.606	.556	.667	.597	N
λ	.022	.009	.040	.082	.063	.019	λ
ν	.023	.154	.207	.218	.127	.089	ν
μ	.056	.070	.068	.113	.041	.077	μ
R	...	...	.008	...	.069	...	R
T	...	...	.122	...	.059	...	T
MS	.021	.031	.034	.030	.033	.031	MS
2SM	.018	.025	.012	.026	.019	.018	2SM
2N	...	...	...	...	...	...	2N
M <sub>2</sub> N	...	...	...	...	...	...	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	...	...	...	...	...	...	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	...	...	...	...	...	...	2M <sub>2</sub> K <sub>1</sub>
Mm	.064	.067	.097	.124	...	.040	Mm
Mf	.038	.010	.032	.047	...	.030	Mf
MSf	.040	.015	.045	.038	...	.030	MSf
Sa	.149	.086	.197	.170	...	.042	Sa
Ssa	.172	.173	.145	.087	...	.165	Ssa

*Values of H's at Kurrachee—(Continued).*

TIDE	H						TIDE
	1880-81	1881-82	1882-83	1883-84	1884-85	1885-86	
	Feet	Feet	Feet	Foot	Feet	Feet	
S <sub>1</sub>	0·135	0·076	0·066	0·074	0·055	0·072	S <sub>1</sub>
S <sub>2</sub>	·969	·960	·962	·952	·963	·950	S <sub>2</sub>
S <sub>4</sub>	·006	·012	·008	·010	·011	·010	S <sub>4</sub>
S <sub>6</sub>	·006	·008	·006	·006	·005	·006	S <sub>6</sub>
S <sub>8</sub>	·001	·000	·001	·002	·001	·001	S <sub>8</sub>
M <sub>1</sub>	·059	·048	·062	·081	·042	·037	M <sub>1</sub>
M <sub>2</sub>	2·536	2·541	2·558	2·566	2·546	2·552	M <sub>2</sub>
M <sub>3</sub>	0·039	0·034	0·030	0·029	0·027	0·036	M <sub>3</sub>
M <sub>4</sub>	·026	·027	·023	·033	·029	·029	M <sub>4</sub>
M <sub>6</sub>	·052	·049	·044	·050	·045	·053	M <sub>6</sub>
M <sub>8</sub>	·002	·009	·002	·005	·001	·005	M <sub>8</sub>
O	·632	·654	·645	·662	·666	·663	O
K <sub>1</sub>	1·246	1·295	1·310	1·301	1·300	1·305	K <sub>1</sub>
K <sub>2</sub>	0·415	0·269	0·234	0·304	0·308	0·269	K <sub>2</sub>
P	·266	·396	·396	·392	·395	·407	P
J	·066	·063	·099	·111	·071	·040	J
Q	·104	·124	·132	·133	·111	·125	Q
L	·123	·096	·076	·053	·076	·075	L
N	·581	·631	·594	·588	·596	·623	N
λ	·020	·029	·001	·006	·065	·066	λ
ν	·169	·211	·125	·028	·179	·208	ν
μ	·037	·081	·039	·064	·041	·084	μ
R	·040	...	·009	...	·019	...	R
T	·094	...	·021	...	·126	...	T
MS	·028	·030	·024	·032	·025	·035	MS
2SM	·031	·030	·021	·028	·017	·020	2SM
2N	...	·107	·064	·110	·084	·109	2N
M <sub>2</sub> N	...	·057	·081	·040	·067	·099	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	...	·035	·061	·068	·020	·024	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	...	·016	·025	·028	·023	·019	2M <sub>2</sub> K <sub>1</sub>
Mm	·036	·055	·040	·022	·027	·064	Mm
Mf	·020	·034	·006	·061	·058	·076	Mf
MSf	·018	·043	·023	·012	·037	·064	MSf
Sa	·102	·100	·099	·089	·139	·224	Sa
Ssa	·139	·116	·098	·189	·137	·109	Ssa



## TIDAL OBSERVATIONS.

*Values of H's at Kurrachee—(Continued).*

TIDE	H						TIDE
	1886-87	1887-88	1888-89	1889-90	1890-91	1891-92	
	Feet	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0.077	0.085	0.079	0.087	0.095	0.093	S <sub>1</sub>
S <sub>2</sub>	.972	.964	.966	.963	.946	.945	S <sub>2</sub>
S <sub>4</sub>	.008	.009	.011	.013	.010	.009	S <sub>4</sub>
S <sub>6</sub>	.010	.006	.007	.006	.007	.008	S <sub>6</sub>
S <sub>8</sub>	.002	.000	.001	.001	.002	.001	S <sub>8</sub>
M <sub>1</sub>	.046	.031	.008	.011	.069	.053	M <sub>1</sub>
M <sub>2</sub>	2.564	2.586	2.559	2.554	2.580	2.615	M <sub>2</sub>
M <sub>3</sub>	0.047	0.053	0.050	0.044	0.035	0.027	M <sub>3</sub>
M <sub>4</sub>	.037	.032	.033	.033	.038	.034	M <sub>4</sub>
M <sub>6</sub>	.044	.048	.046	.046	.043	.050	M <sub>6</sub>
M <sub>8</sub>	.003	.006	.002	.001	.006	.008	M <sub>8</sub>
O	.671	.671	.663	.657	.658	.655	O
K <sub>1</sub>	1.310	1.307	1.298	1.302	1.311	1.317	K <sub>1</sub>
K <sub>2</sub>	0.262	0.297	0.296	0.258	0.277	0.281	K <sub>2</sub>
P	.382	.377	.387	.402	.371	.373	P
J	.084	.101	.079	.057	.100	.119	J
Q	.148	.151	.122	.130	.147	.132	Q
L	.072	.086	.084	.088	.089	.141	L
N	.613	.618	.598	.613	.622	.593	N
λ	...	...	...	...	...	...	λ
ν	.171	.030	.115	.207	.206	.097	ν
μ	.045	.070	.045	.078	.060	.075	μ
R	...	...	...	...	...	...	R
T	.036	.117	.133	.048	.053	.108	T
MS	.026	.037	.040	.048	.033	.042	MS
2SM	.025	.016	.020	.026	.024	.014	2SM
2N	.075	.108	.066	.109	.098	.091	2N
M <sub>2</sub> N	.081	.067	.069	.099	.070	.069	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	.066	.065	.008	.046	.065	.053	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	.015	.005	.011	.023	.027	.027	2M <sub>2</sub> K <sub>1</sub>
Mm	.016	.071	.014	.060	.073	.058	Mm
Mf	.052	.050	.008	.039	.012	.004	Mf
MSf	.004	.050	.012	.029	.023	.045	MSf
Sa	.182	.092	.090	.087	.171	.070	Sa
Ssa	.253	.198	.169	.177	.227	.086	Ssa

*Values of  $\kappa$ 's at Kurrachee.*

TIDE	$\kappa$						TIDE
	1868-69	1869-70	1870-71	1871-72	1872-73	1873-74	
	o	o	o	o	o	o	
S <sub>1</sub>	176·57	187·50	162·29	158·20	147·41	155·03	S <sub>1</sub>
S <sub>2</sub>	322·72	323·68	323·68	321·94	321·56	321·19	S <sub>2</sub>
S <sub>4</sub>	...	...	355·95	4·54	0·00	325·52	S <sub>4</sub>
S <sub>6</sub>	...	...	...	292·99	295·25	311·99	S <sub>6</sub>
S <sub>8</sub>	...	...	...	...	...	26·57	S <sub>8</sub>
M <sub>1</sub>	336·25	...	77·76	23·09	358·57	46·26	M <sub>1</sub>
M <sub>2</sub>	294·47	295·45	294·54	293·53	293·72	292·81	M <sub>2</sub>
M <sub>3</sub>	333·22	333·41	322·35	332·35	316·24	330·32	M <sub>3</sub>
M <sub>4</sub>	44·42	26·83	27·55	22·85	28·31	9·22	M <sub>4</sub>
M <sub>0</sub>	221·99	209·79	218·32	203·18	214·07	208·47	M <sub>0</sub>
M <sub>8</sub>	...	...	...	248·86	265·73	154·66	M <sub>8</sub>
O	47·02	50·26	47·92	47·36	45·81	46·31	O
K <sub>1</sub>	46·69	46·64	48·00	46·43	45·96	45·70	K <sub>1</sub>
K <sub>2</sub>	328·73	315·01	313·32	320·63	321·08	314·74	K <sub>2</sub>
P	46·35	50·27	44·97	47·91	47·44	48·07	P
J	79·12	63·77	38·35	61·14	82·18	157·26	J
Q	46·38	60·66	54·00	50·27	52·23	62·53	Q
L	297·67	321·21	293·55	356·38	263·34	283·63	L
N	279·00	281·04	279·27	279·83	274·85	278·17	N
$\lambda$	335·15	269·77	208·63	207·27	12·06	259·48	$\lambda$
$\nu$	254·32	222·61	343·12	283·85	300·09	237·76	$\nu$
$\mu$	267·37	224·14	300·38	254·23	269·96	232·48	$\mu$
R	...	271·34	...	220·50	...	228·02	R
T	...	319·66	...	22·44	...	232·65	T
MS	215·48	179·51	324·47	357·92	...	307·14	MS
2SM	...	...	...	...	...	128·47	2SM
2N	...	...	...	...	...	...	2N
M <sub>2</sub> N	...	...	...	...	...	...	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	...	...	...	...	...	...	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	...	...	...	...	...	...	2M <sub>2</sub> K <sub>1</sub>
Mm	247·73	175·27	115·90	...	...	55·83	Mm
Mf	317·79	311·48	259·25	...	...	222·95	Mf
MSf	327·50	18·77	158·70	...	...	44·13	MSf
Sa	43·96	80·20	107·11	...	...	95·38	Sa
Ssa	81·98	116·93	69·69	...	...	162·45	Ssa

## TIDAL OBSERVATIONS.

Values of  $\kappa$ 's at Kurrachee—(Continued).

TIDE	$\kappa$						TIDE
	1874-75	1875-76	1876-77	1877-78	1878-79	1879-80	
	o	o	o	o	o	o	
S <sub>1</sub>	152.50	150.45	156.98	180.85	166.94	161.33	S <sub>1</sub>
S <sub>2</sub>	319.93	319.94	318.09	321.14	324.14	324.73	S <sub>2</sub>
S <sub>4</sub>	6.42	353.25	17.21	23.43	29.43	63.09	S <sub>4</sub>
S <sub>6</sub>	308.53	294.60	259.05	274.57	291.09	324.69	S <sub>6</sub>
S <sub>8</sub>	265.60	282.53	206.57	254.06	126.03	222.71	S <sub>8</sub>
M <sub>1</sub>	66.43	36.34	352.53	76.40	54.36	13.99	M <sub>1</sub>
M <sub>2</sub>	291.84	291.40	290.71	291.43	296.46	296.28	M <sub>2</sub>
M <sub>3</sub>	335.89	345.09	343.10	326.90	328.21	319.81	M <sub>3</sub>
M <sub>4</sub>	7.52	14.75	353.07	15.90	1.95	6.89	M <sub>4</sub>
M <sub>6</sub>	211.60	206.24	206.60	196.31	214.75	219.74	M <sub>6</sub>
M <sub>8</sub>	196.09	297.25	281.05	252.46	268.79	19.94	M <sub>8</sub>
O	45.62	45.97	45.15	45.96	49.06	47.33	O
K <sub>1</sub>	45.65	45.87	44.48	44.53	47.68	47.51	K <sub>1</sub>
K <sub>2</sub>	315.77	320.63	317.70	313.88	329.47	324.55	K <sub>2</sub>
P	45.97	44.92	48.97	42.92	44.34	45.06	P
J	35.05	50.12	70.76	87.96	65.97	63.58	J
Q	58.43	46.07	35.38	47.71	46.90	49.69	Q
L	280.33	302.39	306.33	305.37	263.47	311.92	L
N	276.43	274.01	272.97	272.58	274.27	280.14	N
$\lambda$	181.15	94.54	300.20	236.05	184.12	35.42	$\lambda$
$\nu$	320.04	316.72	284.94	235.59	210.82	331.94	$\nu$
$\mu$	274.00	259.66	279.54	216.90	297.04	249.22	$\mu$
R	...	...	307.84	...	273.16	...	R
T	...	...	343.81	...	315.48	...	T
MS	303.72	314.50	313.45	325.81	351.00	337.48	MS
2SM	149.76	97.57	114.71	63.10	167.00	157.65	2SM
2N	...	...	...	...	...	...	2N
M <sub>2</sub> N	...	...	...	...	...	...	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	...	...	...	...	...	...	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	...	...	...	...	...	...	2M <sub>2</sub> K <sub>1</sub>
Mm	23.66	103.22	42.11	49.03	...	25.61	Mm
Mf	40.58	23.74	0.50	29.74	...	327.75	Mf
MSf	333.25	185.68	194.77	313.68	...	318.14	MSf
Sa	56.27	75.77	79.89	119.62	...	86.49	Sa
Ssa	156.65	167.27	163.75	69.72	...	170.97	Ssa

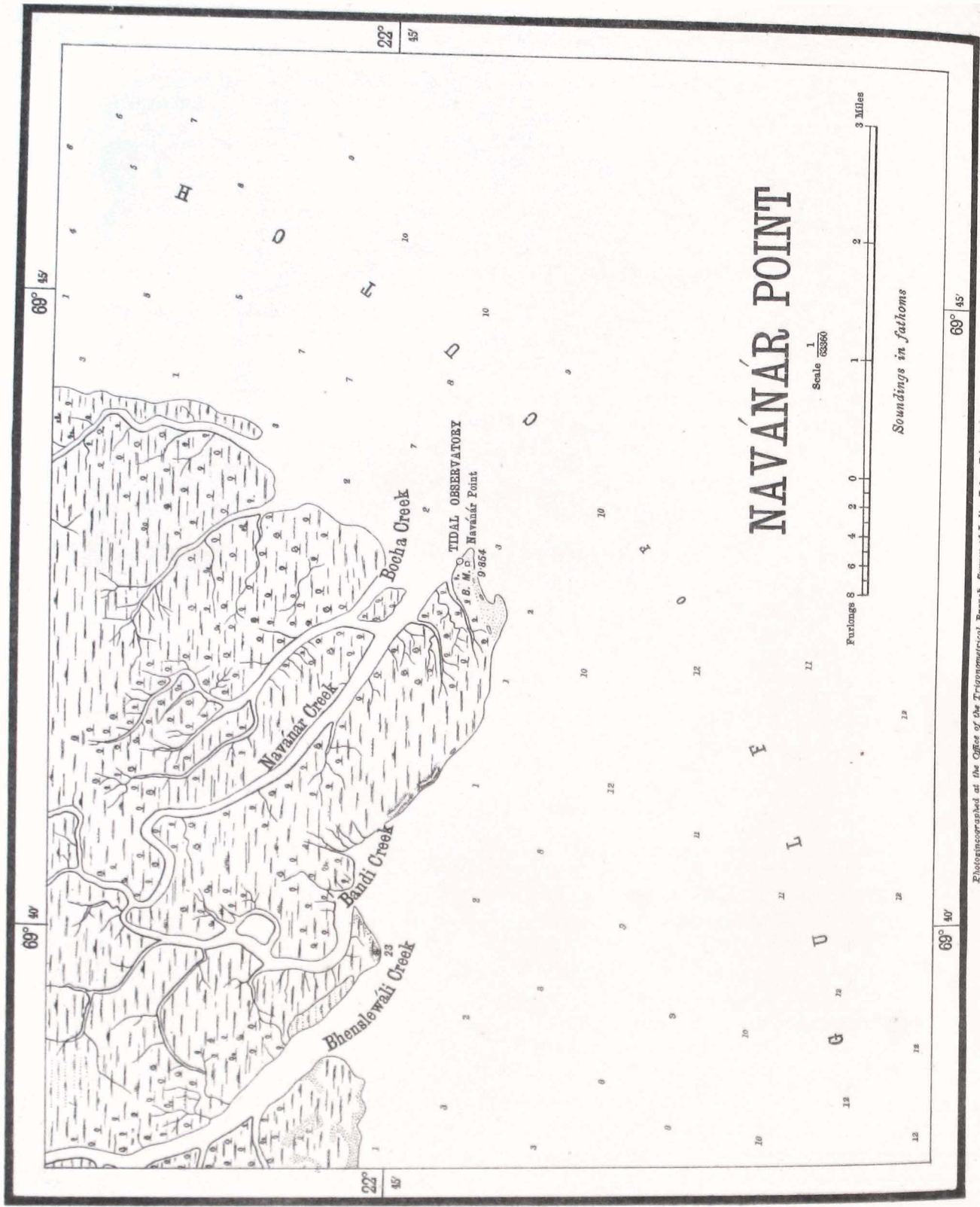
*Values of  $\kappa$ 's at Kurrachee—(Continued).*

TIDE	$\kappa$						TIDE
	1880-81	1881-82	1882-83	1883-84	1884-85	1885-86	
	°	°	°	°	°	°	
S <sub>1</sub>	63.64	173.64	171.86	171.24	182.90	173.62	S <sub>1</sub>
S <sub>2</sub>	323.55	324.03	323.86	323.70	323.13	322.33	S <sub>2</sub>
S <sub>4</sub>	31.43	12.10	35.22	25.26	44.23	43.43	S <sub>4</sub>
S <sub>6</sub>	291.63	313.98	287.24	279.90	323.57	315.69	S <sub>6</sub>
S <sub>8</sub>	11.31	123.69	161.57	288.44	240.26	194.04	S <sub>8</sub>
M <sub>1</sub>	319.00	39.41	61.27	31.39	111.46	133.57	M <sub>1</sub>
M <sub>2</sub>	294.72	294.41	294.11	293.93	294.02	292.50	M <sub>2</sub>
M <sub>3</sub>	319.40	327.02	336.34	347.20	348.93	337.23	M <sub>3</sub>
M <sub>4</sub>	1.65	16.57	359.10	16.07	20.56	15.44	M <sub>4</sub>
M <sub>6</sub>	208.60	207.25	204.42	206.21	206.00	198.57	M <sub>6</sub>
M <sub>8</sub>	340.80	256.51	262.44	196.20	321.50	266.70	M <sub>8</sub>
O	46.28	46.37	46.53	48.21	47.29	47.12	O
K <sub>1</sub>	46.75	46.82	46.87	47.08	45.87	46.30	K <sub>1</sub>
K <sub>2</sub>	321.77	317.11	321.16	321.64	316.14	315.67	K <sub>2</sub>
P	48.51	45.34	44.42	48.34	46.43	44.74	P
J	105.95	52.71	37.69	58.20	80.19	46.12	J
Q	50.81	64.36	61.22	43.15	45.76	52.58	Q
L	309.72	291.37	293.06	284.98	315.51	281.14	L
N	275.70	278.74	280.45	278.05	275.26	275.58	N
$\lambda$	312.88	275.33	235.83	281.57	290.31	240.50	$\lambda$
$\nu$	313.57	263.53	235.76	330.92	320.14	288.47	$\nu$
$\mu$	282.63	267.14	269.57	276.33	287.69	272.34	$\mu$
R	317.15	...	315.36	...	311.51	...	R
T	330.11	...	40.79	...	321.33	...	T
MS	317.49	326.99	328.16	336.17	339.26	344.68	MS
2SM	120.21	120.90	114.93	91.48	113.23	125.06	2SM
2N	...	253.77	270.86	241.12	231.44	237.53	2N
M <sub>2</sub> N	...	34.83	79.22	50.48	41.59	31.09	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	...	6.30	60.52	104.92	153.72	358.44	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	...	31.98	20.45	22.92	6.72	351.83	2M <sub>2</sub> K <sub>1</sub>
Mm	131.23	72.21	93.74	38.51	118.88	0.93	Mm
Mf	70.82	254.15	128.44	340.58	33.82	122.25	Mf
MSf	302.36	130.61	148.42	138.20	196.87	335.97	MSf
Sa	101.51	49.59	50.68	38.72	43.81	105.93	Sa
Ssa	191.73	163.73	193.94	170.24	160.55	150.47	Ssa

## TIDAL OBSERVATIONS.

Values of  $\kappa$ 's at *Kurrachee*—(Continued).

TIDE	$\kappa$						TIDE
	1886-87	1887-88	1888-89	1889-90	1890-91	1891-92	
	°	°	°	°	°	°	
S <sub>1</sub>	179.18	177.18	180.15	180.66	165.17	164.11	S <sub>1</sub>
S <sub>2</sub>	322.84	322.98	323.07	323.61	324.44	323.90	S <sub>2</sub>
S <sub>4</sub>	26.25	38.66	22.74	24.96	42.94	27.93	S <sub>4</sub>
S <sub>6</sub>	284.04	308.81	288.69	308.05	302.99	287.99	S <sub>6</sub>
S <sub>8</sub>	82.24	75.96	104.04	341.57	25.02	82.88	S <sub>8</sub>
M <sub>1</sub>	95.29	12.93	68.57	35.01	55.96	26.18	M <sub>1</sub>
M <sub>2</sub>	293.17	293.77	294.48	293.93	293.91	293.44	M <sub>2</sub>
M <sub>3</sub>	333.25	326.84	323.20	319.19	323.27	332.17	M <sub>3</sub>
M <sub>4</sub>	348.20	358.17	349.45	1.99	354.95	347.53	M <sub>4</sub>
M <sub>6</sub>	199.44	203.11	201.31	197.91	202.93	201.15	M <sub>6</sub>
M <sub>8</sub>	198.47	229.19	205.49	35.10	222.97	262.92	M <sub>8</sub>
O	45.64	45.90	46.01	45.67	45.53	46.32	O
K <sub>1</sub>	46.40	46.44	46.45	46.62	46.09	45.74	K <sub>1</sub>
K <sub>2</sub>	324.55	320.13	316.59	319.77	325.14	319.58	K <sub>2</sub>
P	44.97	46.92	47.22	46.41	46.18	47.58	P
J	42.13	63.90	92.35	63.23	45.10	63.66	J
Q	49.26	42.07	46.16	55.48	53.85	47.42	Q
L	314.99	284.30	310.71	287.77	308.40	268.23	L
N	278.42	278.34	279.32	278.20	279.68	279.51	N
$\lambda$	...	...	...	...	...	...	$\lambda$
$\nu$	246.06	222.02	339.50	301.99	262.91	225.47	$\nu$
$\mu$	257.33	271.80	277.58	281.84	262.11	273.21	$\mu$
R	...	...	...	...	...	...	R
T	47.64	357.93	312.06	274.06	45.01	347.76	T
MS	340.82	342.43	320.80	333.47	344.42	325.95	MS
2SM	108.62	85.07	122.00	125.50	111.22	114.04	2SM
2N	266.87	244.78	228.54	233.22	271.11	244.01	2N
M <sub>2</sub> N	97.88	61.89	64.42	48.61	116.72	77.72	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	59.94	96.28	91.52	21.96	58.11	93.42	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	344.02	82.29	47.26	46.52	37.70	23.86	2M <sub>2</sub> K <sub>1</sub>
Mm	291.35	104.80	221.71	286.36	268.21	346.87	Mm
Mf	30.57	298.93	72.28	335.16	20.06	73.51	Mf
MSf	170.84	51.84	316.26	214.57	39.54	61.80	MSf
Sa	80.84	26.86	58.97	55.84	82.76	41.05	Sa
Ssa	142.18	173.42	126.95	169.76	164.25	125.25	Ssa



Soundings in fathoms

Photoincographed at the Office of the Trigonometrical Branch, Survey of India, Dobra Dui, August 1899.

Regr. No. D. 156, S. I. D. - July 89-90

## NAVÁNÁR POINT.

(*Tidal Observatory, Lat. 22° 44' N., Long. 69° 43' E.*)

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The temporary tidal observatory at Navánár Point on the northern shore of the Gulf of Cutch was set up with a view to determine the existing relations between the level of the land and the sea in this locality. It was situated seven miles south of the town of Mundra, and about half a mile south of the mouth of the Navánár Creek, at the east end of the spit of sand which projects beyond the Point, in the position shown on the accompanying chart. The observatory, masonry well, float-cylinder and communication pipe were very similar to those at Okha Point described on page 23.

The working scale of the tide-gauge was one-sixth.

Registrations were commenced on the 1st May, 1874, and were discontinued on the 5th May, 1875. They were not very successful, owing to the continual alteration in the configuration of the fore-shore, which caused a gap in the observations from the 14th June, 1874, to the 7th March, 1875, and thus reduced the period of the observations available for computation to three and a half lunations. From these observations some of the short period tides have been calculated, and a value of mean-sea-level has been obtained.

Barometrical and anemometrical observations were carried on simultaneously with the tidal observations. The barometer was placed in the observatory, and the anemometer on the top of the same building.

The bench-mark of reference is a stone marked  $\begin{matrix} \text{G.T.S.} \\ \square \\ \text{B.M.} \\ \text{C.} \end{matrix}$  embedded in a three-foot cube of masonry about six inches below the surface of the ground, and situated on a spit of sand to the W. of the creek and about twenty chains S.W. of the light-house. It is nine hundred and eighteen yards from the still-standing cylinder of the tidal observatory, and its bearing from the cylinder is  $254^\circ$ . It is 25·372 feet above the zero of the gauge. Bench-marks A and B, which were placed nearer to the observatory than the above, and in the same line of bearing from it, have disappeared.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = XII<sup>h</sup> 47<sup>m</sup>.

The highest high water recorded was 24·6 feet above the zero of the gauge, and occurred in June, 1874.

The lowest low water recorded was 4·7 feet above the zero of the gauge, and occurred in May, 1874.

In 1874-75 the mean range of largest ordinary springs was found to be 17·6 feet.

The height of mean-sea-level above the zero of the gauge had the following value:—

1874-75    ...    ...    ...    15·441 feet.

NOTE.—The bench-marks of reference at Navánár, Hansthal, and Okha Points were connected by spirit-levelling, and at the time of the establishment of the observatories at these stations, the intention was that a second and final series of tidal observations should be taken at each of them after a sufficient interval had elapsed for a sensible change to have taken place in the relative levels of land and sea.

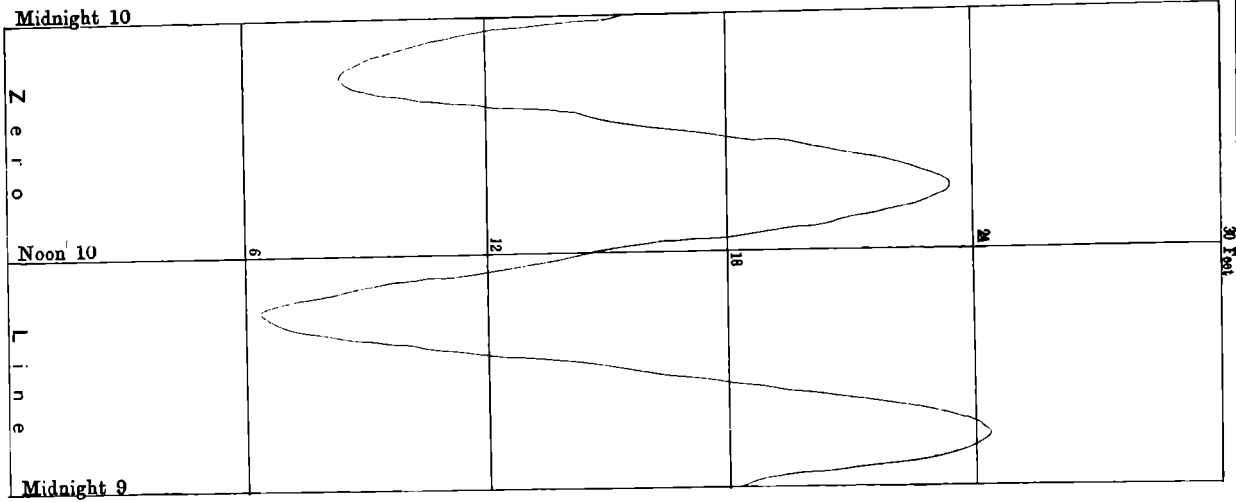
*Values of H's and  $\kappa$ 's at Navánár Point.*

TIDE	H	$\kappa$	TIDE	H	$\kappa$
	1874-75	1874-75		1874-75	1874-75
	Feet	°		Feet	°
S <sub>1</sub>	...	...	N	1·263	10·77
S <sub>2</sub>	1·893	55·33	$\lambda$	0·152	70·15
S <sub>4</sub>	0·013	359·56	$\nu$	·308	4·48
S <sub>6</sub>	...	...	$\mu$	·431	184·55
S <sub>8</sub>	...	...	R	...	...
M <sub>1</sub>	...	...	T	...	...
M <sub>2</sub>	6·044	24·37	MS	...	...
M <sub>3</sub>	...	...	2SM	...	...
M <sub>4</sub>	0·109	273·11	2N	...	...
M <sub>6</sub>	·065	41·47	M <sub>2</sub> N	...	...
M <sub>8</sub>	·023	338·86	M <sub>2</sub> K <sub>1</sub>	...	...
O	·684	65·87	2M <sub>2</sub> K <sub>1</sub>	...	...
K <sub>1</sub>	1·528	62·61	Mm	...	...
K <sub>2</sub>	0·372	62·95	Mf	...	...
P	·281	72·02	MSf	...	...
J	·147	97·00	Sa	...	...
Q	·146	68·97	Ssa	...	...
L	·505	24·81			



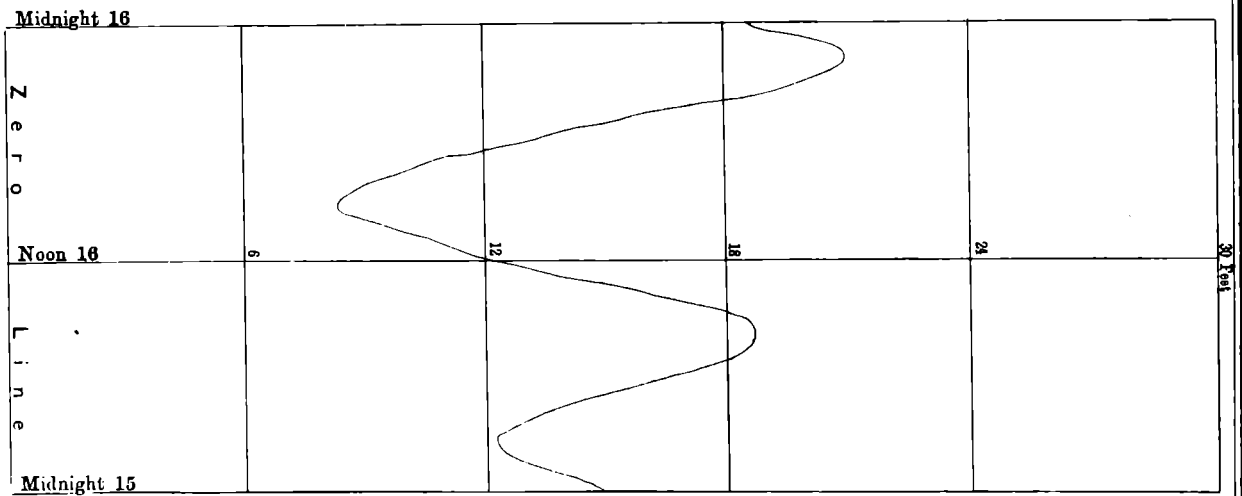
TIDAL CURVES  
at  
NAVÁNAR POINT

Spring Tide — 10th March 1875



New Moon — 7th March 1875

Neap Tide — 16th March 1875

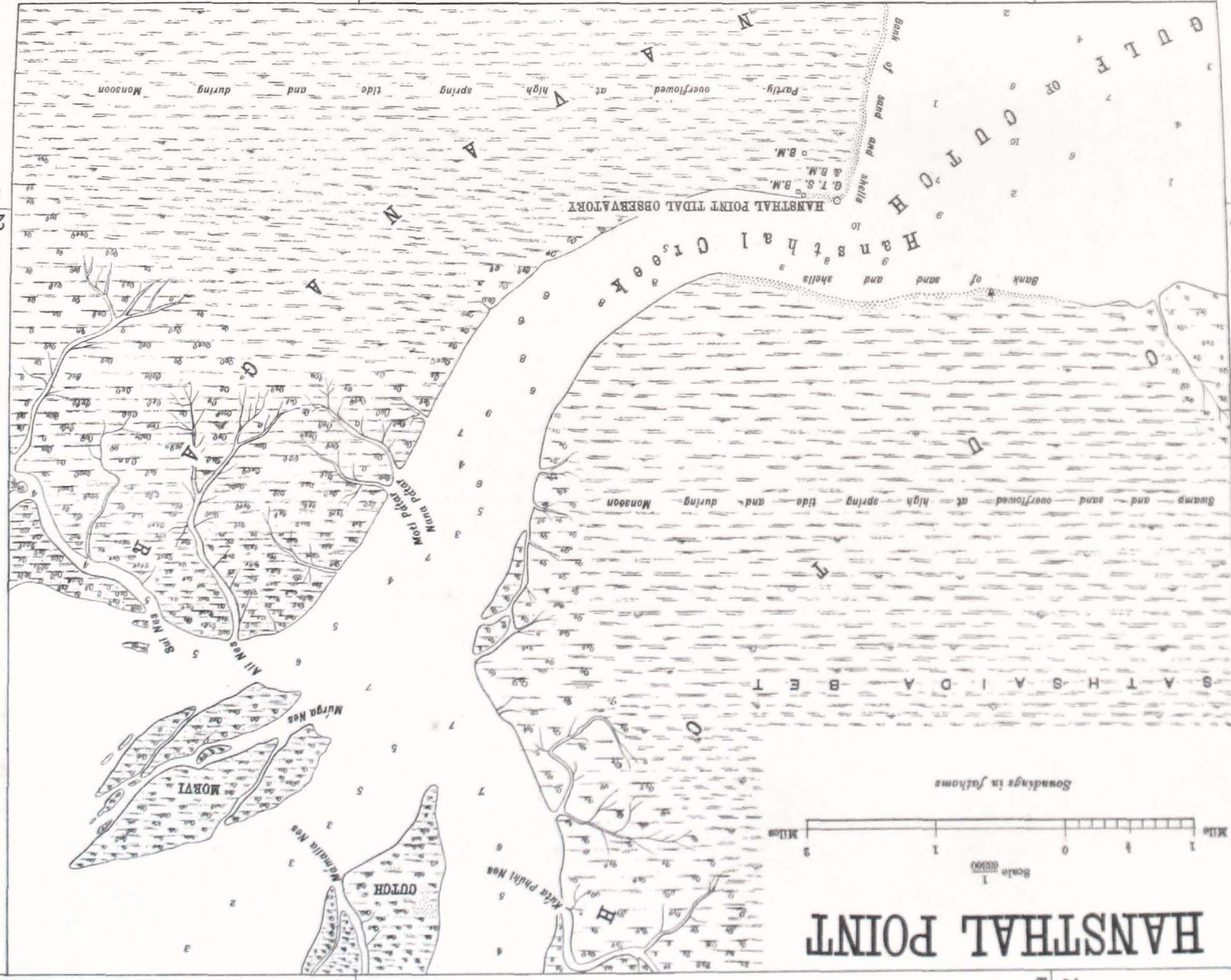
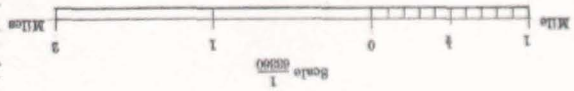


First Quarter — 14th March 1875

*Photostereographed at the Office of the Trigonometrical Branch, Survey of India, Dehra. Din. October 1900.*

# HANSTHAL POINT

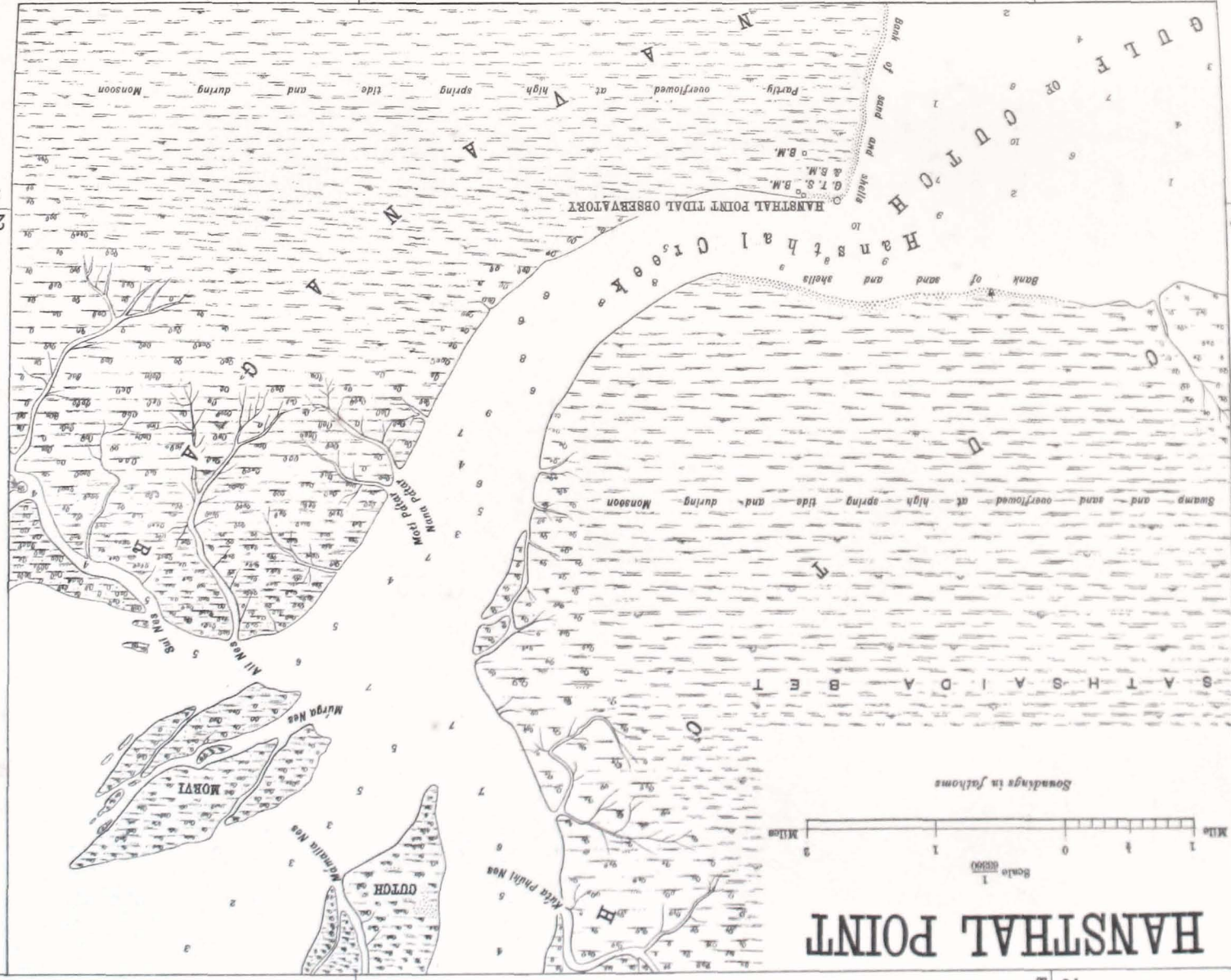
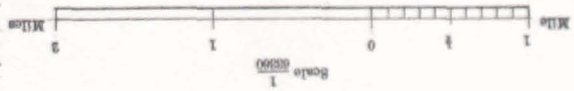
Soundings in fathoms



HANSTHAL POINT TIDAL OBSERVATORY

# HANSTHAL POINT

Soundings in fathoms



HANSTHAL POINT TIDAL OBSERVATORY

## HANSTHAL POINT.

(*Tidal Observatory, Lat. 22° 56' N., Long. 70° 21' E.*)

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The temporary tidal observatory at Hansthal Point, at the head of the Gulf of Cutch, was erected with a view to determine the existing relations between the level of the land and the sea in this locality. It was not considered necessary to continue the first series of tidal observations for more than thirteen and a half months, after which period the observatory was dismantled. The observatory was situated fifteen miles north of the town of Jodiya, on the Káthiáwár or left bank of the Hansthal Creek, about a quarter of a mile above its mouth and one hundred and eighty feet from the bank, in the position shown on the accompanying chart. The observatory, float-cylinder, and communication pipe, were very similar to those at Okha Point described on page 23; but, owing to the ground being black soil, a masonry well was dispensed with and the cylinder was sunk in an excavation of considerable diameter and twenty-five and a half feet deep.

The working scale of the tide-gauge was one-sixth.

Registrations were commenced in April, 1874, and went on very satisfactorily until May, 1875, when they were discontinued and the observatory dismantled.

Barometrical and anemometrical observations were carried on simultaneously with the tidal observations. The barometer was placed in the observatory, and the anemometer on the top of the same building.

The bench-mark of reference is a stone marked  $\begin{matrix} \text{G.T.S.} \\ \square \\ \text{B.M.} \\ \text{A.} \end{matrix}$  embedded in a three-foot cube of masonry, about 6 inches above the surface of the ground. It is situated eight feet E. of a specially built pillar; it is also one hundred and eighty feet W. of the still-standing cylinder of the tidal observatory, and quarter of a mile N.N.E. of a flag-staff called Mustasa Pir-ka-Báota. It is 26.034 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India =  $1^h 40^m$ .

The highest high water recorded was 25·9 feet above the zero of the gauge, and occurred in July, 1874.

The lowest low water recorded was 4·3 feet above the zero of the gauge, and occurred in December, 1874.

In 1874-75 the mean range of largest ordinary springs was found to be 19·3 feet.

The height of mean-sea-level above the zero of the gauge had the following value:—

1874-75      ...      ...      ... 16·332 feet.

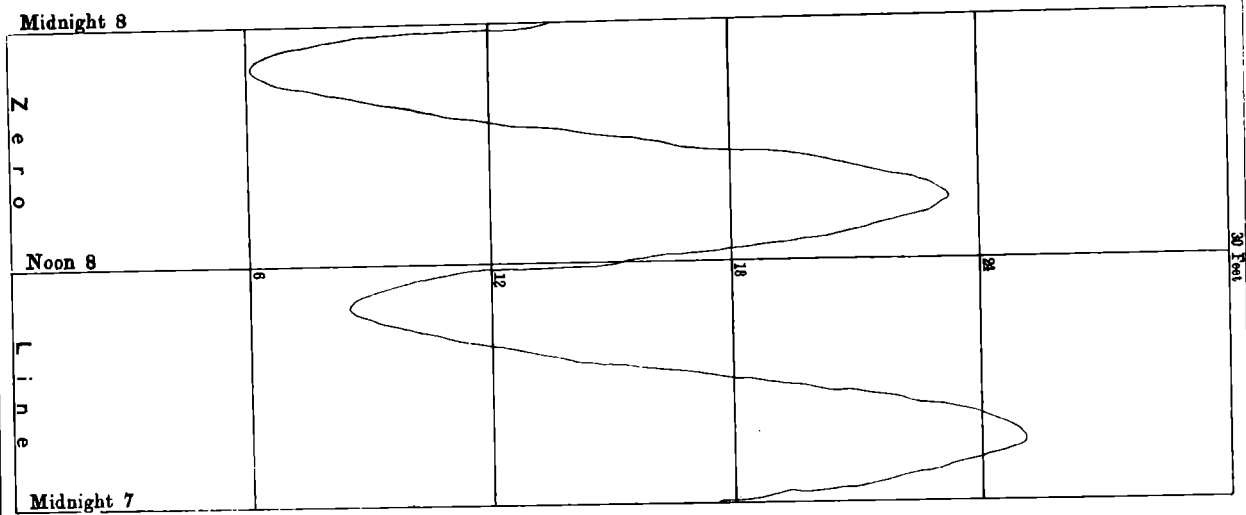
NOTE.—The bench-marks of reference at Hansthal, Okha, and Navánár Points were connected by spirit-levelling, and at the time of the establishment of the observatories at these stations, the intention was that a second and final series of tidal observations should be taken at each of them after a sufficient interval had elapsed for a sensible change to have taken place in the relative levels of land and sea.

*Values of H's and  $\kappa$ 's at Hansthal Point.*

TIDE	H	$\kappa$	TIDE	H	$\kappa$
	1874-75	1874-75		1874-75	1874-75
	Feet	°		Feet	°
S <sub>1</sub>	0·129	164·01	N	1·193	25·79
S <sub>3</sub>	1·928	84·51	$\lambda$	0·235	38·60
S <sub>4</sub>	0·021	61·74	$\nu$	·296	47·27
S <sub>6</sub>	·007	166·57	$\mu$	·595	177·80
S <sub>8</sub>	·003	158·63	R	...	...
M <sub>1</sub>	·055	77·75	T	...	...
M <sub>3</sub>	6·854	45·55	MS	·351	12·04
M <sub>5</sub>	0·056	92·09	2SM	·135	298·71
M <sub>4</sub>	·727	329·61	2N	...	...
M <sub>6</sub>	·305	246·02	M <sub>2</sub> N	...	...
M <sub>8</sub>	·083	150·47	M <sub>2</sub> K <sub>1</sub>	...	...
O	·754	74·70	2M <sub>2</sub> K <sub>1</sub>	...	...
K <sub>1</sub>	1·495	81·11	Mm	·121	14·17
K <sub>2</sub>	0·527	81·25	Mf	·101	36·88
P	·384	83·65	MSf	·169	12·73
J	·095	127·70	Sa	·024	195·32
Q	·139	77·17	Ssa	·090	156·38
L	·570	36·77			

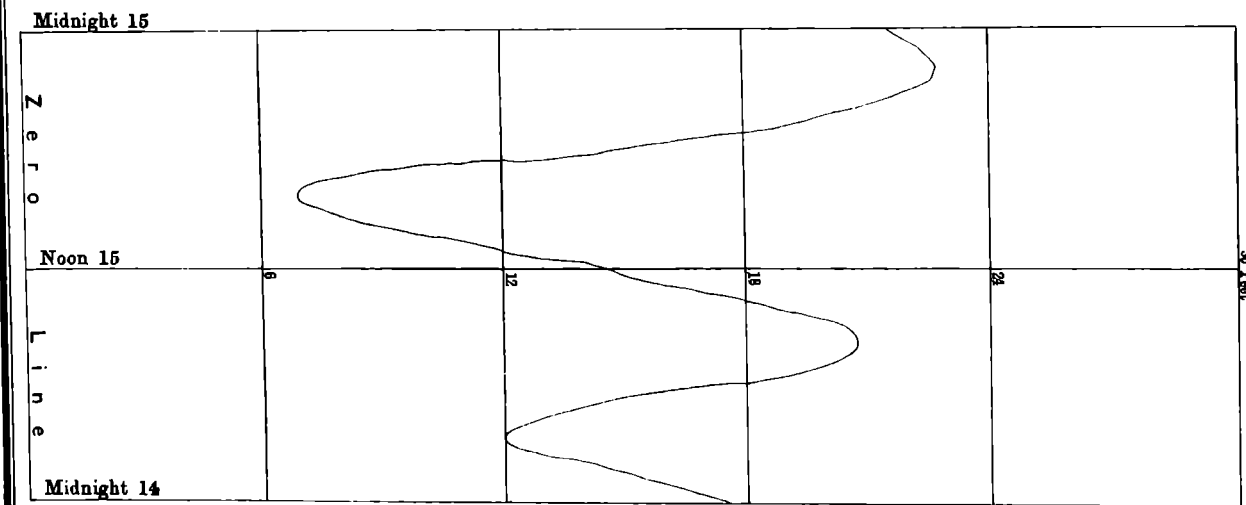
**TIDAL CURVES**  
at  
**HANSTHAL POINT**

Spring Tide — 6th February 1875



New Moon — 6th February 1875

Neap Tide — 16th February 1875



First Quarter — 13th February 1875

*Photoincographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dün, October 1900.*

# OKHA POINT AND BET HARBOUR

G U L F of  
O T T O M A N



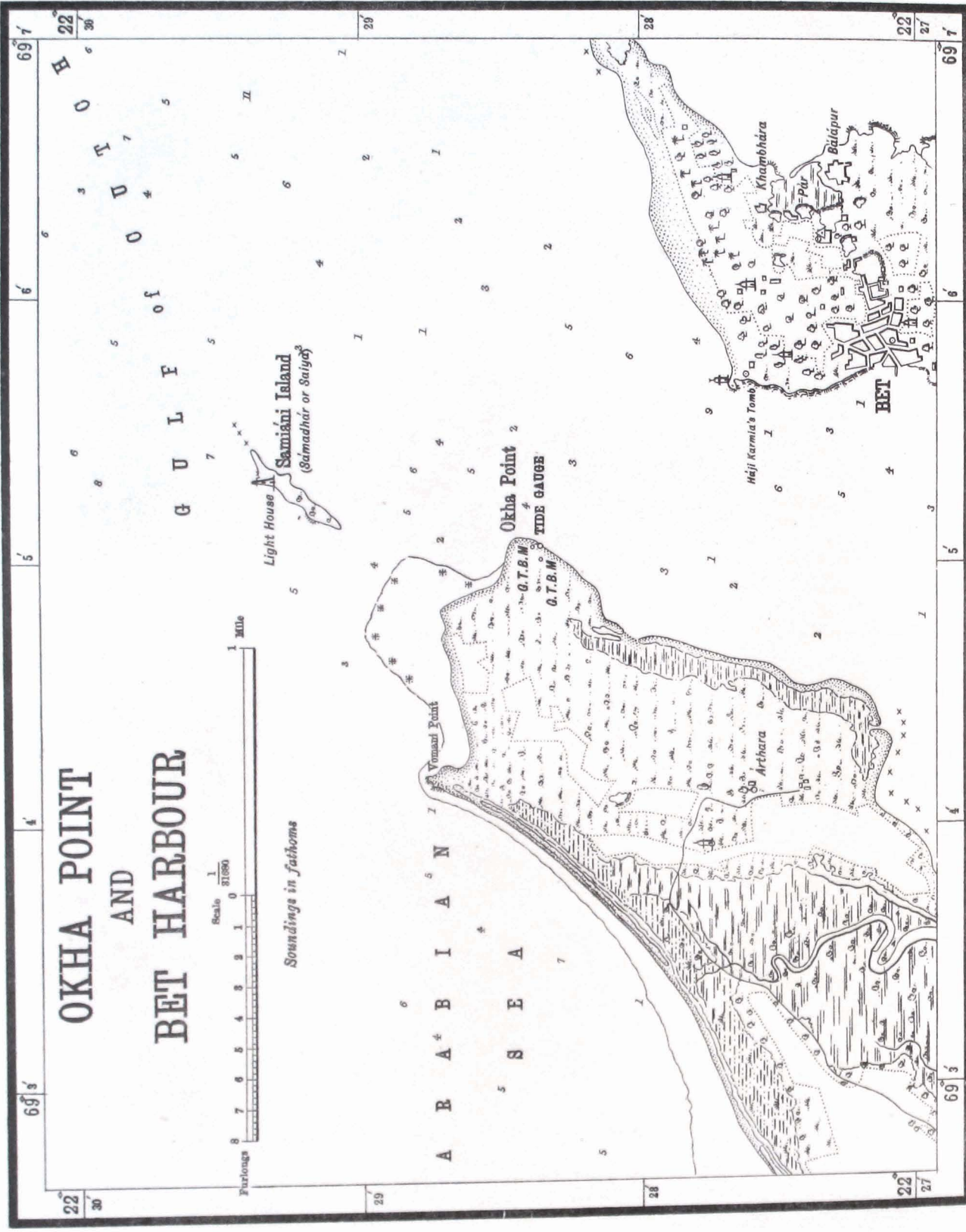
Soundings in fathoms

Light House Samiani Island  
(Samadhār or Saiyō)

A B A I A N  
S E A

Okha Point  
TIDE GAUGE

Miiji Karmia's Tomb  
Khaembhara  
Pur  
Bilapur  
BET



## OKHA POINT AND BET HARBOUR.

*(Tidal Observatory, Lat. 22° 28' N., Long. 69° 5' E.)*

The temporary tidal observatory at Okha Point, on the promontory at the south side of the entrance to the Gulf of Cutch, was erected primarily with a view to determine the existing relations between the level of the land and the sea in this locality. It was consequently not considered necessary to continue the first series of tidal observations at Okha for more than sixteen and a half months, after which period a convenient occasion for dismantling the observatory occurred. The observatory was situated on the shore of the Okhámandal mainland, almost exactly opposite the town and island of Bet, and about three hundred yards south of the north-eastern corner of the land, in the position shown on the accompanying chart. The observatory was a wooden cabin constructed so as to be easily taken to pieces, fixed on three cross beams fitted on the tops of six large piles embedded eight feet in the sand. A brick masonry well, four feet in diameter, to hold the cylinder, was sunk to a depth of five or six feet below low-water springs, and twenty-five feet below the ground level. The float-cylinder was of wrought iron, about twenty-nine feet long and twenty-two inches internal diameter, and rested on the bottom of the well. Nine inches from the bottom of the cylinder a two-inch iron pipe was taken up vertically to within twelve feet six inches of the top of the cylinder: here a stop-cock was placed on a bend, whence the two-inch pipe, having a slight inclination downwards, was carried out to a total length of a hundred and seventy-five feet until it met the natural surface of the sand nearly thirty feet beyond low-water mark. Here a flexible two-inch tube was connected with the iron pipe, and a rose at the end of the tube was held in position by an anchor and sustained by buoys at about six feet from the bottom in a place where there was twenty feet of water at low springs.

The working scale of the tide-gauge was one-fourth.

Registrations were commenced in December, 1873, and went on most satisfactorily until their termination. There were very few breaks in the continuity of the observations and such as occurred were short and of no importance. The observatory was dismantled in May, 1875.

Barometrical and anemometrical observations were carried on simultaneously with the tidal observations. The barometer was placed in the observatory, and the anemometer on the top of the same building.

The bench-mark of reference is a stone marked  $\begin{matrix} \text{G.T.S.} \\ \square \\ \text{B.M.} \\ \text{A.} \end{matrix}$  embedded in a three-foot cube of masonry, about six inches below the surface of the ground. It is situated one hundred feet from the still-standing cylinder of the tidal observatory, and its bearing from the cylinder is 11°. It is 20·074 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = XII<sup>h</sup> 8<sup>m</sup>.

The highest high water recorded was 16·4 feet above the zero of the gauge, and occurred in June, 1874.

The lowest low water recorded was 1·5 feet above the zero of the gauge, and occurred in November, 1874.

In 1874-75 the mean range of largest ordinary springs was found to be 12·4 feet.

The height of mean-sea-level above the zero of the gauge had the following value:—

1874-75      ...      ...      ... 9·650 feet.

NOTE.—The bench-marks of reference at Okha, Navánár, and Hansthal Points were connected by spirit-levelling and at the time of the establishment of the observatories at these stations, the intention was that a second and final series of tidal observations should be taken at each of them after a sufficient interval had elapsed for a sensible change to have taken place in the relative levels of land and sea.

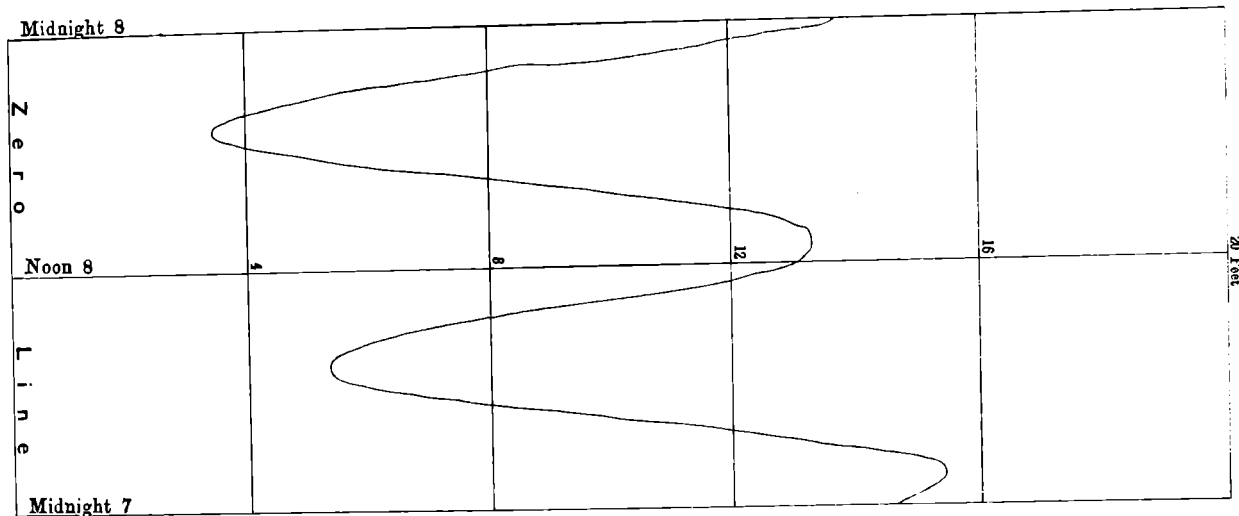
*Values of H's and κ's at Okha Point.*

TIDE	H	κ	TIDE	H	κ
	1874-75	1874-75		1874-75	1874-75
	Feet	°		Feet	°
S <sub>1</sub>	0·074	149·89	N	0·781	321·97
S <sub>2</sub>	1·222	14·37	λ	·073	23·43
S <sub>4</sub>	0·013	116·57	ν	·164	7·53
S <sub>6</sub>	·003	20·92	μ	·203	182·32
S <sub>8</sub>	·001	219·81	R	...	...
M <sub>1</sub>	·051	43·00	T	...	...
M <sub>2</sub>	3·820	347·11	MS	·064	111·40
M <sub>3</sub>	0·030	20·64	2SM	·044	292·21
M <sub>4</sub>	·136	106·94	2N	...	...
M <sub>6</sub>	·007	269·65	M <sub>2</sub> N	...	...
M <sub>8</sub>	·011	96·17	M <sub>2</sub> K <sub>1</sub>	...	...
O	·693	56·61	2M <sub>2</sub> K <sub>1</sub>	...	...
K <sub>1</sub>	1·414	53·11	Mm	·066	311·38
K <sub>2</sub>	0·328	17·44	Mf	·050	43·87
P	·384	49·94	MSf	·141	250·16
J	·107	81·41	Sa	·162	3·11
Q	·137	58·62	Ssa	·121	144·75
L	·221	23·22			



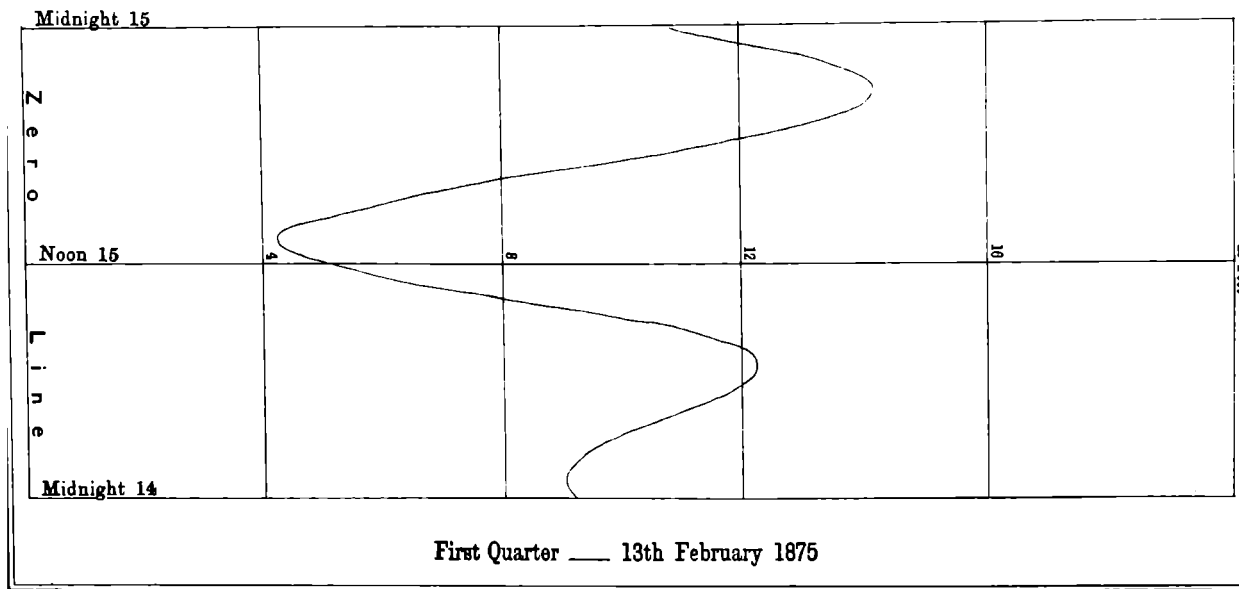
**TIDAL CURVES**  
at  
**OKHA POINT & BET HARBOUR**

Spring Tide — 8th February 1875



New Moon — 6th February 1875

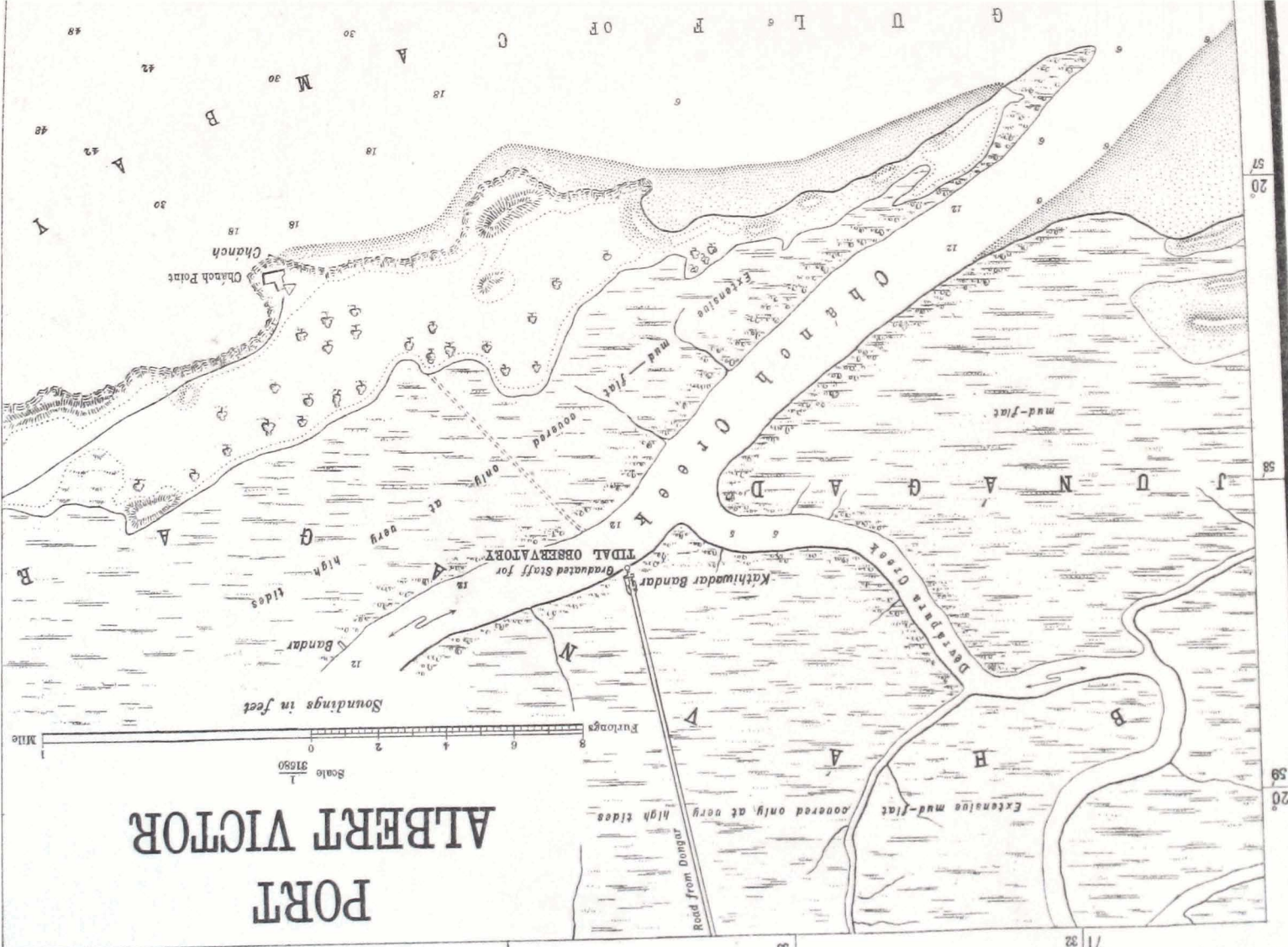
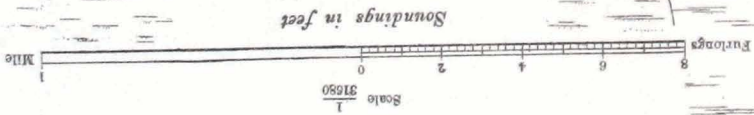
Neap Tide — 15th February 1875



First Quarter — 13th February 1875

*Photoincographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun. July 1899.*

# PORT ALBERT VICTOR



71 35

34

33

71 32

59  
20

58

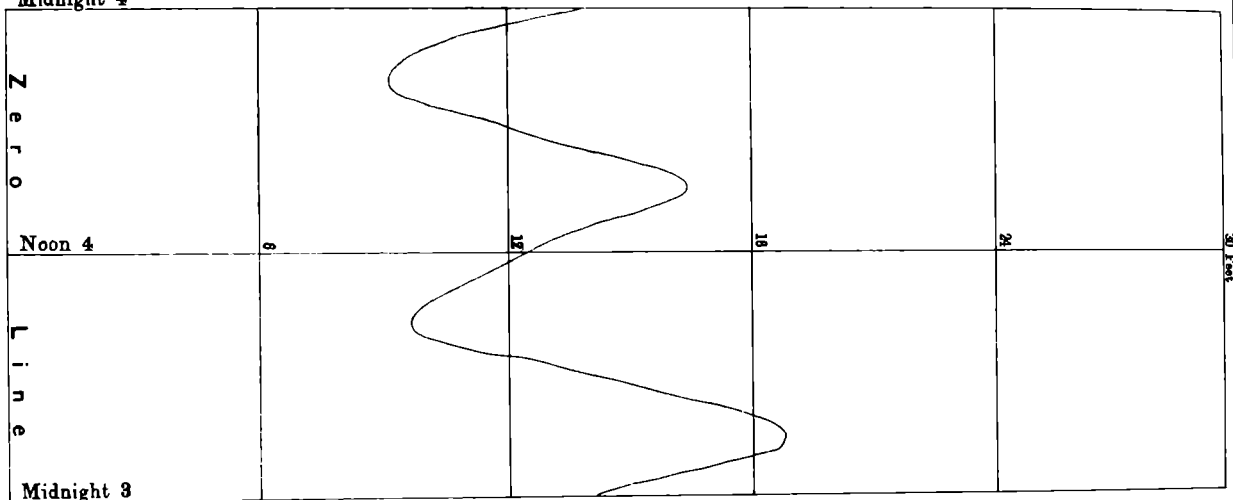
57  
20

G U L S O F C A N A D I A N A R M Y

**TIDAL CURVES**  
at  
**PORT ALBERT VICTOR**

Spring Tide — 4th February 1882

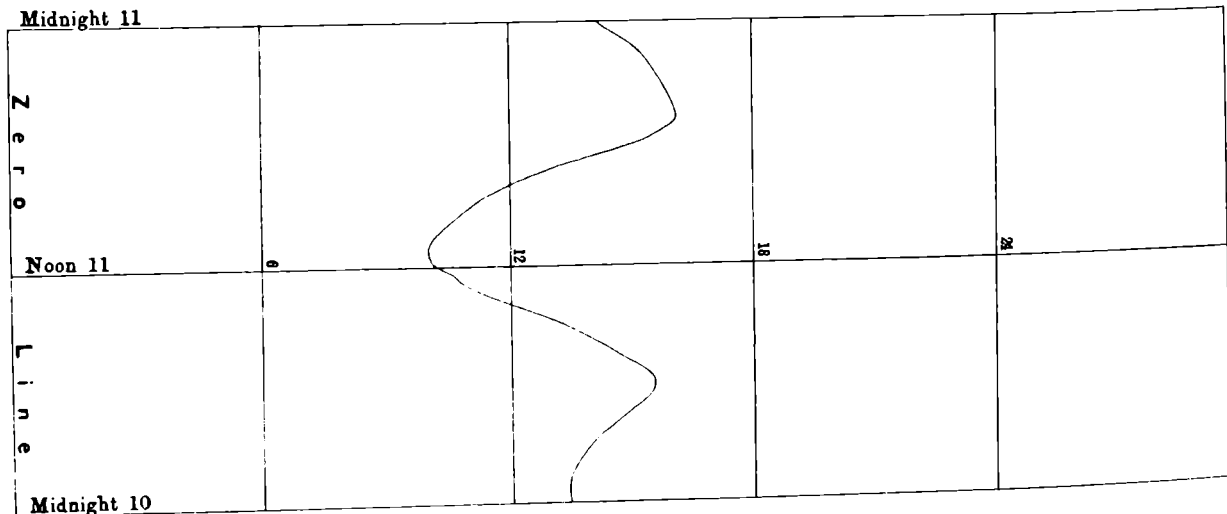
Midnight 4



Full Moon — 3rd February 1882

Neap Tide — 11th February 1882

Midnight 11



Last Quarter — 11th February 1882

*Photocopyographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun, July 1889.*

## PORT ALBERT VICTOR.

(*Tidal Observatory, Lat. 20° 58' N., Long. 71° 33' E.*)

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Tidal observations at Port Albert Victor (Káthiwadar), on the south coast of Káthiáwár, were taken by means of a graduated staff during the preparations for and erection of a tidal observatory at Bhávnagar in Káthiáwár. The graduated staff was fixed in the Cháneh Creek at Káthiwadar just off the new Bandar wall, in the position shown on the accompanying chart; and this staff was observed to, personally, every quarter of an hour, night and day, from 1st November, 1881, to 9th November, 1882, under the direction of the Engineer to H. H. the Maharajah of Bhávnagar.

The bench-mark of reference is on the Bandar, 85 feet from the face wall. It is 24·540 feet above the zero of the graduated staff.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = 11<sup>h</sup> 2<sup>m</sup>.

The highest high water recorded was 22·5 feet above the zero of the graduated staff, and occurred in January, 1882.

The lowest low water recorded was 5·7 feet above the zero of the graduated staff, and occurred in March, 1882.

In 1881-82 the mean range of largest ordinary springs was found to be 11·9 feet.

The height of mean-sea-level above the zero of the graduated staff had the following value:—

1881-82	...	...	...	13·872 feet.
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## TIDAL OBSERVATIONS.

*Values of H's and  $\kappa$ 's at Port Albert Victor.*

TIDE	H	$\kappa$	TIDE	H	$\kappa$
	1881-82	1881-82		1881-82	1881-82
	Feet	°		Feet	°
S <sub>1</sub>	0·134	200·98	N	0·755	33·70
S <sub>2</sub>	1·207	80·89	$\lambda$	·043	107·14
S <sub>3</sub>	0·029	272·78	$\nu$	·131	15·36
S <sub>6</sub>	·013	41·89	$\mu$	·286	343·27
S <sub>8</sub>	·002	263·66	R	...	...
M <sub>1</sub>	·057	35·46	T	...	...
M <sub>2</sub>	2·970	55·28	MS	·159	215·39
M <sub>3</sub>	0·020	151·87	2SM	·029	153·77
M <sub>4</sub>	·220	178·11	2N	...	...
M <sub>6</sub>	·139	137·46	M <sub>2</sub> N	...	...
M <sub>8</sub>	·002	198·64	M <sub>2</sub> K <sub>1</sub>	...	...
O	·720	66·42	2M <sub>2</sub> K <sub>1</sub>	...	...
K <sub>1</sub>	1·611	65·90	Mm	·052	7·56
K <sub>2</sub>	0·324	79·21	Mf	·027	103·41
P	·436	70·67	MSf	·040	152·79
J	·175	106·68	Sa	·236	133·36
Q	·152	67·95	Ssa	·109	155·95
L	·079	260·51			

72° 10'

# BHÁVNAGAR

Scale 1:63550



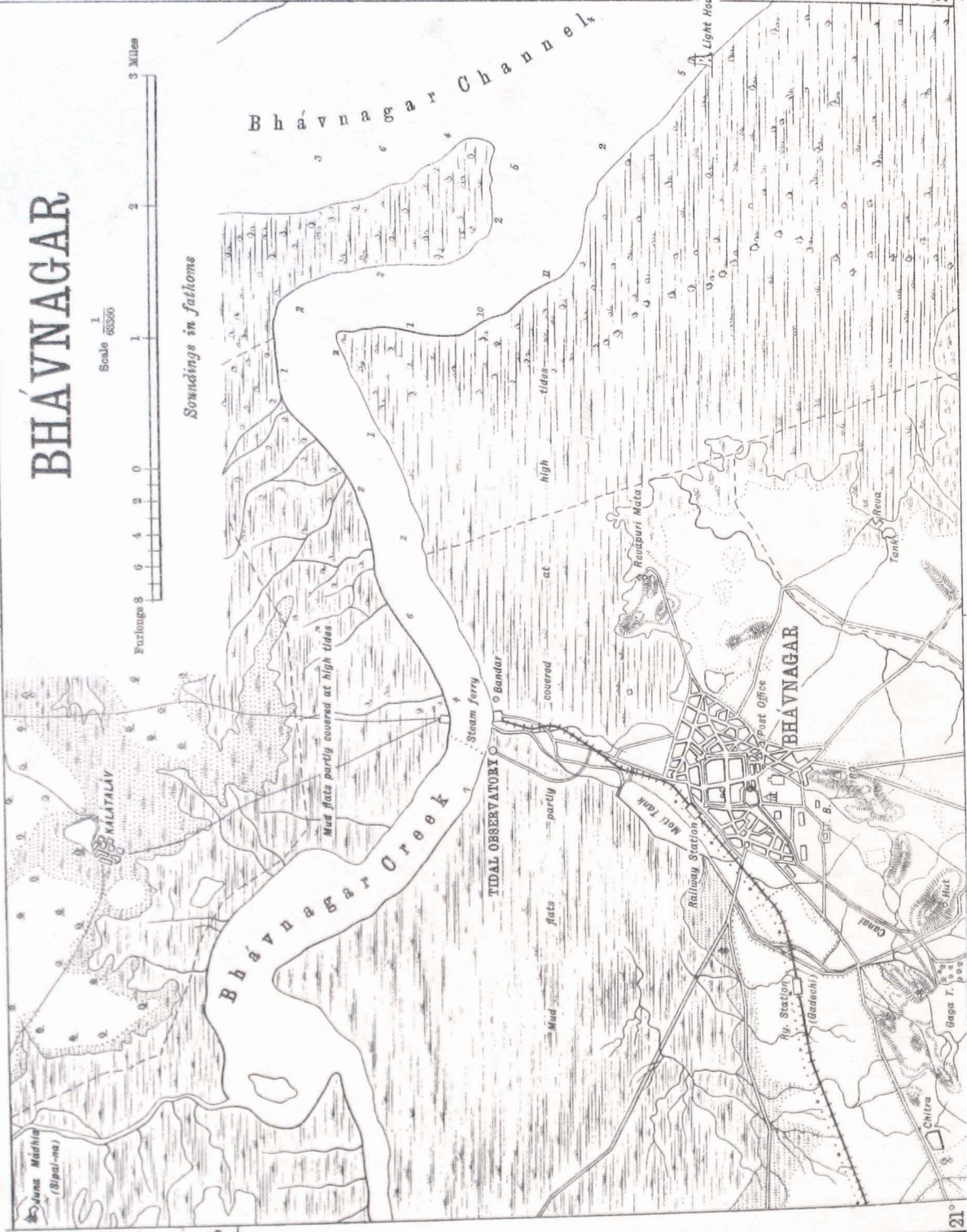
*Soundings in fathoms*

21° 50'

21° 50'

Bhavnagar Creek

Bhavnagar Channel



21°

21° 45'

## BHÁVNAGAR.

(*Tidal Observatory, Lat. 21° 48' N., Long. 72° 9' E.*)

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The observatory at Bhávnagar in Káthiáwár is one of the minor observatories, at which five years' observations are generally considered sufficient, and is situated on the south or right bank of the Bhávnagar Creek, close to the Steam Ferry Incline, in the position shown on the accompanying chart. It is a well-constructed wooden cabin surrounded by a railed-in balcony and supported on piles. The float-cylinder was specially constructed in England and is exceptionally large, as it was originally designed to be the sole support to the observatory; but that arrangement was abandoned when the observatory came to be put up. The cylinder is sunk thirty-five feet in the mud: it is forty-two inches in diameter and forty feet long, thus giving ample range for extreme tides, between which the large difference of thirty-seven feet has been observed. The communication is by a three-inch iron pipe three hundred feet long, bent in the form of a siphon. The short branch rises vertically inside the cylinder for a length of about twenty-one and a half feet from a point, always under water, three inches above the bottom (which is closed with concrete): the pipe then passes firstly through the cylinder, then through eighty feet of mud, and then descends on supports into deep water where it terminates with a rose always under water. An air-chamber with a cock to release the air which accumulates from within the communication pipe, and a stop-cock used for flushing purposes, are placed near each other in the apex of the siphon inside the cylinder; and an iron ladder leads down to the bottom of the cylinder, so that any deposit of mud can be removed when necessary. The observatory and its equipment of instruments belong to H. H. the Maharajah of Bhávnagar, and are under the supervision of the State Engineer.

The working scale of the tide-gauge is one-tenth.



Registrations were commenced on the 1st January, 1886, and have been fairly continuous up to the present, although the periodical flushing out, inevitable leakages in the long communication pipe, and accidents to the cocks have caused numerous trifling interruptions. Up to a late date in November, 1888, the curves, though fairly continuous, presented certain peculiarities which occurred with regularity and which were attributed to idiosyncrasies of the tides in the Bhávnagar Creek. It was then found that the peculiarities were caused by unsuspected accumulations of air in the connection pipe, and that they disappeared if the air-cock was kept open for the whole time that the water was above it. This discovery necessitated the rejection of three years' observations.

Barometrical and anemometrical observations were carried on simultaneously with the tidal observations. The barometer was placed in the observatory and the anemometer on the top of the same building.

The bench-mark of reference is a dressed block of stone marked  $\overset{\text{G.T.S.}}{\circ}$  and fixed in the masonry close to the Steam Ferry Incline, and distant one-hundred and fifty-four yards S.W. of the observatory. It is 43.35 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = IV<sup>h</sup> 32<sup>m</sup>.

The highest high water recorded was 40.7 feet above the zero of the gauge, and occurred in April, 1892.

The lowest low water recorded was 3.7 feet above the zero of the gauge, and occurred in October, 1891.

In 1890 the mean range of largest ordinary springs was found to be 31.4 feet.

The height of mean-sea-level above the zero of the gauge had the following values :—

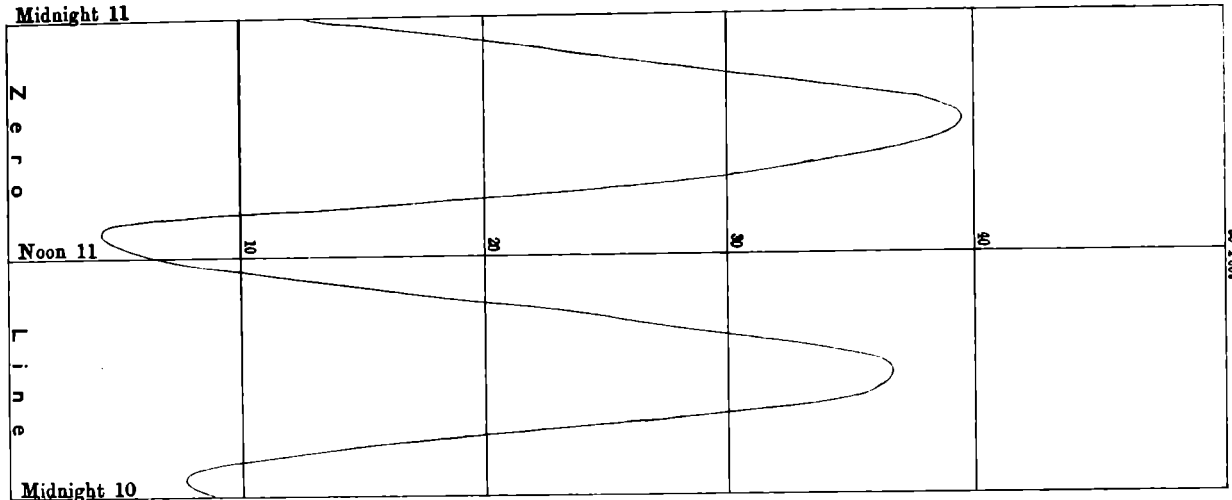
1889	...	...	...	22.703 feet.
1890	...	...	...	22.742 „
1891	...	...	...	22.592 „
1892	...	...	...	22.699 „



TIDAL CURVES  
at  
BHÁVNAGAR

Spring Tide — 11th April 1891

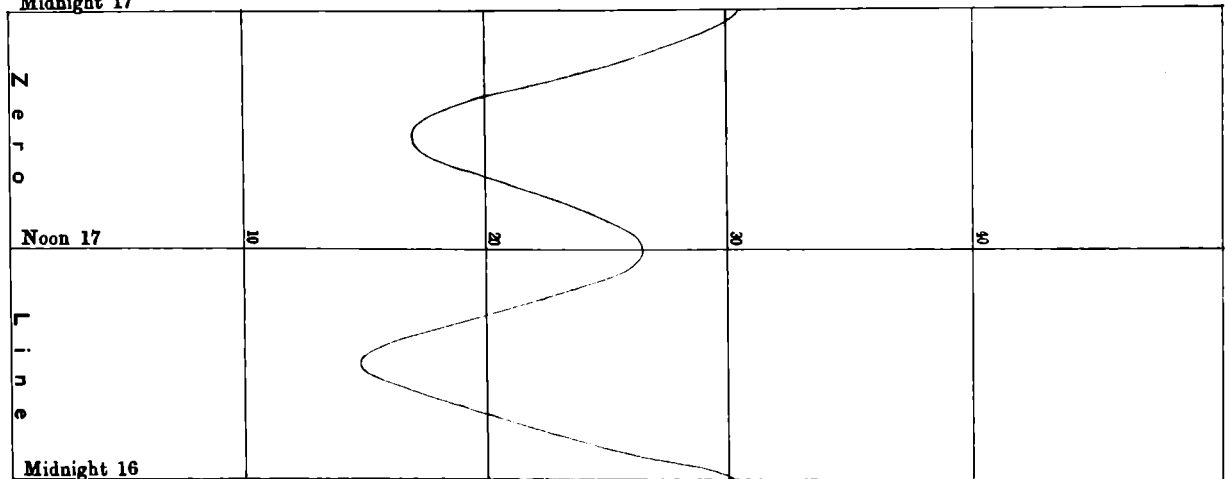
Midnight 11



New Moon — 8th April 1891

Neap Tide — 17th April 1891

Midnight 17



First Quarter — 16th April 1891

Photographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun June 1899.

*Values of H's and  $\kappa$ 's at Bhavnagar.*

TIDE	H				$\kappa$				TIDE
	1889	1890	1891	1892	1889	1890	1891	1892	
	Feet	Feet	Feet	Feet	°	°	°	°	
S <sub>1</sub>	0·105	0·158	0·165	0·107	197·30	182·11	195·69	213·53	S <sub>1</sub>
S <sub>2</sub>	3·469	3·482	3·499	3·522	174·40	176·30	176·72	177·07	S <sub>2</sub>
S <sub>4</sub>	0·116	0·107	0·125	0·121	240·36	236·28	238·87	236·39	S <sub>4</sub>
S <sub>6</sub>	·016	·019	·018	·021	318·25	310·93	291·10	307·52	S <sub>6</sub>
S <sub>8</sub>	·004	·005	·002	·001	7·70	38·66	255·07	56·31	S <sub>8</sub>
M <sub>1</sub>	·059	·039	·088	·125	158·66	281·47	126·02	86·44	M <sub>1</sub>
M <sub>2</sub>	10·723	10·894	11·050	11·278	133·19	133·49	133·94	133·68	M <sub>2</sub>
M <sub>3</sub>	0·092	0·071	0·083	0·066	320·35	302·34	269·20	254·56	M <sub>3</sub>
M <sub>4</sub>	·842	·828	·910	·888	146·13	148·82	151·05	150·38	M <sub>4</sub>
M <sub>6</sub>	·240	·231	·246	·273	112·65	119·74	134·28	131·43	M <sub>6</sub>
M <sub>8</sub>	·034	·015	·016	·006	60·56	321·35	222·16	291·45	M <sub>8</sub>
O	1·000	·972	·980	·974	83·08	83·31	84·11	85·37	O
K <sub>1</sub>	2·288	2·309	2·366	2·365	89·50	90·68	90·19	90·32	K <sub>1</sub>
K <sub>2</sub>	0·855	0·723	0·896	0·984	165·77	172·70	177·07	170·64	K <sub>2</sub>
P	·674	·679	·681	·688	91·73	95·67	97·93	93·37	P
J	·262	·165	·166	·214	161·49	166·89	123·66	118·24	J
Q	·210	·172	·194	·227	81·60	96·09	92·83	82·37	Q
L	·453	·593	·819	·774	138·59	152·05	144·05	119·75	L
N	2·356	2·346	2·510	2·475	113·71	113·71	112·80	116·43	N
$\lambda$	...	...	...	...	...	...	...	...	$\lambda$
$\nu$	0·337	0·437	0·855	0·890	88·14	140·46	114·39	92·96	$\nu$
$\mu$	·288	·379	·243	·322	278·09	259·55	269·84	259·72	$\mu$
R	...	...	...	...	...	...	...	...	R
T	...	·035	·370	·478	...	79·63	237·40	188·08	T
MS	·638	·639	·684	·614	193·16	192·07	196·79	198·75	MS
2SM	·099	·092	·093	·086	340·12	6·74	4·91	341·15	2SM
2N	·468	·424	·101	·270	56·65	96·98	106·46	48·05	2N
M <sub>2</sub> N	·380	·215	·367	·183	67·97	82·13	116·99	97·17	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	·077	·182	·315	·270	148·03	74·86	107·17	142·72	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	·158	·151	·142	·158	359·24	350·52	355·28	339·39	2M <sub>2</sub> K <sub>1</sub>
Mm	·066	·084	·101	·147	343·36	300·85	22·78	354·54	Mm
Mf	·066	·069	·078	·062	328·13	293·94	35·16	19·90	Mf
MSf	·105	·138	·176	·126	45·81	44·21	61·97	27·40	MSf
Sa	·178	·215	·268	·359	104·82	87·91	132·86	111·32	Sa
Ssa	·112	·234	·033	·131	172·06	206·65	11·63	137·56	Ssa

## APOLLO BANDAR, BOMBAY.

(*Tidal Observatory, Lat. 18° 55' N., Long. 72° 50' E.*)

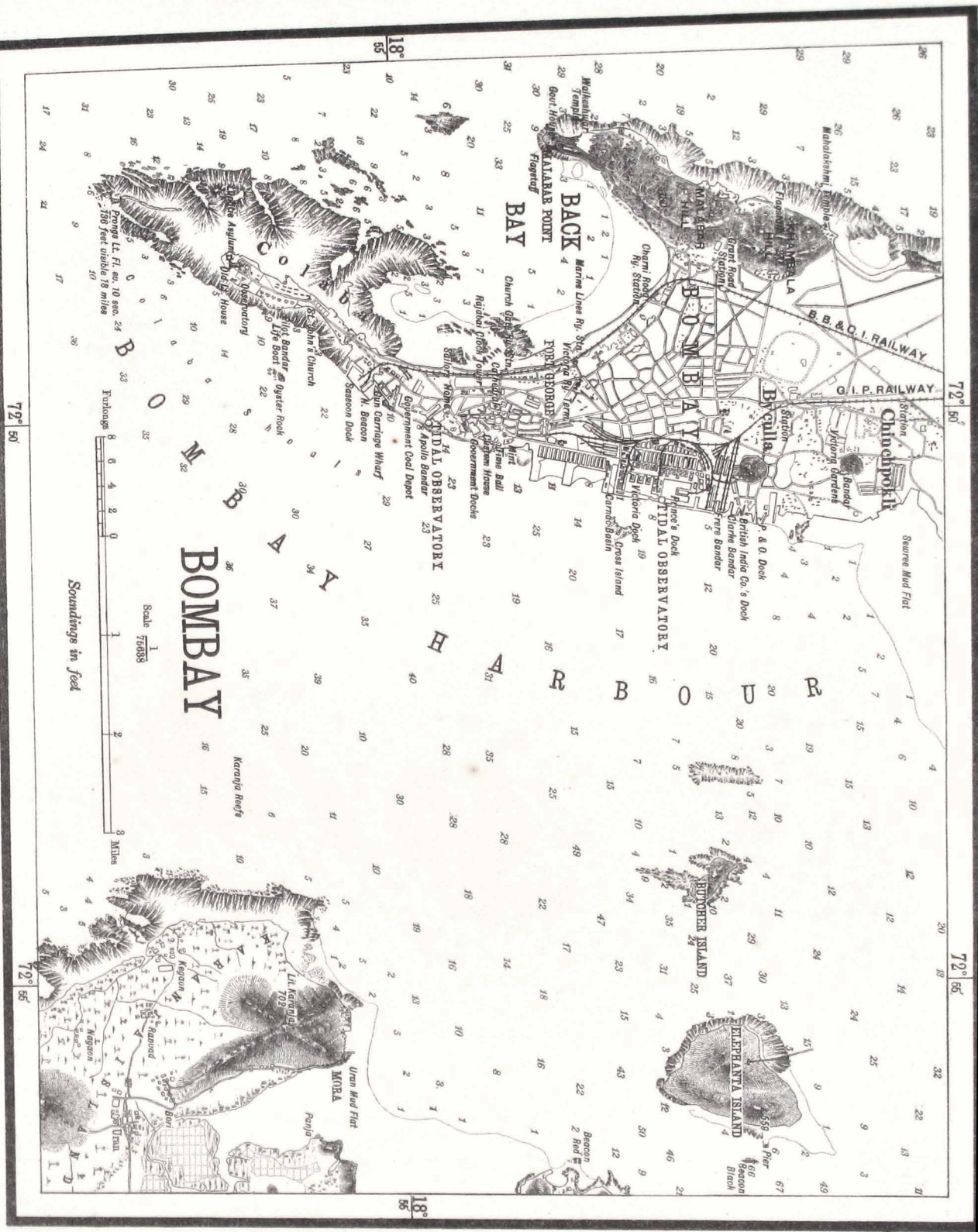
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The tidal observatory at the Apollo Bandar, Bombay, is one of the permanent observatories and is situated at the N.E. corner of the Bandar (or pier), in the position shown on the accompanying chart. It is a neat wooden building covering a well (constructed in the masonry of the Bandar), that prior to the establishment of a tidal observatory, had been used for the tidal measurements taken by the Engineer to the Port Trust. The well is twenty-six feet deep, of circular section, and of a diameter of twelve feet at and for twelve feet above the bottom, whence it narrows gradually to a diameter of eight feet at the mouth. A horizontal passage twelve inches by six inches in section and eleven feet long leads from the bottom of the well straight into the sea, at a level rather more than two feet below the lowest recorded tides. The float-cylinder is of iron, about twenty-two inches in diameter and about twenty-six feet long, which gives range for extreme tides. It is secured above to the flooring of the observatory, whence it descends into the well, and its lower end, which is open, is supported on three short iron pegs or feet fastened to a stone block at the bottom of the well.

The working scale of the tide-gauge is one-fourth.

Registrations were commenced on the 29th January, 1878, and have been remarkably satisfactory up to the present; in fact, this observatory may be held to rank first among Indian tidal observatories not only in respect of the continuity of the observations but in respect of the excellence of the results obtained from them.

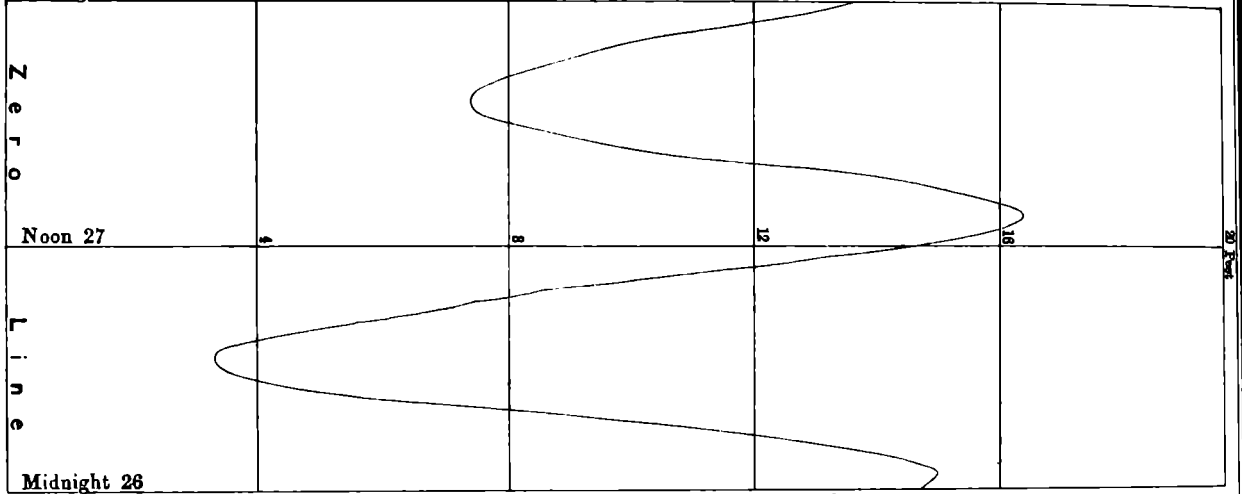
The disturbances of the surface of the ocean, caused by the Krakatoa volcanic eruptions, were recorded at this tidal station by the self-registering tide-gauge on the 27th August, 1883.



**TIDAL CURVES**  
at  
**APOLLO BANDAR, BOMBAY**

Spring Tide — 27th April 1891

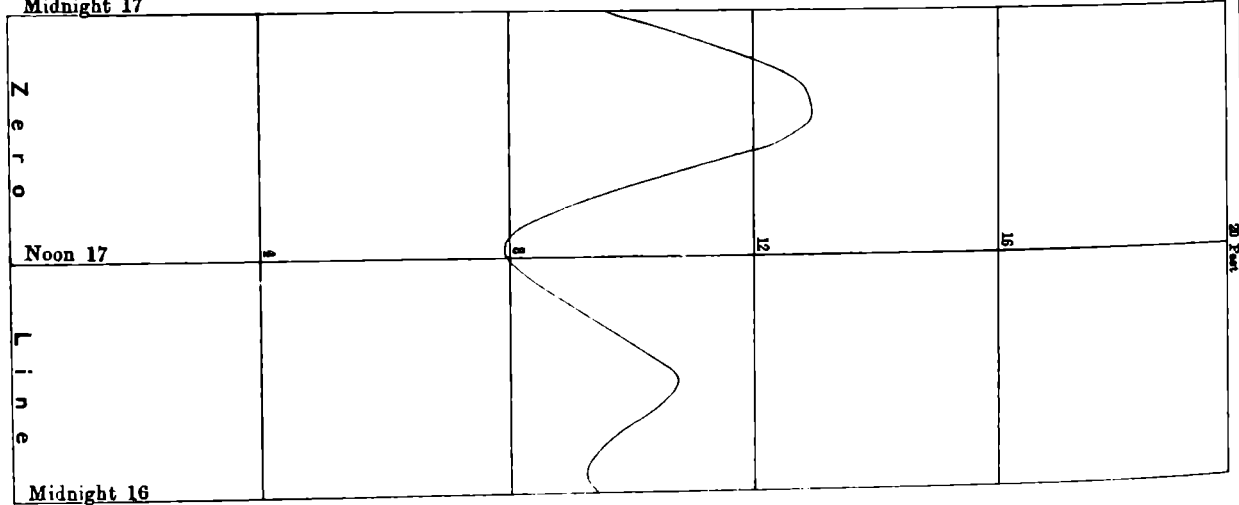
Midnight 27



Full Moon — 24th April 1891

Neap Tide — 17th April 1891

Midnight 17



First Quarter — 16th April 1891

*Photocopyographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun, June 1899.*

Barometrical and anemometrical observations are dispensed with at this tidal observatory, as those taken at the neighbouring Meteorological Observatory at Colaba supply the necessary statistics.

The bench-mark of reference is the Standard Bench-mark, situated at the Public Works Secretariat, consisting of a three-foot cube of polished granite, the top surface of which is the plane of reference. It is 30·000 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = XI<sup>h</sup> 35<sup>m</sup>.

The highest high water recorded was 19·2 feet above the zero of the gauge, and occurred in July, 1881.

The lowest low water recorded was 0·6 foot above the zero of the gauge, and occurred in October, 1879.

In 1890 the mean range of largest ordinary springs was found to be 13·9 feet.

The height of mean-sea-level above the zero of the gauge had the following values:—

1878	...	...	...	10·265 feet.
1879	...	...	...	10·184 „
1880	...	...	...	10·187 „
1881	...	...	...	10·248 „
1882	...	...	...	10·194 „
1883	...	...	...	10·257 „
1884	...	...	...	10·256 „
1885	...	...	...	10·304 „
1886	...	...	...	10·267 „
1887	...	...	...	10·210 „
1888	...	...	...	10·249 „
1889	...	...	...	10·209 „
1890	...	...	...	10·230 „
1891	...	...	...	10·156 „
1892	...	...	...	10·285 „

NOTE.—The level of the zero of the gauge at Apollo Bandar is 2·000 feet below that of the zero of the gauge at Prince's Dock.

*Values of H's at Apollo Bandar, Bombay.*

TIDE	H								TIDE
	1878	1879	1880	1881	1882	1883	1884	1885	
	Feet	Feet	Feet	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0·075	0·083	0·088	0·074	0·072	0·057	0·059	0·053	S <sub>1</sub>
S <sub>2</sub>	1·614	1·634	1·627	1·618	1·616	1·623	1·636	1·627	S <sub>2</sub>
S <sub>4</sub>	0·018	0·013	0·013	0·011	0·006	0·003	0·007	0·010	S <sub>4</sub>
S <sub>6</sub>	·002	·004	·004	·005	·002	·004	·003	·003	S <sub>6</sub>
S <sub>8</sub>	·002	·002	·001	·002	·000	·001	·003	·002	S <sub>8</sub>
M <sub>1</sub>	·024	·036	·086	·065	·045	·067	·125	·050	M <sub>1</sub>
M <sub>2</sub>	3·991	4·041	4·065	4·058	4·014	4·037	4·071	4·072	M <sub>2</sub>
M <sub>3</sub>	0·074	0·067	0·068	0·055	0·060	0·061	0·064	0·079	M <sub>3</sub>
M <sub>4</sub>	·119	·129	·120	·126	·124	·134	·126	·121	M <sub>4</sub>
M <sub>6</sub>	·014	·015	·002	·017	·008	·012	·011	·010	M <sub>6</sub>
M <sub>8</sub>	·003	·004	·002	·004	·005	·007	·008	·007	M <sub>8</sub>
O	·643	·650	·663	·647	·645	·663	·676	·682	O
K <sub>1</sub>	1·384	1·391	1·393	1·398	1·398	1·393	1·401	1·398	K <sub>1</sub>
K <sub>2</sub>	0·412	0·394	0·427	0·431	0·388	0·383	0·435	0·415	K <sub>2</sub>
P	·404	·400	·406	·403	·396	·391	·416	·415	P
J	·043	·083	·128	·122	·067	·109	·143	·099	J
Q	·122	·138	·159	·133	·101	·129	·147	·132	Q
L	·122	·054	·128	·094	·143	·032	·079	·041	L
N	1·024	1·036	·991	·974	·988	·988	·978	·995	N
λ	0·051	0·023	·030	·013	·043	·044	·017	·004	λ
ν	·288	·245	·078	·121	·261	·276	·145	·052	ν
μ	·231	·189	·214	·182	·212	·200	·183	·180	μ
R	...	·046	...	·037	...	·046	...	·029	R
T	...	·086	...	·256	...	·120	...	·237	T
MS	·122	·138	·126	·125	·134	·157	·137	·135	MS
2SM	·039	·025	·048	·036	·033	·036	·049	·046	2SM
2N	·167	·112	·135	·193	·165	·110	·142	·153	2N
M <sub>2</sub> N	·162	·104	·103	·102	·115	·124	·070	·130	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	·083	·039	·027	·084	·090	·034	·030	·103	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	·041	·040	·048	·064	·065	·070	·080	·065	2M <sub>2</sub> K <sub>1</sub>
Mm	·058	·049	·042	·047	·085	·063	·034	·026	Mm
Mf	·068	·054	·054	·029	·052	·046	·046	·083	Mf
MSf	·056	·016	·042	·019	·023	·044	·053	·052	MSf
Sa	·254	·137	·173	·188	·179	·032	·062	·042	Sa
Ssa	·068	·124	·071	·201	·145	·157	·099	·042	Ssa

*Values of H's at Apollo Bandar, Bombay—(Continued).*

TIDE	H							TIDE
	1886	1887	1888	1889	1890	1891	1892	
	Feet	Feet	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0·059	0·055	0·067	0·065	0·073	0·073	0·081	S <sub>1</sub>
S <sub>2</sub>	1·628	1·610	1·631	1·631	1·581	1·567	1·576	S <sub>2</sub>
S <sub>4</sub>	0·011	0·011	0·010	0·003	0·018	0·016	0·016	S <sub>4</sub>
S <sub>6</sub>	·003	·003	·005	·001	·003	·003	·004	S <sub>6</sub>
S <sub>8</sub>	·002	·002	·001	·002	·002	·001	·003	S <sub>8</sub>
M <sub>1</sub>	·003	·048	·053	·047	·029	·056	·069	M <sub>1</sub>
M <sub>2</sub>	4·041	4·040	4·069	4·040	4·027	4·037	4·038	M <sub>2</sub>
M <sub>3</sub>	0·079	0·080	0·076	0·055	0·056	0·058	0·057	M <sub>3</sub>
M <sub>4</sub>	·140	·122	·135	·143	·145	·139	·146	M <sub>4</sub>
M <sub>6</sub>	·006	·012	·010	·006	·006	·006	·013	M <sub>6</sub>
M <sub>8</sub>	·005	·005	·005	·003	·001	·002	·003	M <sub>8</sub>
O	·657	·653	·660	·668	·666	·660	·659	O
K <sub>1</sub>	1·405	1·395	1·388	1·398	1·402	1·403	1·408	K <sub>1</sub>
K <sub>2</sub>	0·364	0·402	0·427	0·407	0·383	0·408	0·418	K <sub>2</sub>
P	·404	·409	·417	·416	·409	·411	·424	P
J	·048	·093	·136	·118	·067	·118	·142	J
Q	·133	·149	·174	·147	·127	·140	·147	Q
L	·095	·031	·104	·076	·136	·143	·038	L
N	1·001	1·026	1·035	1·010	·976	·993	·974	N
λ	...	...	...	...	...	...	...	λ
ν	0·210	0·295	0·211	0·040	·145	·271	·257	ν
μ	·185	·218	·173	·201	·189	·252	·195	μ
R	...	...	...	...	...	...	...	R
T	...	·138	·239	·199	·057	·152	·237	T
MS	·137	·149	·127	·159	·158	·155	·141	MS
2SM	·029	·027	·043	·047	·035	·046	·047	2SM
2N	·182	·145	·180	·121	·160	·140	·182	2N
M <sub>2</sub> N	·096	·143	·064	·147	·093	·155	·056	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	·098	·053	·026	·089	·091	·030	·047	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	·062	·037	·046	·054	·072	·075	·087	2M <sub>2</sub> K <sub>1</sub>
Mm	·045	·064	·034	·067	·088	·042	·071	Mm
Mf	·061	·015	·071	·038	·017	·050	·049	Mf
MSf	·036	·020	·016	·037	·012	·048	·056	MSf
Sa	·110	·121	·079	·072	·086	·057	·076	Sa
Ssa	·176	·205	·174	·105	·244	·062	·132	Ssa



## TIDAL OBSERVATIONS.

*Values of  $\kappa$ 's at Apollo Bandar, Bombay.*

TIDE	$\kappa$								TIDE
	1878	1879	1880	1881	1882	1883	1884	1885	
	o	o	o	o	o	o	o	o	
S <sub>1</sub>	186.71	184.28	182.22	178.60	178.80	164.80	173.14	168.44	S <sub>1</sub>
S <sub>3</sub>	2.54	2.42	3.64	3.33	3.79	2.44	1.48	2.87	S <sub>3</sub>
S <sub>4</sub>	256.52	235.45	238.96	314.62	233.13	5.19	359.18	325.31	S <sub>4</sub>
S <sub>6</sub>	194.74	178.53	140.39	160.35	182.49	193.09	169.05	184.09	S <sub>6</sub>
S <sub>8</sub>	86.19	195.95	151.39	69.44	71.57	53.97	123.69	105.52	S <sub>8</sub>
M <sub>1</sub>	46.19	104.90	51.32	18.71	26.12	77.25	54.86	69.17	M <sub>1</sub>
M <sub>2</sub>	330.11	329.24	329.72	330.66	330.03	328.84	328.38	329.83	M <sub>2</sub>
M <sub>3</sub>	32.10	27.92	25.33	11.10	20.56	24.85	25.35	34.26	M <sub>3</sub>
M <sub>4</sub>	319.69	326.57	314.49	323.51	327.91	326.24	319.68	327.40	M <sub>4</sub>
M <sub>6</sub>	129.57	110.06	78.90	112.87	124.14	83.41	58.13	95.67	M <sub>6</sub>
M <sub>8</sub>	315.99	346.72	312.85	12.97	46.28	351.34	356.81	23.81	M <sub>8</sub>
O	47.99	48.39	47.53	47.53	48.75	47.92	48.16	47.88	O
K <sub>1</sub>	45.75	44.94	45.17	45.12	45.40	44.94	44.90	45.58	K <sub>1</sub>
K <sub>2</sub>	348.54	352.97	354.60	352.54	350.98	354.77	351.07	346.37	K <sub>2</sub>
P	42.31	42.95	43.53	42.23	41.07	44.65	43.84	43.24	P
J	89.12	48.04	61.54	88.09	73.92	40.12	51.97	86.05	J
Q	47.36	60.14	54.73	45.88	50.45	59.38	49.41	35.75	Q
L	299.44	348.38	325.09	306.43	298.18	241.72	328.33	305.05	L
N	311.95	315.21	316.03	314.69	312.23	313.57	312.19	312.50	N
$\lambda$	284.22	253.64	157.31	202.54	276.99	265.57	141.25	95.28	$\lambda$
$\nu$	319.39	283.16	268.52	8.78	335.86	295.75	261.53	12.92	$\nu$
$\mu$	313.00	293.91	314.24	301.06	317.65	293.72	308.10	295.38	$\mu$
R	...	300.59	...	265.00	...	291.97	...	226.82	R
T	...	45.78	...	2.45	...	52.12	...	349.50	T
MS	16.71	30.01	22.73	25.44	25.31	26.82	21.80	21.01	MS
2SM	91.12	124.67	112.30	109.24	93.99	116.00	112.89	99.97	2SM
2N	290.64	289.38	297.58	252.74	287.98	290.68	298.50	245.94	2N
M <sub>2</sub> N	272.04	251.39	311.31	217.90	287.65	266.15	318.00	237.45	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	184.36	238.41	53.75	128.22	176.54	214.96	74.66	130.58	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	66.29	72.21	76.60	89.38	79.67	70.33	55.29	50.86	2M <sub>2</sub> K <sub>1</sub>
Mm	314.52	355.46	86.07	55.55	36.16	93.89	23.18	63.58	Mm
Mf	346.11	6.76	0.52	250.35	47.42	333.44	2.84	49.34	Mf
MSf	197.66	287.47	183.96	333.58	135.67	190.40	186.96	268.04	MSf
Sa	116.57	329.58	312.56	316.59	355.41	284.65	326.49	98.85	Sa
Ssa	304.35	223.28	162.31	232.34	218.18	185.89	209.22	221.16	Ssa

*Values of  $\kappa$ 's at Apollo Bandar, Bombay—(Continued).*

TIDE	$\kappa$							TIDE
	1886	1887	1888	1889	1890	1891	1892	
	o	o	o	o	o	o	o	
S <sub>1</sub>	186.18	191.93	186.74	195.38	201.51	201.63	206.66	S <sub>1</sub>
S <sub>2</sub>	3.01	1.88	2.28	3.01	6.16	5.56	5.15	S <sub>2</sub>
S <sub>4</sub>	251.57	283.64	305.22	209.54	180.96	220.53	148.23	S <sub>4</sub>
S <sub>6</sub>	259.88	173.89	158.81	120.26	222.27	184.09	162.41	S <sub>6</sub>
S <sub>8</sub>	108.44	149.54	196.70	222.51	166.76	221.63	115.56	S <sub>8</sub>
M <sub>1</sub>	274.53	103.01	37.96	354.58	334.75	74.50	37.76	M <sub>1</sub>
M <sub>2</sub>	329.56	328.66	329.55	331.00	331.85	331.56	331.05	M <sub>2</sub>
M <sub>3</sub>	25.01	34.18	31.95	16.39	24.40	16.16	18.23	M <sub>3</sub>
M <sub>4</sub>	323.65	323.93	319.43	337.48	332.48	340.39	336.28	M <sub>4</sub>
M <sub>6</sub>	50.94	123.50	80.43	107.48	46.93	109.78	83.97	M <sub>6</sub>
M <sub>8</sub>	352.03	34.56	28.88	344.93	168.89	340.22	29.64	M <sub>8</sub>
O	47.91	46.95	48.76	48.99	48.06	47.22	48.42	O
K <sub>1</sub>	45.30	45.09	45.11	45.38	45.77	45.69	45.83	K <sub>1</sub>
K <sub>2</sub>	351.81	0.27	353.13	348.04	358.55	1.00	355.05	K <sub>2</sub>
P	44.13	44.96	46.00	45.00	45.59	45.81	45.00	P
J	90.07	42.17	64.05	90.93	77.17	44.59	58.09	J
Q	39.89	52.76	50.00	44.37	51.82	58.90	49.32	Q
L	322.94	250.97	342.60	323.30	321.26	276.07	305.94	L
N	311.89	312.22	315.45	316.35	317.14	315.06	315.76	N
$\lambda$	...	...	...	...	...	...	...	$\lambda$
$\nu$	348.41	310.32	272.90	245.85	5.72	326.94	289.56	$\nu$
$\mu$	317.08	293.75	306.94	292.47	320.59	301.17	306.45	$\mu$
R	...	...	...	...	...	...	...	R
T	...	52.06	19.71	344.79	350.84	49.19	17.30	T
MS	23.26	27.98	19.42	33.59	39.10	42.58	40.87	MS
2SM	98.17	124.05	103.57	90.96	115.83	131.82	103.50	2SM
2N	278.31	288.86	307.43	245.87	272.79	287.10	304.25	2N
M <sub>2</sub> N	291.94	279.12	325.37	256.73	307.53	299.68	311.04	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	180.73	236.45	62.62	122.97	167.44	187.70	108.47	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	49.11	53.68	75.37	93.23	92.81	89.90	83.58	2M <sub>2</sub> K <sub>1</sub>
Mm	283.67	120.88	20.53	226.78	262.98	356.47	269.93	Mm
Mf	63.66	331.70	297.46	348.22	17.82	41.84	3.89	Mf
MSf	198.20	72.49	325.41	188.29	338.77	91.87	308.88	MSf
Sa	16.53	318.34	330.49	346.10	358.62	311.74	120.03	Sa
Ssa	147.71	187.20	190.46	181.50	209.56	236.71	181.42	Ssa

## PRINCE'S DOCK, BOMBAY.

(*Tidal Observatory, Lat. 18° 57' N., Long. 72° 50' E.*)

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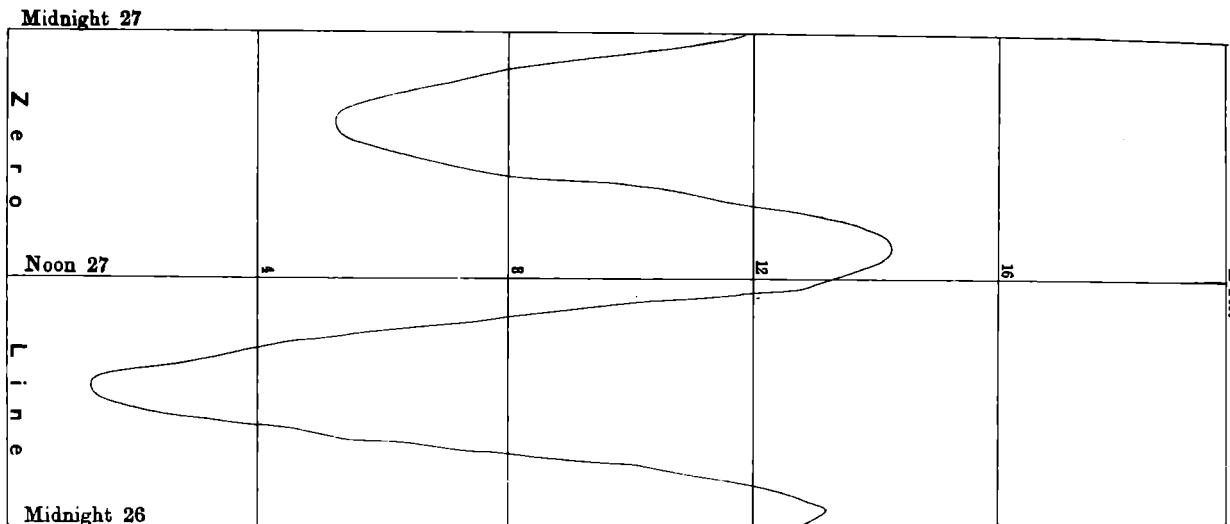
The tidal observatory at Prince's Dock, Bombay, is classed as one of the minor observatories at which five years' observations are generally considered sufficient; but its utility to the port is so great that it seems likely to be kept up indefinitely. It is placed in the light-house tower, a solid masonry structure situated on the pier between the entrances to Prince's Dock, in the position shown on the accompanying chart. A space for the reception of the float-cylinder and a connection with the sea were arranged for in building the pier: the space, twelve feet in diameter and twenty-nine feet deep, forms a well, the walls of which carry the light-house tower: a horizontal communication shaft one foot in diameter and twenty-four feet long leaves the well about three feet above the bottom and passes straight into deep water, between five and six feet below the lowest recorded tides. The float-cylinder is of iron, about twenty-two inches in diameter and twenty-four feet long, which gives ample range for extreme tides. It is supported in the centre of the well by transverse rails built into the walls, its upper end rising two feet above the mouth of the well and its lower end, which is open, being seven feet above the bottom.

The working scale of the tide-gauge is one-twelfth.

Registrations were commenced on the 22nd September, 1888, and, if those taken during the first four months (which were rather frequently interrupted) be excepted, have been highly satisfactory. Such few and unimportant interruptions as have occurred subsequently have generally been due to slight imperfections of the gauge, which is a small one, with upright recording drum, of a less practical design than that of the gauges used at all other Indian tidal observatories, which are of Newman's pattern with long horizontal drum.

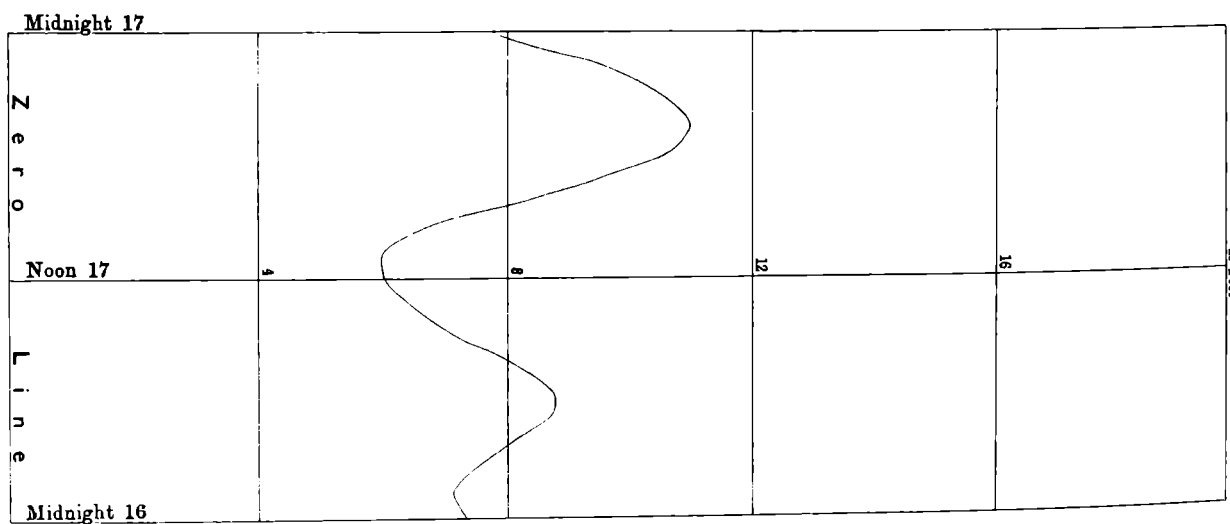
**TIDAL CURVES**  
at  
**PRINCE'S DOCK, BOMBAY**

Spring Tide — 27th April 1891



Full Moon — 24th April 1891

Neap Tide — 17th April 1891



First Quarter — 16th April 1891

*Photocincographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun. July 1899.*

Barometrical and anemometrical observations are dispensed with at this tidal observatory, as those taken at the neighbouring Meteorological Observatory at Colába supply the necessary statistics.

The bench-mark of reference is the Standard Bench-mark situated at the Public Works Secretariat, consisting of a three-foot cube of polished granite, the top surface of which is the plane of reference. It is 28·000 feet above the zero of the gauge.

The establishment of the Port calculated according to the method employed by the Marine Survey of India = XI<sup>h</sup> 28<sup>m</sup>.

The highest high water recorded was 17·0 feet above the zero of the gauge, and occurred in December, 1889.

The lowest low water recorded was 1·6 feet *below* the zero of the gauge, and occurred in November, 1892.

In 1891 the mean range of largest ordinary springs was found to be 13·9 feet.

The height of mean-sea-level above the zero of the gauge had the following values:—

1888-89	...	...	...	8·306 feet.
1889	...	...	...	8·285 „
1890	...	...	...	8·329 „
1891	...	...	...	8·226 „
1892	...	...	...	8·386 „

NOTE.—The level of the zero of the gauge at Prince's Dock is 2·000 feet above that of the zero of the gauge at Apollo Bandar.

The observatory was inspected in January, 1892, and the following remarks were made on the design and working of the tide-gauge:—

“As the float-band is a very long and thin copper ribbon, it is apt to twist. Much inconvenience is caused by the tearing of the diagram paper by the zero pencil. The arrangement of this pencil must be changed. Its position is between the recording drum over which the diagram paper passes and the cylindrical roll from which that paper unwinds. It therefore acts on a part of the paper which is not supported behind. As the unwinding roll pays out the paper, the diameter of the roll diminishes, and the unsupported surface of the paper comes gradually forward and presses more and more on the point of the zero pencil, until at last a tear is made. This pattern of tide-gauge appears inferior to that in general use at Indian tidal observatories (Newman's pattern with long horizontal drum). It is more complicated and liable to get out of order. It is not so easily cleaned. The scale on which it registers the tidal curve is small and cannot be changed. The float-band, pencil-wire and some other parts are too frail. There is no arrangement for adjusting the height of the curve-recording pencil; so that setting to zero is both troublesome and tedious. Measurements cannot be taken from the diagram while the instrument is working, as may often be desired. Interruptions to the registrations, damage to the diagram paper, such as tears caused by the zero pencil, etc., may not become known until the paper is removed, for the faulty or damaged parts may have been rolled up on the receiving cylinder and have become concealed during the absence of the clerk from the observatory.”

*Values of H's at Prince's Dock, Bombay.*

TIDE	H					TIDE
	1888-89	1889	1890	1891	1892	
	<i>Feet</i>	<i>Feet</i>	<i>Feet</i>	<i>Feet</i>	<i>Feet</i>	
S <sub>1</sub>	0·052	0·067	0·086	0·083	0·092	S <sub>1</sub>
S <sub>2</sub>	1·656	1·644	1·640	1·605	1·614	S <sub>2</sub>
S <sub>3</sub>	0·015	0·013	0·030	0·027	0·017	S <sub>3</sub>
S <sub>6</sub>	·005	·007	·003	·004	·003	S <sub>6</sub>
S <sub>8</sub>	·002	·002	·002	·001	·002	S <sub>8</sub>
M <sub>1</sub>	·023	·052	·033	·057	·070	M <sub>1</sub>
M <sub>2</sub>	4·095	4·115	4·102	4·106	4·112	M <sub>2</sub>
M <sub>3</sub>	0·082	0·067	0·061	0·067	0·068	M <sub>3</sub>
M <sub>4</sub>	·128	·126	·134	·113	·128	M <sub>4</sub>
M <sub>6</sub>	·002	·006	·007	·015	·011	M <sub>6</sub>
M <sub>8</sub>	·006	·005	·004	·003	·005	M <sub>8</sub>
O	·662	·680	·651	·649	·654	O
K <sub>1</sub>	1·387	1·390	1·397	1·395	1·404	K <sub>1</sub>
K <sub>2</sub>	0·410	0·421	0·388	0·403	0·421	K <sub>2</sub>
P	·379	·410	·411	·403	·423	P
J	·069	·123	·063	·114	·146	J
Q	·135	·150	·124	·145	·145	Q
L	·113	·068	·148	·184	·045	L
N	1·013	1·004	·986	1·001	·993	N
λ	...	...	...	...	...	λ
ν	0·347	0·097	·148	0·272	·257	ν
μ	·245	·204	·192	·250	·204	μ
R	...	...	...	...	...	R
T	...	·173	·051	·153	·243	T
MS	·158	·154	·138	·139	·179	MS
2SM	·044	·037	·039	·047	·056	2SM
2N	·198	·142	·164	·147	·185	2N
M <sub>2</sub> N	·090	·137	·092	·152	·053	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	·110	·086	·086	·027	·032	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	·048	·052	·067	·069	·081	2M <sub>2</sub> K <sub>1</sub>
Mm	·025	·063	·079	·054	·069	Mm
Mf	·049	·052	·023	·057	·055	Mf
MSf	·020	·020	·030	·062	·049	MSf
Sa	·076	·091	·083	·105	·057	Sa
Ssa	·130	·122	·239	·065	·134	Ssa

*Values of  $\kappa$ 's at Prince's Dock, Bombay.*

TIDE	$\kappa$					TIDE
	1888-89	1889	1890	1891	1892	
	°	°	°	°	°	
S <sub>1</sub>	153·39	189·72	204·20	198·89	200·59	S <sub>1</sub>
S <sub>2</sub>	1·23	0·99	3·99	3·80	4·14	S <sub>2</sub>
S <sub>4</sub>	204·70	209·91	202·87	220·44	176·06	S <sub>4</sub>
S <sub>6</sub>	279·09	301·76	206·57	204·44	185·53	S <sub>6</sub>
S <sub>8</sub>	141·71	189·46	262·57	172·88	81·03	S <sub>8</sub>
M <sub>1</sub>	113·89	342·17	319·55	73·95	36·80	M <sub>1</sub>
M <sub>2</sub>	328·62	329·44	329·62	329·22	329·38	M <sub>2</sub>
M <sub>3</sub>	32·44	24·15	26·33	12·51	17·52	M <sub>3</sub>
M <sub>4</sub>	329·94	330·55	320·81	329·60	326·29	M <sub>4</sub>
M <sub>6</sub>	2·43	162·18	211·48	170·53	122·87	M <sub>6</sub>
M <sub>8</sub>	76·98	36·04	85·18	85·59	74·58	M <sub>8</sub>
O	48·34	48·18	47·29	45·86	47·76	O
K <sub>1</sub>	44·14	44·65	44·77	44·28	44·93	K <sub>1</sub>
K <sub>2</sub>	1·96	353·50	358·01	359·64	354·41	K <sub>2</sub>
P	42·95	43·37	43·88	44·05	44·22	P
J	85·54	97·44	78·21	46·56	57·40	J
Q	54·95	42·37	53·31	58·39	49·01	Q
L	284·75	291·50	326·56	271·83	278·05	L
N	311·61	313·37	314·32	314·18	314·88	N
$\lambda$	...	...	...	...	...	$\lambda$
$\nu$	321·83	280·40	1·91	326·19	289·59	$\nu$
$\mu$	307·79	303·80	319·05	303·31	309·38	$\mu$
R	...	...	...	...	...	R
T	...	319·93	339·65	46·93	13·02	T
MS	29·97	31·99	35·27	42·79	33·66	MS
2SM	74·27	41·71	122·77	120·43	104·68	2SM
2N	258·96	244·02	266·58	287·51	304·04	2N
M <sub>2</sub> N	58·16	258·80	302·98	300·10	318·94	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	152·22	136·92	176·46	212·40	93·43	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	62·89	79·23	84·83	81·80	79·65	2M <sub>2</sub> K <sub>1</sub>
Mm	297·68	229·72	265·35	1·10	274·41	Mm
Mf	344·23	345·69	10·18	36·52	5·83	Mf
MSf	116·96	159·51	27·21	65·40	324·98	MSf
Sa	283·61	330·18	339·21	314·06	132·36	Sa
Ssa	133·91	177·90	208·96	203·13	176·16	Ssa

## MORMUGÁO.

(*Tidal Observatory, Lat. 15° 25' N., Long. 73° 48' E.*)

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The tidal observatory at the Portuguese port of Mormugáo, near Goa, was one of the minor observatories, at which five years' observations are generally sufficient, and was situated on the south side of the iron jetty of the Harbour Works in the position shown on the accompanying chart. The observatory (a small wooden cabin) and the cylinder and tide-gauge, &c., had previously been in use at Kárwár, but the instruments were modified and improved before erection at Mormugáo. The floor of the observatory, which was supported on four wooden piles driven twelve feet into the ground, was on a level with and braced to the platform of the jetty. The float-cylinder, which was eighteen feet long, was fixed with its upper end about four feet below the floor, and this interval was filled by a wooden frame of nineteen and a half inches square section. The top of the cylinder was about five feet above the highest tides and the bottom six feet below the lowest. The communication was by seven small holes drilled about eighteen inches above the bottom of the cylinder which was closed by an iron plate.

The working scale of the tide-gauge was one-half.

Registrations were commenced on the 14th March, 1884, and were continued most satisfactorily, with very few and insignificant interruptions, till the 27th March, 1889, when the observatory was dismantled.



73° 47'

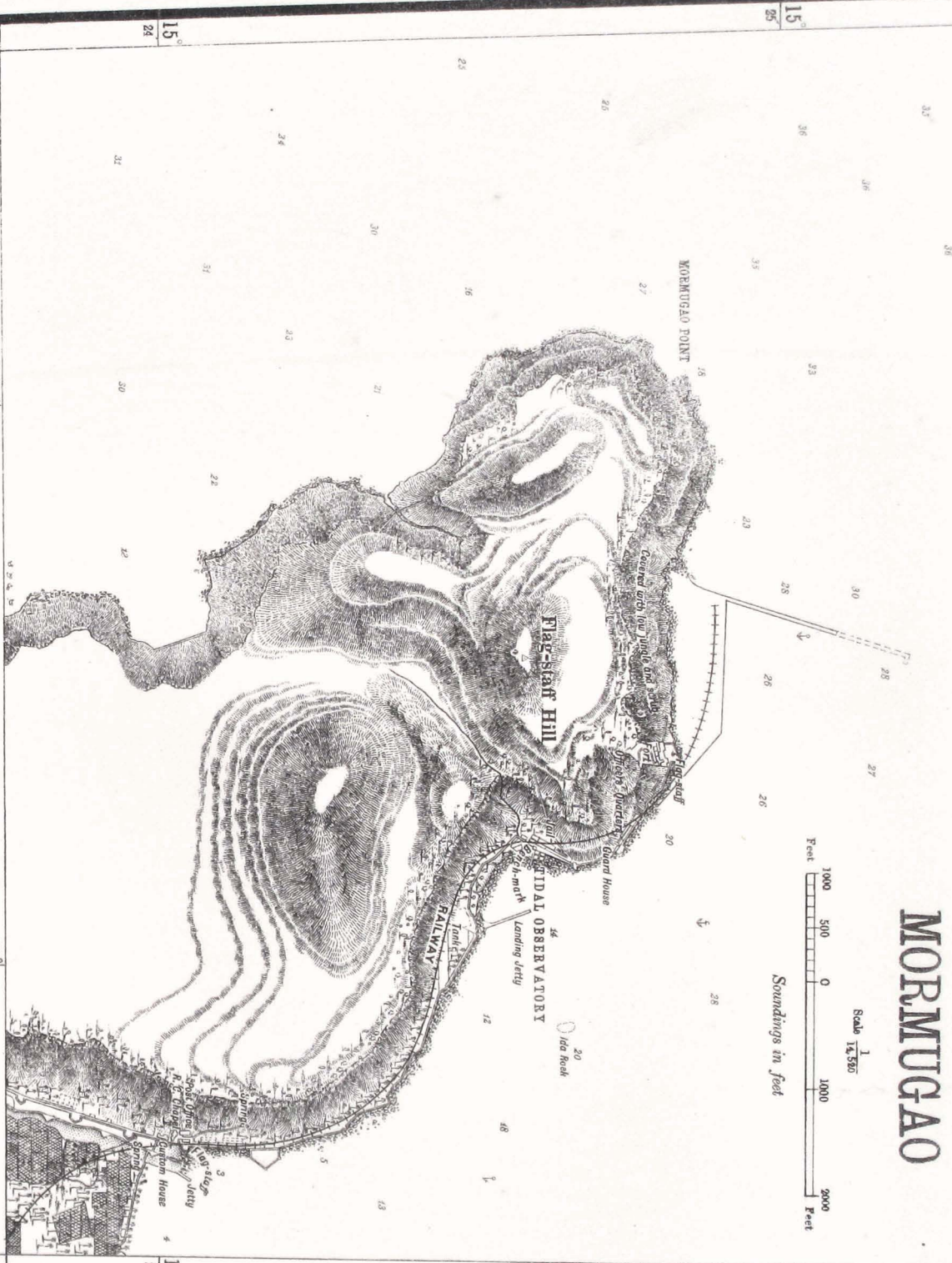
73° 48'

# MORMUGAO

Scale  $\frac{1}{14,520}$



Soundings in feet



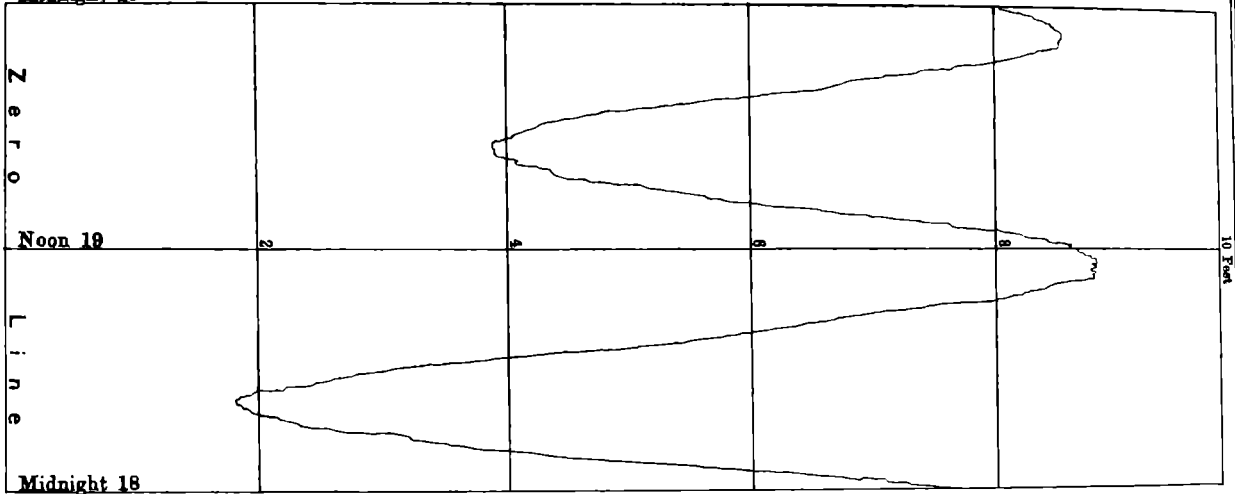
# TIDAL CURVES

at

## MORMUGAO

Spring Tide — 19th April 1886

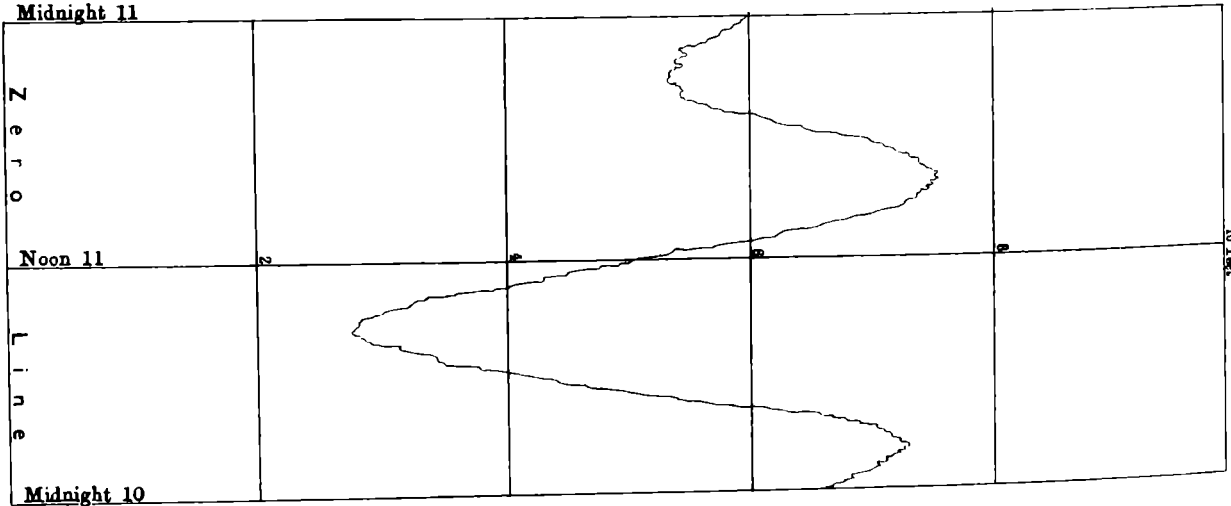
Midnight 19



Full Moon 18th April 1886

Neap Tide 11th April 1886

Midnight 11



First Quarter 11th April 1886

*Photoreproduced at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun, April 1900.*

Barometrical and anemometrical observations were carried on simultaneously with the tidal observations. The barometer was placed near the standard mercurial barometer in the verandah of the building known as the Palace. The anemometer was erected on the top of the fort above the Palace.

The bench-mark of reference is inscribed <sup>G.T.S.</sup> B. □ M. and embedded in masonry, about two and a half feet under the surface of the ground, and about nine feet west of the first embrasure of the old fort (counting from the jetty end) near the iron pile pier. It is 17·823 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = X<sup>h</sup> 33<sup>m</sup>.

The highest high water recorded was 9·9 feet above the zero of the gauge, and occurred in January, 1885.

The lowest low water recorded was 0·1 foot above the zero of the gauge, and occurred in May, 1884.

In 1886 the mean range of largest ordinary springs was found to be 6·8 feet.

The height of mean-sea-level above the zero of the gauge had the following values:—

1884-85	...	...	...	5·512 feet.
1885-86	...	...	...	5·577 „
1886-87	...	...	...	5·573 „
1887-88	...	...	...	5·486 „
1888-89	...	...	...	5·451 „

## TIDAL OBSERVATIONS.

*Values of H's at Mormugão.*

TIDE	H					TIDE
	1884-85	1885-86	1886-87	1887-88	1888-89	
	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0.080	0.041	0.047	0.046	0.050	S <sub>1</sub>
S <sub>2</sub>	.638	.641	.643	.638	.644	S <sub>2</sub>
S <sub>4</sub>	.008	.009	.008	.009	.010	S <sub>4</sub>
S <sub>6</sub>	.003	.005	.004	.005	.004	S <sub>6</sub>
S <sub>8</sub>	.003	.004	.003	.001	.004	S <sub>8</sub>
M <sub>1</sub>	.045	.055	.015	.017	.011	M <sub>1</sub>
M <sub>2</sub>	1.766	1.820	1.835	1.820	1.809	M <sub>2</sub>
M <sub>3</sub>	0.018	0.015	0.017	0.018	0.019	M <sub>3</sub>
M <sub>4</sub>	.041	.047	.051	.049	.049	M <sub>4</sub>
M <sub>6</sub>	.010	.013	.012	.014	.007	M <sub>6</sub>
M <sub>8</sub>	.012	.011	.017	.013	.012	M <sub>8</sub>
O	.516	.524	.520	.522	.522	O
K <sub>1</sub>	1.020	1.033	1.026	1.027	1.021	K <sub>1</sub>
K <sub>2</sub>	0.182	0.179	0.205	0.187	0.182	K <sub>2</sub>
P	.300	.305	.289	.300	.305	P
J	.061	.085	.075	.049	.056	J
Q	.099	.119	.111	.099	.112	Q
L	.030	.053	.039	.075	.050	L
N	.427	.438	.427	.434	.439	N
λ	.011	.014	...	...	...	λ
ν	.153	.104	.018	.084	.137	ν
μ	.062	.042	.058	.048	.064	μ
R	...	.006	...	...	...	R
T	...	.068	...	.073	.096	T
MS	.022	.028	.025	.016	.031	MS
2SM	.002	.003	.007	.007	.011	2SM
2N	.062	.069	.074	.050	.062	2N
M <sub>2</sub> N	.045	.057	.022	.068	.039	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	.019	.035	.039	.016	.020	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	.009	.006	.005	.008	.007	2M <sub>2</sub> K <sub>1</sub>
Mm	.048	.029	.015	.049	.010	Mm
Mf	.048	.075	.089	.027	.056	Mf
MSf	.021	.057	.041	.010	.025	MSf
Sa	.306	.165	.291	.356	.226	Sa
Ssa	.075	.055	.133	.191	.128	Ssa

*Values of  $\kappa$ 's at Mormugão.*

TIDE	$\kappa$					TIDE
	1884-85	1885-86	1886-87	1887-88	1888-89	
	o	o	o	o	o	
S <sub>1</sub>	157·27	177·47	171·52	181·50	184·93	S <sub>1</sub>
S <sub>2</sub>	336·75	332·23	330·54	330·05	329·36	S <sub>2</sub>
S <sub>4</sub>	108·91	99·97	89·25	86·96	76·10	S <sub>4</sub>
S <sub>6</sub>	119·75	109·89	127·48	114·34	101·04	S <sub>6</sub>
S <sub>8</sub>	94·57	24·44	30·58	45·00	43·92	S <sub>8</sub>
M <sub>1</sub>	97·69	98·02	43·12	31·94	97·64	M <sub>1</sub>
M <sub>2</sub>	305·20	300·10	299·36	299·18	297·80	M <sub>2</sub>
M <sub>3</sub>	307·67	299·19	295·64	289·25	283·85	M <sub>3</sub>
M <sub>4</sub>	20·58	5·62	5·60	2·38	357·30	M <sub>4</sub>
M <sub>6</sub>	260·96	245·04	254·19	237·94	249·18	M <sub>6</sub>
M <sub>8</sub>	24·42	19·98	16·29	29·47	22·91	M <sub>8</sub>
O	53·03	49·59	47·85	47·66	47·03	O
K <sub>1</sub>	48·07	45·78	44·84	44·76	44·48	K <sub>1</sub>
K <sub>2</sub>	324·00	331·45	324·14	315·57	320·87	K <sub>2</sub>
P	49·40	42·88	41·74	44·79	43·50	P
J	42·76	43·16	70·57	74·65	44·50	J
Q	64·02	51·56	41·80	45·16	56·55	Q
L	306·67	338·19	302·74	342·98	309·09	L
N	287·03	282·22	281·15	279·00	278·27	N
$\lambda$	323·22	102·50	...	...	...	$\lambda$
$\nu$	278·16	253·59	233·27	335·21	301·90	$\nu$
$\mu$	247·48	246·35	248·30	247·73	262·26	$\mu$
R	...	137·86	...	...	...	R
T	...	277·82	...	357·21	312·50	T
MS	59·73	67·22	44·40	28·80	39·70	MS
2SM	201·24	138·43	70·18	150·34	121·40	2SM
2N	238·89	263·34	238·87	228·82	228·49	2N
M <sub>2</sub> N	342·97	342·35	336·98	4·55	16·88	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	335·49	53·64	108·23	159·67	349·54	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	350·96	29·69	91·58	68·74	69·02	2M <sub>2</sub> K <sub>1</sub>
Mm	74·73	358·85	285·62	106·43	300·58	Mm
Mf	13·85	13·91	11·24	153·63	317·72	Mf
MSf	150·99	279·30	354·01	288·86	305·53	MSf
Sa	307·36	333·22	327·53	297·45	301·14	Sa
Ssa	162·57	67·51	147·38	175·30	139·58	Ssa

## K Á R W Á R .

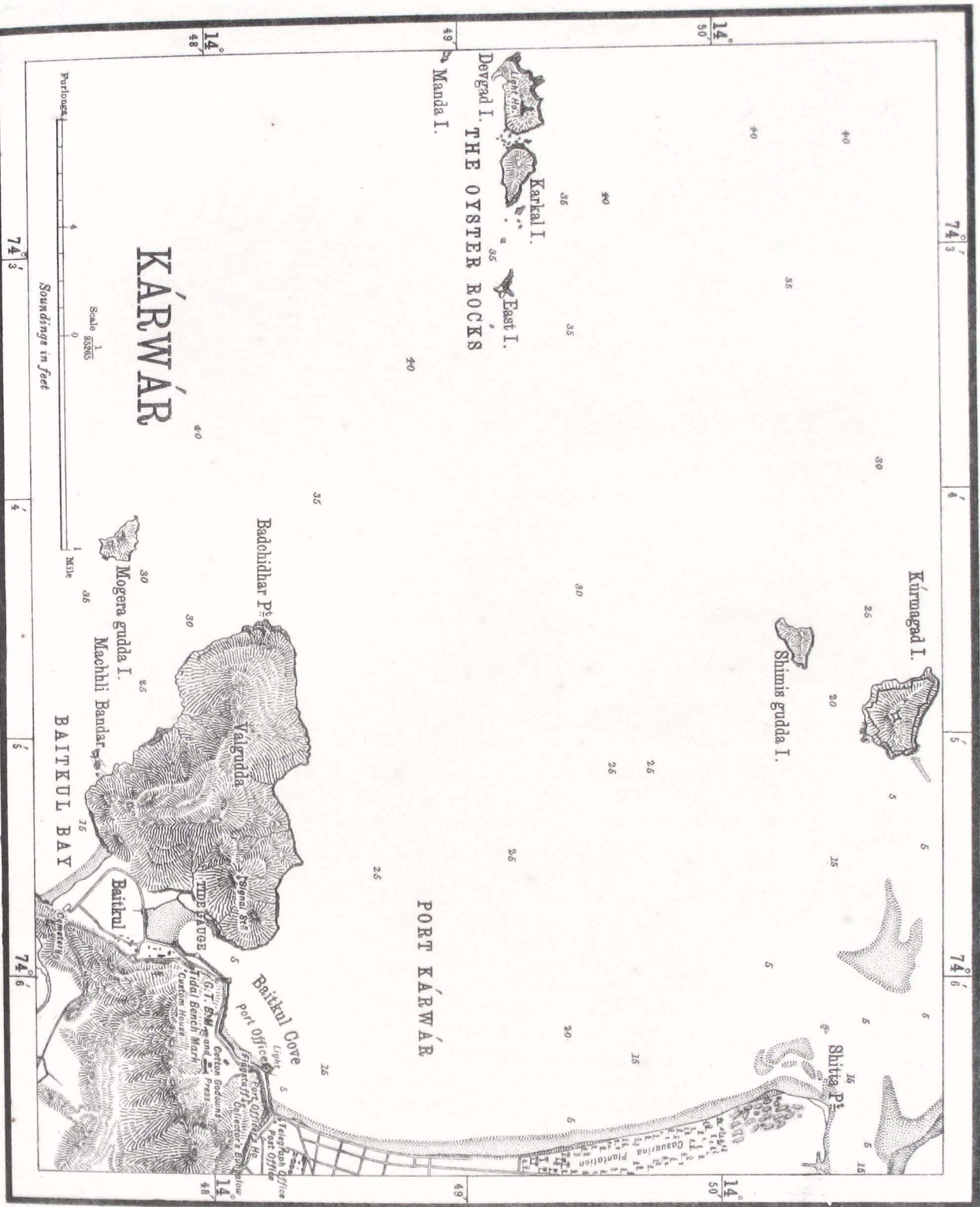
(*Tidal Observatory, Lat. 14° 48' N., Long. 74° 6' E.*)

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The tidal observatory at Kárwár in North Kánara on the west coast of India was one of the minor observatories, at which five years' observations are considered sufficient, and was situated on the east side of the Baitkul Cove, three feet away from the wharf wall, in the position shown on the accompanying chart. It was a wooden structure supported by four iron screw-piles. The float-cylinder, of wrought iron, about twenty-two inches in internal diameter, fourteen feet long, and closed at the bottom with an iron plate, descended through the floor of the observatory and was sunk to a depth of about one foot into the ground, there being never less than two feet of water within it or about a foot of water outside it even at the lowest tides. The communication, when the gauge was first set up, was through a short external pipe rising from the bottom length of the cylinder and bent so as to be horizontal at the top where a stop-cock, always under water, was placed, and whence about one hundred and twenty feet of two-inch piping was carried under water, ending in a rose supported some two or three feet above the bottom on a tripod, and having about five feet of water above it at the lowest tides. It was found that by this arrangement the flow of water was retarded, and in the second year the long communication pipe was consequently removed, the short bend attached to the cylinder being retained. The mouth of this bend was closed with a wooden plug perforated with a communication hole one inch in diameter.

The working scale of the tide-gauge was one-half.

Registrations were commenced on the 1st March, 1878, and were carried on without any break of importance until the 15th April, 1883.

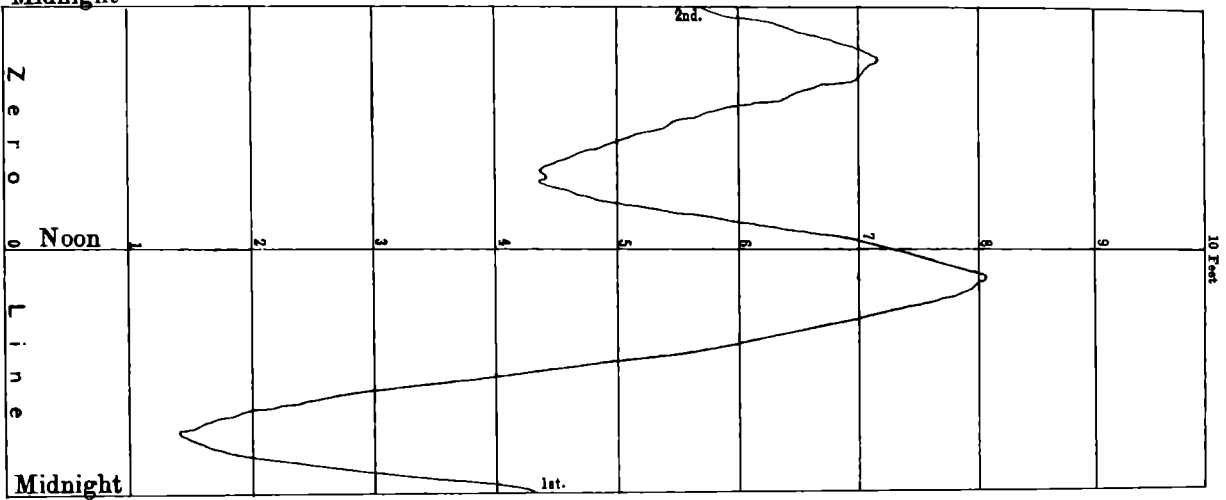


Hydrographic Survey of the Office of the Trigonometrical Branch, Survey of India, Dabra Dera, August 1894.

TIDAL CURVES  
at  
KÁRWÁR

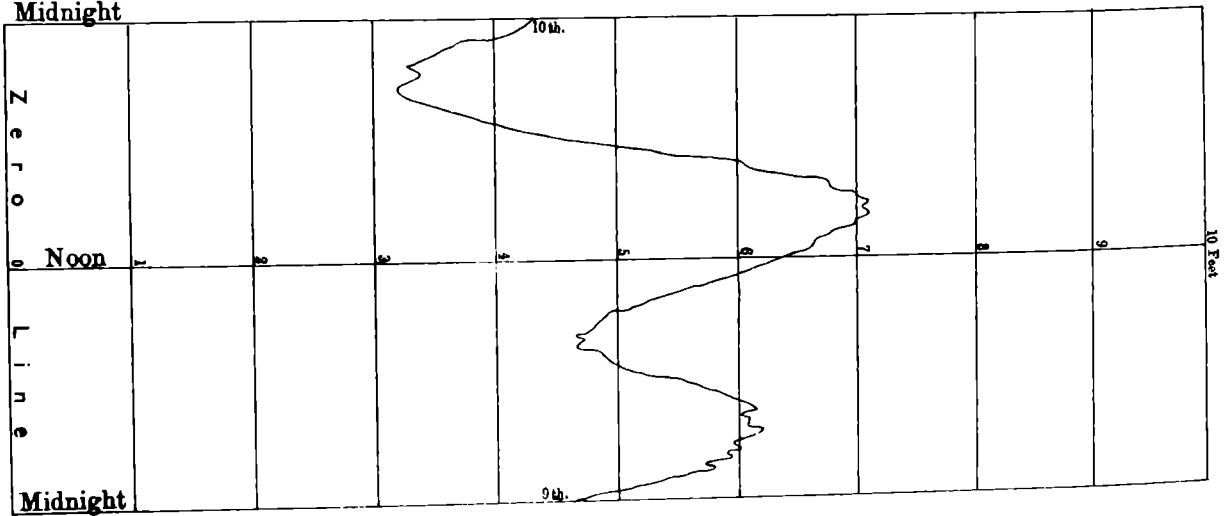
Spring Tide — 1st. August 1879.

Midnight



Neap Tide — 9th. August 1879.

Midnight

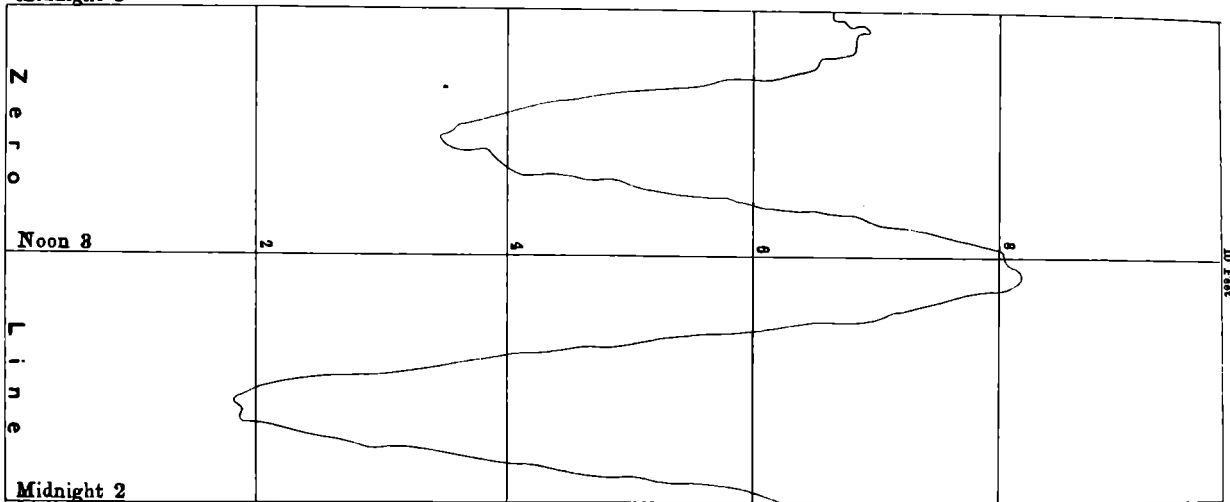




TIDAL CURVES  
at  
KÁRWÁR

Spring Tide — 3rd August 1879

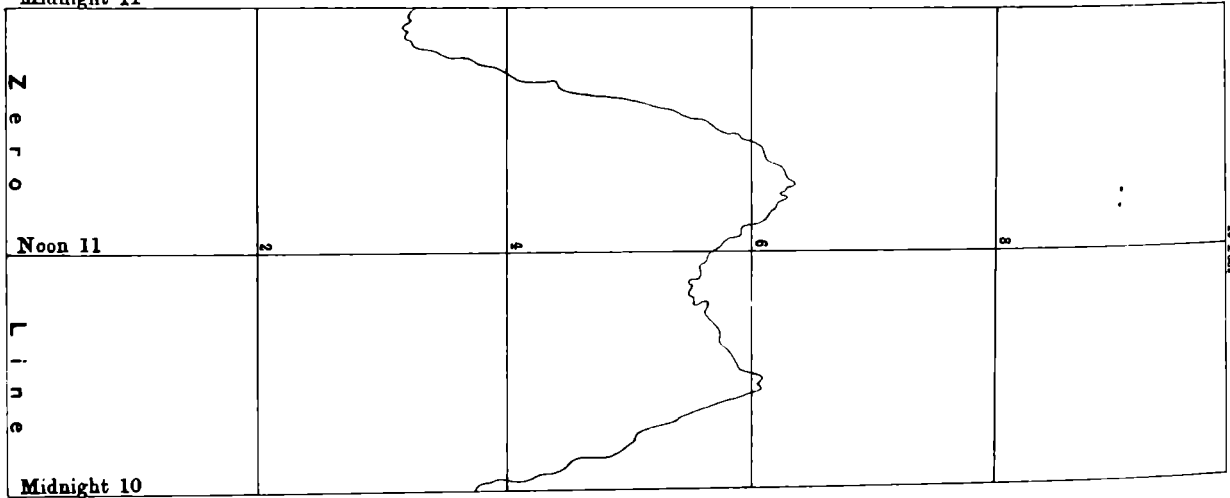
Midnight 3



Full Moon — 2nd August 1879

Neap Tide — 11th August 1879

Midnight 11



Last Quarter — 10th August 1879

*Photoincographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun, September 1899.*

The action of the tides at Baitkul Cove was peculiar. At rising tide the water would continue to rise in the cylinder for, say, twenty minutes; stop dead; fall for perhaps four or five minutes; rise steadily for half an hour, and then repeat what had happened before. A similar action took place at falling tide. It was not a pumping action in the cylinder due to roughness of the surface water, for on the calmest day the peculiar motion of the water was often most distinct. The cause of this action is obscure. It may perhaps be found in the shape of Baitkul Cove. The gentle currents caused to circulate by the ebb and flow of the tide round the margins of the cove may produce the vibrations observed, which appear to bear some resemblance to those noticed in other confined sheets of water, *e.g.* in the lake of Geneva, where there is a gentle flow of water through the lake.

Barometrical and anemometrical observations were carried on simultaneously with the tidal observations. The barometer was placed in the observatory, but as that site was not suitable for the anemometer, the latter instrument was placed about four miles off, on Devgad island, one of the Oyster Rocks, where the light-house is situated.

The bench-mark of reference is inscribed  $\begin{matrix} \text{G.T.S.} \\ \square \\ \text{B.M.} \end{matrix}$  and embedded in a block of masonry close to the Travellers' Bungalow. It is 17·324 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = X<sup>h</sup> 36<sup>m</sup>.

The highest high water recorded was 9·7 feet above the zero of the gauge, and occurred in January, 1882.

The lowest low water recorded was 0·2 feet above the zero of the gauge, and occurred in June, 1880.

In 1878-79 the mean range of largest ordinary springs was found to be 6·7 feet.

The height of mean-sea-level above the zero of the gauge had the following values:—

1878-79	...	...	...	5·650 feet.
1879-80	...	...	...	5·541 „
1880-81	...	...	...	5·564 „
1881-82	...	...	...	5·515 „
1882-83	...	...	...	5·492 „

## TIDAL OBSERVATIONS.

*Values of H's at Kárwár.*

TIDE	H					TIDE
	1878-79	1879-80	1880-81	1881-82	1882-83	
	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0·067	0·075	0·055	0·052	0·035	S <sub>1</sub>
S <sub>2</sub>	·631	·629	·621	·616	·625	S <sub>2</sub>
S <sub>4</sub>	·007	·007	·016	·011	·011	S <sub>4</sub>
S <sub>6</sub>	·002	·007	·004	·006	·006	S <sub>6</sub>
S <sub>8</sub>	·002	·002	·000	·002	·004	S <sub>8</sub>
M <sub>1</sub>	·019	·017	·049	·045	·036	M <sub>1</sub>
M <sub>2</sub>	1·724	1·733	1·757	1·754	1·741	M <sub>2</sub>
M <sub>3</sub>	0·012	0·014	0·018	0·012	0·012	M <sub>3</sub>
M <sub>4</sub>	·045	·059	·054	·059	·060	M <sub>4</sub>
M <sub>6</sub>	·013	·010	·013	·011	·009	M <sub>6</sub>
M <sub>8</sub>	·001	·003	·004	·002	·002	M <sub>8</sub>
O	·496	·498	·505	·494	·493	O
K <sub>1</sub>	1·001	·996	1·010	1·008	1·006	K <sub>1</sub>
K <sub>2</sub>	0·175	·174	0·164	0·175	0·180	K <sub>2</sub>
P	·269	·274	·282	·287	·274	P
J	·046	·078	·087	·064	·065	J
Q	·111	·133	·130	·101	·097	Q
L	·093	·041	·059	·038	·050	L
N	·416	·426	·413	·400	·397	N
λ	·022	·004	·032	·021	·021	λ
ν	·077	·136	·122	·057	·047	ν
μ	·033	·057	·046	·051	·033	μ
R	...	·006	...	·009	...	R
T	...	·046	...	·075	...	T
MS	·022	·028	·021	·029	·028	MS
2SM	·012	·004	·004	·007	·009	2SM
2N	·054	·050	·084	·043	·052	2N
M <sub>2</sub> N	·067	·063	·028	·068	·042	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	·017	·023	·034	·020	·010	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	·002	·008	·010	·011	·008	2M <sub>2</sub> K <sub>1</sub>
Mm	·046	·061	·048	·043	·126	Mm
Mf	·051	·058	·034	·038	·027	Mf
MSf	·029	·023	·021	·009	·030	MSf
Sa	·170	·344	·491	·383	·373	Sa
Ssa	·045	·083	·128	·053	·033	Ssa

*Values of  $\kappa$ 's at Kárvár.*

TIDE	$\kappa$					TIDE
	1878-79	1879-80	1880-81	1881-82	1882-83	
	°	°	°	°	°	
S <sub>1</sub>	158·71	148·57	156·16	164·75	167·47	S <sub>1</sub>
S <sub>2</sub>	335·49	336·44	333·98	333·29	334·73	S <sub>2</sub>
S <sub>4</sub>	114·66	87·36	84·37	109·55	91·64	S <sub>4</sub>
S <sub>6</sub>	31·61	57·53	82·24	51·34	39·14	S <sub>6</sub>
S <sub>8</sub>	343·61	295·46	296·57	282·53	302·91	S <sub>8</sub>
M <sub>1</sub>	70·05	45·49	28·59	10·24	48·45	M <sub>1</sub>
M <sub>2</sub>	303·21	303·34	300·55	300·87	300·72	M <sub>2</sub>
M <sub>3</sub>	279·86	285·59	275·29	263·62	260·70	M <sub>3</sub>
M <sub>4</sub>	28·20	22·11	11·48	16·37	7·26	M <sub>4</sub>
M <sub>6</sub>	288·51	282·53	277·11	283·85	287·36	M <sub>6</sub>
M <sub>8</sub>	210·08	50·95	8·76	58·37	215·12	M <sub>8</sub>
O	49·72	50·23	48·75	48·39	48·88	O
K <sub>1</sub>	46·55	46·56	44·66	44·33	44·85	K <sub>1</sub>
K <sub>2</sub>	329·58	328·70	327·07	333·49	329·56	K <sub>2</sub>
P	41·49	42·73	42·59	40·86	40·05	P
J	51·36	54·61	70·68	67·07	42·28	J
Q	57·10	61·56	54·03	58·23	62·86	Q
L	326·01	325·14	318·48	291·59	323·70	L
N	281·60	283·57	282·57	281·16	279·48	N
$\lambda$	243·58	122·14	28·65	340·85	268·47	$\lambda$
$\nu$	339·76	296·95	260·60	232·42	338·36	$\nu$
$\mu$	283·28	244·88	260·00	244·24	284·47	$\mu$
R	...	61·03	...	229·83	...	R
T	...	9·46	...	300·28	...	T
MS	80·36	75·49	60·64	59·79	59·77	MS
2SM	30·76	353·33	14·58	106·45	351·28	2SM
2N	238·25	249·05	239·63	252·12	241·42	2N
M <sub>2</sub> N	209·78	184·05	183·19	156·13	208·87	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	270·35	15·49	89·46	151·59	338·28	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	83·44	120·14	87·98	67·41	44·24	2M <sub>2</sub> K <sub>1</sub>
Mm	350·58	14·28	99·91	0·47	31·69	Mm
Mf	345·14	0·82	345·59	14·42	37·39	Mf
MSf	213·90	267·52	221·88	89·22	26·66	MSf
Sa	321·95	307·25	302·72	302·56	317·09	Sa
Ssa	296·82	201·81	191·21	224·01	225·45	Ssa

## BEYPORE.

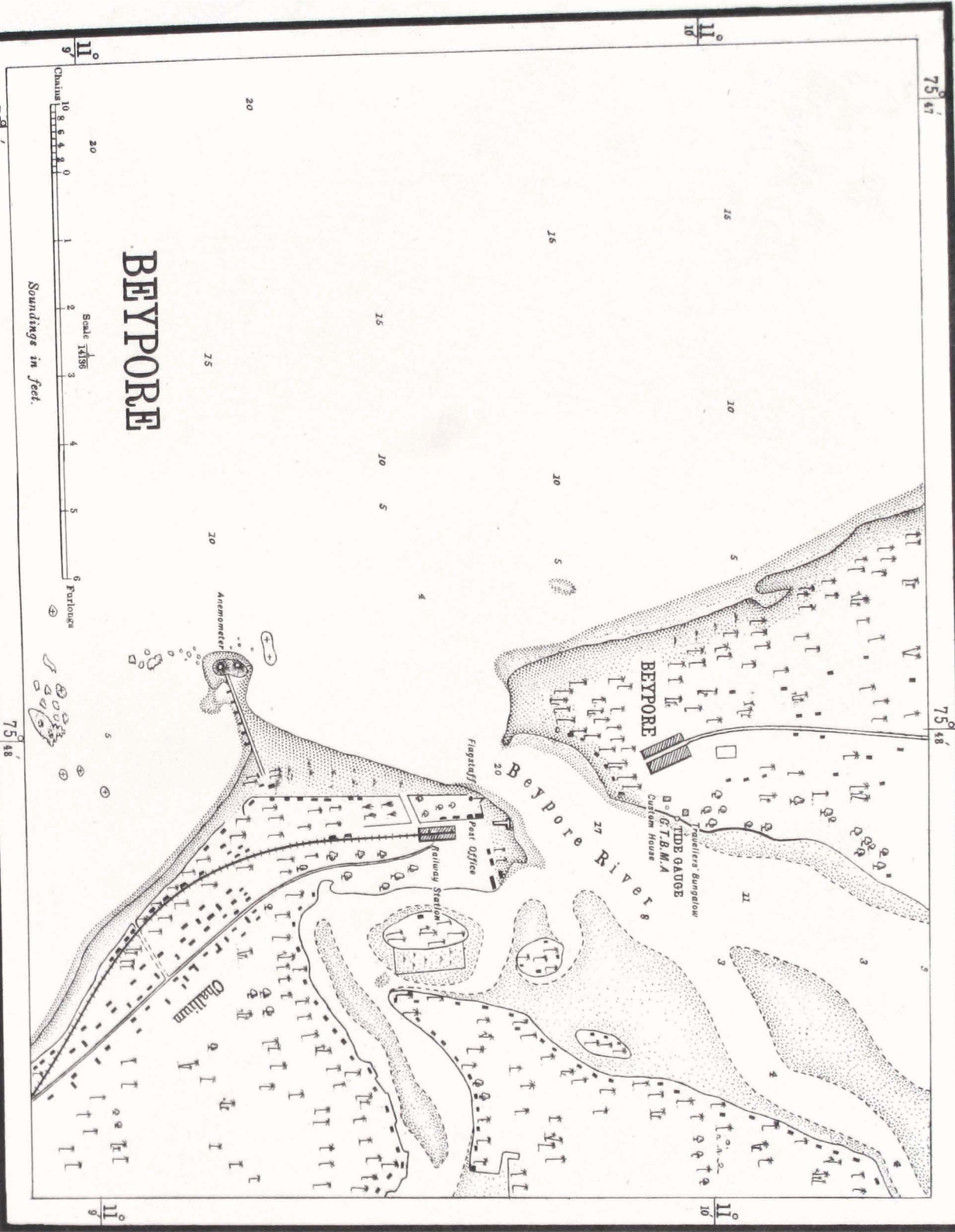
*(Tidal Observatory, Lat. 11° 10' N., Long. 75° 48' E.)*

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The tidal observatory at Beypore, about seven miles south of Calicut, on the west coast of India, was one of the minor observatories at which five years' observations are generally considered sufficient, and was situated on the northern bank of the Back-water about fifty yards south of the Travellers' Bungalow and some six hundred yards from the open sea, in the position shown on the accompanying chart. It was a wooden cabin supported partly on piles and partly on the wall of a former wharf. The iron float-cylinder, twenty-four inches in diameter and about sixteen feet long, was sunk about twelve feet into the bank of the Back-water, there being generally about seven feet of the cylinder below the lowest tides and about four feet of it above the highest. The communication was through a two inch iron external pipe rising vertically from the cylinder near its bottom to a point about two feet below mean-sea-level where a stop-cock, manipulated at high-tide, was fixed for the escape of air. From the stop-cock, which was enclosed in a protecting box, the pipe sloped gently downwards, first through and then over the bank into deep water, its length being about seventy feet. To its outer end a further length of twenty-five feet of flexible tubing was originally attached: this ended in a rose, supported so as to be about twelve feet below the lowest tides. But, after nearly two years' experience of this contrivance, during which time there must have been considerable retardation the tubing was examined and found choked with mud, although admitting water through a break in it, one foot beyond the mouth of the iron pipe. The tubing and rose were therefore removed, and it was found that the iron pipe alone (protected at its mouth by a strong basket) gave, on the whole, satisfactory passage to the water.

The working scale of the tide-gauge was one-half.

Registrations were commenced on the 1st December, 1878, and, in consequence of some uncertainty about the accuracy of the early observations, were continued to the 14th March, 1885. They were absolutely continuous, and so far satisfactory; but the agreement between the predicted values of the times and heights of high and low water obtained from them and the actual values, is below the average.



# BEYPORE

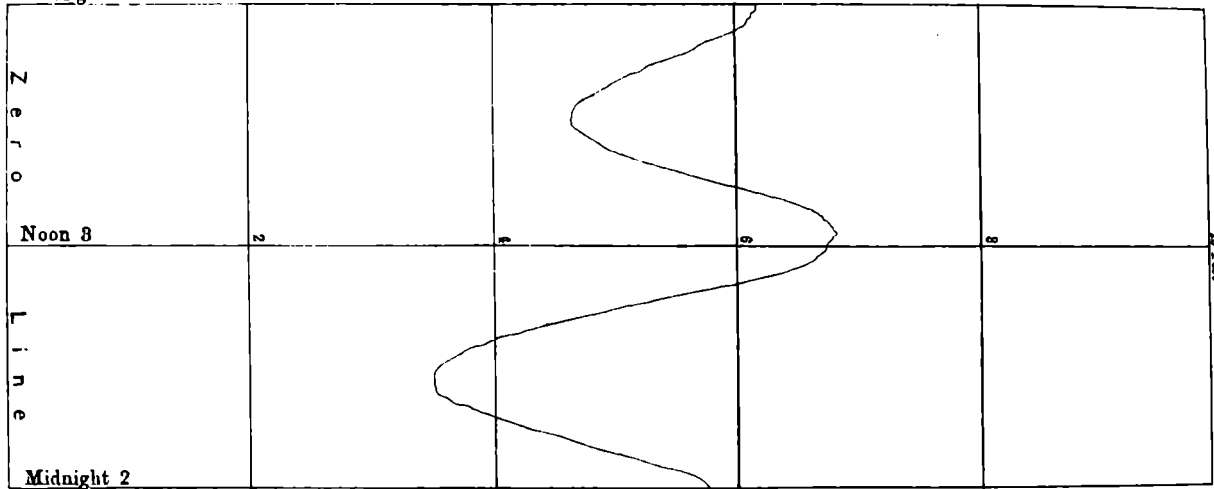
Scale 1:150  
Soundinge in feet.

Photostereograph of the Office of the Trigonometrical Branch, Survey of India, Dehra Dun, April 1884.

TIDAL CURVES  
at  
BEYPORE

Spring Tide — 3rd August 1879

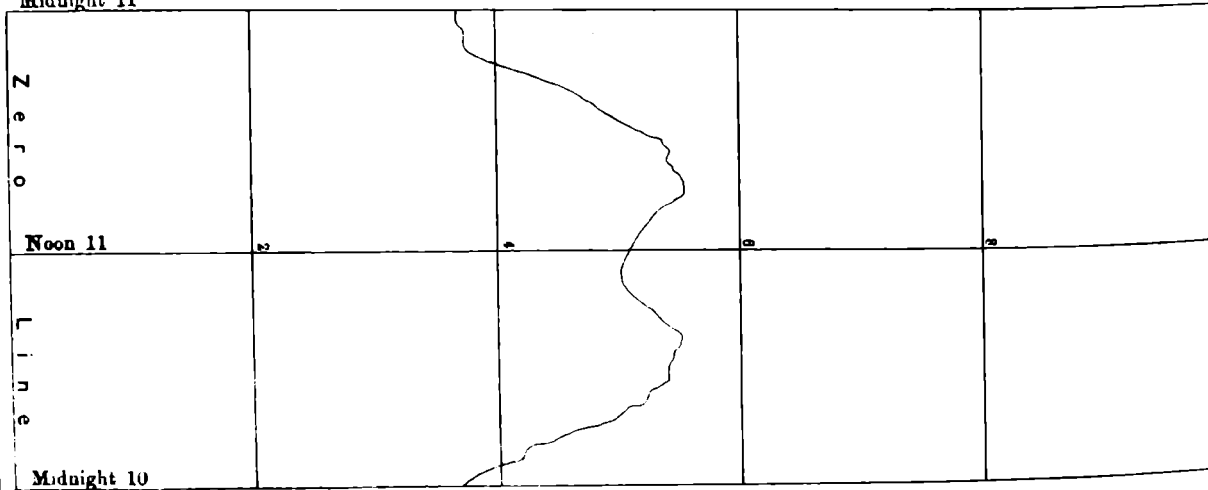
Midnight 3



Full Moon — 2nd August 1879

Neap Tide — 11th August 1879

Midnight 11



Last Quarter — 10th August 1879

*Photostereographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun, April 1900.*

The disturbances of the surface of the ocean, caused by the Krakatoa volcanic eruptions, were recorded at this Tidal Station by the self-registering tide-gauge on the 27th August, 1883.

Barometrical and anemometrical observations were carried on simultaneously with the tidal observations. The barometer was placed in the observatory, but as that site was not suitable for the anemometer, the latter instrument was set up on the small rocky island situated about half a mile south-west of the Flag-staff.

The bench-mark of reference is a stone embedded in a block of masonry and marked  $\begin{matrix} \text{G. T. S.} \\ \square \\ \text{B. A. M.} \end{matrix}$ , situated about a hundred feet east of the front door of the Custom House. It is 19·707 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = XI<sup>h</sup> 16<sup>m</sup>.

The highest high water recorded was 8·4 feet above the zero of the gauge, and occurred in January, 1882.

The lowest low water recorded was 1·9 feet above the zero of the gauge, and occurred in May, 1884.

In 1878-79 the mean range of largest ordinary springs was found to be 4·1 feet.

The height of mean-sea-level above the zero of the gauge had the following values:—

1878-79	...	...	...	5·385 feet.
1879-80	...	...	...	5·392 „
1880-81	...	...	...	5·412 „
1881-82	...	...	...	5·412 „
1882-83	...	...	...	5·395 „
1883-84	...	...	...	5·301 „



## TIDAL OBSERVATIONS.

*Values of H's at Beypore.*

TIDE	H						TIDE
	1878-79	1879-80	1880-81	1881-82	1882-83	1883-84	
	Feet	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0·021	0·083	0·093	0·073	0·035	0·048	S <sub>1</sub>
S <sub>3</sub>	·331	·310	·308	·341	·359	·350	S <sub>2</sub>
S <sub>4</sub>	·004	·003	·004	·006	·007	·007	S <sub>4</sub>
S <sub>6</sub>	·004	·004	·003	·006	·010	·009	S <sub>6</sub>
S <sub>8</sub>	·001	·000	·001	·001	·001	·003	S <sub>8</sub>
M <sub>1</sub>	·017	·032	·038	·024	·032	·055	M <sub>1</sub>
M <sub>2</sub>	·907	·904	·895	·950	1·001	·999	M <sub>2</sub>
M <sub>3</sub>	·011	·010	·011	·010	0·009	·008	M <sub>3</sub>
M <sub>4</sub>	·021	·015	·018	·020	·026	·027	M <sub>4</sub>
M <sub>6</sub>	·010	·004	·003	·006	·012	·013	M <sub>6</sub>
M <sub>8</sub>	·008	·010	·007	·008	·009	·009	M <sub>8</sub>
O	·337	·338	·334	·337	·356	·362	O
K <sub>1</sub>	·704	·691	·683	·715	·727	·730	K <sub>1</sub>
K <sub>3</sub>	·065	·079	·089	·069	·098	·105	K <sub>2</sub>
P	·184	·188	·197	·177	·211	·230	P
J	·035	·047	·064	·040	·034	·073	J
Q	·078	·089	·082	·078	·078	·091	Q
L	·018	·037	·020	·033	·025	·028	L
N	·191	·189	·190	·199	·215	·221	N
λ	·004	·012	·013	·017	·011	·002	λ
ν	·035	·041	·050	·095	·053	·003	ν
μ	·024	·020	·008	·014	·030	·009	μ
R	...	·017	...	·028	...	·013	R
T	...	·043	...	·036	...	·061	T
MS	·010	·004	·005	·008	·016	·015	MS
2SM	·006	·004	·004	·004	·007	·004	2SM
2N	·027	·023	·046	·011	·021	·019	2N
M <sub>2</sub> N	·058	·020	·043	·014	·047	·016	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	·008	·016	·022	·023	·010	·003	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	·011	·019	·014	·009	·004	·004	2M <sub>2</sub> K <sub>1</sub>
Mm	·073	·072	·105	·144	·059	·031	Mm
Mf	·086	·086	·022	·118	·044	·054	Mf
MSf	·066	·037	·017	·041	·028	·037	MSf
Sa	·307	·344	·328	·321	·243	·308	Sa
Ssa	·139	·252	·180	·189	·123	·113	Ssa

*Values of  $\kappa$ 's at Bey pore.*

TIDE	$\kappa$						TIDE
	1878-79	1879-80	1880-81	1881-82	1882-83	1883-84	
	°	°	°	°	°	°	
S <sub>1</sub>	119·85	206·72	187·29	185·05	172·85	171·77	S <sub>1</sub>
S <sub>2</sub>	19·96	19·36	21·78	16·61	11·58	11·32	S <sub>2</sub>
S <sub>4</sub>	139·69	118·30°	132·80	144·69	147·53	128·40	S <sub>4</sub>
S <sub>6</sub>	252·47	244·06	265·76	226·93	247·65	244·94	S <sub>6</sub>
S <sub>8</sub>	20·56	251·57	45·00	319·40	339·44	95·91	S <sub>8</sub>
M <sub>1</sub>	145·76	68·68	22·56	39·56	90·35	60·51	M <sub>1</sub>
M <sub>2</sub>	330·23	329·74	332·96	328·89	323·67	323·52	M <sub>2</sub>
M <sub>3</sub>	213·51	183·64	199·61	195·90	193·50	198·96	M <sub>3</sub>
M <sub>4</sub>	45·30	35·80	53·33	40·78	31·39	22·52	M <sub>4</sub>
M <sub>6</sub>	120·50	114·14	184·37	137·66	132·67	106·13	M <sub>6</sub>
M <sub>8</sub>	136·69	130·03	139·68	161·96	161·87	158·34	M <sub>8</sub>
O	58·02	56·82	58·87	57·03	55·13	55·64	O
K <sub>1</sub>	52·37	53·35	54·16	50·71	47·07	48·17	K <sub>1</sub>
K <sub>2</sub>	11·24	2·79	13·04	11·35	17·06	359·99	K <sub>2</sub>
P	48·93	56·07	57·29	53·82	48·46	51·48	P
J	66·65	44·07	84·25	81·78	39·75	33·80	J
Q	67·77	75·93	59·17	62·31	67·28	62·43	Q
L	349·01	340·99	341·51	347·41	1·09	1·88	L
N	305·94	309·11	302·47	306·94	298·94	296·36	N
$\lambda$	186·90	1·13	288·64	13·56	354·41	252·58	$\lambda$
$\nu$	248·75	20·19	354·07	296·15	276·57	15·13	$\nu$
$\mu$	201·54	349·25	203·27	298·75	238·84	269·00	$\mu$
R	...	163·16	...	100·70	...	126·16	R
T	...	37·30	...	0·13	...	16·94	T
MS	76·22	80·10	100·39	57·14	69·18	60·44	MS
2SM	65·06	218·50	241·47	243·10	350·07	0·54	2SM
2N	236·65	261·18	257·79	265·66	241·61	242·94	2N
M <sub>2</sub> N	315·67	32·02	326·03	318·61	350·51	37·88	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	89·79	350·89	34·80	87·62	130·57	334·69	M <sub>2</sub> K
2M <sub>2</sub> K <sub>1</sub>	66·24	40·08	39·44	42·44	104·87	133·24	2M <sub>2</sub> K
Mm	5·95	85·42	349·81	33·01	43·74	144·22	Mm
Mf	14·59	18·49	50·01	48·04	345·81	158·34	Mf
MSf	228·09	166·84	274·53	197·13	213·94	201·77	MSf
Sa	311·24	315·68	310·74	328·87	298·01	300·79	Sa
Ssa	225·98	181·30	208·39	193·16	214·49	208·26	Ssa

## COCHIN.

(*Tidal Observatory, Lat. 9° 58' N., Long. 76° 15' E.*)

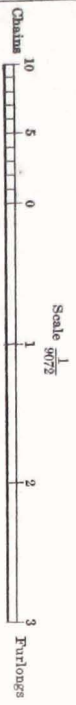
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The tidal observatory at Cochin, the southernmost tidal observatory on the west coast of India, was one of the minor observatories at which five years' observations are generally considered sufficient. It was situated in the town, and within the Store-yard of the Marine Department, on the left or southern bank of what is known as the Cochin River (a passage from the backwater to the sea dividing Vypin from the town of Cochin), in the position shown on the accompanying chart. It was a wooden cabin supported on the bank by nine short piles. The float-cylinder was twenty-four inches in diameter and twelve feet long and was sunk nine feet in the bank so that its lower end should be about four feet below the lowest tides and its upper end about four feet above the highest. Both observatory and cylinder were brought from Beypore after the dismantling of the tidal observatory at that station in March, 1885; three out of the four lengths forming the cylinder being utilised. The communication was through a straight, horizontal, three-inch pipe, thirty-six feet long, which left the cylinder two feet above its bottom and after passing through about ten feet of the bank entered the water about two feet below the lowest tides. Its outer end was about one foot above the river-bed and was fitted originally with a rose; but after being over four years in use, the rose, which was greatly corroded, fell off, and a basket was substituted for it and found to answer.

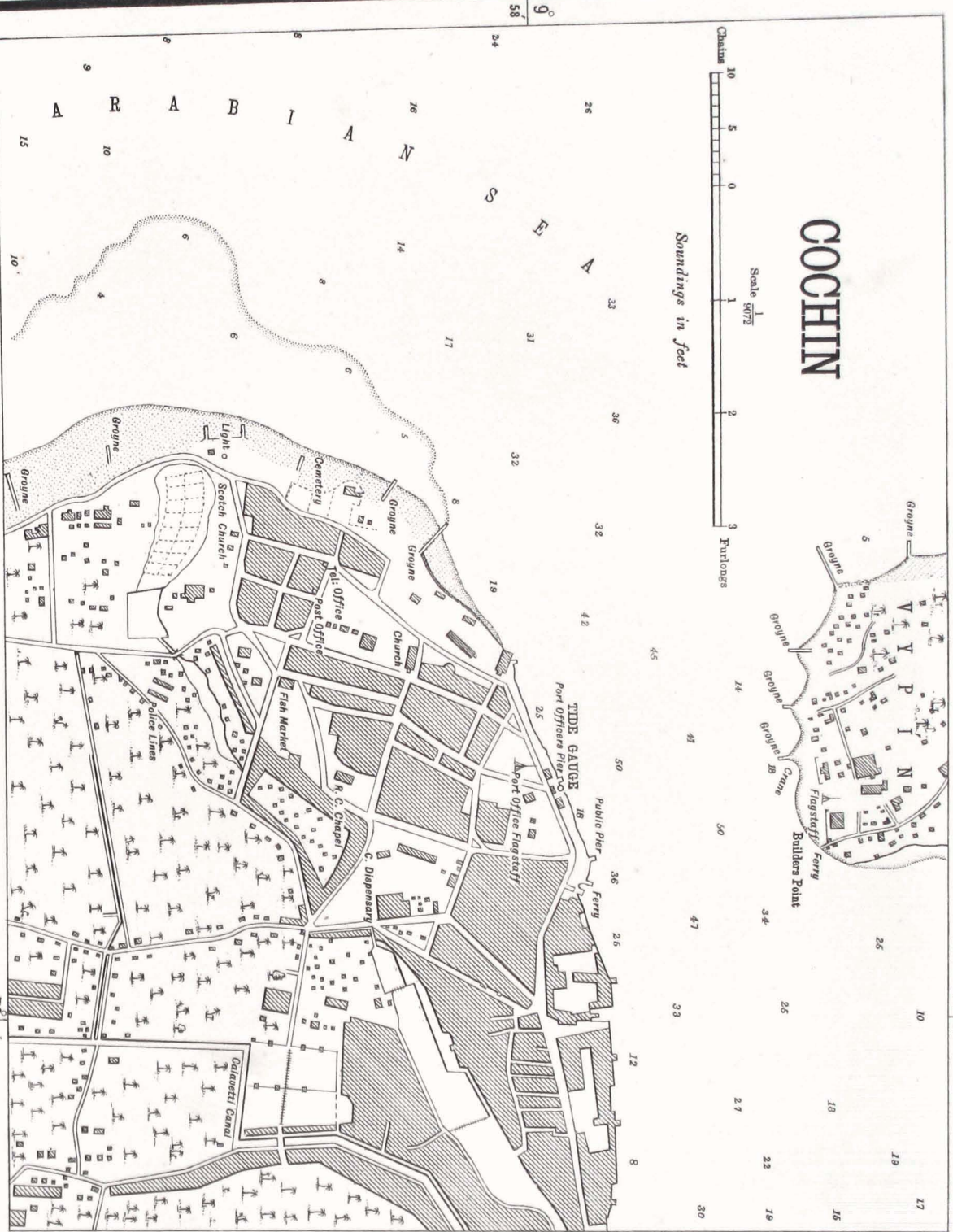
The working scale of the tide-gauge was the natural scale.

Registrations were commenced on the 25th January, 1886, and continued satisfactorily until the 9th of the following July, when the driving clock stopped and could not be set going again for about a fortnight. On the 4th April, 1887, during boisterous weather, a surprising accumulation of sand formed over the mouth of the communication pipe and in spite of strenuous, but unavailing, efforts to clear it away, rendered the tidal curves inaccurate and interrupted until the 26th of the following month, when the action of the water unexpectedly removed the accumulation. After this, the registrations were highly satisfactory until their close, on the 20th March, 1892, when an extra year's observations (taken in consideration of the imperfections mentioned) were completed.

# COCHIN



Soundings in feet



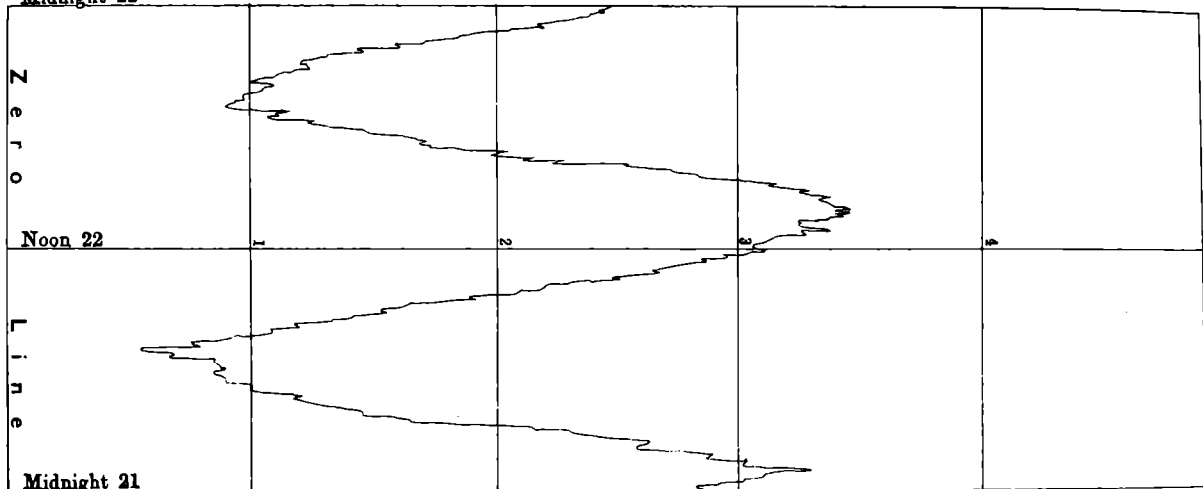
# TIDAL CURVES

at

## COCHIN

Spring Tide — 22nd August 1891

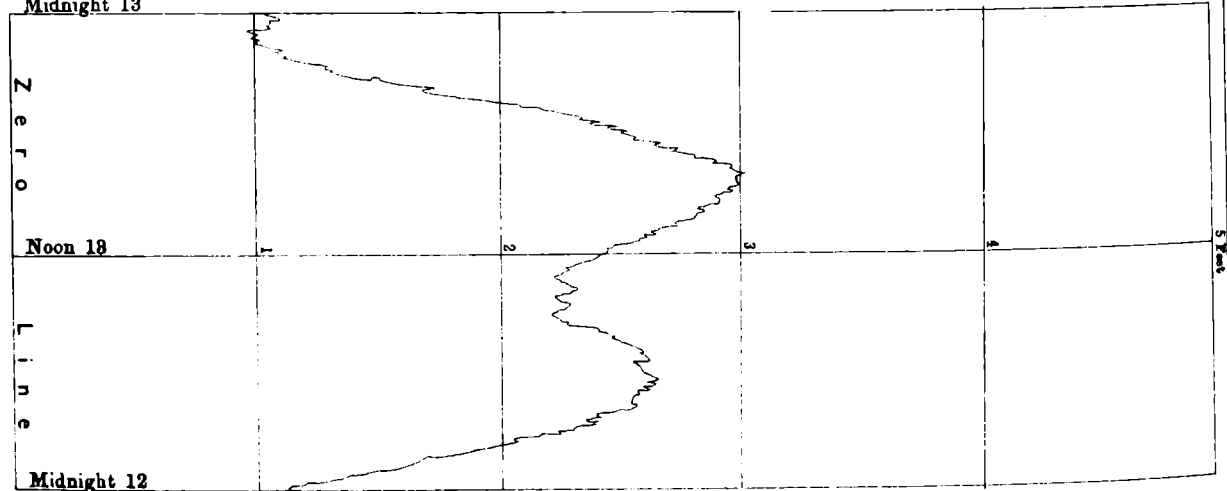
Midnight 22



Full Moon — 19th August 1891

Neap Tide — 13th August 1891

Midnight 13



First Quarter — 12th August 1891

*Photocircographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dún, March 1900.*

Occasional very rapid changes of level of the water to the extent of about a foot—due to squalls—are a feature of the Cochin tides.

Barometrical and anemometrical observations were carried on simultaneously with the tidal observations. The barometer was placed in the observatory; but as that site was not suitable for the anemometer, the latter instrument was set up about half a mile away, on a mound close to, and N.W. of the Light-house.

The bench-mark of reference is a granite stone, six feet long and two and a half feet broad, inscribed  $\square_{\substack{\text{G.T.S.} \\ \text{A} \\ \text{B.M.}}}$ , and embedded in a block of masonry in the centre of the verandah of the Port Office, which is about fifty yards south of the site of the tidal observatory. It is 8.93 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = XI<sup>h</sup> 26<sup>m</sup>.

The highest high water recorded was 4.7 feet above the zero of the gauge, and occurred in December, 1887.

The lowest low water recorded was 0.2 foot *below* the zero of the gauge, and occurred in May, 1889.

In 1890 the mean range of largest ordinary springs was found to be 3.2 feet.

The height of mean-sea-level above the zero of the gauge had the following values:—

1886-87	...	...	...	2.422 feet.
1887-88	...	...	...	2.359 „
1888-89	...	...	...	2.307 „
1889-90	...	...	...	2.421 „
1890-91	...	...	...	2.345 „
1891-92	...	...	...	2.331 „

## TIDAL OBSERVATIONS.

*Values of H's at Cochin.*

TIDE	H						TIDE
	1886-87	1887-88	1888-89	1889-90	1890-91	1891-92	
	Feet	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0·031	0·039	0·024	0·028	0·026	0·024	S <sub>1</sub>
S <sub>2</sub>	·256	·270	·259	·256	·260	·265	S <sub>2</sub>
S <sub>3</sub>	·006	·008	·007	·005	·004	·005	S <sub>4</sub>
S <sub>6</sub>	·007	·005	·005	·005	·005	·007	S <sub>6</sub>
S <sub>8</sub>	·002	·002	·002	·002	·002	·001	S <sub>8</sub>
M <sub>1</sub>	·010	·008	·017	·033	·024	·017	M <sub>1</sub>
M <sub>2</sub>	·731	·731	·722	·730	·720	·727	M <sub>2</sub>
M <sub>3</sub>	·005	·004	·007	·008	·016	·016	M <sub>3</sub>
M <sub>4</sub>	·028	·025	·024	·024	·027	·029	M <sub>4</sub>
M <sub>6</sub>	·009	·011	·009	·011	·008	·008	M <sub>6</sub>
M <sub>8</sub>	·002	·003	·005	·002	·004	·007	M <sub>8</sub>
O	·306	·326	·307	·308	·298	·306	O
K <sub>1</sub>	·586	·602	·596	·591	·580	·591	K <sub>1</sub>
K <sub>2</sub>	·089	·063	·083	·078	·083	·086	K <sub>2</sub>
P	·163	·175	·162	·165	·163	·168	P
J	·026	·039	·048	·052	·031	·034	J
Q	·068	·082	·084	·085	·069	·063	Q
L	·027	·041	·035	·029	·019	·031	L
N	·153	·175	·160	·154	·147	·145	N
λ	·013	...	...	...	...	...	λ
ν	·033	·053	·053	·029	·016	·048	ν
μ	·009	·032	·006	·007	·008	·003	μ
R	...	...	...	...	...	...	R
T	...	·058	·030	·025	·039	·028	T
MS	·020	·018	·020	·017	·023	·021	MS
2SM	·004	·009	·003	·003	·005	·002	2SM
2N	·014	·022	·015	·031	·021	·013	2N
M <sub>2</sub> N	·023	·014	·027	·014	·023	·021	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	·037	·025	·020	·035	·038	·025	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	·017	·021	·021	·015	·018	·020	2M <sub>2</sub> K <sub>1</sub>
Mm	·014	·035	·055	·058	·054	·031	Mm
Mf	·070	·072	·056	·041	·025	·071	Mf
MSf	·037	·042	·026	·025	·015	·024	MSf
Sa	·309	·418	·286	·363	·352	·295	Sa
Ssa	·134	·161	·159	·072	·109	·073	Ssa

*Values of  $\kappa$ 's at Cochin.*

TIDE	$\kappa$						TIDE
	1886-87	1887-88	1888-89	1889-90	1890-91	1891-92	
	°	°	°	°	°	°	
S <sub>1</sub>	161.45	226.56	187.83	179.39	186.19	189.26	S <sub>1</sub>
S <sub>2</sub>	25.81	37.09	26.88	26.87	28.42	30.71	S <sub>2</sub>
S <sub>4</sub>	203.07	138.24	153.82	173.29	188.13	192.76	S <sub>4</sub>
S <sub>6</sub>	226.17	222.44	221.99	211.37	250.77	228.01	S <sub>6</sub>
S <sub>8</sub>	162.47	296.57	327.27	210.47	277.43	284.04	S <sub>8</sub>
M <sub>1</sub>	5.49	87.01	86.67	20.37	356.30	71.36	M <sub>1</sub>
M <sub>2</sub>	331.52	330.48	332.84	331.79	333.27	332.79	M <sub>2</sub>
M <sub>3</sub>	158.79	264.85	211.29	216.22	206.55	206.26	M <sub>3</sub>
M <sub>4</sub>	76.36	64.29	74.42	71.18	80.33	83.99	M <sub>4</sub>
M <sub>6</sub>	95.32	79.89	79.07	82.92	83.54	98.45	M <sub>6</sub>
M <sub>8</sub>	287.28	12.21	318.35	338.23	305.64	332.41	M <sub>8</sub>
O	58.21	56.03	58.22	59.31	59.63	59.46	O
K <sub>1</sub>	50.99	52.68	52.11	51.60	52.24	52.16	K <sub>1</sub>
K <sub>2</sub>	26.05	20.65	21.99	22.55	23.98	23.26	K <sub>2</sub>
P	52.49	42.88	50.65	50.69	53.31	49.70	P
J	77.35	48.60	49.78	81.80	80.72	43.85	J
Q	60.49	61.60	70.55	65.31	69.85	80.11	Q
L	24.44	332.37	355.33	338.58	1.79	359.25	L
N	300.67	299.91	304.86	305.43	303.53	302.08	N
$\lambda$	320.82	...	...	...	...	...	$\lambda$
$\nu$	355.39	334.48	286.74	255.74	10.22	344.51	$\nu$
$\mu$	168.39	203.60	196.44	176.20	160.15	101.83	$\mu$
R	...	...	...	...	...	...	R
T	...	8.92	6.88	84.48	47.25	3.16	T
MS	135.40	143.47	125.91	139.14	149.26	146.10	MS
2SM	324.13	128.55	334.33	324.85	333.56	310.49	2SM
2N	274.08	185.45	256.90	245.29	268.07	275.28	2N
M <sub>2</sub> N	101.66	64.94	146.75	76.07	125.40	101.89	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	131.29	137.81	113.83	117.17	140.75	143.79	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	107.19	108.24	109.46	98.96	110.54	106.82	2M <sub>2</sub> K <sub>1</sub>
Mm	50.00	111.89	20.82	185.96	229.68	315.04	Mm
Mf	355.35	36.39	285.07	343.46	31.82	6.95	Mf
MSf	292.52	310.90	295.51	252.88	138.11	317.23	MSf
Sa	312.98	296.49	296.46	293.32	299.46	312.95	Sa
Ssa	153.95	160.90	136.80	167.72	193.41	89.46	Ssa



## TUTICORIN.

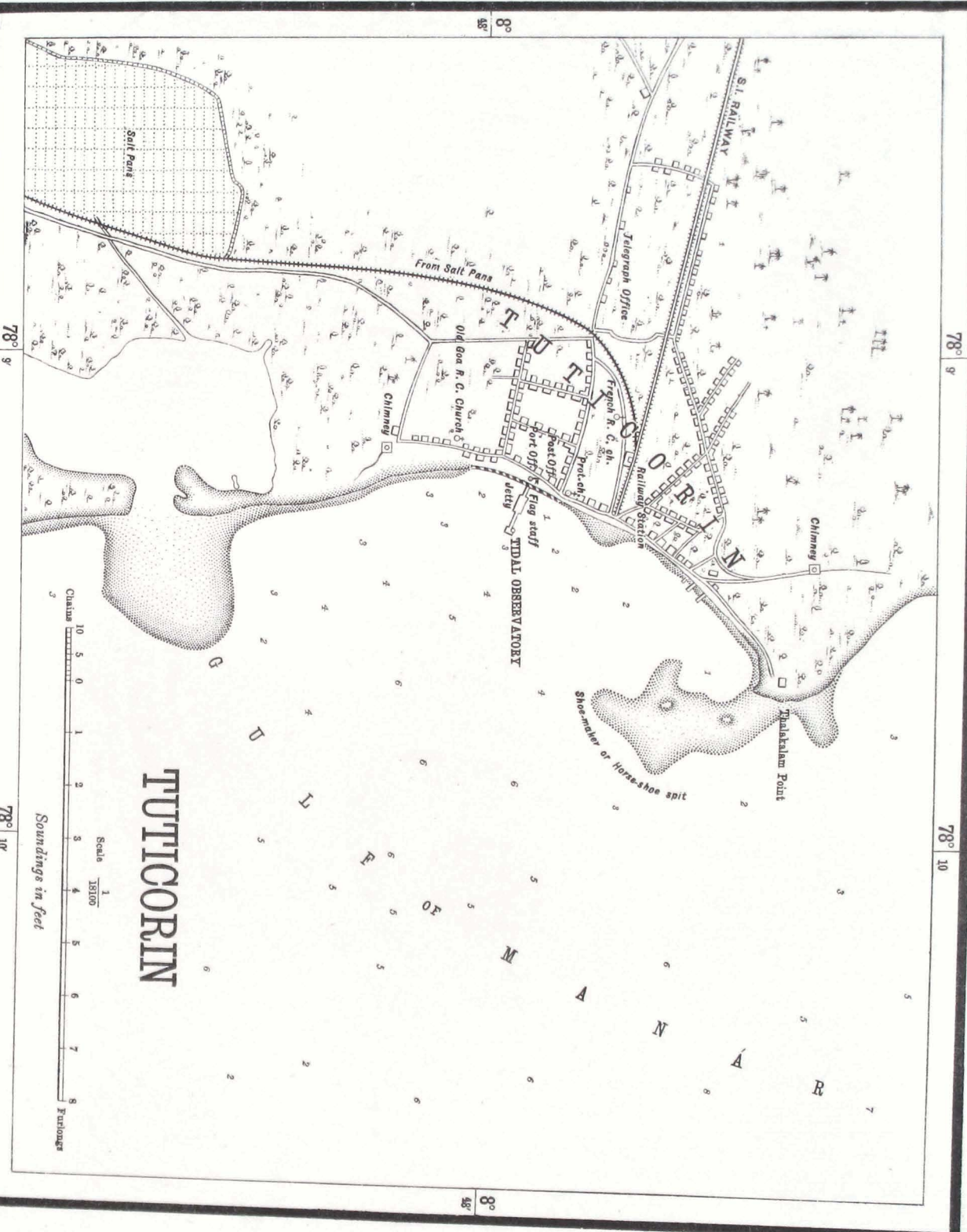
*(Tidal Observatory, Lat. 8° 48' N., Long. 78° 9' E.)*

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The tidal observatory at Tuticorin on the western shore of the Gulf of Manar, and the southernmost tidal observatory on the east coast of India, is one of the minor observatories at which five years' observations are considered sufficient. It is situated in the north re-entering angle of the T-head of the Government Jetty, in the position shown on the accompanying chart. It is a well-constructed wooden cabin supported on stout piles. It is isolated from the jetty, and made safe from the impact of boats by outer piles braced together. The iron float-cylinder is twenty-four inches in diameter and eight feet long. It is suspended from its upper flange which rests on the strongly-framed floor of the observatory, three feet above the highest tides: its lower portion is firmly secured by iron bars extending to the supporting piles: its bottom is closed with an iron plate containing five half-inch perforations for the passage of the water, and is about one foot below the lowest tides.

The working scale of the tide-gauge is the natural scale.

Registrations were commenced on the 1st June, 1888, and have been proceeding most satisfactorily up to the present. A feature of the Tuticorin tides is their great susceptibility to the influence of the wind; sudden changes of the level of the water, as much as a foot in an hour, due to wind, having been recorded. Another peculiarity of the Tuticorin tides, and of the tides in the Gulf of Manar generally, is that, contrary to what might be expected, the mean-sea-level during the south-west monsoon



Photoducy prepared at the Office of the Tri-geometrical Branch, Survey of India, Dehra Dun, January 1888.

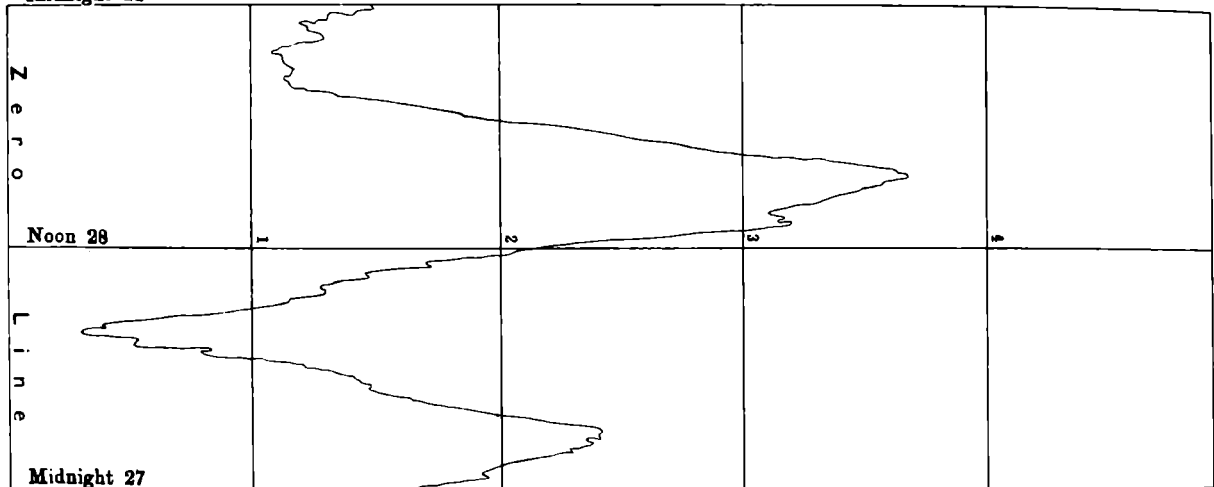
# TIDAL CURVES

at

## TUTICORIN

Spring Tide — 28th May 1892

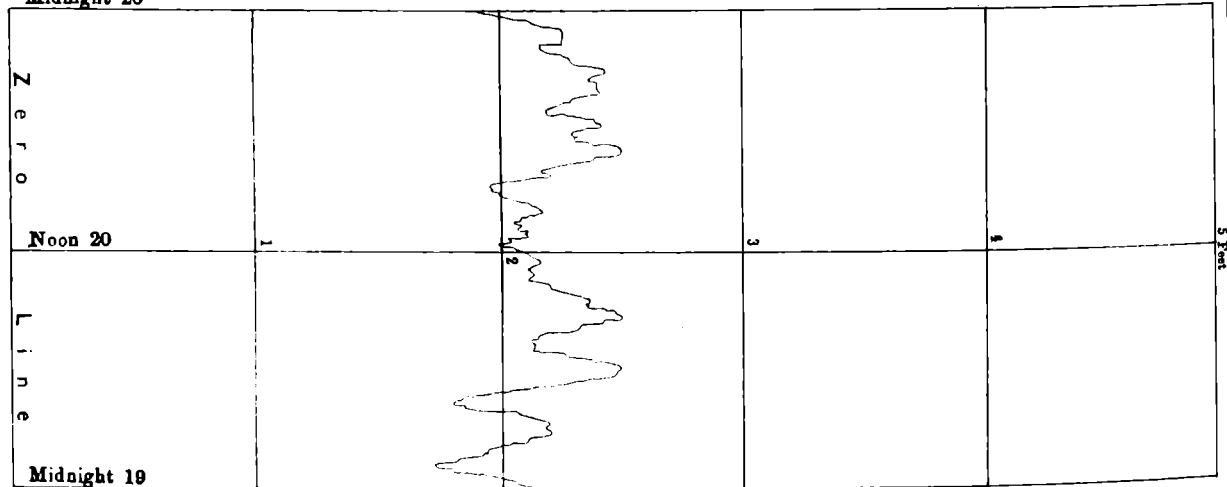
Midnight 28



New Moon — 26th May 1892

Neap Tide — 20th May 1892

Midnight 20



Last Quarter — 19th May 1892

*Photostitographed at the Office of the Trigonometrical Branch, Survey of India, Dacca Din. September 1900.*

is considerably lower than during the north-east monsoon. The yearly mean range of the tide in the Gulf is less than two feet, but during August the monthly mean value of mean-sea-level falls lower than during December by as much as 10·6 inches. This well illustrates the fact that tidal observations taken during one lunation only, may not, as it is sometimes assumed they do, supply a good working value of mean-sea-level for spirit-levelling purposes.

Barometrical and anemometrical observations have been carried on simultaneously with the tidal observations. The barometer was placed in the observatory and the anemometer on the top of the same building.

The bench-mark of reference is a stone inscribed  $\square$  <sup>G.T.S.</sup> and set flush with the level of the verandah <sub>B.M.</sub> floor immediately under the staircase of the Port Office. It is 9·063 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = 1<sup>h</sup> 28<sup>m</sup>.

The highest high water recorded was 4·5 feet above the zero of the gauge, and occurred in April, 1893.

The lowest low water recorded was 0·1 foot *below* the zero of the gauge, and occurred in June, 1891.

In 1890-91 the mean range of largest ordinary springs was found to be 3·2 feet.

The height of mean-sea-level above the zero of the gauge had the following values:—

1888-89	...	...	...	2·091 feet.
1889-90	...	...	...	2·186 „
1890-91	...	...	...	2·149 „
1891-92	...	...	...	2·074 „

## TIDAL OBSERVATIONS.

*Values of H's at Tuticorin.*

TIDE	H				TIDE
	1888-89	1889-90	1890-91	1891-92	
	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0.034	0.043	0.057	0.040	S <sub>1</sub>
S <sub>2</sub>	.458	.466	.478	.473	S <sub>2</sub>
S <sub>4</sub>	.005	.005	.005	.006	S <sub>4</sub>
S <sub>6</sub>	.007	.007	.007	.004	S <sub>6</sub>
S <sub>8</sub>	.005	.015	.014	.007	S <sub>8</sub>
M <sub>1</sub>	.003	.017	.017	.004	M <sub>1</sub>
M <sub>2</sub>	.656	.658	.666	.667	M <sub>2</sub>
M <sub>3</sub>	.018	.022	.022	.019	M <sub>3</sub>
M <sub>4</sub>	.024	.024	.024	.026	M <sub>4</sub>
M <sub>6</sub>	.013	.016	.015	.016	M <sub>6</sub>
M <sub>8</sub>	.006	.002	.006	.013	M <sub>8</sub>
O	.114	.127	.119	.111	O
K <sub>1</sub>	.300	.294	.300	.308	K <sub>1</sub>
K <sub>2</sub>	.128	.135	.123	.128	K <sub>2</sub>
P	.076	.072	.078	.075	P
J	.021	.010	.021	.022	J
Q	.032	.042	.039	.028	Q
L	.026	.023	.032	.042	L
N	.083	.080	.085	.084	N
λ	...	...	...	...	λ
ν	.002	.027	.031	.024	ν
μ	.019	.021	.025	.028	μ
R	...	...	...	...	R
T	...	.021	.008	.025	T
MS	.008	.011	.012	.013	MS
2SM	.005	.004	.009	.009	2SM
2N	.005	.003	.021	.010	2N
M <sub>2</sub> N	.019	.022	.014	.023	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	.009	.007	.002	.005	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	.005	.008	.007	.005	2M <sub>2</sub> K <sub>1</sub>
Mm	.059	.048	.007	.051	Mm
Mf	.039	.029	.037	.063	Mf
MSf	.013	.012	.011	.046	MSf
Sa	.289	.348	.289	.241	Sa
Ssa	.241	.093	.109	.152	Ssa

*Values of  $\kappa$ 's at Tuticorin.*

TIDE	$\kappa$				TIDE
	1868-69	1869-90	1890-91	1891-92	
	o	o	o	o	
S <sub>1</sub>	62.98	58.39	59.38	51.16	S <sub>1</sub>
S <sub>2</sub>	84.90	84.20	82.70	83.10	S <sub>2</sub>
S <sub>4</sub>	227.35	238.63	232.70	238.86	S <sub>4</sub>
S <sub>6</sub>	180.83	176.68	201.16	145.22	S <sub>6</sub>
S <sub>8</sub>	224.09	230.60	227.92	222.17	S <sub>8</sub>
M <sub>1</sub>	137.47	52.68	39.21	354.88	M <sub>1</sub>
M <sub>2</sub>	44.10	44.32	42.71	42.71	M <sub>2</sub>
M <sub>3</sub>	163.26	161.82	159.65	160.30	M <sub>3</sub>
M <sub>4</sub>	161.88	154.32	155.15	152.33	M <sub>4</sub>
M <sub>6</sub>	8.51	22.70	23.14	22.79	M <sub>6</sub>
M <sub>8</sub>	304.57	264.50	245.76	292.36	M <sub>8</sub>
O	48.90	44.58	46.17	47.45	O
K <sub>1</sub>	26.77	27.72	27.85	27.04	K <sub>1</sub>
K <sub>2</sub>	85.28	81.55	81.09	85.57	K <sub>2</sub>
P	9.97	11.81	3.31	13.13	P
J	65.05	19.57	32.27	63.59	J
Q	79.63	66.77	73.54	77.88	Q
L	63.90	41.93	78.48	23.20	L
N	32.26	32.43	33.21	35.11	N
$\lambda$	...	...	...	...	$\lambda$
$\nu$	33.40	63.61	24.83	3.50	$\nu$
$\mu$	92.71	95.14	92.87	91.48	$\mu$
R	...	...	...	...	R
T	...	45.80	173.07	130.87	T
MS	263.31	250.88	260.97	259.05	MS
2SM	303.44	359.04	315.01	304.64	2SM
2N	6.39	299.61	43.41	95.65	2N
M <sub>2</sub> N	75.24	47.58	91.63	81.97	M <sub>2</sub> N
M <sub>3</sub> K <sub>1</sub>	94.36	140.22	264.97	32.67	M <sub>3</sub> K <sub>1</sub>
2M <sub>3</sub> K <sub>1</sub>	353.54	322.71	297.24	232.92	2M <sub>3</sub> K <sub>1</sub>
Mm	22.76	74.70	125.95	219.93	Mm
Mf	358.52	328.37	4.48	359.84	Mf
MSf	348.03	293.96	258.80	276.09	MSf
Sa	311.80	297.57	313.80	316.17	Sa
Ssa	71.95	111.84	77.25	55.62	Ssa

## MINICOY.

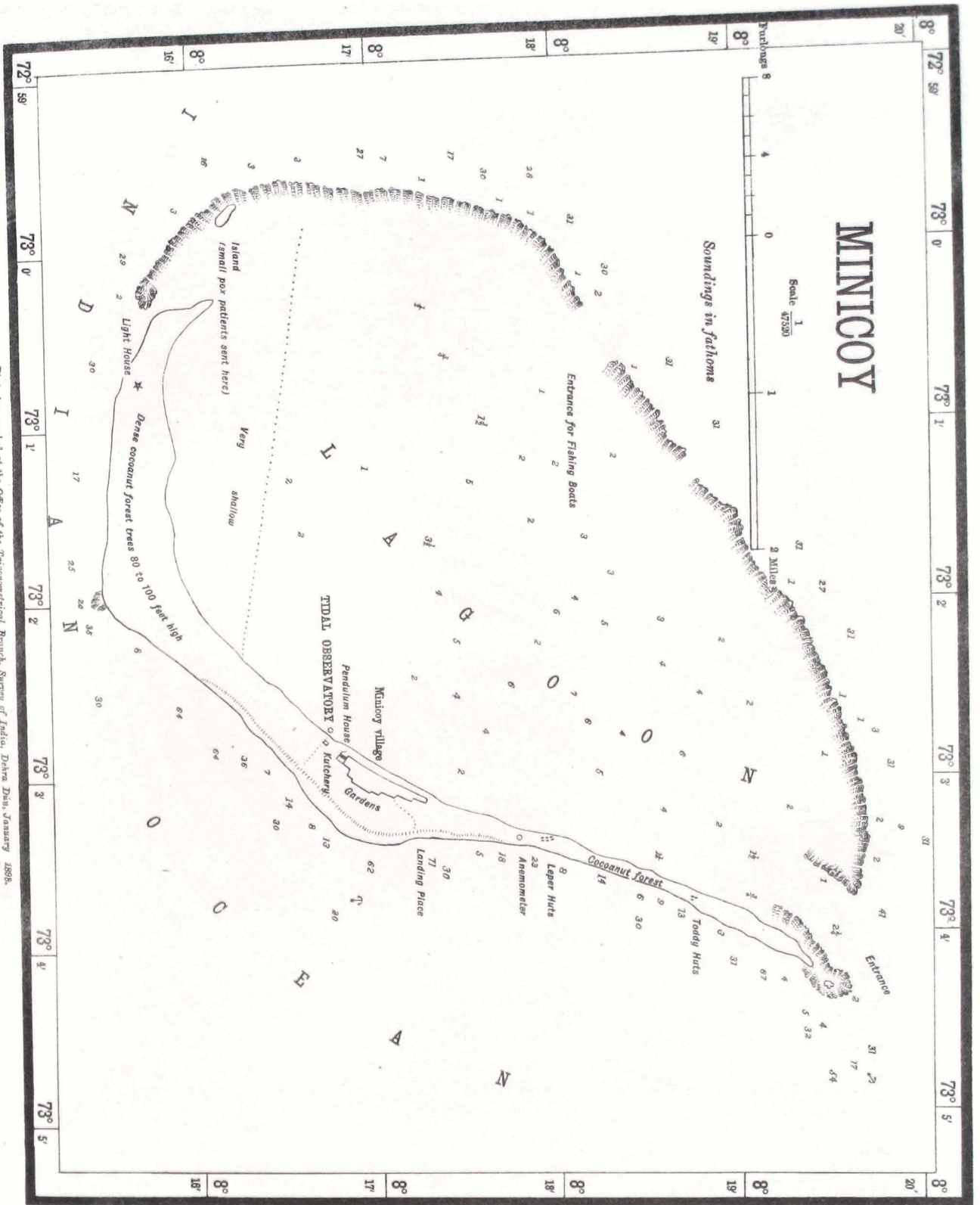
*(Tidal Observatory, Lat. 8° 17' N., Long. 73° 3' E.)*

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Minicoy is a solitary coral island situated in the Indian Ocean between the 8° and 9° channels, two hundred and seventy nautical miles west of Cape Comorin. The tidal observatory is one of the minor observatories, at which five years' observations are considered sufficient, and special interest attaches to it owing to its position in mid-ocean. It stands within the lagoon, in the position shown on the accompanying chart, one hundred and ten feet from the shore, and opposite the kacheri, at the southern end of the only village on the island. It is a wooden cabin, ten feet square, resting on a stout level framework of cocoanut logs supported on nine cocoanut piles sixteen or seventeen feet long, well driven into the sand and coral, and firmly braced. The float-cylinder is a massive iron drainage pipe, twenty inches in internal diameter and twelve and a half feet long, braced firmly to the piles by beams, and having its bottom about two and a half feet below lowest tides and its top about six feet above highest. Its bottom is plugged with a perforated wooden disc and rests on a large stone block whose upper face is grooved to take the rim and hollowed out under the centre of the cylinder, the hollow being connected by openings on each side with the external water which has thus free communication with the float.

The working scale of the tide-gauge is one-half.

Registrations were commenced on the 12th January, 1891, and have been highly satisfactory up to the present.



Photolithographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun, January 1885.



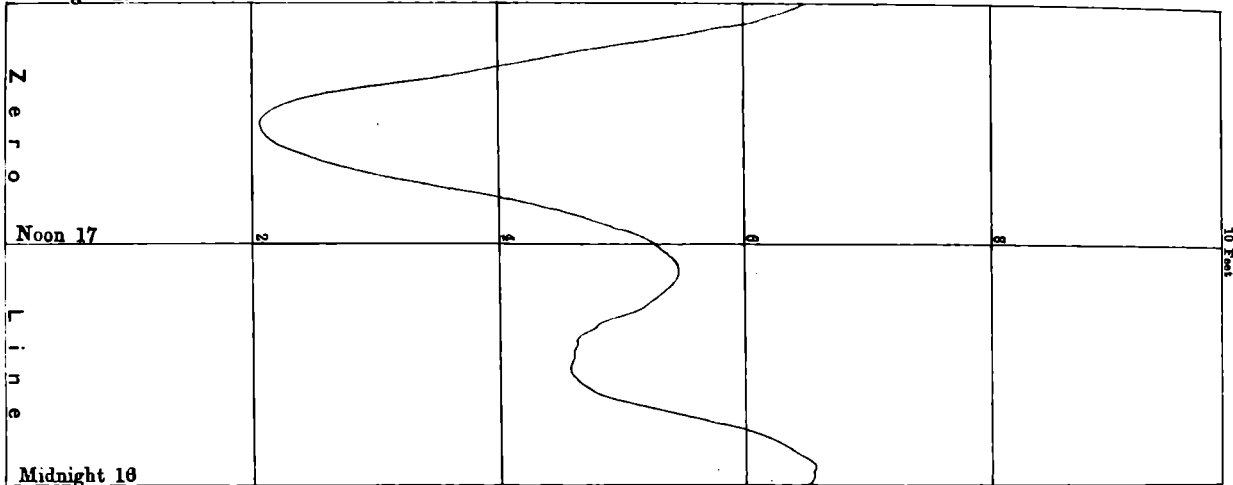
TIDAL CURVES

at

MINICOY

Spring Tide — 17th November 1891

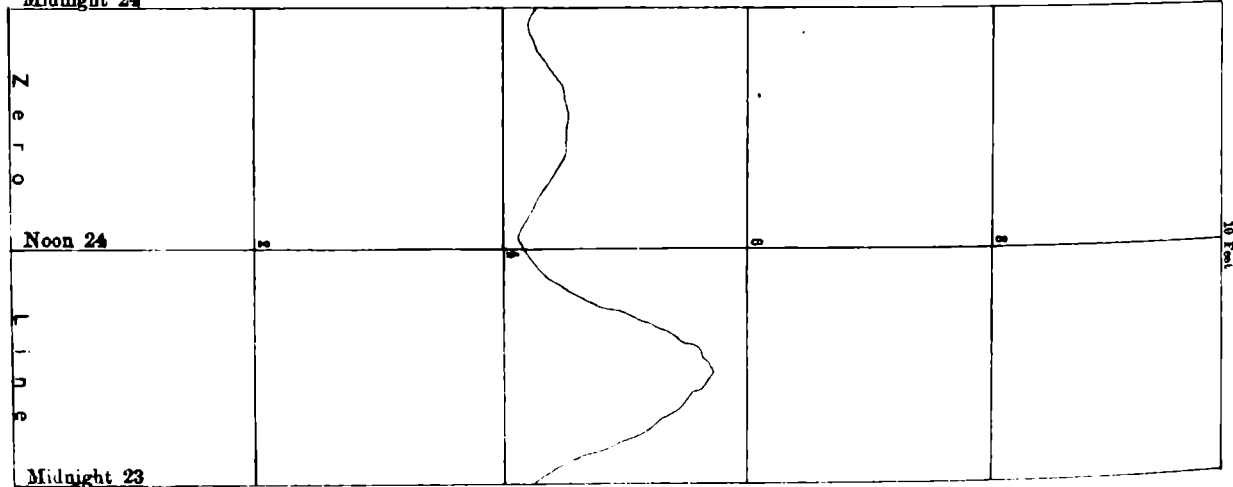
Midnight 17



Full Moon — 16th November 1891

Neap Tide — 24th November 1891

Midnight 24



Last Quarter — 23rd November 1891

Photocopyographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun, September 1900.

Barometrical and anemometrical observations are being carried on simultaneously with the tidal observations. The barometer was placed in the observatory, but as that site was unsuitable for the anemometer, the latter instrument was set up two miles north of the tidal observatory on a slight elevation which is exceptionally open, and free from tall trees.

The bench-mark of reference is a stone inscribed <sup>G.T.S.</sup> <sub>B.M.</sub> embedded one hundred and thirteen and a half feet east of the N.E. corner of the kacheri. It is 10·046 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = X<sup>h</sup> 52<sup>m</sup>.

The highest high water recorded was 7·7 feet above the zero of the gauge, and occurred in January, 1893.

The lowest low water recorded was 1·8 feet above the zero of the gauge, and occurred in November, 1892.

In 1891-92 the mean range of largest ordinary springs was found to be 4·0 feet.

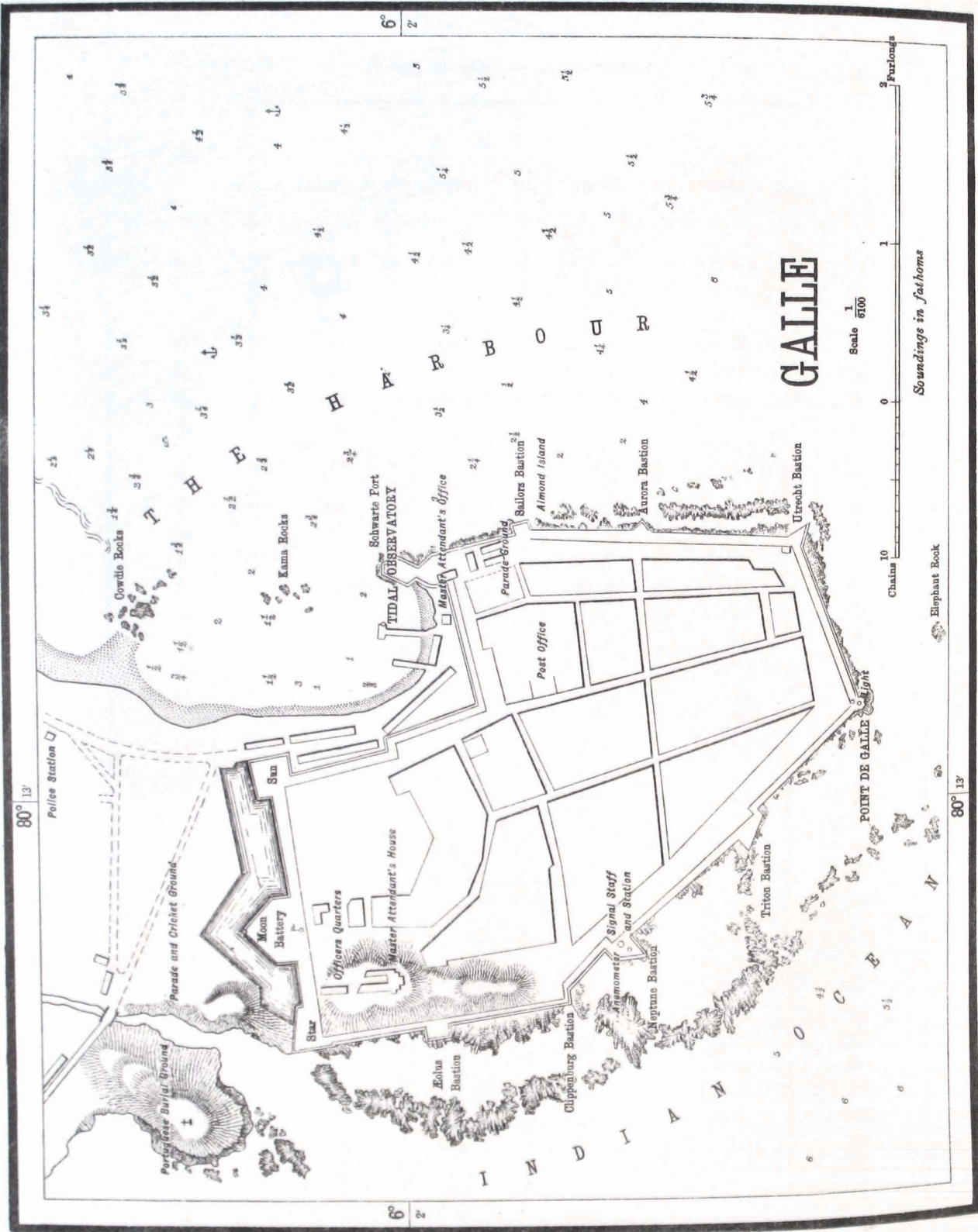
The height of mean-sea-level above the zero of the gauge had the following values:—

1891-92	...	...	...	5·174 feet.
1892-93	...	...	...	5·269 ,,

## TIDAL OBSERVATIONS.

*Values of H's and  $\kappa$ 's at Minicoy.*

TIDE	H		$\kappa$		TIDE
	1891-92	1892-93	1891-92	1892-93	
	Feet	Feet	o	o	
S <sub>1</sub>	0·037	0·061	209·86	198·35	S <sub>1</sub>
S <sub>2</sub>	·360	·332	18·83	21·74	S <sub>2</sub>
S <sub>4</sub>	·003	·001	128·05	12·10	S <sub>4</sub>
S <sub>6</sub>	·001	·001	170·54	291·80	S <sub>6</sub>
S <sub>8</sub>	·000	·001	213·69	145·01	S <sub>8</sub>
M <sub>1</sub>	·032	·020	25·56	37·76	M <sub>1</sub>
M <sub>3</sub>	·880	·835	327·78	331·97	M <sub>3</sub>
M <sub>5</sub>	·007	·003	175·36	188·30	M <sub>5</sub>
M <sub>7</sub>	·011	·004	17·91	170·60	M <sub>7</sub>
M <sub>9</sub>	·004	·001	105·81	39·77	M <sub>9</sub>
M <sub>9</sub>	·002	·003	138·95	244·83	M <sub>9</sub>
O	·338	·327	58·49	59·70	O
K <sub>1</sub>	·695	·682	49·76	52·24	K <sub>1</sub>
K <sub>3</sub>	·096	·093	11·14	24·41	K <sub>2</sub>
P	·224	·226	47·35	45·78	P
J	·065	·035	76·08	82·20	J
Q	·075	·055	63·23	60·35	Q
L	·021	·039	18·49	14·84	L
N	·180	·172	300·67	304·38	N
$\lambda$	...	...	...	...	$\lambda$
$\nu$	·058	·071	316·76	283·64	$\nu$
$\mu$	·005	·016	278·79	273·15	$\mu$
R	...	...	...	...	R
T	...	·034	...	321·76	T
MS	·005	·011	127·36	299·28	MS
2SM	·002	·004	305·83	315·38	2SM
2N	·024	·014	246·19	240·01	2N
M <sub>2</sub> N	·015	·051	223·52	261·03	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	·008	·005	45·51	236·16	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	·002	·004	207·90	263·25	2M <sub>2</sub> K <sub>1</sub>
Mm	·032	·039	68·31	146·97	Mm
Mf	·063	·054	10·86	357·04	Mf
MSf	·011	·016	55·56	49·93	MSf
Sa	·369	·283	355·19	358·24	Sa
Sea	·106	·170	273·92	228·86	Ssa



# GALLE

Scale 1/6100



Soundings in fathoms

Elephant Rock

## GALLE.

(*Tidal Observatory, Lat. 6° 2' N., Long. 80° 13' E.*)

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The tidal observatory at Galle, near the southern extremity of the west coast of Ceylon, was one of the minor observatories at which five years' observations are generally considered sufficient, and was situated in the angle formed by the T-head of the end of the landing pier, in the position shown on the accompanying chart. It was a small wooden cabin having its floor on a level with that of the pier and isolated from it, and was supported on four piles protected by copper sheathing from the action of the water. The float-cylinder was twenty-two inches in diameter and eleven feet long, formed in two sections. The lower section, nine feet long, was of iron and rested on the bed of the harbour which is about three and a half feet below lowest tides: the upper, two feet long, was of wood and had its top on a level with the floor of the observatory, about three feet above highest tides. The communication was through two small holes near the bottom of the cylinder.

The working scale of the tide-gauge was the natural scale.

Registrations were commenced on the 23rd March, 1884. In September of the same year rough weather displaced the cylinder, and caused about a fortnight's interruption to the observations. The water was found to have a very corrosive action on the iron of the cylinder. Holes due to this cause began to appear, and in July of the following year the cylinder had to be repaired at the cost of a week's break in the observations. In December, 1886, the cylinder had become useless through corrosion and there was a month's break in the observations while it was being renewed. After this, for nearly two years, the registrations were satisfactory, but between November, 1888, and June, 1889, they suffered many short interruptions due to various causes, and the curves for about nine weeks preceding the latter date (owing to the corrosion of the bottom of the cylinder and the consequent excessive flow of water through openings so made) were rendered difficult to read from the great oscillation of the pencil. It was considered expedient to extend the observations to the 8th April, 1890, when the observatory was dismantled after having been in operation for six years.

Barometrical and anemometrical observations were carried on simultaneously with the tidal observations. The barometer was placed in the observatory. The anemometer after being at work for a year on the top of the same building was removed to the top of the signal house on the southern rampart of the Fort, a much better position for it.

The bench-mark of reference is a stone embedded in a block of masonry and inscribed <sup>G. T. S.</sup>  $\square$  ; it <sub>B. M.</sub> ; it <sub>A. D. 1884.</sub> is situated four feet outside the Fort-wall and nine feet east of the northern gateway through which the road from the landing-pier enters the Fort, and on the wall of the Fort just opposite the bench-mark, the inscription <sup>G. T. S.</sup> <sub>B. M.</sub> has been cut. The bench-mark is 7·710 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = II<sup>h</sup> 3<sup>m</sup>.

The highest high water recorded was 4·9 feet above the zero of the gauge, and occurred in December, 1889.

The lowest low water recorded was 0·7 foot above the zero of the gauge, and occurred in July, 1886.

In 1889 the mean range of largest ordinary springs was 2·3 feet.

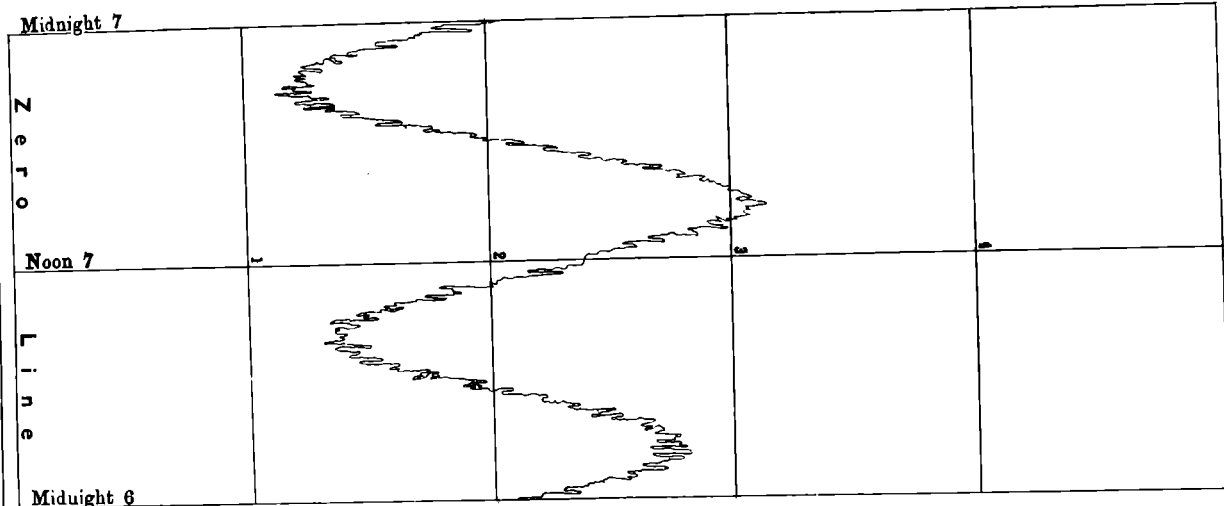
The height of mean-sea-level above the zero of the gauge had the following values :—

1884-85	...	...	...	2·656 feet.
1885-86	...	...	...	2·700 „
1886-87	...	...	...	2·679 „
1887-88	...	...	...	2·606 „
1888-89	...	...	...	2·570 „
1889-90	...	...	...	2·685 „

# TIDAL CURVES

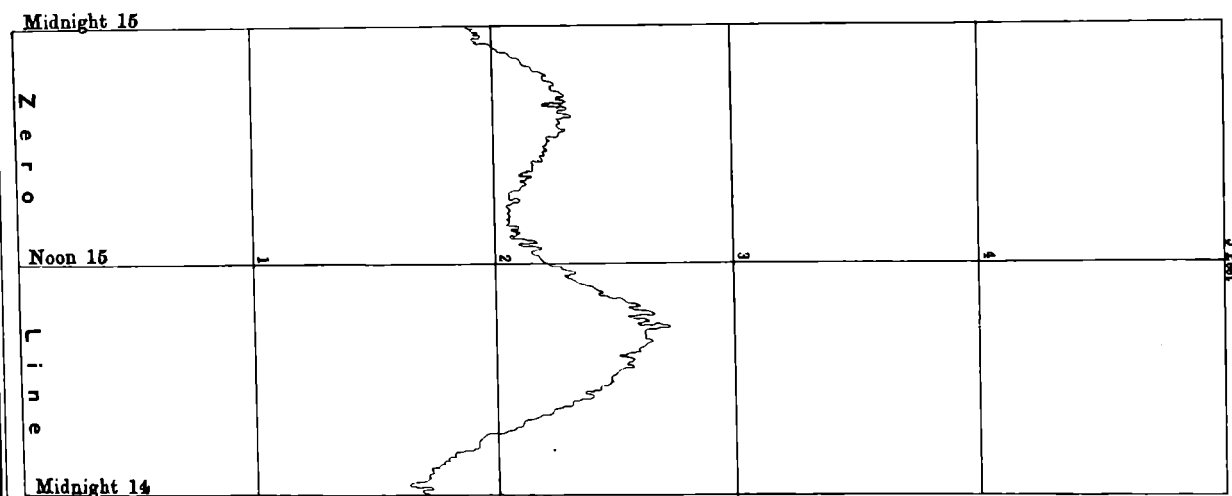
at  
**GALLE**

Spring Tide — 7th August 1884



Full Moon — 6th August 1884

Neap Tide — 15th August 1884



Last Quarter — 14th August 1884

*Photostitographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dún, September 1900.*

*Values of H's at Galle.*

TIDE	H						TIDE
	1884-85	1885-86	1886-87	1887-88	1888-89	1889-90	
	Feet	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0·011	0·012	0·031	0·011	0·012	0·011	S <sub>1</sub>
S <sub>2</sub>	·357	·357	·370	·369	·358	·361	S <sub>2</sub>
S <sub>4</sub>	·002	·004	·002	·003	·004	·003	S <sub>4</sub>
S <sub>6</sub>	·001	·000	·004	·001	·001	·000	S <sub>6</sub>
S <sub>8</sub>	·001	·001	·001	·001	·003	·001	S <sub>8</sub>
M <sub>1</sub>	·010	·008	·004	·007	·007	·003	M <sub>1</sub>
M <sub>2</sub>	·526	·525	·530	·524	·527	·531	M <sub>2</sub>
M <sub>3</sub>	·014	·012	·014	·012	·013	·010	M <sub>3</sub>
M <sub>4</sub>	·009	·011	·013	·014	·015	·012	M <sub>4</sub>
M <sub>6</sub>	·004	·003	·003	·002	·002	·002	M <sub>6</sub>
M <sub>8</sub>	·002	·002	·001	·001	·001	·002	M <sub>8</sub>
O	·044	·052	·046	·049	·049	·041	O
K <sub>1</sub>	·165	·165	·168	·170	·166	·166	K <sub>1</sub>
K <sub>2</sub>	·093	·089	·154	·115	·098	·108	K <sub>2</sub>
P	·053	·049	·037	·043	·053	·046	P
J	·010	·006	·012	·013	·008	·010	J
Q	·023	·024	·028	·030	·024	·025	Q
L	·036	·028	·042	·029	·024	·020	L
N	·053	·066	·054	·060	·072	·071	N
λ	·018	·012	...	...	...	...	λ
ν	·048	·038	·013	·005	·028	·030	ν
μ	·025	·025	·026	·020	·024	·021	μ
R	...	·018	...	...	...	...	R
T	...	·041	...	·016	·039	·024	T
MS	·006	·006	·009	·007	·007	·005	MS
2SM	·007	·012	·008	·007	·009	·012	2SM
2N	·007	·020	·009	·009	·004	·009	2N
M <sub>2</sub> N	·026	·013	·024	·014	·017	·016	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	·005	·008	·005	·004	·002	·002	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	·002	·001	·003	·004	·006	·007	2M <sub>2</sub> K <sub>1</sub>
Mm	·067	·017	·017	·058	·035	·038	Mm
Mf	·020	·027	·066	·073	·030	·012	Mf
MSf	·013	·013	·030	·028	·013	·020	MSf
Sa	·377	·287	·346	·371	·324	·392	Sa
Ssa	·097	·089	·142	·096	·178	·159	Ssa



## TIDAL OBSERVATIONS.

*Values of  $\kappa$ 's at Galle.*

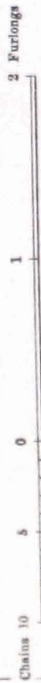
TIDE	$\kappa$						TIDE
	1884-85	1885-86	1886-87	1887-88	1888-89	1889-90	
	o	o	o	o	o	o	
S <sub>1</sub>	65.77	74.88	27.87	34.29	63.02	13.64	S <sub>1</sub>
S <sub>2</sub>	96.56	93.95	91.80	92.94	93.51	96.40	S <sub>2</sub>
S <sub>4</sub>	205.20	245.56	252.65	241.93	213.28	248.96	S <sub>4</sub>
S <sub>6</sub>	264.29	135.00	106.14	26.57	296.57	206.57	S <sub>6</sub>
S <sub>8</sub>	196.70	258.69	274.09	296.57	322.70	261.87	S <sub>8</sub>
M <sub>1</sub>	225.42	245.42	332.67	349.16	3.06	64.08	M <sub>1</sub>
M <sub>2</sub>	59.80	57.32	54.95	54.56	55.76	58.93	M <sub>2</sub>
M <sub>3</sub>	166.23	161.03	149.98	157.80	159.14	174.32	M <sub>3</sub>
M <sub>4</sub>	171.06	164.32	166.44	161.51	162.32	159.44	M <sub>4</sub>
M <sub>6</sub>	1.98	335.69	24.27	302.84	270.57	31.23	M <sub>6</sub>
M <sub>8</sub>	284.91	211.54	255.33	138.67	235.43	31.38	M <sub>8</sub>
O	78.75	79.25	78.47	73.81	70.95	72.20	O
K <sub>1</sub>	19.87	17.59	15.66	18.82	17.83	19.61	K <sub>1</sub>
K <sub>2</sub>	91.99	104.40	100.97	90.42	88.95	94.72	K <sub>2</sub>
P	26.58	14.67	24.19	20.42	19.87	23.91	P
J	68.55	53.28	355.41	16.93	57.87	22.11	J
Q	88.84	95.68	94.72	91.11	104.02	104.13	Q
L	67.31	6.56	79.98	25.77	75.28	32.98	L
N	47.26	41.97	44.77	44.58	46.38	53.69	N
$\lambda$	100.75	17.88	...	...	...	...	$\lambda$
$\nu$	66.52	16.39	351.33	160.33	82.39	46.46	$\nu$
$\mu$	101.82	106.19	100.12	98.93	102.90	87.81	$\mu$
R	...	357.83	...	...	...	...	R
T	...	58.79	...	103.36	72.91	39.43	T
MS	312.74	240.89	238.24	236.91	258.86	243.16	MS
2SM	23.69	340.19	319.94	306.21	4.55	7.54	2SM
2N	208.91	66.21	148.64	70.24	171.42	49.31	2N
M <sub>2</sub> N	164.87	228.78	189.31	250.29	181.64	258.78	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	284.39	28.48	126.55	165.12	10.48	5.73	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	135.25	95.67	82.31	14.46	11.38	335.54	2M <sub>2</sub> K <sub>1</sub>
Mm	21.93	337.01	339.95	42.49	22.06	42.16	Mm
Mf	12.20	38.74	338.73	12.56	55.13	17.96	Mf
MSf	324.41	133.17	267.51	212.44	47.40	213.83	MSf
Sa	314.15	330.35	311.78	297.53	304.80	296.59	Sa
Ssa	124.75	102.12	121.83	125.34	84.63	135.85	Ssa

79° 51'

# COLOMBO

# T H E H A R B O U R

Scale 1/6857



*Soundings in feet*



79° 51'

6° 56' 30"

6° 56' 30"

Photographed at the Office of the Triangulation Branch, Survey of India, Dehra Dun, March 1897.

## COLOMBO.

(*Tidal Observatory, Lat. 6° 57' N., Long. 79° 51' E.*)

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The tidal observatory at Colombo, on the west coast of Ceylon, was one of the minor observatories at which five years' observations are generally considered sufficient, and was situated over the small water-space between the end of the Import Jetty and the masonry pedestal of the large crane in front of the Master Attendant's and Customs Offices, in the position shown on the accompanying chart. It was the wooden cabin previously used at Pámban, but reduced in size to fit the rather cramped space available for its reception. It was fixed on substantial cross beams each of which rested at first with one of its ends on the beams of the Jetty and the other inserted in the pedestal of the crane; but after a year's trial it was found necessary to isolate the observatory as the shocks caused by boats striking against the Jetty stopped the driving clock. Piles were therefore driven to act as supports in lieu of the Jetty, and the cross beams were securely fixed to them and into the pedestal of the crane, an arrangement which was found to give the necessary stability. The float-cylinder was of iron, twenty-two inches in diameter and eleven feet long. Its top projected about six inches above the floor of the observatory and was four feet above the highest tides; and its bottom, which was closed, rested on stones laid on the bed of the harbour, and was two and a half feet below the lowest tides. The communication was at first through a hole, covered with a perforated copper nozzle, close to the bottom of the cylinder. After trial for about a year and a half this arrangement had to be discarded as the pencil was found to oscillate to such an extent as to make the tidal curves almost illegible. In lieu of it, a short external pipe in two pieces and bent downwards was fitted to the hole. Its lower piece was fitted within with a wooden block having a half-inch tube passing through its centre, at the top and bottom of which a rose was attached. This arrangement made the curves legible; but it was troublesome, as the pipe frequently became choked, and retardation was caused.

The working scale of the tide-gauge was the natural scale.

Registrations were commenced on the 24th January, 1884. In September of the same year about a fortnight's observations had to be rejected owing to retardation. For a similar reason the curves between the 1st November and 5th December, 1885, and those between the 21st October and 18th November, 1889, had also to be rejected—otherwise the registrations may be considered satisfactory. The observatory was closed on the 29th March, 1890, after a period of six years' observations, it being found convenient to close both the Colombo and Galle tidal observatories about the same time.

Barometrical and anemometrical observations were not taken, as the Colombo meteorological statistics are obtainable from the Surveyor General of Ceylon.

The bench-mark of reference is a stone engraved  $\begin{matrix} \text{G. T. S.} \\ \square \\ \text{B. M.} \end{matrix}$  embedded six inches under ground in a block of masonry, close under the outer wall of the double flight of steps leading (on the Harbour side) to the Customs House and Master Attendant's Office, and ten and a half feet east of the lowest step of the western flight. Just above the bench-mark there is a slab of cement let into the wall bearing the inscription  $\begin{matrix} \text{G. T. S.} \\ \text{B. M.} \\ \text{Below.} \end{matrix}$  The bench-mark is 10·075 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = 1<sup>h</sup> 50<sup>m</sup>.

The highest high water recorded was 4·4 feet above the zero of the gauge, and occurred in October, 1886.

The lowest low water recorded was 0·3 foot above the zero of the gauge, and occurred in September, 1888.

In 1889-90 the mean range of largest ordinary springs was found to be 2·6 feet.

The height of mean-sea-level above the zero of the gauge had the following values:—

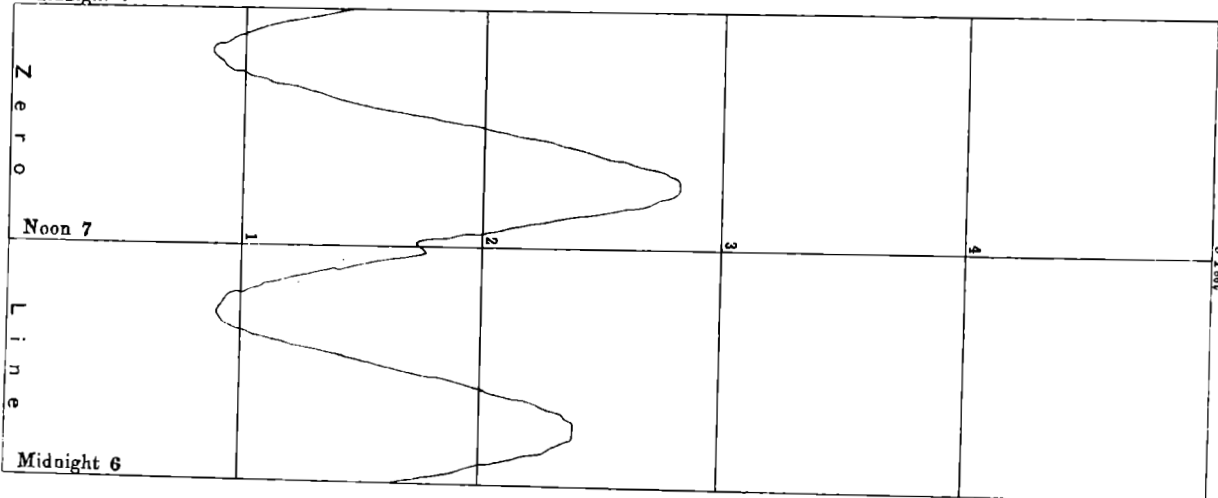
1884-85	...	...	...	2·208 feet.
1885-86	...	...	...	2·261 „
1886-87	...	...	...	2·304 „
1887-88	...	...	...	2·199 „
1888-89	...	...	...	2·112 „
1889-90	...	...	...	2·216 „

# TIDAL CURVES

at  
COLOMBO

Spring Tide — 7th August 1884

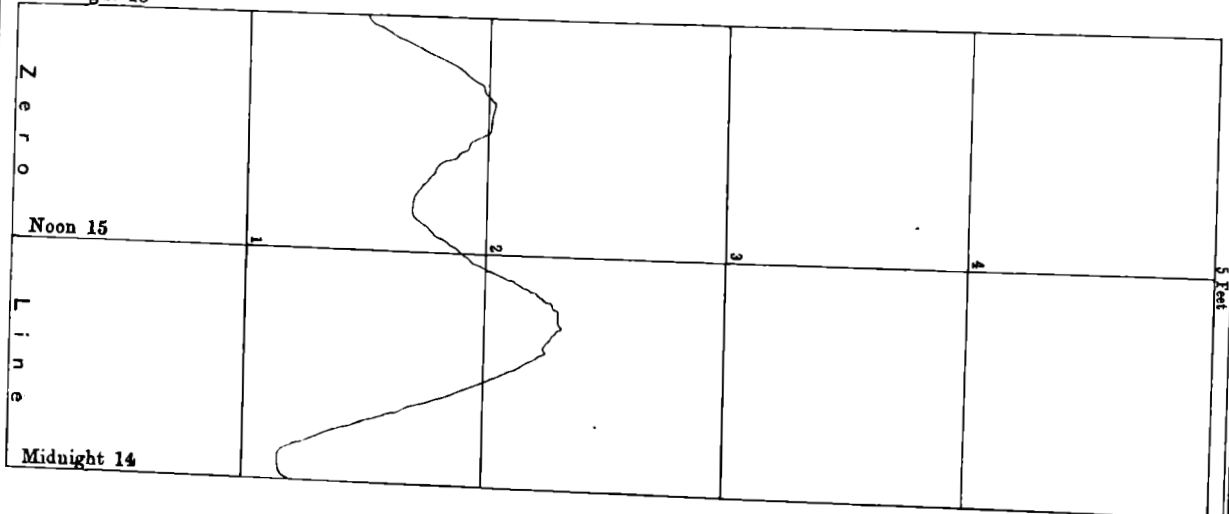
Midnight 7



Full Moon — 6th August 1884

Neap Tide — 15th August 1884

Midnight 15



Last Quarter — 14th August 1884

*Photoincographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun, September 1900.*

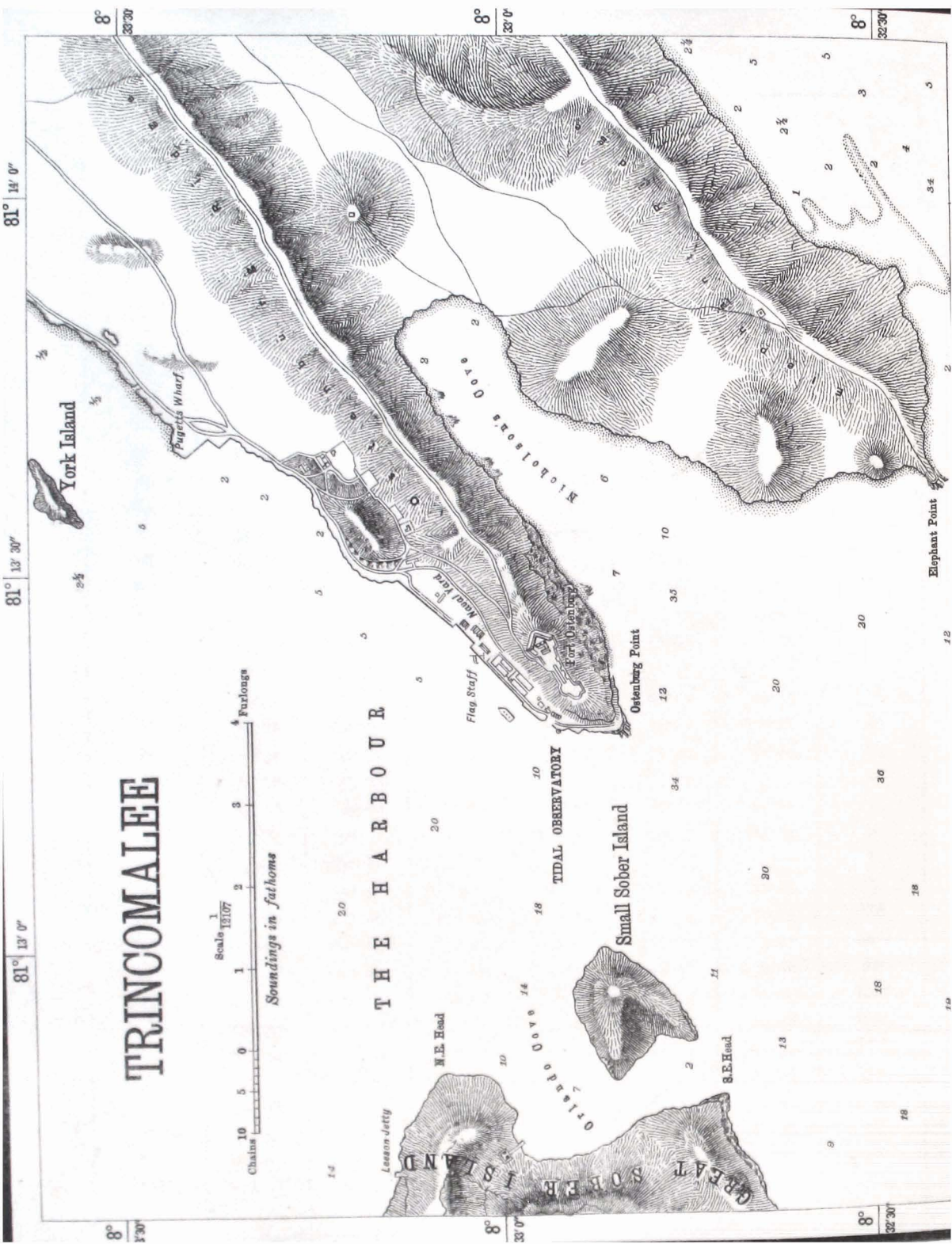
*Values of H's at Colombo.*

TIDE	H						TIDE
	1884-85	1885-86	1886-87	1887-88	1888-89	1889-90	
	Feet	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0.018	0.030	0.003	0.006	0.004	0.016	S <sub>1</sub>
S <sub>2</sub>	.362	.389	.404	.404	.392	.394	S <sub>2</sub>
S <sub>3</sub>	.004	.004	.004	.006	.005	.005	S <sub>3</sub>
S <sub>6</sub>	.002	.002	.002	.001	.002	.002	S <sub>6</sub>
S <sub>8</sub>	.001	.001	.000	.000	.000	.001	S <sub>8</sub>
M <sub>1</sub>	.008	.013	.006	.007	.015	.014	M <sub>1</sub>
M <sub>2</sub>	.546	.563	.590	.593	.596	.586	M <sub>2</sub>
M <sub>3</sub>	.015	.015	.014	.016	.012	.016	M <sub>3</sub>
M <sub>4</sub>	.015	.014	.017	.018	.017	.018	M <sub>4</sub>
M <sub>6</sub>	.002	.003	.005	.004	.004	.004	M <sub>6</sub>
M <sub>8</sub>	.000	.001	.000	.001	.001	.001	M <sub>8</sub>
O	.093	.101	.091	.092	.098	.091	O
K <sub>1</sub>	.237	.231	.239	.240	.240	.238	K <sub>1</sub>
K <sub>2</sub>	.072	.104	.126	.115	.127	.105	K <sub>2</sub>
P	.082	.062	.068	.066	.071	.081	P
J	.030	.006	.013	.022	.017	.008	J
Q	.029	.027	.031	.036	.035	.031	Q
L	.028	.018	.038	.028	.035	.016	L
N	.063	.050	.073	.075	.085	.090	N
λ	.024	.032	.016	...	...	...	λ
ν	.023	.014	.011	.022	.021	.017	ν
μ	.020	.017	.018	.016	.019	.014	μ
R	...	.059	...	...	...	...	R
T	...	.041	...	.014	.033	.047	T
MS	.005	.008	.009	.009	.010	.012	MS
2SM	.008	.005	.008	.005	.007	.014	2SM
2N	.011	.012	.008	.015	.008	.008	2N
M <sub>2</sub> N	.031	.014	.009	.013	.027	.037	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	.004	.002	.007	.009	.010	.001	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	.005	.002	.005	.005	.005	.005	2M <sub>2</sub> K <sub>1</sub>
Mm	.043	.035	.040	.028	.051	.026	Mm
Mf	.033	.064	.049	.066	.015	.030	Mf
MSf	.014	.012	.026	.025	.010	.016	MSf
Sa	.328	.267	.323	.331	.276	.353	Sa
Ssa	.123	.060	.155	.105	.190	.165	Ssa

## TIDAL OBSERVATIONS.

Values of  $\kappa$ 's at Colombo.

TIDE	$\kappa$						TIDE
	1884-85	1885-86	1886-87	1887-88	1888-89	1889-90	
$S_1$	61.68	59.87	142.77	358.09	62.85	61.63	$S_1$
$S_2$	99.60	101.28	90.30	92.48	94.11	94.34	$S_2$
$S_4$	211.50	248.46	225.94	218.33	247.38	265.60	$S_4$
$S_6$	188.53	214.38	144.16	148.00	195.95	170.13	$S_6$
$S_8$	236.31	105.95	108.44	108.44	291.80	172.03	$S_8$
$M_1$	56.56	192.29	288.84	15.35	347.82	340.92	$M_1$
$M_2$	52.78	54.04	45.83	46.95	51.14	48.40	$M_2$
$M_3$	169.49	166.04	161.36	168.12	170.48	181.62	$M_3$
$M_4$	179.76	174.19	164.55	171.35	167.93	164.14	$M_4$
$M_6$	76.27	62.83	346.03	1.97	5.30	27.83	$M_6$
$M_8$	54.23	228.21	145.52	107.37	227.24	87.71	$M_8$
O	64.30	67.36	59.23	62.03	60.76	58.25	O
$K_1$	35.72	35.67	29.26	30.70	33.48	31.77	$K_1$
$K_2$	108.98	82.45	84.74	90.42	93.12	81.39	$K_2$
P	34.05	11.86	29.87	27.72	36.65	17.12	P
J	36.95	59.88	1.80	26.24	50.47	45.03	J
Q	80.79	88.34	81.74	86.57	90.82	99.45	Q
L	53.79	46.01	64.41	27.22	54.67	57.11	L
N	28.53	46.72	29.94	31.09	33.40	31.44	N
$\lambda$	59.07	55.85	16.40	...	...	...	$\lambda$
$\nu$	39.47	49.84	76.34	47.53	22.13	11.07	$\nu$
$\mu$	105.63	96.51	122.45	111.12	108.33	82.94	$\mu$
R	...	339.70	...	...	...	...	R
T	...	353.08	...	117.48	77.94	27.24	T
MS	258.28	267.88	260.33	237.22	243.94	251.55	MS
2SM	279.95	348.65	357.28	321.69	334.31	5.41	2SM
2N	50.96	122.83	15.61	91.58	342.25	79.30	2N
$M_2N$	252.45	256.23	262.00	306.29	281.20	280.19	$M_2N$
$M_2K_1$	154.35	107.03	27.42	91.86	140.40	174.28	$M_2K_1$
$2M_2K_1$	181.94	83.42	86.55	49.39	355.63	314.72	$2M_2K_1$
Mm	18.39	321.39	23.98	76.28	16.47	67.06	Mm
Mf	320.88	13.97	343.51	22.76	65.08	304.32	Mf
MSf	35.96	60.25	274.83	280.39	261.77	277.82	MSf
Sa	308.75	326.88	314.71	298.52	303.70	296.17	Sa
Ssa	128.39	83.27	121.94	116.65	88.52	130.01	Ssa



# TRINCOMALEE

## THE HARBOUR

Scale 1/13107  
Chains 10 5 0 1 2 3 4  
Furlongs  
Soundings in fathoms

81° 13' 00" 81° 13' 30" 81° 14' 00"

8° 32' 30" 8° 33' 00" 8° 32' 30"



## TRINCOMALEE.

(*Tidal Observatory, Lat. 8° 33' N., Long. 81° 13' E.*)

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The tidal observatory at Trincomalee, on the north-east coast of Ceylon, is one of the minor observatories at which five years' observations are considered sufficient, and is situated on the small stone wharf at the south end of the Naval Dockyard on the east side of Trincomalee Harbour, in the position shewn on the accompanying chart. It is twelve feet square, with wooden walls and a tiled roof. Half the building rests on the wharf wall, to which it is secured by iron bolts, while the other half, which projects beyond the wharf, is supported by three iron struts thrown out from the wall. The float-cylinder is a massive iron drainage pipe twenty inches in internal diameter and twelve and a half feet long. Its top rises one foot four inches above the floor of the observatory, and is three feet above the highest tides; and the bottom, which is closed with an iron-wood plug, is five and a half feet below the lowest tides, and rests on three stout iron pegs driven into the bed of the harbour above which they project about nine inches. The communication is through five perforations (each an inch in diameter) in the iron-wood plug at the bottom of the cylinder.

The working scale of the tide-gauge is the natural scale.

Registrations were commenced on the 10th November, 1890, and have been very satisfactory up to the present.

Barometrical and anemometrical observations are being carried on simultaneously with the tidal observations. The barometer has been set up in the tidal observatory. The anemometer was at first

on the roof of the same building and worked there until the 9th March, 1893, when it was removed to the top of Fort Ostenburg immediately above the Dockyard, a much better position as it is exposed to the wind from every quarter, whereas the tidal observatory is much shut in.

The bench-mark of reference is on a large stone in the wharf wall of the Naval Dockyard, twenty-five feet from the tidal observatory door, bearing the inscription  $\overset{\text{G. T. S.}}{\text{A. } \square} \underset{\text{B. M.}}{\text{.}}$  1890. It is 5.900 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = IX<sup>h</sup> 23<sup>m</sup>.

The highest high water recorded was 4.3 feet above the zero of the gauge, and occurred in November, 1892.

The lowest low water recorded was 0.2 foot above the zero of the gauge, and occurred in March, 1892.

In 1890-91 the mean range of largest ordinary springs was found to be 2.1 feet.

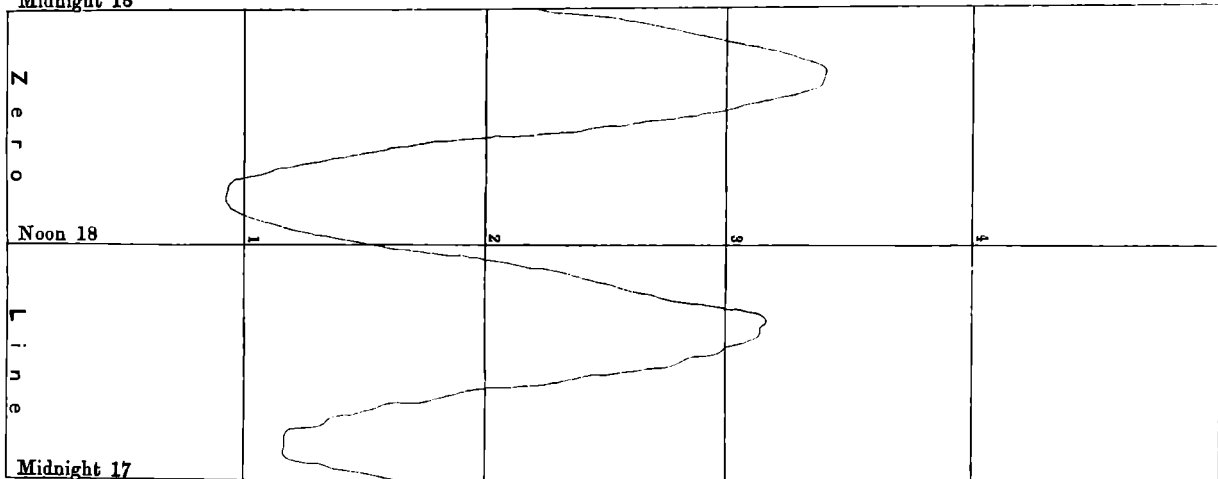
The height of mean-sea-level above the zero of the gauge had the following values:—

1890-91	...	...	...	1.842 feet.
1891	...	...	...	1.826 „
1892	...	...	...	2.043 „

TIDAL CURVES  
at  
TRINCOMALEE

Spring Tide — 18th October 1891

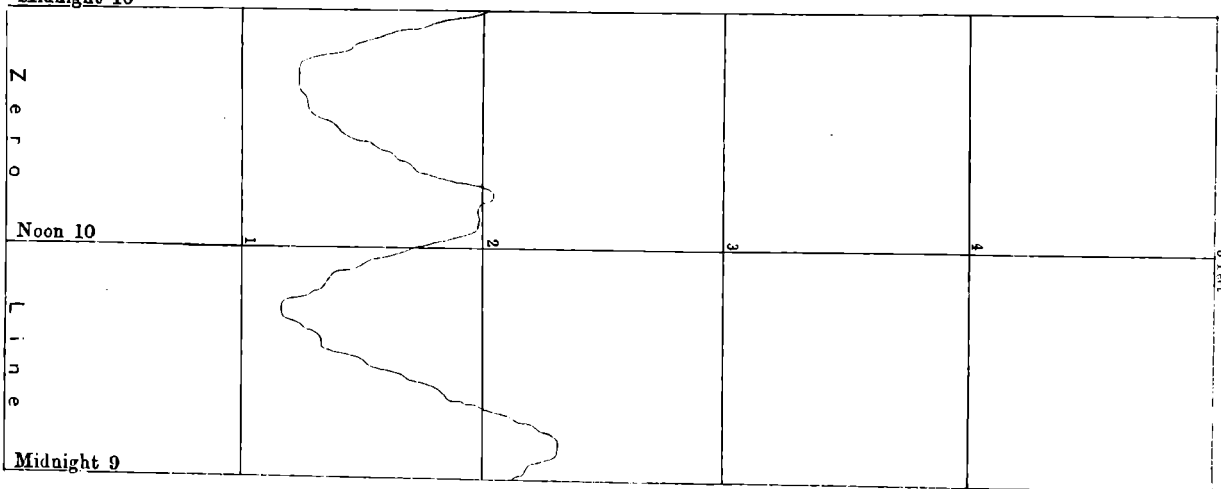
Midnight 18



Full Moon — 17th October 1891

Neap Tide — 10th October 1891

Midnight 10



First Quarter — 10th October 1891

*Photoincographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dún, September 1900.*

*Values of H's and  $\kappa$ 's at Trincomalee.*

TIDE	H			$\kappa$			TIDE
	1890-91	1891	1892	1890-91	1891	1892	
	Feet	Feet	Feet	°	°	°	
S <sub>1</sub>	0·018	0·020	0·015	65·25	64·86	55·11	S <sub>1</sub>
S <sub>2</sub>	·191	·192	·208	269·31	264·50	266·49	S <sub>2</sub>
S <sub>3</sub>	·007	·006	·003	251·57	258·89	272·05	S <sub>3</sub>
S <sub>6</sub>	·000	·001	·001	45·00	48·37	167·47	S <sub>6</sub>
S <sub>8</sub>	·001	·001	·000	323·13	336·80	26·57	S <sub>8</sub>
M <sub>1</sub>	·008	·007	·006	4·92	23·99	305·74	M <sub>1</sub>
M <sub>2</sub>	·587	·591	·621	240·15	242·08	237·86	M <sub>2</sub>
M <sub>3</sub>	·004	·001	·005	194·03	340·82	124·92	M <sub>3</sub>
M <sub>4</sub>	·013	·012	·009	224·67	258·82	238·27	M <sub>4</sub>
M <sub>6</sub>	·006	·006	·002	108·71	115·51	112·73	M <sub>6</sub>
M <sub>8</sub>	·002	·003	·001	159·61	82·72	214·69	M <sub>8</sub>
O	·062	·064	·064	307·58	308·31	307·40	O
K <sub>1</sub>	·211	·211	·213	330·86	331·61	330·97	K <sub>1</sub>
K <sub>2</sub>	·072	·079	·065	249·29	264·36	265·33	K <sub>2</sub>
P	·074	·076	·068	343·26	340·21	330·02	P
J	·020	·019	·011	279·21	273·03	300·91	J
Q	·011	·009	·009	177·27	192·95	212·39	Q
L	·053	·058	·067	308·76	332·51	248·78	L
N	·144	·147	·127	227·80	224·76	226·30	N
$\lambda$	...	...	...	...	...	...	$\lambda$
$\nu$	·048	·054	·059	208·88	245·16	200·29	$\nu$
$\mu$	·033	·037	·039	160·13	165·91	163·28	$\mu$
R	...	...	...	...	...	...	R
T	...	·056	·050	...	187·56	239·26	T
MS	·010	·013	·011	189·70	198·21	212·41	MS
2SM	·010	·007	·024	248·07	231·97	248·23	2SM
2N	·024	·020	·043	231·60	195·37	238·47	2N
M <sub>2</sub> N	·007	·007	·028	322·30	245·28	84·55	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	·008	·005	·008	197·68	213·45	280·69	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	·005	·005	·005	21·62	14·11	141·01	2M <sub>2</sub> K <sub>1</sub>
Mm	·023	·031	·067	330·72	338·68	135·61	Mm
Mf	·055	·050	·055	14·54	19·54	4·26	Mf
MSf	·015	·012	·009	235·75	266·46	237·18	MSf
Sa	·291	·266	·255	281·40	287·80	231·24	Sa
Ssa	·207	·165	·169	133·69	139·70	122·30	Ssa

## P Á M B A N .

(PÁMBAN PASS.)

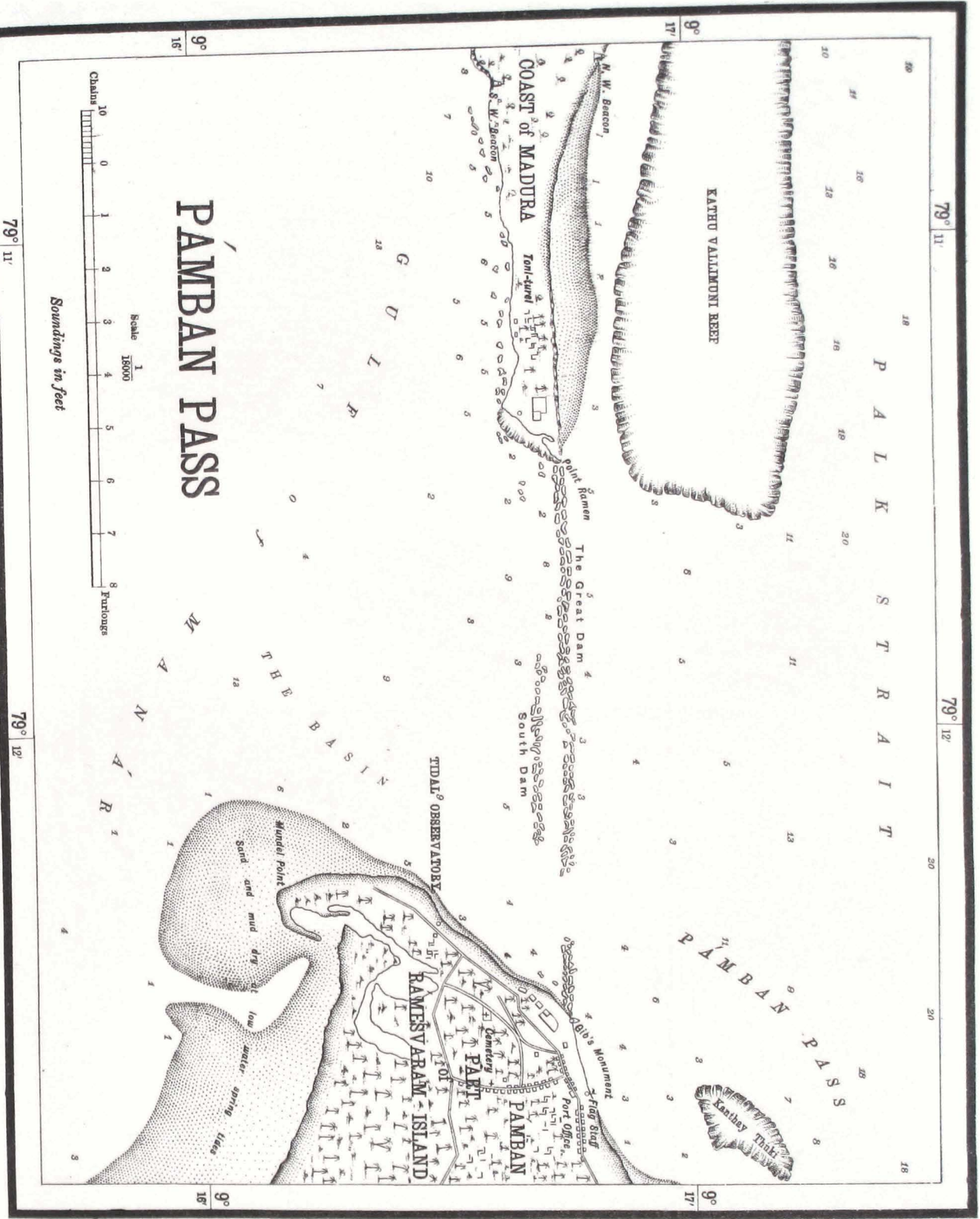
*(Tidal Observatory, Lat. 9° 16' N., Long. 79° 12' E.)*

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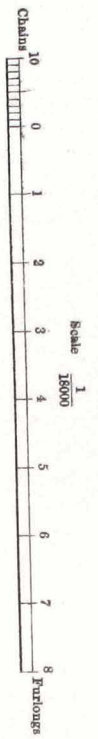
Pámban Pass is the channel connecting the Gulf of Manar and Palk Straits, and separating the island of Rámesvaram (adjoining it on the east) from a remarkable, straight reef of rocks (immediately on its west) called the Great Dam, which extends westwards for a mile and a quarter and then joins the coast of India at the point known as Toni-turei. The tidal observatory was situated on the western shore of Rámesvaram, about half a mile south of the town of Pámban and a hundred yards south of the Telegraph Cable House, in the position shown on the accompanying chart, and was one of the minor observatories at which five years' observations are considered sufficient. It was a wooden cabin, twelve feet square, supported on six piles driven about five feet into the sand, and having its floor well above high water. The float-cylinder was of iron, twenty-two inches in diameter and nine feet long. The top was about a foot above the floor of the observatory and about two feet above highest tides, and the bottom (which was closed) was sunk in the sand and was about three feet below lowest tides. The communication was through a two-inch pipe, eighty-one feet in length, and bent so as to form a siphon, the first fifty-six feet of it being iron piping and the outer twenty-five feet being flexible tubing. The short branch left the cylinder about one and a half feet above the bottom and rose about three feet vertically to a point where an air cock was placed at about mean-sea-level; from this point the pipe sloped downwards into deep water and ended, about ten feet below the lowest tides, in a rose supported on a tripod.

The working scale of the tide-gauge was the natural scale.

Registrations were commenced on the 1st October, 1878. In December of the same year, during bad weather, the piles of the observatory were denuded of their supporting sand, but prompt measures being taken, no interruption occurred. In January, February and March, 1880, air got into the communication pipe through the packing round the joints and caused a small amount of retardation. In 1881



Soundings in feet



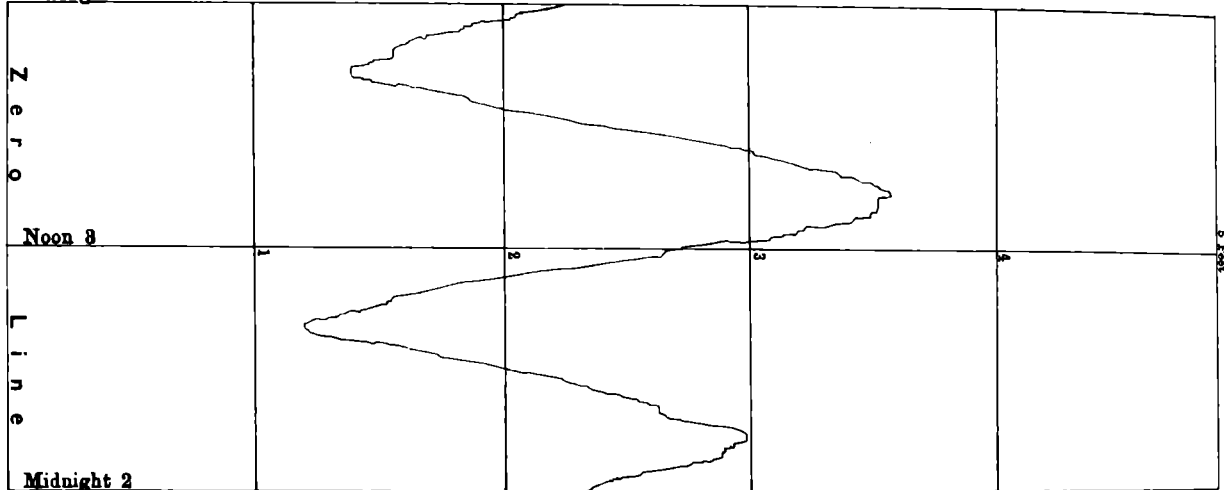
# PAMBAN PASS

Photostereograph at the Office of the Tri-geometrical Branch, Survey of India, Dehra Dun, January 1888.

TIDAL CURVES  
at  
PÁMBAN PASS

Spring Tide — 3rd August 1879

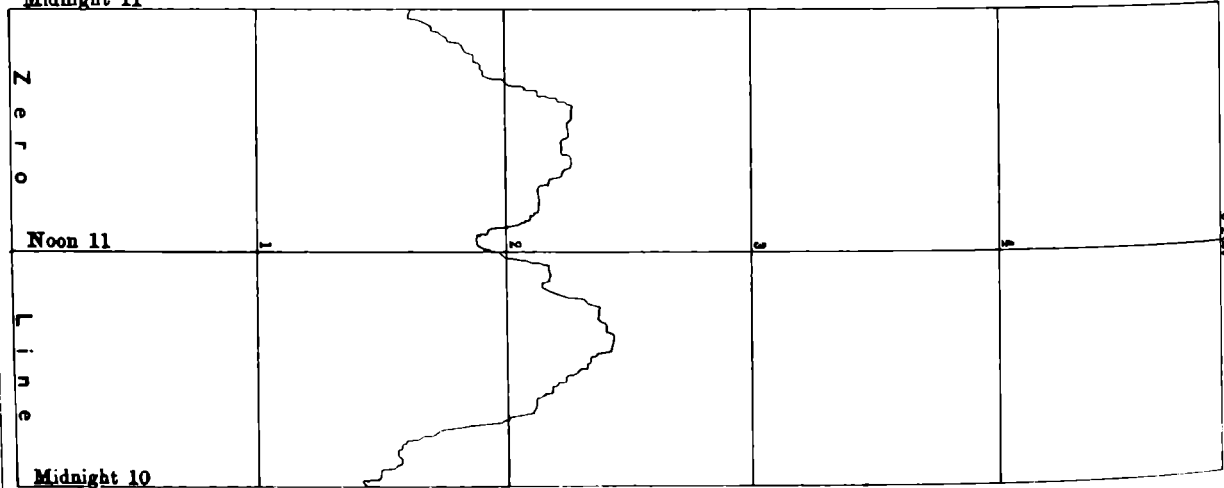
Midnight 8



Full Moon — 2nd August 1879

Neap Tide — 11th August 1879

Midnight 11



Last Quarter — 10th August 1879

*Photocopyographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dún, September 1900.*

there were several short stoppages caused by accidents to various parts of the mechanism of the tide-gauge: and finally, in February, 1882, parts of the communication pipe having been eaten into holes had to be renewed thus causing an interruption of work for three days. The observations were continued until the 28th December, 1882, when heavy weather endangered the safety of the observatory, and the instruments had to be removed. The necessary strengthening of the observatory would have caused a large break in the fifth year's observations, and as four years' satisfactory registrations had been obtained it was not thought necessary to extend the observations further. The disturbances of the surface of the ocean caused by an earthquake whose centre lay between Port Blair and Car Nicobar were recorded at this station by the self-registering tide-gauge on the 31st December, 1881.

Barometrical and anemometrical observations were carried on simultaneously with the tidal observations. The barometer was placed in the observatory and the anemometer on the top of the same building.

The bench-mark of reference is a stone embedded in a block of masonry close to the western wall of the Telegraph Cable House and marked  $\begin{matrix} \text{G. T. S.} \\ \square \\ \text{B. M.} \\ \text{A.} \end{matrix}$ . It is 10·18 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = 1<sup>h</sup> 48<sup>m</sup>.

The highest high water recorded was 4·8 feet above the zero of the gauge, and occurred in December, 1880.

The lowest low water recorded was 0·9 foot above the zero of the gauge, and occurred in August, 1880.

In 1878-79 the mean range of largest ordinary springs was found to be 2·6 feet.

The height of mean-sea-level above the zero of the gauge had the following values:—

1878-79	...	...	...	2·666 feet.
1879-80	...	...	...	2·707 „
1880-81	...	...	...	2·759 „
1881-82	...	...	...	2·705 „



## TIDAL OBSERVATIONS.

*Values of H's at Pámban.*

TIDE	H				TIDE
	1878-79	1879-80	1880-81	1881-82	
	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0'036	0'049	0'035	0'022	S <sub>1</sub>
S <sub>2</sub>	'377	'375	'377	'360	S <sub>2</sub>
S <sub>4</sub>	'005	'001	'004	'003	S <sub>4</sub>
S <sub>6</sub>	'002	'001	'005	'006	S <sub>6</sub>
S <sub>8</sub>	'004	'005	'002	'001	S <sub>8</sub>
M <sub>1</sub>	'013	'009	'013	'008	M <sub>1</sub>
M <sub>2</sub>	'589	'585	'598	'569	M <sub>2</sub>
M <sub>3</sub>	'016	'016	'015	'017	M <sub>3</sub>
M <sub>4</sub>	'020	'016	'015	'014	M <sub>4</sub>
M <sub>6</sub>	'011	'011	'011	'009	M <sub>6</sub>
M <sub>8</sub>	'005	'004	'004	'007	M <sub>8</sub>
O	'114	'113	'116	'115	O
K <sub>1</sub>	'297	'293	'295	'291	K <sub>1</sub>
K <sub>2</sub>	'103	'110	'116	'121	K <sub>2</sub>
P	'105	'110	'108	'115	P
J	'008	'013	'014	'021	J
Q	'025	'021	'023	'016	Q
L	'023	'026	'016	'026	L
N	'076	'087	'084	'082	N
λ	'017	'023	'008	'014	λ
ν	'016	'034	'030	'027	ν
μ	'004	'010	'012	'011	μ
R	...	'012	...	'019	R
T	...	'038	...	'012	T
MS	'021	'017	'018	'017	MS
2SM	'010	'008	'012	'008	2SM
2N	'003	'015	'008	'008	2N
M <sub>2</sub> N	'022	'023	'013	'015	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	'005	'005	'007	'001	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	'003	'007	'007	'008	2M <sub>2</sub> K <sub>1</sub>
Mm	'063	'053	'033	'043	Mm
Mf	'045	'040	'053	'033	Mf
MSf	'016	'013	'027	'007	MSf
Sa	'122	'138	'164	'171	Sa
Ssa	'138	'178	'184	'129	Ssa

*Values of  $\kappa$ 's at Pámban.*

TIDE	$\kappa$				TIDE
	1878-79	1879-80	1880-81	1881-82	
	°	°	°	°	
S <sub>1</sub>	146·13	130·89	153·29	163·15	S <sub>1</sub>
S <sub>2</sub>	90·11	92·31	91·35	94·19	S <sub>2</sub>
S <sub>4</sub>	286·82	191·31	261·87	304·16	S <sub>4</sub>
S <sub>6</sub>	245·56	167·91	195·46	179·05	S <sub>6</sub>
S <sub>8</sub>	248·50	254·75	257·20	135·00	S <sub>8</sub>
M <sub>1</sub>	16·74	38·20	64·33	18·94	M <sub>1</sub>
M <sub>2</sub>	46·55	46·75	45·99	48·51	M <sub>2</sub>
M <sub>3</sub>	170·37	168·41	164·79	177·45	M <sub>3</sub>
M <sub>4</sub>	198·68	190·48	199·10	187·35	M <sub>4</sub>
M <sub>6</sub>	41·90	50·29	40·24	34·25	M <sub>6</sub>
M <sub>8</sub>	294·01	347·63	303·29	312·85	M <sub>8</sub>
O	46·52	44·83	42·81	46·77	O
K <sub>1</sub>	43·66	45·02	45·17	48·73	K <sub>1</sub>
K <sub>2</sub>	83·59	92·07	88·59	94·19	K <sub>2</sub>
P	43·73	46·84	45·78	49·57	P
J	68·24	44·49	37·95	42·10	J
Q	84·20	98·42	91·24	81·48	Q
L	56·01	48·86	78·71	50·20	L
N	29·10	30·26	32·20	31·83	N
$\lambda$	63·03	24·06	353·92	173·02	$\lambda$
$\nu$	81·70	49·26	14·96	334·12	$\nu$
$\mu$	77·62	98·04	94·88	148·26	$\mu$
R	...	132·75	...	94·37	R
T	...	104·14	...	79·27	T
MS	291·60	293·92	285·94	294·52	MS
2SM	5·58	338·44	339·81	288·49	2SM
2N	356·91	13·86	75·61	331·14	2N
M <sub>2</sub> N	157·69	229·65	170·99	265·83	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	155·64	243·16	309·65	48·17	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	346·54	319·17	297·41	277·23	2M <sub>2</sub> K <sub>1</sub>
Mm	348·98	57·52	22·84	39·72	Mm
Mf	1·56	355·31	359·13	343·58	Mf
MSf	173·59	208·90	156·88	26·51	MSf
Sa	298·92	318·05	286·80	304·03	Sa
Ssa	95·54	109·88	116·70	111·04	Ssa

## NEGAPATAM.

(*Tidal Observatory, Lat. 10° 46' N., Long. 79° 51' E.*)

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The tidal observatory at Negapatam at the southern extremity of the Coromandel Coast of India was one of the minor observatories at which five years' observations are generally considered sufficient, and was situated on the south side of the backwater locally called Kadavcár, and about a hundred yards east of the Quay wall, in the position shown on the accompanying chart. It was a wooden cabin built on piles driven about eight feet into the ground, and having its floor about three feet above highest tides. Instead of an iron float-cylinder a strong teak casing about two feet square in section and twelve feet long, protected by sheet copper, was used. The top of the casing was about three and a half feet above the highest tides and the bottom an equal distance below the lowest tides. The communication was through holes pierced in the casing about two feet below the lowest tides.

The working scale of the tide-gauge was the natural scale.

Registrations were commenced on the 1st November, 1881, but were not properly recorded until the 6th of the following month. They were then satisfactory till November, 1883; but about that time the observations were quite vitiated owing to the extreme retardation caused by a serious accumulation of sand round the float-casing. Attempts were made to clear away the sand, and improve the communication by boring more holes in the casing and using a copper communication pipe about eleven feet long; but the observations continued to be untrustworthy until March, 1885, when the natural conditions that had caused the accumulation seem to have changed, and the casing was again left free and was with much care kept so until the 30th April, 1888, when the observations were completed and the observatory closed. The years in which the observations were satisfactory and have been accepted are 1881-82, 1882-83, 1885-86, 1886-87, 1887-88.

79 51

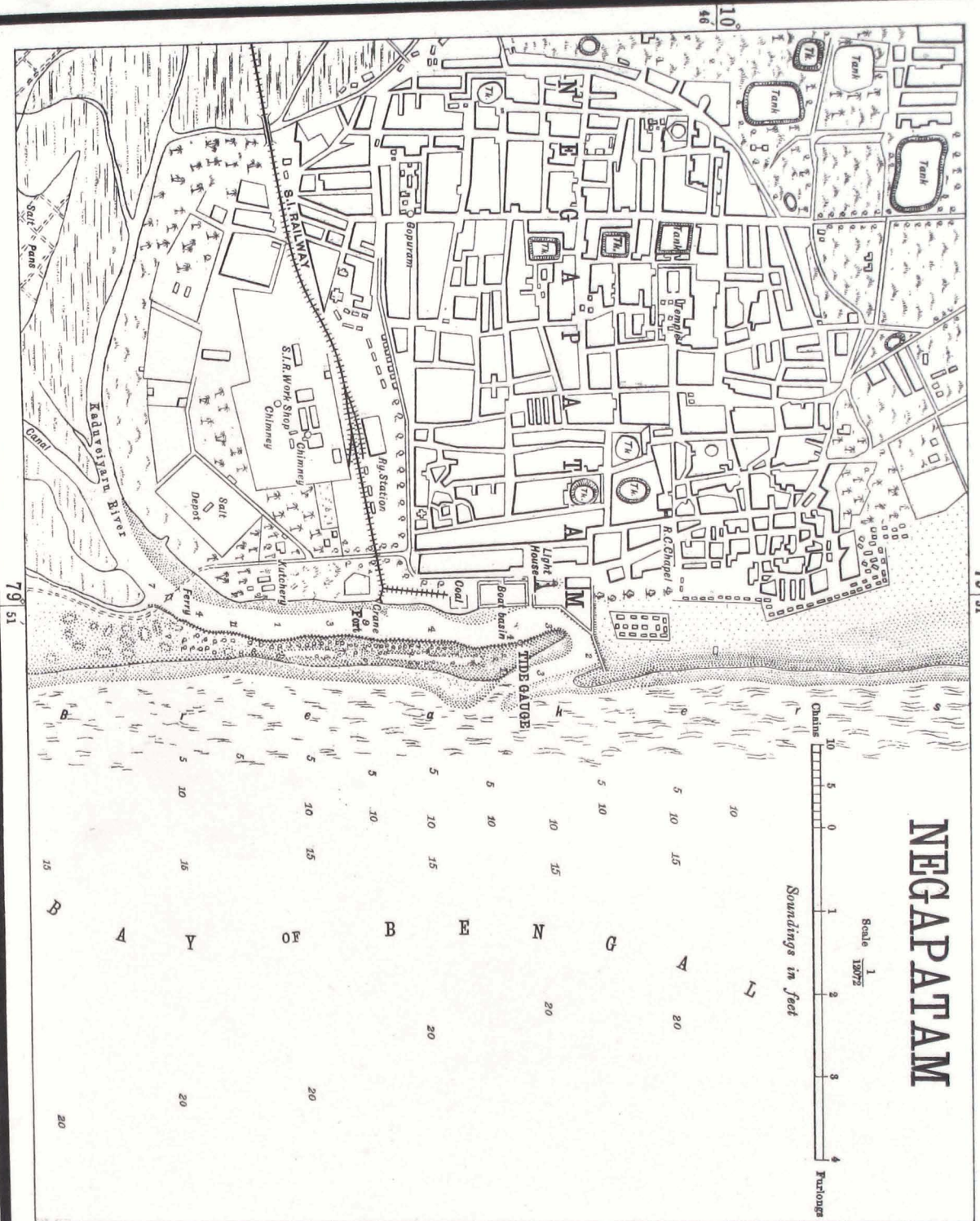
# NEGAPATAM

Scale  
1  
1207 1/2

Soundings in feet



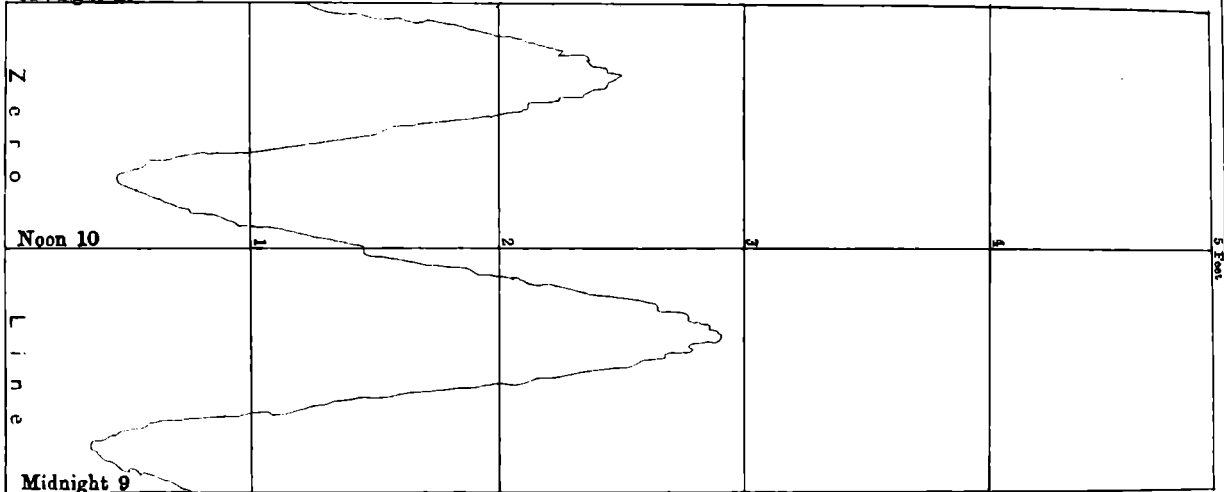
79 51



TIDAL CURVES  
at  
NEGAPATAM

Spring Tide — 10th August 1885

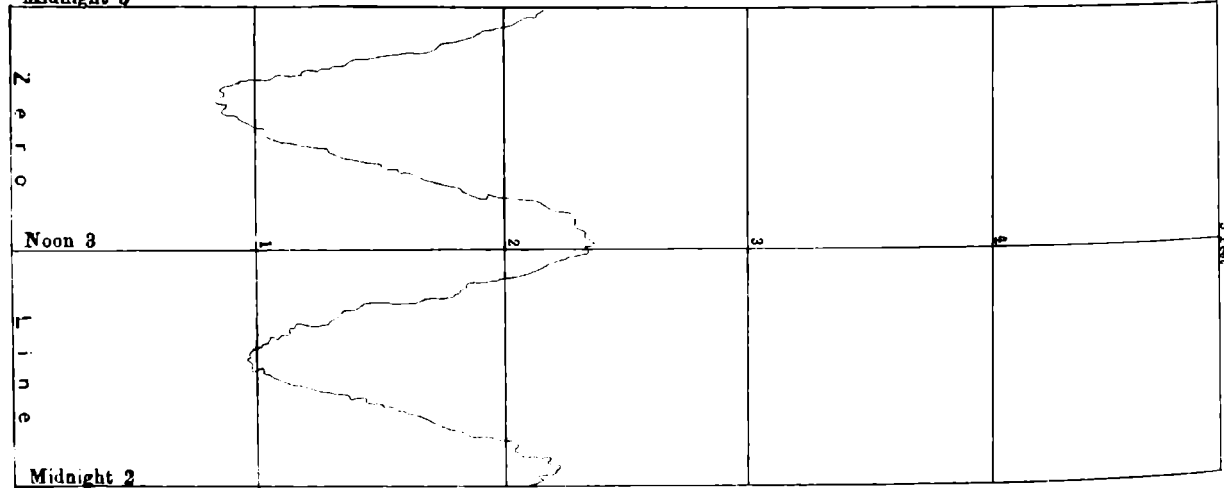
Midnight 10



New Moon — 10th August 1885

Neap Tide — 3rd August 1885

Midnight 3



Last Quarter — 3rd August 1885

*Photocopyographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun, September 1900.*

The disturbances of the surface of the ocean, caused by an earthquake whose centre lay between Port Blair and Car Nicobar, were recorded at this station by the self-registering tide-gauge on the 31st December, 1881, and those caused by the Krakatoa volcanic eruptions were similarly recorded on the 27th August, 1883.

Barometrical and anemometrical observations were carried on simultaneously with the tidal observations. The barometer was placed in the observatory and the anemometer on the top of the same building.

The bench-mark of reference is a flag stone embedded in the verandah of the Port Office and opposite the Custom Office window, and engraved  $\begin{matrix} \text{G. T. S.} \\ \text{O} \\ \text{B.M.} \end{matrix}$  A. It is 11·605 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = IX<sup>h</sup> 0<sup>m</sup>.

The highest high water recorded was 5·1 feet above the zero of the gauge, and occurred in November, 1886.

The lowest low water recorded was identical with the zero of the gauge, and occurred in August, 1885.

In 1881-82 the mean range of largest ordinary springs was found to be 2·6 feet.

The height of mean-sea-level above the zero of the gauge had the following values:—

1881-82	...	...	...	1·996 feet.
1882-83	...	...	...	2·048 „
1885-86	...	...	...	1·811 „
1886-87	...	...	...	2·048 „
1887-88	...	...	...	2·047 „

## TIDAL OBSERVATIONS.

*Values of H's at Negapatam.*

TIDE	H					TIDE
	1881-82	1882-83	1885-86	1886-87	1887-88	
	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0.048	0.044	0.040	0.021	0.055	S <sub>1</sub>
S <sub>2</sub>	.271	.277	.284	.261	.249	S <sub>2</sub>
S <sub>4</sub>	.006	.004	.006	.006	.004	S <sub>4</sub>
S <sub>6</sub>	.000	.000	.001	.001	.002	S <sub>6</sub>
S <sub>8</sub>	.001	.001	.001	.001	.000	S <sub>8</sub>
M <sub>1</sub>	.003	.006	.017	.016	.008	M <sub>1</sub>
M <sub>2</sub>	.712	.727	.739	.706	.654	M <sub>2</sub>
M <sub>3</sub>	.003	.003	.004	.002	.004	M <sub>3</sub>
M <sub>4</sub>	.023	.018	.017	.021	.031	M <sub>4</sub>
M <sub>6</sub>	.010	.013	.011	.010	.009	M <sub>6</sub>
M <sub>8</sub>	.005	.004	.004	.003	.001	M <sub>8</sub>
O	.092	.089	.087	.087	.088	O
K <sub>1</sub>	.222	.227	.224	.216	.210	K <sub>1</sub>
K <sub>2</sub>	.071	.082	.078	.097	.091	K <sub>2</sub>
P	.083	.085	.080	.075	.074	P
J	.006	.016	.019	.014	.008	J
Q	.007	.007	.007	.001	.003	Q
L	.022	.031	.039	.047	.030	L
N	.164	.152	.168	.151	.157	N
λ	.025	.005	.016	.031	...	λ
ν	.048	.047	.039	.015	.020	ν
μ	.018	.024	.016	.015	.014	μ
R	...	.031	...	.031	...	R
T	...	.050	...	.037	...	T
MS	.019	.017	.018	.018	.024	MS
2SM	.007	.006	.006	.003	.006	2SM
2N	.027	.026	.035	.015	.020	2N
M <sub>2</sub> N	.015	.032	.024	.048	.022	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	.012	.012	.010	.015	.020	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	.007	.007	.006	.009	.007	2M <sub>2</sub> K <sub>1</sub>
Mm	.081	.032	.076	.008	.048	Mm
Mf	.061	.017	.080	.098	.073	Mf
MSf	.084	.097	.025	.026	.043	MSf
Sa	.543	.522	.348	.444	.364	Sa
Ssa	.400	.316	.300	.328	.377	Ssa

*Values of  $\kappa$ 's at Negapatam.*

TIDE	$\kappa$					TIDE
	1881-82	1882-83	1885-86	1886-87	1887-88	
	o	o	o	o	o	
S <sub>1</sub>	116.78	99.59	95.91	97.36	120.32	S <sub>1</sub>
S <sub>2</sub>	282.72	285.69	280.91	281.07	285.44	S <sub>2</sub>
S <sub>4</sub>	136.36	166.33	106.61	125.88	139.69	S <sub>4</sub>
S <sub>6</sub>	135.00	165.96	146.31	251.57	97.60	S <sub>6</sub>
S <sub>8</sub>	225.00	228.37	240.95	218.66	153.44	S <sub>8</sub>
M <sub>1</sub>	148.92	72.88	303.16	289.39	3.75	M <sub>1</sub>
M <sub>2</sub>	251.22	252.05	249.31	250.99	252.74	M <sub>2</sub>
M <sub>3</sub>	73.46	133.35	85.49	72.57	78.35	M <sub>3</sub>
M <sub>4</sub>	76.06	77.16	71.18	75.58	96.36	M <sub>4</sub>
M <sub>6</sub>	130.33	126.07	124.49	135.14	133.53	M <sub>6</sub>
M <sub>8</sub>	297.26	308.82	252.11	334.54	149.21	M <sub>8</sub>
O	319.82	323.24	318.05	325.84	321.25	O
K <sub>1</sub>	345.11	345.32	346.55	348.58	349.04	K <sub>1</sub>
K <sub>2</sub>	280.50	290.52	285.04	286.09	281.93	K <sub>2</sub>
P	342.47	350.18	339.72	347.52	344.40	P
J	348.09	307.30	356.72	34.82	355.74	J
Q	143.17	218.60	284.01	310.17	34.46	Q
L	278.33	278.85	264.92	219.13	272.14	L
N	242.78	245.55	237.00	231.62	239.46	N
$\lambda$	233.77	228.84	306.94	324.38	...	$\lambda$
$\nu$	228.46	206.21	209.02	273.36	279.22	$\nu$
$\mu$	131.73	112.94	127.70	103.32	104.27	$\mu$
R	...	348.88	...	300.28	...	R
T	...	254.78	...	243.38	...	T
MS	95.94	96.39	85.61	107.12	111.26	MS
2SM	160.57	216.11	198.15	230.46	207.74	2SM
2N	213.32	219.95	219.33	183.27	213.73	2N
M <sub>2</sub> N	72.18	83.72	120.70	181.63	155.28	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	154.04	184.11	69.02	143.81	195.41	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	331.17	346.54	334.53	335.54	336.23	2M <sub>2</sub> K <sub>1</sub>
Mm	345.28	310.44	318.25	346.87	352.42	Mm
Mf	34.83	338.46	354.06	5.40	351.26	Mf
MSf	1.78	13.12	81.65	51.16	15.11	MSf
Sa	230.61	232.64	248.80	229.60	227.97	Sa
Ssa	125.53	134.13	128.63	129.04	120.86	Ssa



## M A D R A S.

(*Tidal Observatory, Lat. 13° 5' N., Long. 80° 18' E.*)

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The tidal station of Madras was originally (and will be again) classed as one of the permanent stations; but tidal observations there are at present in abeyance, owing to the Madras Government having closed the tidal observatory after ten years' registrations had been obtained. Observations in the Madras Harbour were attempted first in 1879 with a float-cylinder about twelve feet long sunk in the sand to a depth of about five feet below low water, at a spot on the beach, beneath the flooring of the iron pier, one hundred feet above high water mark. The communication was through a three-inch pipe which left the cylinder at the bottom and which was in the form of a siphon. The short branch rose vertically outside the cylinder to about the level of mid-tide, and the pipe then sloped gently downwards for about six hundred feet into deep water. The observatory was a wooden cabin, twelve feet long by nine feet wide, firmly fixed to the beams and piles of the pier so that it could not settle. During the cyclone of the 20th and 21st May, 1879, the communication pipe was destroyed by the surf. It was found choked and dislocated, and the greater part of it so deeply buried in the sand that it could not be recovered. Another plan was then devised for connecting the cylinder with the sea. A siphon, made of one-inch gas piping, was carried from the bottom of the cylinder up to about three feet below the flooring of the pier so as to be safe from the action of the surf and was thence carried out under the flooring for about six hundred feet to a point whence it descended vertically into deep water. This arrangement also failed owing to the difficulty of expelling the air from so great a length of pipe. Observations at this site had consequently to be discontinued, and those which had been taken are not employed in the tidal calculations.

Early in 1880 a new tidal observatory was erected on the iron pier, in the position shown on the accompanying chart. The conditions of its construction, imposed by the Madras Government, were that the space occupied by it, should be the minimum possible, and that it should not interfere with the traffic. The original cabin was accordingly cut down to the smallest possible dimensions, and placed about the centre of the T-head of the pier. The new float-cylinder was twenty-seven feet long and only seven inches in diameter so as to present as small a surface as possible to the action of the surf. Its upper end was secured to, and rose a few inches above, the floor of the observatory, and its

80° 17'

80° 18'

# MADRAS

Scale 3754



Soundings in feet



13° 5'

13° 5'

80° 17'

80° 18'

Photostereographed at the Office of the Trigonometrical Branch, Survey of India, Dabra Dam, February 1897.

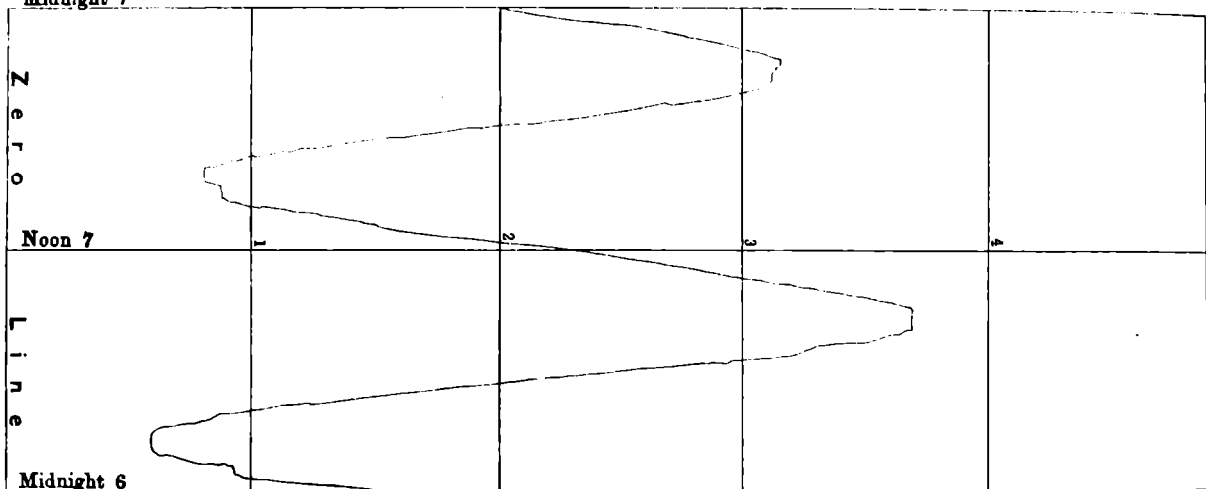
# TIDAL CURVES

at

## MADRAS

Spring Tide — 7th August 1884

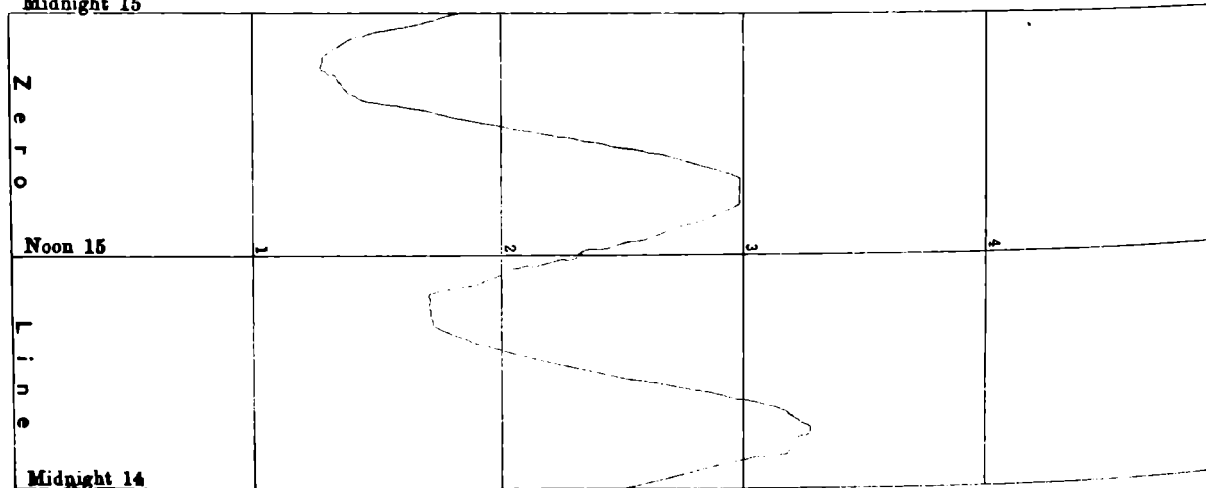
Midnight 7



Full Moon — 6th August 1884

Neap Tide — 15th August 1884

Midnight 15



Last Quarter — 14th August 1884

*Photomicrographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun, April 1900.*

lower end was about ten feet above the harbour-bed and about six feet below lowest tides. It was held in position vertically by three upright iron bars driven to a depth of about nine feet into the harbour-bed, and the whole was attached by a system of chain lashings to the contiguous piles of the pier. The communication was through a double rose protecting the bottom of the cylinder from sand and sea-weed, above which, and plugging the cylinder, was a wooden block through which a central hole one inch in diameter had been drilled, and which was capped by a copper cone in the apex of which there was a small perforation an eighth of an inch in diameter to hinder the momentary undulations of the external water being transmitted to the float. A specially constructed float was employed, six inches in diameter and three feet long, weighted at the bottom so as to remain vertical. The float-band after passing up from the float over the stud-wheel went down into a vertical pipe made for the reception of a specially devised counterpoise. The pipe, which was of three-inch bore, nine feet long, and closed at bottom, was fixed a couple of feet below the stud-wheel and passed down through the floor of the observatory.

The working scale of the tide-gauge was the natural scale.

Registrations were commenced on the 1st February, 1880. The gauge with which they were taken was modified to suit the peculiarities of the float and float-cylinder, the modification precluding the possibility of changing the working scale, so that special arrangements had to be made in order to register the extreme tides, which went beyond the limits of the recording drum. The gauge worked continuously during the first year and the registrations during the second were only interrupted for one period of seventeen days while the cylinder was being cleaned. There were many interruptions afterwards, and all along there was probably considerable retardation, though (owing to the surf, which rendered readings to a graduated staff impossible) it could not be measured. On the whole, owing to faults of design, to the choking of the double rose and minute communication hole, to friction of the stud-wheel and between the cylinder and float, which became covered with marine incrustations, to the small size of the float, to the counterpoise arrangement, and above all to the constant stopping of the driving clock from shocks caused by the traffic on the pier, the observations cannot be considered satisfactory. They were discontinued on the 10th October, 1890; but the Madras Government have recently consented to their resumption on the lines followed at other important tidal stations, at first temporarily, at the iron pier, and eventually, as a permanent measure, in a properly designed tidal observatory on one of the arms of the Harbour.

The disturbances of the surface of the ocean, caused by an earthquake whose centre lay between Port Blair and Car Nicobar, were recorded at this tidal station by the self-registering tide-gauge on the 31st December, 1881, and those caused by the Krakatoa volcanic eruptions were similarly recorded on the 27th August, 1883.

Barometrical, but not anemometrical observations were taken in the Port Office. They were not satisfactory; but all requisite meteorological statistics can be obtained from the Astronomical and Meteorological Observatories.

The bench-mark of reference consists of the inscription  $\overset{\text{G. T. S.}}{\underset{\text{B. M.}}{\text{O}}}$  cut on the west side of the Madras Memorial Stone laid by H. R. Highness the Prince of Wales on the 15th December, 1875, as a memorial of the commencement of the Madras Harbour Works. It is 17.97 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = IX<sup>h</sup> 1<sup>m</sup>.

The highest high water recorded was 5.3 feet above the zero of the gauge, and occurred in November, 1889.

The lowest low water recorded was 0·3 foot *below* the zero of the gauge, and occurred in April, 1882.

In 1880-81 the mean range of largest ordinary springs was found to be 3·5 feet.

The height of mean-sea-level above the zero of the gauge had the following values:—

1880-81	...	...	...	2·251 feet.
1881-82	...	...	...	2·209 „
1882-83	...	...	...	2·179 „
1883-84	...	...	...	2·180 „
1884-85	...	...	...	2·134 „
1885-86	...	...	...	2·051 „
1886-87	...	...	...	2·320 „
1887-88	...	...	...	2·266 „
1888-89	...	...	...	2·133 „
1889-90	...	...	...	2·353 „

*Values of H's at Madras.*

TIDE	H					TIDE
	1880-81	1881-82	1882-83	1883-84	1884-85	
	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0·037	0·026	0·012	0·026	0·056	S <sub>1</sub>
S <sub>2</sub>	·437	·445	·440	·436	·450	S <sub>2</sub>
S <sub>4</sub>	·002	·002	·001	·002	·005	S <sub>4</sub>
S <sub>6</sub>	·002	·001	·001	·001	·001	S <sub>6</sub>
S <sub>8</sub>	·001	·000	·001	·000	·001	S <sub>8</sub>
M <sub>1</sub>	·019	·001	·004	·003	·038	M <sub>1</sub>
M <sub>2</sub>	1·047	1·051	1·049	1·033	1·058	M <sub>2</sub>
M <sub>3</sub>	0·004	0·003	0·006	0·004	0·003	M <sub>3</sub>
M <sub>4</sub>	·002	·001	·005	·002	·019	M <sub>4</sub>
M <sub>6</sub>	·010	·011	·009	·006	·008	M <sub>6</sub>
M <sub>8</sub>	·002	·001	·002	·002	·001	M <sub>8</sub>
O	·094	·096	·101	·096	·100	O
K <sub>1</sub>	·294	·291	·293	·291	·296	K <sub>1</sub>
K <sub>2</sub>	·121	·120	·094	·116	·086	K <sub>2</sub>
P	·093	·094	·103	·091	·104	P
J	·029	·012	·021	·022	·030	J
Q	·004	·003	·009	·002	·007	Q
L	·037	·017	·054	·037	·026	L
N	·246	·235	·238	·229	·265	N
λ	·027	·025	·035	·009	·071	λ
ν	·053	·007	·072	·079	·145	ν
μ	·046	·048	·030	·046	·063	μ
R	...	·016	...	·016	...	R
T	...	·056	...	·019	...	T
MS	·004	·001	·004	·002	·015	MS
2SM	·020	·022	·023	·018	·021	2SM
2N	·064	·026	·023	·044	·061	2N
M <sub>2</sub> N	·019	·050	·029	·040	·102	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	·011	·016	·010	·014	·025	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	·008	·007	·006	·005	·006	2M <sub>2</sub> K <sub>1</sub>
Mm	·040	·047	·055	·027	·017	Mm
Mf	·030	·050	·055	·044	·020	Mf
MSf	·001	·034	·021	·023	·026	MSf
Sa	·372	·335	·449	·520	·366	Sa
Ssa	·275	·383	·257	·300	·362	Ssa

*Values of H's at Madras—(Continued).*

TIDE	H					TIDE
	1885-86	1886-87	1887-88	1888-89	1889-90	
	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0·017	0·078	0·005	0·023	0·035	S <sub>1</sub>
S <sub>2</sub>	·415	·442	·393	·461	·435	S <sub>2</sub>
S <sub>4</sub>	·003	·002	·003	·002	·003	S <sub>4</sub>
S <sub>6</sub>	·001	·002	·001	·001	·001	S <sub>6</sub>
S <sub>8</sub>	·001	·001	·000	·001	·002	S <sub>8</sub>
M <sub>1</sub>	·018	·014	·013	·019	·008	M <sub>1</sub>
M <sub>2</sub>	·983	1·019	·950	1·063	1·069	M <sub>2</sub>
M <sub>3</sub>	·003	0·004	·004	0·006	0·005	M <sub>3</sub>
M <sub>4</sub>	·014	·008	·003	·010	·008	M <sub>4</sub>
M <sub>6</sub>	·006	·011	·004	·008	·009	M <sub>6</sub>
M <sub>8</sub>	·003	·003	·003	·001	·001	M <sub>8</sub>
O	·089	·107	·089	·098	·104	O
K <sub>1</sub>	·286	·281	·280	·301	·305	K <sub>1</sub>
K <sub>2</sub>	·118	·163	·108	·132	·102	K <sub>2</sub>
P	·090	·070	·084	·098	·106	P
J	·006	·014	·029	·029	·020	J
Q	·009	·019	·013	·010	·005	Q
L	·040	·094	·020	·044	·030	L
N	·193	·183	·237	·268	·268	N
λ	·012	...	...	...	...	λ
ν	·050	·118	·053	·073	·086	ν
μ	·063	·037	·049	·050	·047	μ
R	·053	...	...	...	...	R
T	·080	·067	·036	·017	·027	T
MS	·010	·010	·001	·006	·008	MS
2SM	·009	·012	·022	·021	·015	2SM
2N	·032	·041	·038	·062	·051	2N
M <sub>2</sub> N	·021	·041	·029	·022	·022	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	·010	·004	·014	·014	·013	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	·007	·003	·004	·006	·006	2M <sub>2</sub> K <sub>1</sub>
Mm	·056	·005	·023	·060	·044	Mm
Mf	·054	·055	·044	·056	·033	Mf
MSf	·035	·006	·004	·044	·030	MSf
Sa	·351	·491	·286	·397	·408	Sa
Ssa	·289	·363	·307	·391	·219	Ssa

*Values of  $\kappa$ 's at Madras.*

TIDE	$\kappa$					TIDE
	1880-81	1881-82	1882-83	1883-84	1884-85	
	°	°	°	°	°	
S <sub>1</sub>	80·49	96·10	98·75	87·56	99·61	S <sub>1</sub>
S <sub>2</sub>	277·36	274·77	276·38	279·54	279·79	S <sub>2</sub>
S <sub>4</sub>	97·77	168·69	217·88	216·87	302·28	S <sub>4</sub>
S <sub>6</sub>	60·64	98·75	175·91	56·31	63·44	S <sub>6</sub>
S <sub>8</sub>	131·19	63·44	290·56	198·44	333·44	S <sub>8</sub>
M <sub>1</sub>	3·63	312·47	64·66	41·22	282·99	M <sub>1</sub>
M <sub>2</sub>	249·43	246·71	248·05	250·41	248·36	M <sub>2</sub>
M <sub>3</sub>	65·44	55·15	66·81	57·11	8·41	M <sub>3</sub>
M <sub>4</sub>	129·65	114·89	192·58	154·43	225·93	M <sub>4</sub>
M <sub>6</sub>	160·80	148·61	153·53	160·40	165·04	M <sub>6</sub>
M <sub>8</sub>	331·11	84·49	83·08	29·13	18·81	M <sub>8</sub>
O	326·83	323·65	324·77	330·69	321·88	O
K <sub>1</sub>	339·58	338·26	342·06	342·39	340·85	K <sub>1</sub>
K <sub>2</sub>	277·59	276·44	285·72	268·22	269·19	K <sub>2</sub>
P	340·64	341·06	350·05	344·11	346·29	P
J	336·70	314·06	303·71	317·89	346·06	J
Q	140·43	150·02	43·21	68·08	280·23	Q
L	277·81	334·52	309·82	287·20	359·29	L
N	242·97	240·19	242·38	244·21	238·02	N
$\lambda$	347·86	282·51	267·77	215·60	73·29	$\lambda$
$\nu$	208·58	287·30	317·66	255·43	224·36	$\nu$
$\mu$	183·67	167·31	183·46	190·28	194·85	$\mu$
R	...	103·18	...	357·92	...	R
T	...	256·61	...	19·34	...	T
MS	176·87	54·27	280·06	36·52	256·91	MS
2SM	228·14	219·84	177·87	232·71	256·55	2SM
2N	231·35	248·36	254·08	229·24	201·21	2N
M <sub>2</sub> N	81·73	81·83	199·81	140·39	76·94	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	33·46	98·25	185·05	290·88	10·18	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	79·00	68·35	65·64	51·89	14·48	2M <sub>2</sub> K <sub>1</sub>
Mm	40·65	130·38	68·07	284·73	0·23	Mm
Mf	4·84	349·21	24·86	64·88	25·41	Mf
MSf	84·35	45·82	44·09	29·70	128·19	MSf
Sa	200·56	224·82	211·31	234·73	215·09	Sa
Ssa	119·83	148·67	114·65	139·09	137·41	Ssa

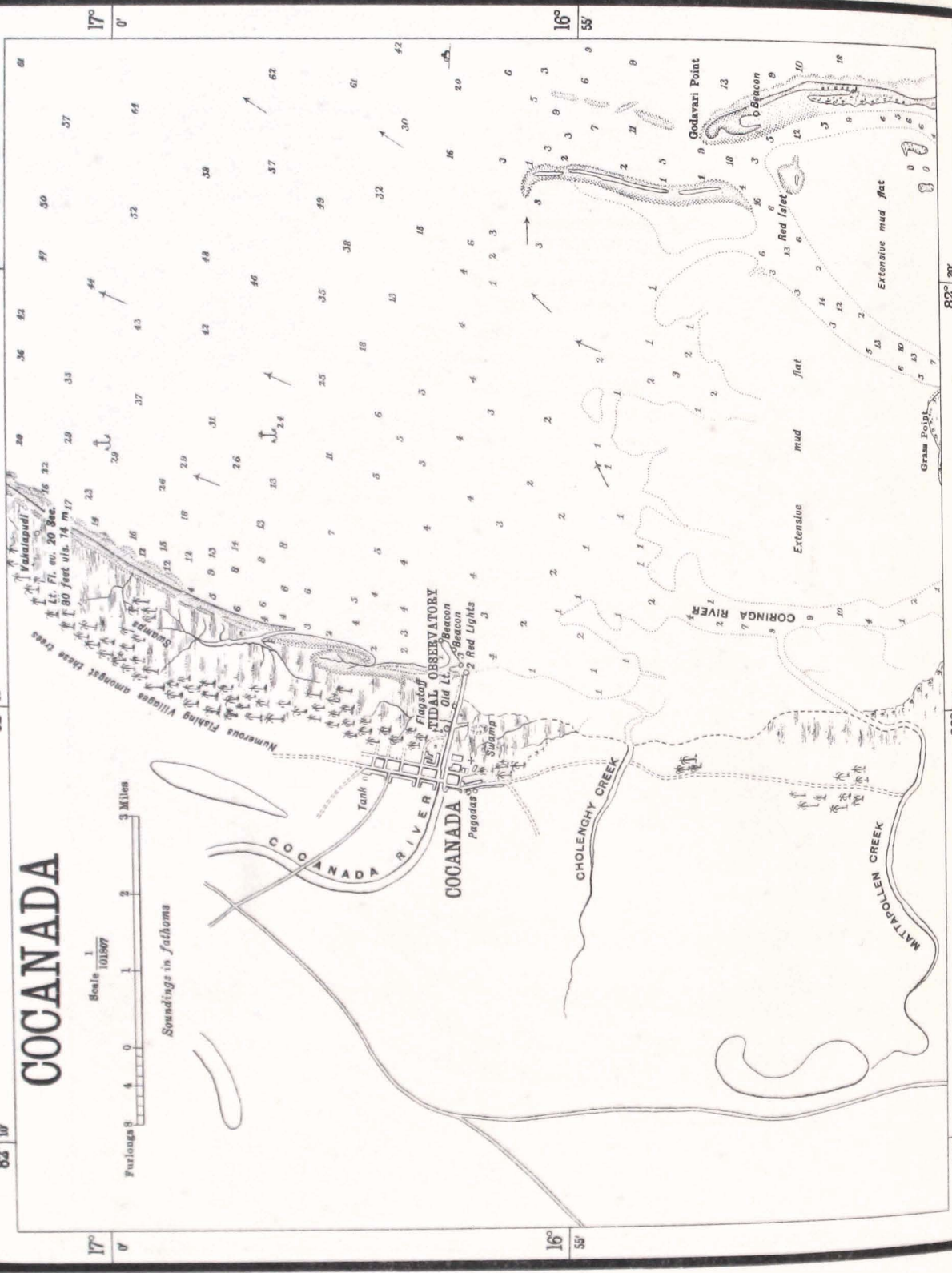


Values of  $\kappa$ 's at Madras—(Continued).

TIDE	$\kappa$					TIDE
	1885-86	1886-87	1887-88	1888-89	1889-90	
	°	°	°	°	°	
S <sub>1</sub>	75·22	147·89	353·16	95·04	65·52	S <sub>1</sub>
S <sub>2</sub>	289·92	286·34	291·44	278·36	271·25	S <sub>2</sub>
S <sub>4</sub>	287·75	272·86	263·42	236·98	276·12	S <sub>4</sub>
S <sub>6</sub>	66·04	141·34	201·80	135·00	53·97	S <sub>6</sub>
S <sub>8</sub>	50·19	39·29	243·44	304·99	304·70	S <sub>8</sub>
M <sub>1</sub>	268·91	302·80	353·99	326·07	344·93	M <sub>1</sub>
M <sub>2</sub>	258·54	251·69	262·45	250·13	242·64	M <sub>2</sub>
M <sub>3</sub>	359·58	33·67	30·37	28·67	71·10	M <sub>3</sub>
M <sub>4</sub>	225·20	247·99	237·13	212·78	196·35	M <sub>4</sub>
M <sub>6</sub>	203·94	157·75	176·45	164·00	114·30	M <sub>6</sub>
M <sub>8</sub>	192·00	295·30	166·00	3·08	175·55	M <sub>8</sub>
O	332·80	324·97	339·74	326·70	322·22	O
K <sub>1</sub>	345·82	343·29	350·62	341·26	338·78	K <sub>1</sub>
K <sub>2</sub>	305·28	276·11	278·34	280·84	255·01	K <sub>2</sub>
P	348·17	343·84	356·63	345·29	334·48	P
J	323·27	249·39	336·07	339·03	322·93	J
Q	96·33	87·07	78·95	117·00	175·81	Q
L	298·72	275·37	313·20	313·63	224·20	L
N	250·21	242·09	247·77	239·22	231·50	N
$\lambda$	222·48	...	...	...	...	$\lambda$
$\nu$	177·44	341·31	267·30	267·68	249·21	$\nu$
$\mu$	170·03	154·02	201·64	187·99	160·02	$\mu$
R	145·65	...	...	...	...	R
T	224·68	264·22	316·28	56·27	284·69	T
MS	269·98	296·62	339·34	239·73	221·74	MS
2SM	236·08	110·57	247·90	246·71	197·35	2SM
2N	287·81	245·55	221·60	200·32	214·04	2N
M <sub>2</sub> N	100·87	95·25	175·20	252·32	216·64	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	85·49	202·92	312·63	61·69	301·97	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	102·88	34·10	62·27	40·60	69·66	2M <sub>2</sub> K <sub>1</sub>
Mm	335·70	104·90	308·39	341·27	20·02	Mm
Mf	343·37	75·83	318·19	28·52	2·78	Mf
MSf	334·12	135·60	121·71	332·69	121·82	MSf
Sa	227·84	201·37	222·83	223·85	203·37	Sa
Ssa	140·09	128·63	105·48	113·46	114·92	Ssa

# COCANADA

Furlongs 0 1 2 3 4  
Scale 1:101897  
SOUNDINGS IN FATHOMS



## COCANADA.

(Tidal Observatory, Lat.  $16^{\circ} 56' N.$ , Long.  $82^{\circ} 15' E.$ )

The tidal observatory at Cocanada, on the east coast of India, near the mouth of the Godávari, was one of the minor observatories at which five years' observations are considered sufficient, and was situated on the northern bank of the Godávari Canal, twenty feet from the bank and near the Port Officer's landing jetty, in the position shown on the accompanying chart. It was a wooden cabin resting on piles about sixteen feet long driven five feet into the mud. The observatory and the instruments contained in it, including the iron float-cylinder, had been used before at Vizagapatam. The float-cylinder was twenty-two inches in internal diameter and twelve feet long, with a wooden addition three feet long above it. It was supported by iron collars and rods attached to the piles on which the observatory rested. The bottom of the cylinder was about four feet below the lowest tides and the wooden top about two feet above the highest. The communication was by a short bent pipe which left the cylinder about nine inches above the bottom, and after turning upwards for about a foot ended in a rose two feet below the lowest tides.

The working scale of the tide-gauge was one-half.

Registrations were commenced on the 31st March, 1886. For the first three years they were absolutely without interruption, and the few subsequent stoppages were quite insignificant. Five years' perfectly satisfactory observations were completed on the 18th April, 1891, and the observatory was then dismantled.

Barometrical and anemometrical observations were carried on simultaneously with the tidal observations. The barometer was placed in the Port Office and the anemometer on the roof of the same building.

## TIDAL OBSERVATIONS.

The bench-mark of reference is a stone inscribed  $\begin{matrix} \text{G. T. S.} \\ \square \\ \text{B. M.} \end{matrix}$  A, embedded in a block of masonry, near the S.E. corner of the Port Office, and three feet away from the compound wall. It is 11.298 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = VIII<sup>h</sup> 50<sup>m</sup>.

The highest high water recorded was 9.9 feet above the zero of the gauge, and occurred in November, 1886.

The lowest low water recorded was 1.4 feet above the zero of the gauge, and occurred in March, 1888.

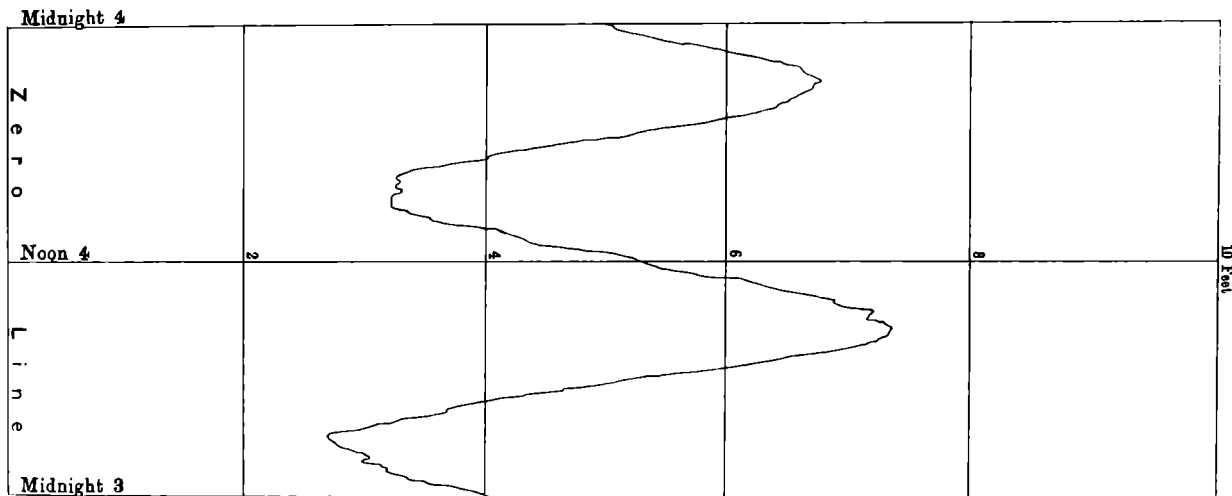
In 1890-91 the mean range of largest ordinary springs was found to be 5.0 feet.

The height of mean-sea-level above the zero of the gauge had the following values:—

1886-87	...	...	...	5.488 feet.
1887-88	...	...	...	5.324 ,,
1888-89	...	...	...	5.154 ,,
1889-90	...	...	...	5.413 ,,
1890-91	...	...	...	5.308 ,,

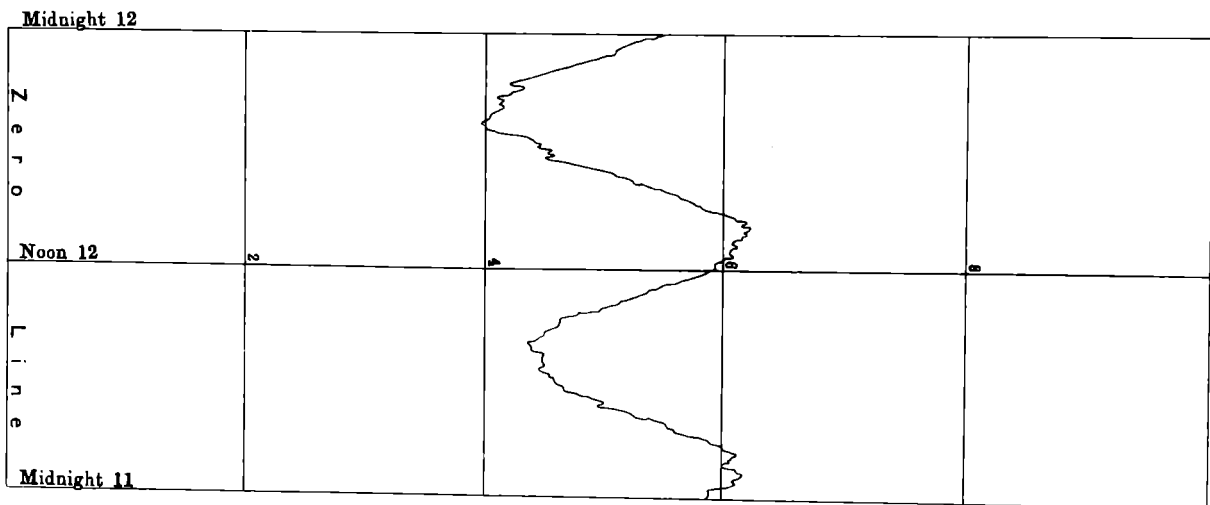
TIDAL CURVES  
at  
COCANADA

Spring Tide — 4th August 1887



Full Moon — 3rd August 1887

Neap Tide — 12th August 1887



Last Quarter — 11th August 1887

*Photocopyographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dún. January 1900.*

*Values of H's at Cocanada.*

TIDE	H					TIDE
	1886-87	1887-88	1888-89	1889-90	1890-91	
	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0.036	0.037	0.034	0.034	0.038	S <sub>1</sub>
S <sub>2</sub>	.644	.628	.642	.632	.648	S <sub>2</sub>
S <sub>4</sub>	.003	.007	.008	.006	.007	S <sub>4</sub>
S <sub>6</sub>	.003	.004	.003	.001	.002	S <sub>6</sub>
S <sub>8</sub>	.003	.003	.003	.002	.002	S <sub>8</sub>
M <sub>1</sub>	.019	.023	.018	.022	.010	M <sub>1</sub>
M <sub>2</sub>	1.486	1.545	1.525	1.493	1.517	M <sub>2</sub>
M <sub>3</sub>	0.006	0.009	0.006	0.007	0.009	M <sub>3</sub>
M <sub>4</sub>	.026	.027	.032	.030	.034	M <sub>4</sub>
M <sub>6</sub>	.014	.016	.017	.016	.018	M <sub>6</sub>
M <sub>8</sub>	.002	.002	.001	.003	.003	M <sub>8</sub>
O	.133	.137	.138	.144	.135	O
K <sub>1</sub>	.347	.352	.347	.346	.344	K <sub>1</sub>
K <sub>2</sub>	.175	.169	.161	.161	.180	K <sub>2</sub>
P	.099	.089	.100	.096	.091	P
J	.028	.036	.035	.019	.023	J
Q	.017	.008	.002	.002	.001	Q
L	.075	.082	.066	.061	.046	L
N	.308	.326	.316	.325	.322	N
λ	.008	...	...	...	...	λ
ν	.071	.018	.105	.115	.092	ν
μ	.019	.032	.024	.029	.014	μ
R	...	...	...	...	...	R
T	...	.064	.087	.053	.011	T
MS	.014	.023	.027	.023	.024	MS
2SM	.015	.018	.020	.014	.014	2SM
2N	.043	.060	.041	.072	.042	2N
M <sub>2</sub> N	.031	.041	.055	.045	.045	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	.024	.024	.017	.013	.014	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	.011	.010	.009	.012	.007	2M <sub>2</sub> K <sub>1</sub>
Mm	.029	.076	.089	.066	.056	Mm
Mf	.078	.095	.084	.089	.073	Mf
MSf	.033	.023	.061	.059	.013	MSf
Sa	.853	.671	.583	.731	.763	Sa
Ssa	.403	.522	.403	.394	.237	Ssa

## TIDAL OBSERVATIONS.

*Values of  $\kappa$ 's at Cocanada.*

TIDE	$\kappa$					TIDE
	1886-87	1887-88	1888-89	1889-90	1890-91	
	°	°	°	°	°	
S <sub>1</sub>	92.89	77.05	82.47	61.55	81.31	S <sub>1</sub>
S <sub>2</sub>	284.85	285.83	287.43	287.58	284.73	S <sub>2</sub>
S <sub>4</sub>	125.54	146.54	131.58	143.70	121.66	S <sub>4</sub>
S <sub>6</sub>	204.78	159.62	185.19	146.31	142.43	S <sub>6</sub>
S <sub>8</sub>	220.60	83.09	81.12	114.23	24.23	S <sub>8</sub>
M <sub>1</sub>	341.40	341.58	345.08	62.48	56.66	M <sub>1</sub>
M <sub>2</sub>	252.29	252.43	253.74	253.41	251.86	M <sub>2</sub>
M <sub>3</sub>	346.15	19.88	18.01	28.32	16.10	M <sub>3</sub>
M <sub>4</sub>	108.73	105.95	105.10	106.96	103.35	M <sub>4</sub>
M <sub>6</sub>	97.59	100.84	98.22	92.89	95.24	M <sub>6</sub>
M <sub>8</sub>	66.46	294.65	318.20	270.92	57.01	M <sub>8</sub>
O	332.93	332.37	332.65	333.81	331.70	O
K <sub>1</sub>	340.18	338.20	339.03	339.56	339.03	K <sub>1</sub>
K <sub>2</sub>	286.38	283.50	282.07	290.30	279.41	K <sub>2</sub>
P	344.27	343.11	343.00	344.09	341.72	P
J	338.46	336.26	11.20	329.05	299.98	J
Q	35.95	20.99	113.10	93.11	325.01	Q
L	272.21	235.22	255.89	232.42	266.69	L
N	243.91	242.06	247.39	245.38	247.37	N
$\lambda$	82.90	...	...	...	...	$\lambda$
$\nu$	190.83	302.68	289.52	252.51	208.57	$\nu$
$\mu$	256.73	264.01	319.18	261.12	271.94	$\mu$
R	...	...	...	...	...	R
T	...	293.60	257.62	208.39	276.22	T
MS	130.69	144.98	143.13	141.79	120.12	MS
2SM	214.74	181.26	190.66	167.51	156.10	2SM
2N	241.70	230.09	206.38	242.37	247.28	2N
M <sub>3</sub> N	120.41	134.83	56.68	126.38	90.07	M <sub>3</sub> N
M <sub>1</sub> K <sub>1</sub>	295.91	16.47	114.42	206.59	313.30	M <sub>1</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	326.42	317.82	317.08	327.16	317.35	2M <sub>2</sub> K <sub>1</sub>
Mm	197.51	290.30	331.68	338.77	85.32	Mm
Mf	54.62	196.47	30.03	336.35	344.89	Mf
MSf	18.60	125.06	342.22	354.78	54.21	MSf
Sa	199.64	199.26	205.36	212.85	190.79	Sa
Ssa	108.63	98.77	112.06	119.13	85.78	Ssa

# VIZAGAPATAM

83° 16'

83° 18'

83° 20'

Scale  $\frac{1}{48428}$

Feet 2000 1000 0 2000 4000 6000 8000 10000 Feet

17° 44'

17° 42'

17° 40'

17° 44'

17° 42'

17° 40'

Soundings in feet



Photoincographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dún, October 1900.



## VIZAGAPATAM.

(*Tidal Observatory, Lat. 17° 41' N., Long. 83° 17' E.*)

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The tidal observatory at Vizagapatam, about the centre of the east coast of India, was one of the minor observatories, at which five years' observations are generally considered sufficient, and was situated on the northern bank of the back-water, about fifty yards west of the landing or "bandar" house, in the position shown on the accompanying chart. It was a wooden structure, of the usual substantial kind, supported at its outer end on piles and at its inner end on a wharf wall. The flooring was intended to be well above the water at all times; but on one occasion, the 6th December, 1878, a violent storm, assisted by the flooding of the river from inland rains, raised the water into the observatory, and did serious damage, including the displacement of the float-cylinder. The cylinder was of iron, twenty-two inches in internal diameter and twelve feet long. After its displacement by the storm, its bottom was bolted to a huge flat stone and its upper end was secured by beams to the observatory floor. There were then two feet of the cylinder below the lowest tides and three feet of it above the highest, except when the water was raised by storms. The communication was at first by a two-inch piping thirty feet long, partly of iron and partly of flexible tubing, terminating in a rose ten feet below the lowest tides; but after two years' experience of it this arrangement was found to be unnecessary, and direct communication through the rose, fixed to the inlet-hole near the bottom of the cylinder, was substituted for it.

The working scale of the tide-gauge was one-half.

Registrations were commenced originally in August, 1878, and were proceeding satisfactorily when the storm above-mentioned occurred. The damage caused by it was repaired and work was restarted at the beginning of February, 1879, all preceding registrations being rejected. The record from the 3rd February, 1879, on which day the accepted registrations commenced, was satisfactory until the 7th November, 1882, when two months were devoted to repairing the piles: at the end of 1883 there were several interruptions, but as a whole the record was good until the dismantling of the observatory in March, 1885, on the completion of the observations. The disturbances of the surface of the ocean, caused by an earthquake whose centre lay between Port Blair and Car Nicobar, were recorded at this station by the self-registering tide-gauge on the 31st December, 1881, and those caused by the

Krakatoa volcanic eruptions were similarly recorded on the 27th August, 1883.

Barometrical and anemometrical observations were carried on simultaneously with the tidal observations. The barometer was placed in the observatory, and the anemometer was placed on the "Dolphin's nose," a hill about a mile south of the town.

The bench-mark of reference is a stone embedded in the floor of the verandah of the Port Office and marked  $\begin{matrix} \text{G. T. S.} \\ \square \\ \text{D. M.} \\ \text{C.} \end{matrix}$ . It is 18·955 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = VIII<sup>h</sup> 26<sup>m</sup>.

The highest high water recorded was 8·9 feet above the zero of the gauge, and occurred in November, 1879.

The lowest low water recorded was 0·8 foot above the zero of the gauge, and occurred in March, 1880.

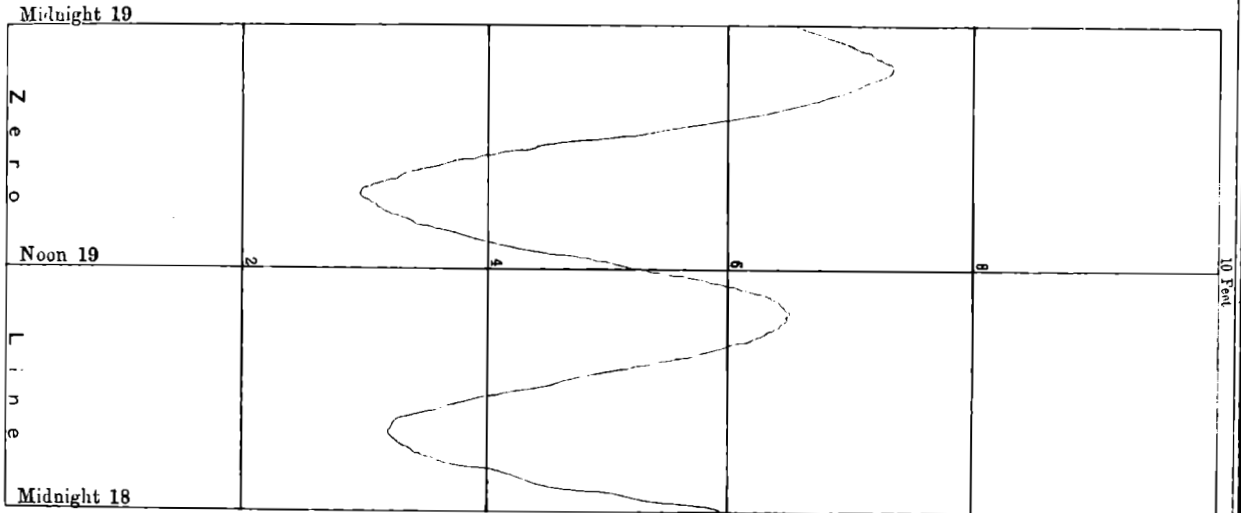
In 1879-80 the mean range of largest ordinary springs was found to be 5·1 feet.

The height of mean-sea-level above the zero of the gauge had the following values :—

1879-80	...	...	...	4·991 feet.
1880-81	...	...	...	4·917 „
1881-82	...	...	...	4·809 „
1882-83	...	...	...	4·812 „
1883-84	...	...	...	4·813 „
1884-85	...	...	...	4·630 „

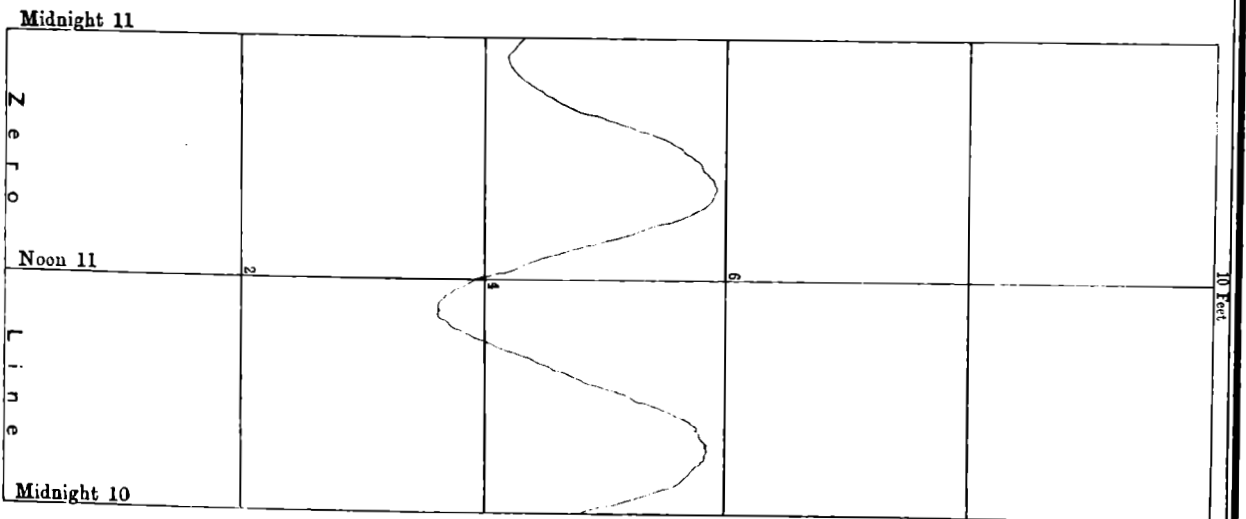
**TIDAL CURVES**  
at  
**VIZAGAPATAM**

Spring Tide — 19th December 1884



New Moon — 17th December 1884

Neap Tide — 11th December 1884



Last Quarter — 9th December 1884

*Photoinographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun, September 1900.*

*Values of H's at Vizagapatam.*

TIDE	H						TIDE
	1879-80	1880-81	1881-82	1882-83	1883-84	1884-85	
	Feet	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0.028	0.047	0.035	0.096	0.037	0.044	S <sub>1</sub>
S <sub>2</sub>	.674	.659	.651	.641	.640	.625	S <sub>2</sub>
S <sub>3</sub>	.001	.007	.006	.006	.004	.003	S <sub>4</sub>
S <sub>6</sub>	.001	.001	.001	.002	.001	.001	S <sub>6</sub>
S <sub>8</sub>	.001	.001	.003	.001	.001	.000	S <sub>8</sub>
M <sub>1</sub>	.023	.021	.001	.004	.007	.016	M <sub>1</sub>
M <sub>2</sub>	1.532	1.460	1.459	1.439	1.464	1.462	M <sub>2</sub>
M <sub>3</sub>	0.007	0.001	0.006	0.008	0.007	0.009	M <sub>3</sub>
M <sub>4</sub>	.014	.014	.015	.018	.013	.004	M <sub>4</sub>
M <sub>6</sub>	.003	.004	.005	.008	.004	.007	M <sub>6</sub>
M <sub>8</sub>	.004	.002	.002	.005	.005	.004	M <sub>8</sub>
O	.139	.140	.144	.142	.138	.129	O
K <sub>1</sub>	.371	.364	.366	.335	.355	.358	K <sub>1</sub>
K <sub>2</sub>	.179	.157	.168	.306	.181	.163	K <sub>2</sub>
P	.112	.104	.117	.049	.116	.109	P
J	.035	.027	.014	.024	.026	.024	J
Q	.010	.007	.004	.014	.020	.014	Q
L	.049	.044	.027	.088	.046	.078	L
N	.355	.300	.291	.309	.296	.298	N
λ	.021	.019	.022	.024	.012	.039	λ
ν	.114	.055	.002	.127	.116	.095	ν
μ	.030	.026	.016	.034	.028	.036	μ
R	...	.015	...	.039	...	.025	R
T	...	.021	...	.080	...	.036	T
MS	.007	.010	.014	.015	.012	.007	MS
2SM	.008	.010	.015	.016	.004	.012	2SM
2N	.066	.059	.044	.046	.039	.056	2N
M <sub>2</sub> N	.019	.031	.063	.037	.042	.030	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	.024	.029	.006	.007	.022	.022	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	.006	.010	.014	.014	.010	.015	2M <sub>2</sub> K <sub>1</sub>
Mm	.022	.078	.049	.072	.029	.010	Mm
Mf	.030	.051	.061	.027	.082	.073	Mf
MSf	.076	.021	.038	.048	.025	.019	MSf
Sa	.740	.833	.577	.707	.612	.694	Sa
Ssa	.301	.348	.458	.241	.364	.350	Ssa

## TIDAL OBSERVATIONS.

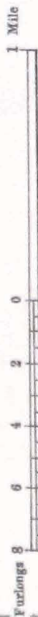
*Values of  $\kappa$ 's at Vizagapatam.*

TIDE	$\kappa$						TIDE
	1870-80	1880-81	1881-82	1882-83	1883-84	1884-85	
	°	°	°	°	°	°	
S <sub>1</sub>	100° 62	76° 97	92° 47	1° 49	92° 65	93° 63	S <sub>1</sub>
S <sub>2</sub>	280° 15	285° 86	286° 00	289° 50	287° 46	288° 28	S <sub>2</sub>
S <sub>4</sub>	359° 93	76° 61	50° 19	59° 81	66° 62	45° 00	S <sub>4</sub>
S <sub>6</sub>	123° 69	127° 88	213° 69	214° 70	146° 31	113° 96	S <sub>6</sub>
S <sub>8</sub>	72° 90	103° 00	60° 52	77° 91	75° 96	288° 44	S <sub>8</sub>
M <sub>1</sub>	355° 35	23° 44	198° 68	241° 70	351° 40	288° 96	M <sub>1</sub>
M <sub>2</sub>	248° 57	253° 43	254° 44	255° 02	254° 75	255° 78	M <sub>2</sub>
M <sub>3</sub>	332° 20	208° 03	41° 42	13° 89	10° 16	21° 56	M <sub>3</sub>
M <sub>4</sub>	310° 31	330° 58	338° 94	342° 39	10° 58	226° 74	M <sub>4</sub>
M <sub>6</sub>	143° 75	77° 90	29° 76	35° 02	60° 69	66° 47	M <sub>6</sub>
M <sub>8</sub>	173° 70	214° 14	243° 13	205° 65	214° 77	241° 00	M <sub>8</sub>
O	329° 82	332° 21	332° 92	329° 45	331° 80	333° 33	O
K <sub>1</sub>	338° 24	342° 06	341° 64	345° 88	342° 32	342° 51	K <sub>1</sub>
K <sub>2</sub>	269° 95	274° 07	284° 80	278° 35	278° 86	279° 20	K <sub>2</sub>
P	335° 86	346° 07	346° 12	329° 35	340° 31	345° 49	P
J	328° 23	355° 63	313° 86	351° 11	342° 87	18° 02	J
Q	20° 37	277° 12	305° 98	335° 85	348° 49	337° 74	Q
L	256° 97	245° 07	296° 64	216° 85	280° 56	256° 26	L
N	243° 13	249° 79	251° 26	241° 50	248° 12	251° 80	N
$\lambda$	200° 61	331° 77	244° 04	278° 17	213° 86	299° 35	$\lambda$
$\nu$	243° 58	198° 62	72° 20	282° 51	257° 14	222° 81	$\nu$
$\mu$	234° 03	258° 86	217° 61	326° 23	257° 70	264° 38	$\mu$
R	...	129° 92	...	245° 98	...	68° 68	R
T	...	336° 23	...	189° 27	...	282° 19	T
MS	345° 10	20° 01	19° 81	356° 76	28° 23	283° 37	MS
2SM	209° 68	292° 41	250° 23	147° 75	312° 24	219° 67	2SM
2N	234° 44	219° 03	258° 65	224° 66	244° 06	218° 29	2N
M <sub>2</sub> N	84° 25	32° 93	344° 66	28° 55	30° 12	58° 55	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	329° 67	19° 85	66° 94	294° 42	334° 47	25° 11	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	355° 03	319° 83	316° 40	334° 15	322° 76	326° 50	2M <sub>2</sub> K <sub>1</sub>
Mm	22° 48	52° 54	104° 02	35° 07	264° 82	7° 00	Mm
Mf	22° 72	340° 43	1° 76	2° 26	46° 98	31° 98	Mf
MSf	22° 27	12° 97	314° 43	101° 95	358° 32	39° 49	MSf
Sa	190° 06	173° 28	188° 65	174° 73	194° 53	182° 48	Sa
Ssa	88° 60	126° 02	140° 37	100° 78	127° 12	128° 64	Ssa

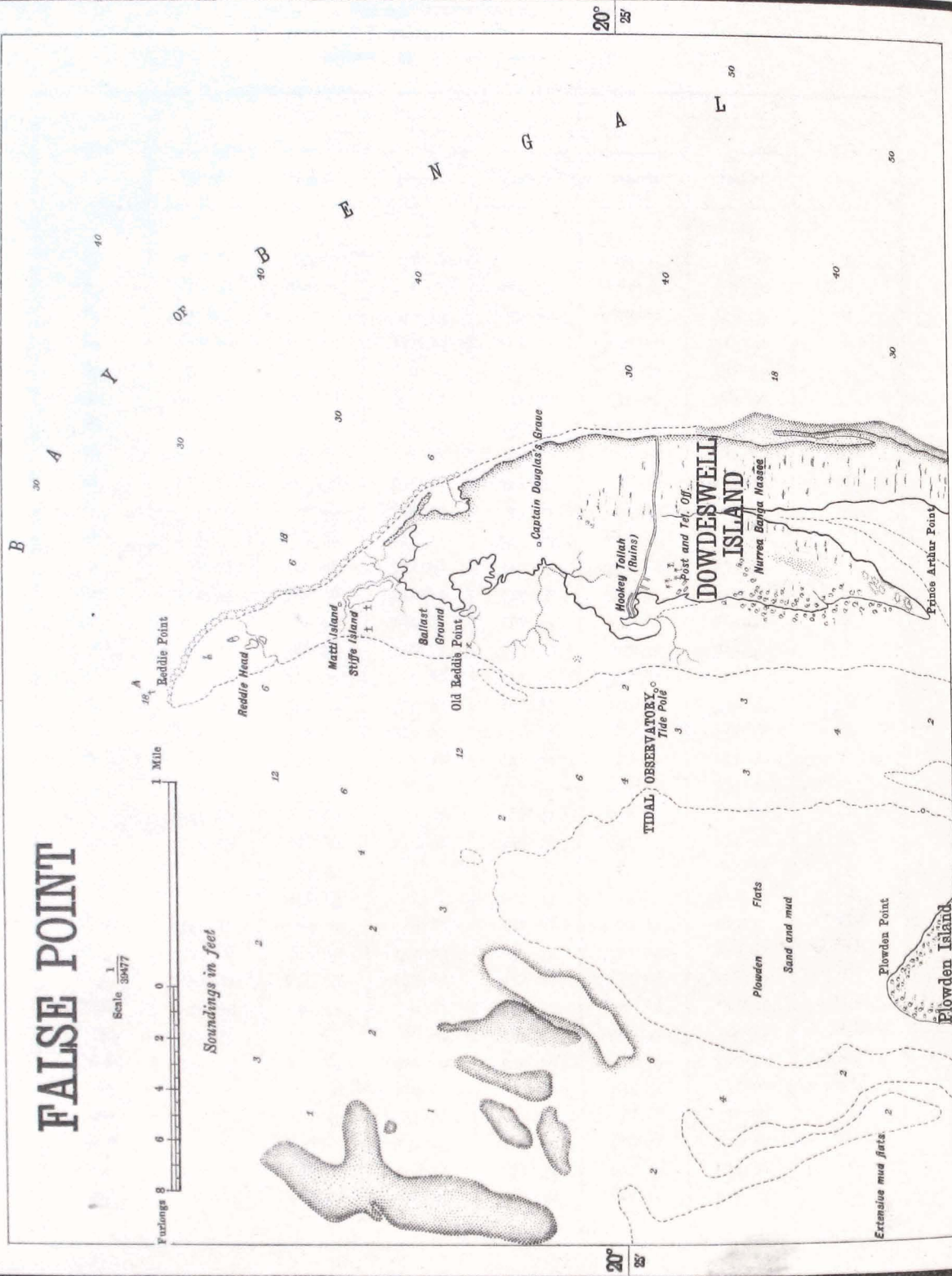
86° 47'

# FALSE POINT

Scale  $\frac{1}{32477}$



Soundings in feet



20° 25'

86° 47'

Photographed at the Office of the Hydrographic Branch, Survey of India, Simla, March 1907.

## FALSE-POINT.

(*Tidal Observatory, Lat. 20° 25' N., Long. 86° 47' E.*)

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The tidal observatory at False-Point, near the mouth of the Mahanadi river, on the east coast of India, was one of the minor observatories, and was situated to the west of the Travellers' Bungalow at Hookey Tollah, in the position shown on the accompanying chart. It was a wooden cabin, substantially built on a heavy timber staging well secured by a mass of stone rubble and also by chain guys to piles embedded in rubble. It was only accessible by boat, but the shore was only three hundred yards distant. The float-cylinder was of the exceptionally large internal diameter of four feet and was about fifteen feet long. It was embedded about ten feet in the stone rubble and secured by cross beams to the staging, so that its bottom was about five feet below the lowest tides and its top about two feet above the highest, where it passed through the floor of the observatory. The communication was by a straight horizontal two-inch pipe about twelve feet long with a rose at its outer end. It passed through the rubble about two feet below the lowest tides and entered the cylinder three feet above the bottom.

The working scale of the tide-gauge was one-third.

Registrations were commenced on the 27th September, 1880, and were fairly continuous until the 2nd October, 1882, when a twenty days' gap occurred owing to the driving clock having to be sent to Calcutta for repairs. The observatory during the first seven months after its erection settled down to the extent of seven inches, and the observations for this period were consequently rejected. In the next year it sank two inches more, and then the sinking ceased for more than a year: but between December, 1883, and March, 1885, a further settlement of one and a half inches was found to have taken place. From the 22nd October, 1882, when observations were resumed after the break above mentioned, the record, though impaired by several unimportant stoppages of the clock due to the vibration of the observatory, was fairly continuous to the end. On the 22nd September, 1885, the tidal observatory, with all the instruments, was carried away by the cyclonic sea-wave that passed over False-Point on that date, destroying all the buildings at Hookey Tollah and drowning nearly all the inhabitants. It was not considered necessary to resume operations, and a fifth year's observations were dispensed with.

The disturbances of the surface of the ocean, caused by an earthquake whose centre lay between Port Blair and Car Nicobar, were recorded at this tidal station by the self-registering tide-gauge on the 31st December, 1881, and those caused by the Krakatoa volcanic eruptions were similarly recorded on the 27th August, 1883.

Barometrical and anemometrical observations were carried on simultaneously with the tidal observations. The barometer was placed in the observatory and the anemometer on the top of the same building.

The bench-mark of reference is a Marine Survey bench-mark consisting of the mark  $\frac{O}{\wedge}$  cut on the south-west pile of the Refuge House at Hookey Tollah. It is 17·951 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = IX<sup>h</sup> 18<sup>m</sup>.

The highest high water recorded was 13·1 feet above the zero of the gauge, and occurred in November, 1883.

The lowest low water recorded was 2·4 feet above the zero of the gauge, and occurred in March, 1883.

In 1881-82 the mean range of largest ordinary springs was found to be 7·3 feet.

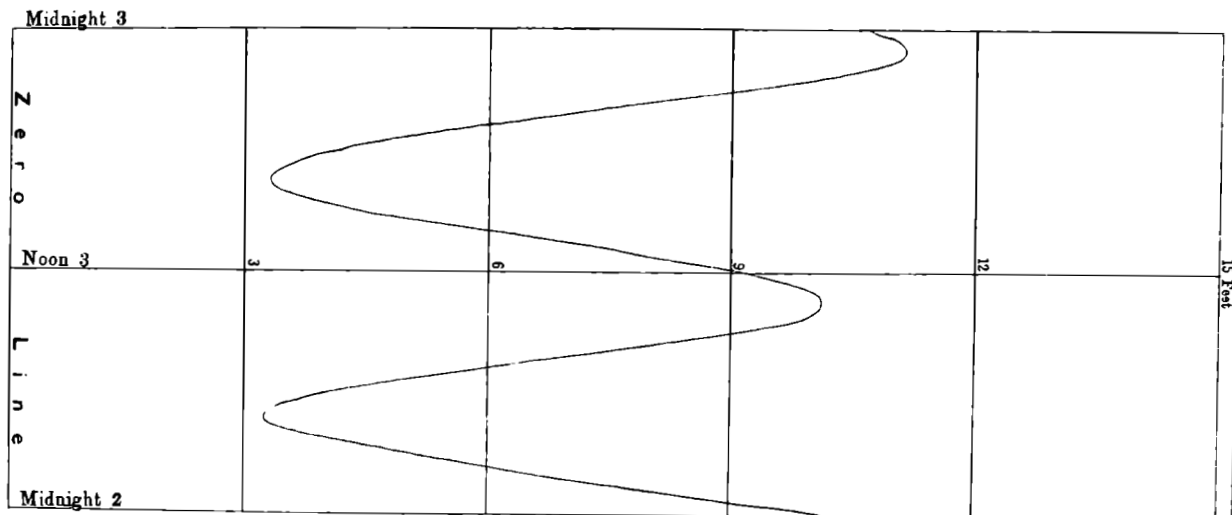
The height of mean-sea-level above the zero of the gauge had the following values:—

1881-82	...	...	...	7·552 feet.
1882-83	...	...	...	7·597 „
1883-84	...	...	...	7·593 „
1884-85	...	...	...	7·492 „



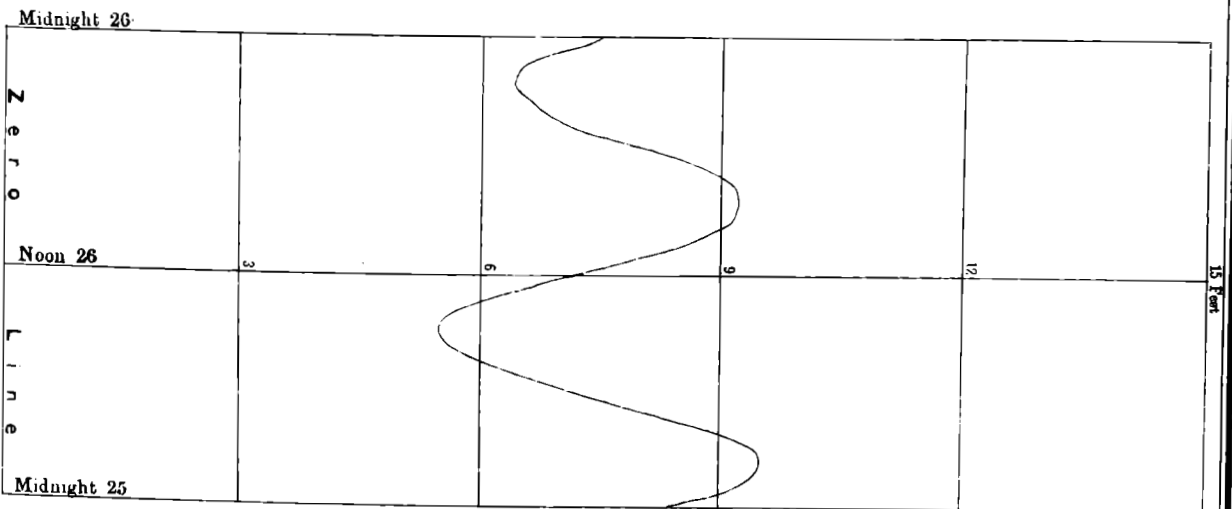
TIDAL CURVES  
at  
FALSE-POINT

Spring Tide — 3rd January 1885



Full Moon — 1st January 1885

Neap Tide — 26th December 1884



First Quarter — 25th December 1884

*Photocopyographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun. July 1899.*

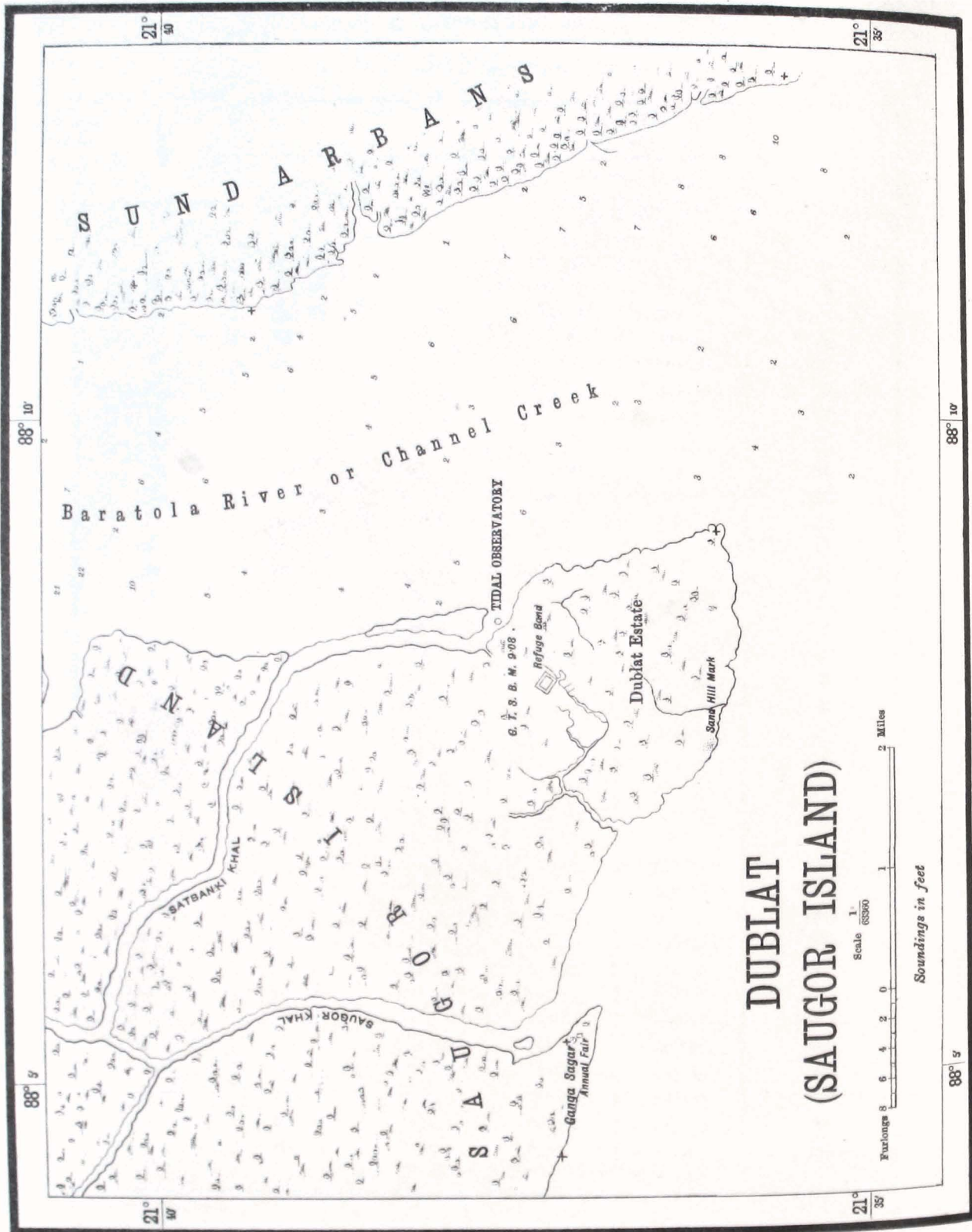
*Values of H's at False-Point.*

TIDE	H				TIDE
	1881-82	1882-83	1883-84	1884-85	
	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0.006	0.024	0.006	0.008	S <sub>1</sub>
S <sub>2</sub>	1.005	1.030	.993	1.000	S <sub>2</sub>
S <sub>4</sub>	0.007	0.008	.009	0.006	S <sub>4</sub>
S <sub>6</sub>	.003	.003	.003	.005	S <sub>6</sub>
S <sub>8</sub>	.003	.003	.004	.005	S <sub>8</sub>
M <sub>1</sub>	.009	.008	.014	.009	M <sub>1</sub>
M <sub>2</sub>	2.247	2.253	2.267	2.237	M <sub>2</sub>
M <sub>3</sub>	0.012	0.016	0.012	0.016	M <sub>3</sub>
M <sub>4</sub>	.035	.041	.035	.029	M <sub>4</sub>
M <sub>6</sub>	.006	.014	.014	.004	M <sub>6</sub>
M <sub>8</sub>	.003	.002	.006	.004	M <sub>8</sub>
O	.175	.179	.176	.172	O
K <sub>1</sub>	.408	.407	.413	.406	K <sub>1</sub>
K <sub>2</sub>	.268	.241	.289	.292	K <sub>2</sub>
P	.133	.157	.127	.132	P
J	.021	.030	.031	.020	J
Q	.004	.017	.012	.005	Q
L	.068	.050	.068	.095	L
N	.471	.481	.425	.439	N
λ	.045	.081	.019	.066	λ
ν	.163	.120	.036	.136	ν
μ	.070	.080	.069	.042	μ
R	...	.034	...	.014	R
T	...	.017	...	.099	T
MS	.039	.042	.041	.039	MS
2SM	.019	.014	.020	.028	2SM
2N	.080	.075	.066	.050	2N
M <sub>2</sub> N	.076	.062	.017	.047	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	.029	.033	.027	.015	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	.006	.013	.010	.010	2M <sub>2</sub> K <sub>1</sub>
Mm	.053	.072	.045	.014	Mm
Mf	.061	.073	.067	.099	Mf
MSf	.041	.059	.039	.014	MSf
Sa	.746	.840	.841	.888	Sa
Ssa	.364	.210	.282	.260	Ssa

## TIDAL OBSERVATIONS.

*Values of  $\kappa$ 's at False-Point.*

TIDE	$\kappa$				TIDE
	1881-82	1882-83	1883-84	1884-85	
	°	°	°	°	
S <sub>1</sub>	325·24	47·52	47·55	86·42	S <sub>1</sub>
S <sub>2</sub>	301·55	304·26	302·09	298·22	S <sub>2</sub>
S <sub>4</sub>	331·19	326·94	315·96	306·67	S <sub>4</sub>
S <sub>6</sub>	153·44	185·04	163·30	158·20	S <sub>6</sub>
S <sub>8</sub>	218·93	261·12	280·54	181·10	S <sub>8</sub>
M <sub>1</sub>	66·41	354·55	286·59	226·80	M <sub>1</sub>
M <sub>2</sub>	268·81	271·10	269·40	267·05	M <sub>2</sub>
M <sub>3</sub>	33·67	26·87	35·98	27·09	M <sub>3</sub>
M <sub>4</sub>	224·18	235·89	223·90	233·04	M <sub>4</sub>
M <sub>6</sub>	80·09	46·67	43·84	142·18	M <sub>6</sub>
M <sub>8</sub>	229·19	262·39	191·97	220·08	M <sub>8</sub>
O	335·42	335·24	334·24	333·70	O
K <sub>1</sub>	343·65	346·25	343·77	341·23	K <sub>1</sub>
K <sub>2</sub>	296·45	296·82	307·24	295·23	K <sub>2</sub>
P	349·22	339·51	345·62	344·08	P
J	306·02	318·76	329·20	359·46	J
Q	306·91	340·10	311·94	187·36	Q
L	280·88	226·85	265·77	286·15	L
N	265·34	268·12	263·65	258·37	N
$\lambda$	276·88	82·96	330·52	272·09	$\lambda$
$\nu$	246·84	240·63	304·50	300·58	$\nu$
$\mu$	266·20	279·61	265·21	252·43	$\mu$
R	...	217·22	...	283·66	R
T	...	149·15	...	280·00	T
MS	272·34	274·77	266·28	260·66	MS
2SM	195·98	177·10	189·22	212·73	2SM
2N	248·65	267·67	238·31	240·22	2N
M <sub>2</sub> N	17·46	41·39	359·87	26·84	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	317·08	25·78	100·95	226·83	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	322·40	331·93	345·91	0·61	2M <sub>2</sub> K <sub>1</sub>
Mm	53·15	57·50	114·53	42·90	Mm
Mf	37·43	33·15	12·63	32·42	Mf
MSf	278·80	73·33	157·77	242·10	MSf
Sa	166·12	165·73	172·28	161·65	Sa
Ssa	142·23	149·02	153·59	157·89	Ssa



# DUBLAT (SAUGOR ISLAND)

Scale 1" = 63000  
 Furlongs 8 6 4 2 0 1 2 Miles  
 Soundings in feet

Photocopying at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun, January 1986.

## DUBLAT (SAUGOR ISLAND).

## ON THE HOOGLY RIVER.

(*Tidal Observatory, Lat. 21° 38' N., Long. 88° 6' E.*)

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The tidal observatory at Dublat, on Saugor Island in the mouth of the Hooghly, was one of the minor observatories at which five years' observations are considered sufficient, and was situated on the western side of the Dublat Creek and about one mile N.E. of the village of that name, in the position shown on the accompanying chart. The observatory, a substantial wooden structure, rested on four stout piles driven fourteen feet into the mud, and was connected with the shore by a plank bridge two hundred feet long. The float-cylinder, twenty-two inches in internal diameter and thirty feet long, giving ample range for extreme tides, passed through and rose three feet above the flooring of the observatory and was supported on posts and secured below by an iron bar fastened to the beams bracing the piles. The communication was through holes bored in the closed bottom of the cylinder.

The working scale of the tide-gauge was one-sixth.

Registrations were commenced on the 23rd April, 1881, and were fairly continuous until their termination, though on one occasion there was a gap of nineteen days owing to the plank bridge being washed away, and there were frequent unimportant stoppages of the pendulum driving clock, due to the vibration of the observatory, which caused short breaks until the clock was replaced by one with spring escapement in December, 1884. A settlement of two and a half inches occurred, caused by the additional weight of some rail bracing added in June, 1885. On the 29th September, 1886, the tidal observatory, with all its contents, was swept away at night by a heavy wind and sea.

The disturbances of the surface of the ocean caused by an earthquake, whose centre lay between Port Blair and Car Nicobar, were recorded at this tidal station by the self-registering tide-gauge on the 31st December, 1881, and those caused by the Krakatoa volcanic eruptions were similarly recorded on the 27th August, 1883.

Barometrical and anemometrical observations were carried on simultaneously with the tidal observations. The barometer was placed in the observatory and the anemometer on the top of the same building.

The bench-mark of reference is a stone embedded in masonry and inscribed  $\overset{\text{G. T. S.}}{\circ}$ ,  $\underset{\text{B. M. A.}}{\circ}$ , situated about six hundred and thirty feet south of the site of the tidal observatory at the foot of the main embankment. It is 18.398 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India =  $X^h 4^m$ .

The highest high water recorded was 24.2 feet above the zero of the gauge, and occurred in September, 1882.

The lowest low water recorded was 5.3 feet above the zero of the gauge, and occurred in March, 1882.

In 1881-82 the mean range of largest ordinary springs was found to be 14.2 feet.

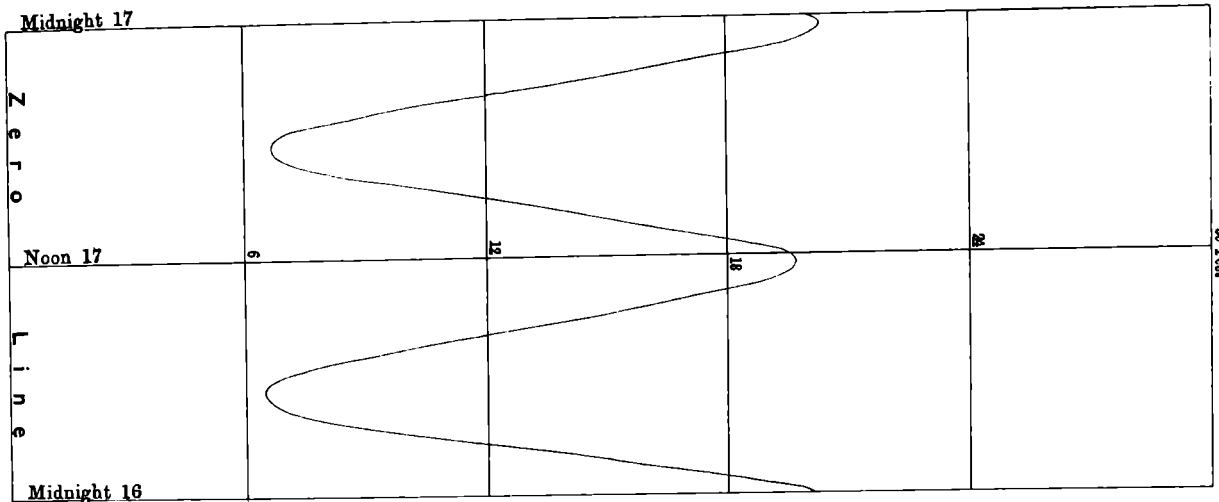
The height of mean-sea-level above the zero of the gauge had the following values:—

1881-82	...	...	...	14.394 feet.
1882-83	...	...	...	14.499 „
1883-84	...	...	...	14.417 „
1884-85	...	...	...	14.379 „
1885-86	...	...	...	14.263 „

NOTE.—The level of the zero of the gauge at Dublat is 6.222 feet below that of the zeros of the gauges at Diamond Harbour and Kidderpore.

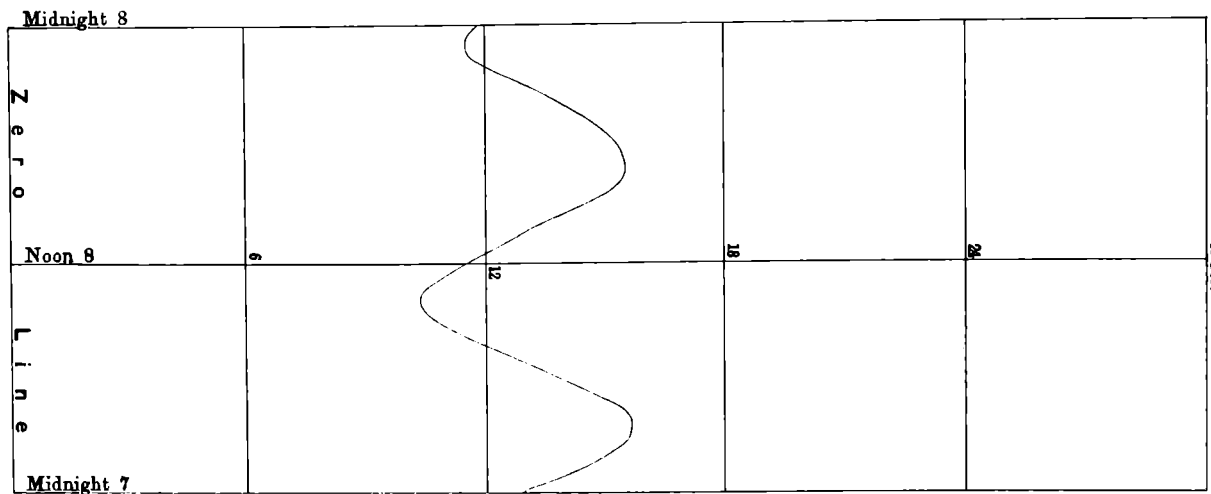
**TIDAL CURVES**  
at  
**DUBLAT (Saugor Island)**

Spring Tide — 17th February 1885



New Moon — 15th February 1885

Neap Tide — 8th February 1885



Last Quarter — 6th February 1885

*Photocopyographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun, August 1889.*

*Values of H's at Dublin.*

TIDE	H					TIDE
	1881-82	1882-83	1893-84	1884-85	1895-86	
	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0·044	0·050	0·040	0·047	0·047	S <sub>1</sub>
S <sub>2</sub>	2·053	2·163	2·147	2·071	2·099	S <sub>2</sub>
S <sub>4</sub>	0·025	0·011	0·017	0·015	0·011	S <sub>4</sub>
S <sub>6</sub>	·002	·005	·005	·001	·002	S <sub>6</sub>
S <sub>8</sub>	·004	·007	·003	·002	·009	S <sub>8</sub>
M <sub>1</sub>	·008	·007	·017	·024	·027	M <sub>1</sub>
M <sub>2</sub>	4·623	4·596	4·594	4·626	4·603	M <sub>2</sub>
M <sub>3</sub>	0·049	0·043	0·051	0·048	0·049	M <sub>3</sub>
M <sub>4</sub>	·101	·089	·081	·086	·081	M <sub>4</sub>
M <sub>6</sub>	·014	·013	·008	·013	·007	M <sub>6</sub>
M <sub>8</sub>	·014	·009	·012	·006	·009	M <sub>8</sub>
O	·181	·197	·186	·183	·196	O
K <sub>1</sub>	·498	·488	·503	·490	·493	K <sub>1</sub>
K <sub>2</sub>	·573	·618	·599	·634	·691	K <sub>2</sub>
P	·158	·151	·141	·156	·148	P
J	·031	·016	·022	·053	·033	J
Q	·010	·008	·013	·012	·010	Q
L	·175	·158	·210	·170	·245	L
N	1·041	·852	·820	·875	·882	N
λ	0·298	·139	·085	·063	·163	λ
ν	·271	·192	·142	·276	·328	ν
μ	·218	·111	·172	·107	·141	μ
R	...	·219	...	·095	...	R
T	...	·137	...	·175	...	T
MS	·094	·059	·067	·074	·077	MS
2SM	·097	·046	·053	·058	·044	2SM
2N	·207	·124	·096	·200	·147	2N
M <sub>2</sub> N	·088	·094	·172	·050	·198	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	·090	·070	·023	·053	·072	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	·033	·032	·028	·050	·031	2M <sub>2</sub> K <sub>1</sub>
Mm	·045	·035	·060	·027	·020	Mm
Mf	·056	·039	·092	·086	·032	Mf
MSf	·049	·077	·050	·027	·042	MSf
Sa	·796	1·003	·864	·930	·787	Sa
Ssa	·234	0·182	·202	·211	·146	Ssa



## TIDAL OBSERVATIONS.

*Values of  $\kappa$ 's at Dublin.*

TIDE	$\kappa$					TIDE
	1881-82	1882-83	1883-84	1884-85	1885-86	
	°	°	°	°	°	
S <sub>1</sub>	99.12	120.94	142.28	124.40	131.20	S <sub>1</sub>
S <sub>2</sub>	326.81	326.29	328.84	326.36	330.45	S <sub>2</sub>
S <sub>3</sub>	202.44	219.54	201.23	255.12	237.49	S <sub>3</sub>
S <sub>6</sub>	120.47	78.23	40.24	59.04	259.38	S <sub>6</sub>
S <sub>8</sub>	115.94	110.35	88.26	58.39	129.89	S <sub>8</sub>
M <sub>1</sub>	344.54	96.83	62.44	264.52	291.07	M <sub>1</sub>
M <sub>2</sub>	290.10	289.67	290.49	290.38	293.80	M <sub>2</sub>
M <sub>3</sub>	131.12	134.96	138.02	132.61	136.53	M <sub>3</sub>
M <sub>4</sub>	142.52	144.83	148.83	148.94	159.65	M <sub>4</sub>
M <sub>6</sub>	274.98	235.85	249.69	165.08	180.69	M <sub>6</sub>
M <sub>8</sub>	315.90	273.02	279.22	302.24	298.43	M <sub>8</sub>
O	332.09	335.44	342.23	343.00	335.68	O
K <sub>1</sub>	353.36	350.31	351.62	350.29	353.56	K <sub>1</sub>
K <sub>2</sub>	310.19	325.25	328.38	332.77	327.33	K <sub>2</sub>
P	335.50	350.64	347.41	350.11	349.66	P
J	351.62	296.42	307.33	2.05	17.33	J
Q	305.51	0.81	10.96	312.40	57.70	Q
L	290.56	291.81	295.09	299.65	301.84	L
N	284.86	286.37	285.06	282.67	286.51	N
$\lambda$	339.00	292.51	261.20	276.85	325.19	$\lambda$
$\nu$	260.94	240.22	294.91	302.68	276.15	$\nu$
$\mu$	10.10	19.01	14.11	355.12	9.96	$\mu$
R	...	288.94	...	306.69	...	R
T	...	299.43	...	60.70	...	T
MS	171.25	138.91	173.83	177.20	191.00	MS
2SM	194.72	216.91	193.00	198.08	196.20	2SM
2N	271.70	297.04	221.44	252.65	263.53	2N
M <sub>2</sub> N	310.22	238.61	55.23	70.14	19.88	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	193.14	246.22	353.34	141.58	191.61	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	151.14	146.72	125.09	124.28	97.06	2M <sub>2</sub> K <sub>1</sub>
Mm	29.34	125.40	75.39	43.17	171.00	Mm
Mf	60.95	70.93	45.93	34.48	85.92	Mf
MSf	277.68	74.99	128.16	233.84	25.57	MSf
Sa	146.93	154.05	152.91	145.51	153.64	Sa
Ssa	162.17	109.69	133.60	161.91	136.80	Ssa

88° 15'

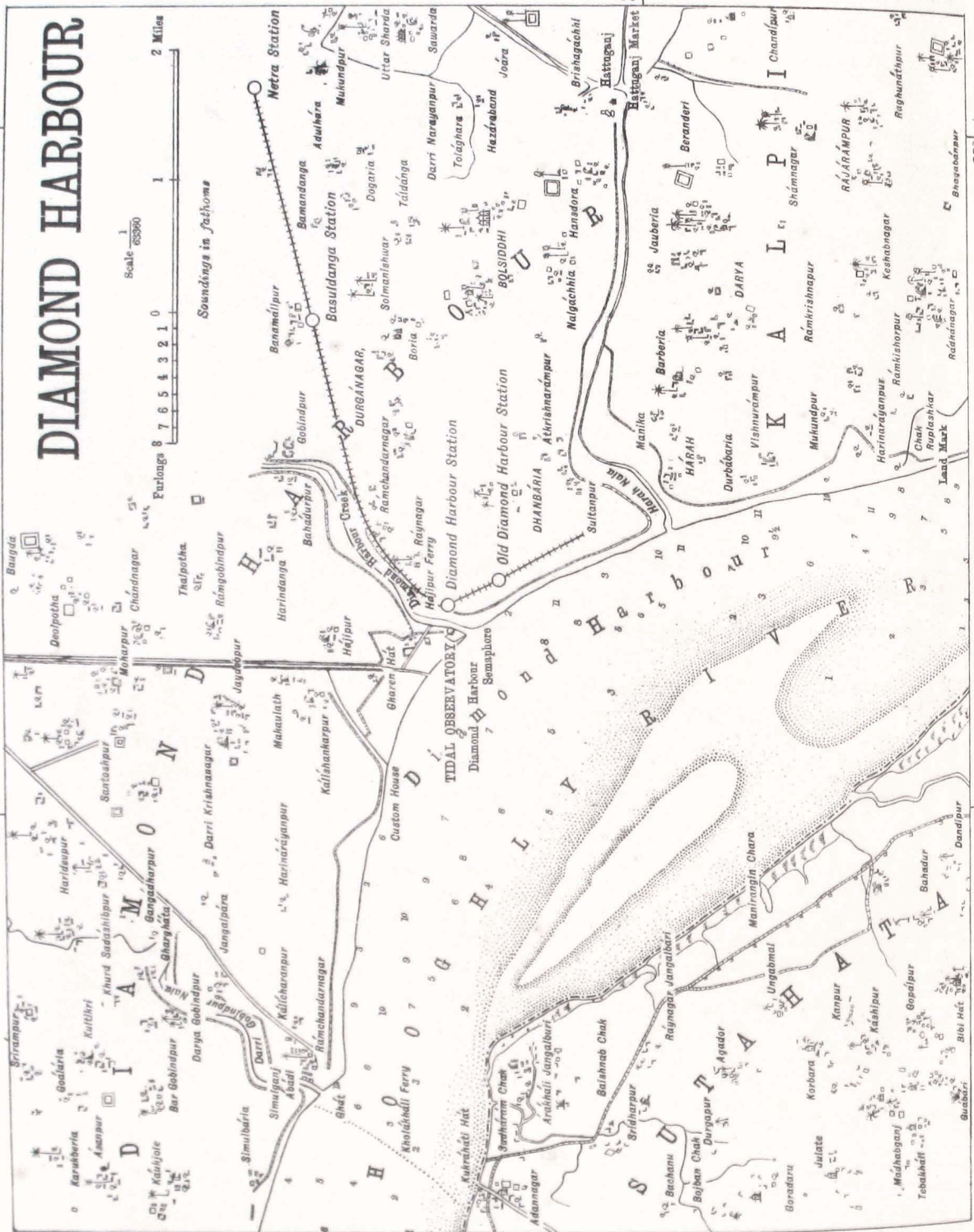
# DIAMOND HARBOUR

Scale 1/63500

Furlongs 8 7 6 5 4 3 2 1 0

Soundings in Fathoms

88° 10'



88° 15'

88° 10'

## DIAMOND HARBOUR.

## ON THE HOOGLY RIVER.

(*Tidal Observatory, Lat. 22° 11' N., Long. 88° 12' E.*)

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The tidal observatory at Diamond Harbour, about forty miles below Calcutta on the left bank of the Hooghly and about halfway between Kidderpore and Dublat, was one of the minor observatories at which five years' observations are considered sufficient, and was situated on the west side of the Diamond Harbour Creek in the position shown on the accompanying chart. It was a substantial wooden cabin built on the piles of a former observatory. The float-cylinder, thirty feet in length, which gave ample range for extreme tides, passed through and was secured to the flooring, above which it rose three and a half feet, and was also bound to the frame-work supporting the observatory by an iron band halfway down. The communication was through holes bored in the closed bottom of the cylinder.

The working scale of the tide-gauge was one-sixth.

Registrations were commenced on the 4th April, 1881, and, in spite of frequent stoppages of the clock due to vibration, were tolerably satisfactory until the beginning of August, 1885, when, during very heavy freshets, the observatory gave way and tilted on one side. The instruments were removed, and the repairs were completed and registrations resumed by the end of the same month. On the 12th April, 1886, the observations, which during the seven preceding months had become more and more frequently interrupted by vibration, were concluded; and the observatory, which during the same period had been growing dangerously unstable and had settled five inches, was dismantled.

The disturbances of the surface of the ocean, caused by the Krakatoa volcanic eruptions, were recorded at this tidal station by the self-registering tide-gauge on the 27th August, 1883.

Barometrical and anemometrical observations were carried on simultaneously with the tidal observations. The barometer was placed in the observatory and the anemometer on the top of the same building.

The bench-mark of reference bears in its centre the inscription  $\begin{matrix} \text{G. T. S.} \\ \text{O} \\ \text{B. M. A.} \end{matrix}$ , and is situated two hundred and ten feet west of the site of the tidal observatory, just below the embankment near its junction with the path leading to the burial ground. It is 19·882 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = XI<sup>h</sup> 55<sup>m</sup>.

The highest high water recorded was 21·8 feet above the zero of the gauge, and occurred in August, 1885.

The lowest low water recorded was 0·4 foot *below* the zero of the gauge, and occurred in February, 1886.

In 1881-82 the mean range of largest ordinary springs was found to be 15·8 feet.

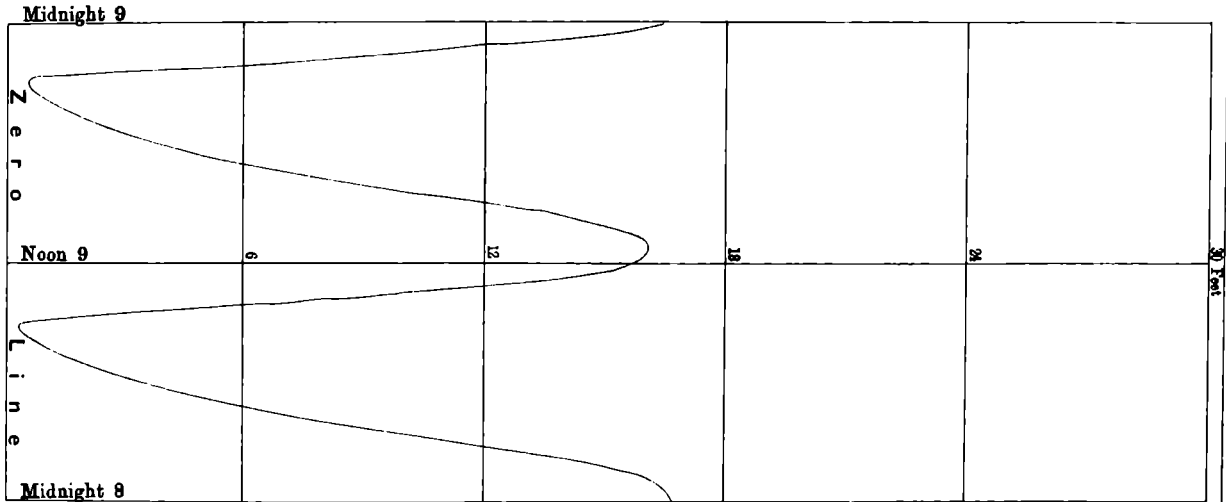
The height of mean-water-level above the zero of the gauge had the following values :—

1881-82	...	...	...	8·976 feet.
1882-83	...	...	...	9·011 „
1883-84	...	...	...	8·999 „
1884-85	...	...	...	8·897 „
1885-86	...	...	...	8·804 „

NOTE.—The level of the zero of the gauge at Diamond Harbour is identical with that of the zero of the gauge at Kidderpore, and is 6·222 feet above that of the zero of the gauge at Dublat.

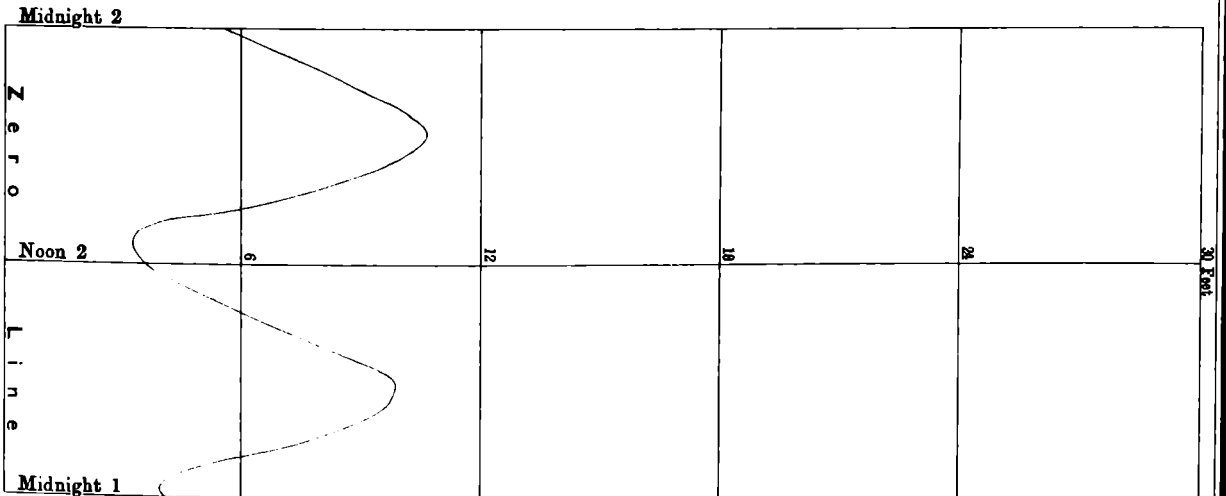
**TIDAL CURVES**  
at  
**DIAMOND HARBOUR**

Spring Tide — 9th February 1883



New Moon — 7th February 1883

Neap Tide — 2nd February 1883



Last Quarter — 31st January 1883

*Photocopyographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun. September 1889.*

*Values of H's at Diamond Harbour.*

TIDE	H					TIDE
	1881-82	1882-83	1883-84	1884-85	1885-86	
	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0·082	0·088	0·093	0·092	0·101	S <sub>1</sub>
S <sub>2</sub>	2·215	2·288	2·252	2·202	2·199	S <sub>2</sub>
S <sub>4</sub>	0·117	0·122	0·132	0·123	0·123	S <sub>4</sub>
S <sub>6</sub>	·013	·013	·015	·013	·006	S <sub>6</sub>
S <sub>8</sub>	·002	·004	·004	·007	·002	S <sub>8</sub>
M <sub>1</sub>	·020	·020	·022	·052	·032	M <sub>1</sub>
M <sub>2</sub>	5·175	5·179	5·177	5·135	5·154	M <sub>2</sub>
M <sub>3</sub>	0·042	0·028	0·061	0·062	0·058	M <sub>3</sub>
M <sub>4</sub>	·756	·734	·752	·753	·765	M <sub>4</sub>
M <sub>6</sub>	·156	·148	·163	·141	·144	M <sub>6</sub>
M <sub>8</sub>	·065	·058	·060	·053	·053	M <sub>8</sub>
O	·237	·230	·211	·217	·233	O
K <sub>1</sub>	·499	·492	·508	·498	·515	K <sub>1</sub>
K <sub>2</sub>	·667	·644	·730	·718	·622	K <sub>2</sub>
P	·176	·174	·173	·184	·171	P
J	·029	·033	·006	·035	·045	J
Q	·024	·036	·036	·019	·016	Q
L	·174	·347	·201	·280	·276	L
N	·988	·914	·898	·945	1·030	N
λ	·171	·058	·046	·192	0·267	λ
ν	·420	·186	·204	·387	·203	ν
μ	·272	·333	·298	·338	·268	μ
R	...	·216	...	·175	...	R
T	...	·078	...	·317	...	T
MS	·687	·702	·702	·728	·709	MS
2SM	·095	·053	·058	·069	·074	2SM
2N	·138	·076	·212	·167	·147	2N
M <sub>2</sub> N	·200	·088	·100	·085	·116	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	·130	·065	·124	·159	·107	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	·067	·050	·066	·059	·065	2M <sub>2</sub> K <sub>1</sub>
Mm	·147	·057	·156	·145	·078	Mm
Mf	·157	·142	·216	·155	·096	Mf
MSf	·401	·501	·453	·424	·483	MSf
Sa	1·011	1·189	·980	·991	1·119	Sa
Ssa	0·023	0·109	·103	·069	0·182	Ssa

## TIDAL OBSERVATIONS.

*Values of  $\kappa$ 's at Diamond Harbour.*

TIDE	$\kappa$					TIDE
	1881-82	1882-83	1883-84	1884-85	1885-86	
	o	o	o	o	o	
S <sub>1</sub>	156·14	147·38	149·53	161·09	162·94	S <sub>1</sub>
S <sub>2</sub>	26·06	25·14	26·15	26·49	25·98	S <sub>2</sub>
S <sub>4</sub>	328·35	323·01	330·30	328·73	326·18	S <sub>4</sub>
S <sub>6</sub>	266·42	234·83	267·73	269·56	233·13	S <sub>6</sub>
S <sub>8</sub>	304·70	41·50	240·64	285·95	175·03	S <sub>8</sub>
M <sub>1</sub>	87·65	103·07	145·06	202·53	277·22	M <sub>1</sub>
M <sub>2</sub>	344·81	343·56	344·30	344·71	344·82	M <sub>2</sub>
M <sub>3</sub>	219·54	225·47	244·68	237·14	224·72	M <sub>3</sub>
M <sub>4</sub>	246·42	245·36	246·27	249·01	249·81	M <sub>4</sub>
M <sub>6</sub>	106·44	104·98	105·93	112·37	110·03	M <sub>6</sub>
M <sub>8</sub>	347·24	343·26	343·91	348·72	354·04	M <sub>8</sub>
O	344·11	345·98	342·12	350·44	348·26	O
K <sub>1</sub>	14·99	13·83	15·50	14·32	13·49	K <sub>1</sub>
K <sub>2</sub>	19·58	26·50	24·65	22·76	30·05	K <sub>2</sub>
P	6·13	11·57	8·61	11·94	11·16	P
J	299·22	339·95	67·95	28·37	24·04	J
Q	8·89	9·66	304·32	301·12	43·56	Q
L	356·98	344·19	335·29	344·23	8·11	L
N	339·18	339·74	335·80	335·79	347·01	N
$\lambda$	18·73	296·13	22·48	356·71	358·05	$\lambda$
$\nu$	293·85	284·10	346·13	330·53	299·30	$\nu$
$\mu$	79·18	89·95	90·05	82·05	85·34	$\mu$
R	...	9·60	...	16·53	...	R
T	...	55·45	...	86·44	...	T
MS	285·58	283·67	287·52	288·57	288·26	MS
2SM	251·34	289·79	273·77	271·17	289·76	2SM
2N	343·33	42·64	287·50	313·80	321·11	2N
M <sub>2</sub> N	31·77	62·68	71·01	25·04	67·71	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	294·89	283·72	249·04	278·74	300·80	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	226·71	224·58	214·03	220·25	200·75	2M <sub>2</sub> K <sub>1</sub>
Mm	11·65	351·22	25·72	16·59	2·94	Mm
Mf	36·00	41·48	57·21	40·40	33·23	Mf
MSf	25·74	40·25	40·61	36·15	29·36	MSf
Sa	139·77	146·81	140·81	142·83	140·31	Sa
Saa	64·21	76·79	91·82	150·10	262·35	Saa



# KIDDERPORE CALCUTTA

Scale 1:63,360



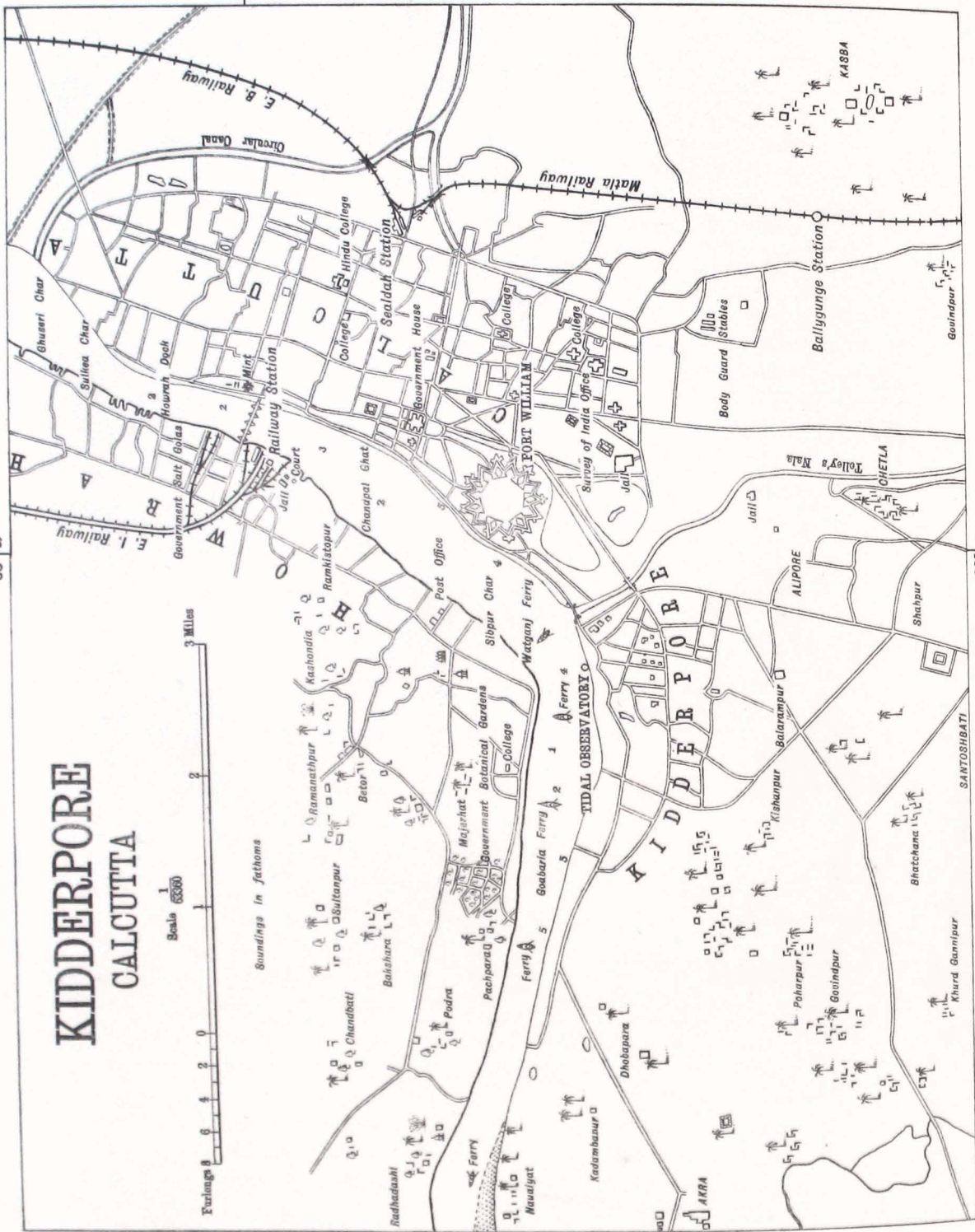
Soundings in fathoms

22° 22' 35"

22° 35'

88° 20'

88° 20'





## KIDDERPORE (CALCUTTA).

ON THE HOOGLHY RIVER.

*(Tidal Observatory, Lat. 22° 32' N., Long. 88° 20' E.)*

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The tidal observatory at Kidderpore in Calcutta is one of the permanent observatories, and is situated on the south or left side of the Hooghly, well out in the stream, just below and close to the main entrance of the Kidderpore New Dock, in the position shown on the accompanying chart. It is a substantial wooden cabin resting on stout piles driven firmly into the mud, and reached by a roadway constructed on the protecting piles of the dock-entrance. The float-cylinder, twenty-four inches in internal diameter and thirty feet long, giving ample range for extreme tides, is supported by the floor of the observatory, through which it rises, and is also securely attached to the frame-work of the supporting piles. The communication is by holes bored in the closed bottom of the cylinder; and there is a man-hole near the bottom of the cylinder for clearing out any accumulation of mud.

The working scale of the tide-gauge is one-sixth.

Registrations were commenced on the 22nd March, 1881, and have been continued satisfactorily without any serious interruption up to the present. On the 10th May, 1881, a sudden and very violent gale tore off the roof of the observatory, but caused no material gap in the registrations. Throughout the period of the observations the clock has experienced short stoppages through vibration of the observatory, which have caused insignificant breaks in the tidal curves: of late these stoppages have been considerably less frequent.

The disturbances of the surface of the ocean, caused by the Krakatoa volcanic eruptions, were recorded at this tidal station by the self-registering tide-gauge on the 27th August, 1883.

Barometrical and anemometrical observations have been carried on simultaneously with the tidal observations. The barometer was placed in the observatory, and the anemometer was at first set up on a neighbouring Sail Loft; but in 1887 this building was taken down during dockyard alterations, and the anemometer was then transferred to the top of the tidal observatory.

The bench-mark of reference consists of the inscription  $\begin{matrix} \text{G. T. S.} \\ \text{O} \\ \text{B. M.} \end{matrix}$  A, engraved on the coping of the west wall of the main entrance of the Kidderpore New Dock, ten and a half feet north of the Swing Bridge. It is 23·928 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = 11<sup>h</sup> 2<sup>m</sup>.

The highest high water recorded was 24·1 feet above the zero of the gauge, and occurred in August, 1890.

The lowest low water recorded was 2·2 feet above the zero of the gauge, and occurred in February, 1882.

In 1881-82 the mean range of largest ordinary springs was found to be 11·7 feet.

The height of mean-water-level above the zero of the gauge had the following values:—

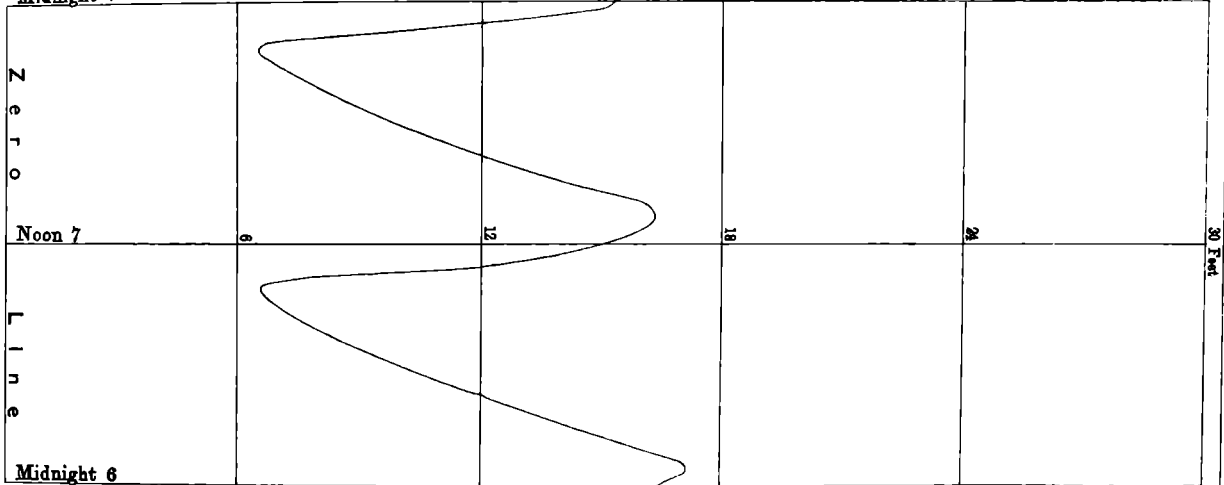
1881-82	...	...	...	10·739 feet.
1882-83	...	...	...	10·686 „
1883-84	...	...	...	10·599 „
1884-85	...	...	...	10·669 „
1885-86	...	...	...	10·950 „
1886-87	...	...	...	11·383 „
1887-88	...	...	...	11·080 „
1888-89	...	...	...	10·842 „
1889-90	...	...	...	11·232 „
1890-91	...	...	...	11·364 „
1891-92	...	...	...	10·618 „

NOTE.—The level of the zero of the gauge at Kidderpore is identical with that of the zero of the gauge at Diamond Harbour, and is 6·222 feet above that of the zero of the gauge at Dublat.

**TIDAL CURVES**  
at  
**KIDDERPORE (Calcutta)**

Spring Tide — 7th November 1889

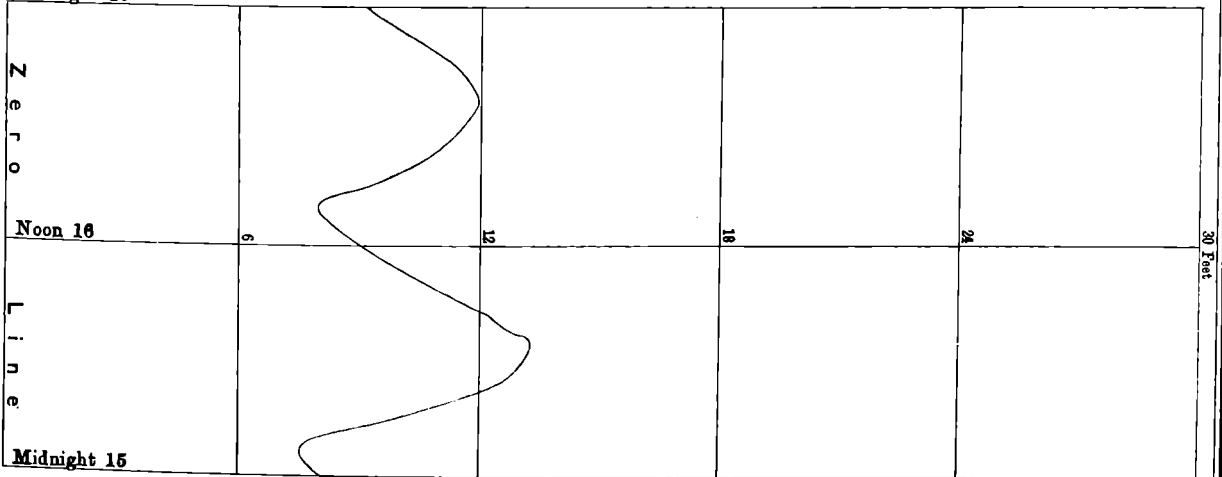
Midnight 7



Full Moon — 7th November 1889

Neap Tide — 16th November 1889

Midnight 16



Last Quarter — 15th November 1889

*Photoincographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun, January 1900.*

*Values of H's at Kidderpore.*

TIDE	H					TIDE
	1881-82	1882-83	1883-84	1884-85	1885-86	
	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0.094	0.088	0.097	0.082	0.088	S <sub>1</sub>
S <sub>2</sub>	1.427	1.508	1.513	1.462	1.459	S <sub>2</sub>
S <sub>4</sub>	0.066	0.084	0.095	0.080	0.074	S <sub>4</sub>
S <sub>6</sub>	.006	.004	.003	.001	.008	S <sub>6</sub>
S <sub>8</sub>	.006	.009	.002	.007	.005	S <sub>8</sub>
M <sub>1</sub>	.012	.013	.034	.052	.051	M <sub>1</sub>
M <sub>2</sub>	3.593	3.660	3.646	3.674	3.627	M <sub>2</sub>
M <sub>3</sub>	0.012	0.018	0.028	0.043	0.060	M <sub>3</sub>
M <sub>4</sub>	.734	.719	.691	.729	.736	M <sub>4</sub>
M <sub>6</sub>	.158	.160	.156	.156	.161	M <sub>6</sub>
M <sub>8</sub>	.074	.082	.073	.067	.065	M <sub>8</sub>
O	.228	.211	.206	.210	.209	O
K <sub>1</sub>	.390	.387	.400	.398	.394	K <sub>1</sub>
K <sub>2</sub>	.439	.431	.504	.489	.381	K <sub>2</sub>
P	.146	.142	.140	.153	.132	P
J	.016	.012	.017	.031	.011	J
Q	.039	.039	.036	.034	.016	Q
L	.201	.173	.222	.151	.221	L
N	.677	.599	.628	.662	.675	N
λ	.126	.075	.091	.055	.098	λ
ν	.323	.152	.170	.318	.320	ν
μ	.224	.260	.294	.220	.206	μ
R	...	.167	...	.123	...	R
T	...	.147	...	.175	...	T
MS	.646	.643	.645	.625	.654	MS
2SM	.084	.086	.063	.066	.096	2SM
2N	.079	.038	.124	.127	.099	2N
M <sub>2</sub> N	.033	.184	.108	.105	.043	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	.086	.125	.144	.085	.082	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	.036	.034	.032	.032	.040	2M <sub>2</sub> K <sub>1</sub>
Mm	.316	.172	.290	.288	.269	Mm
Mf	.301	.293	.346	.238	.317	Mf
MSf	.829	.920	.905	.834	.981	MSf
Sa	2.809	2.670	2.312	2.361	3.006	Sa
Ssa	0.935	0.708	0.714	0.651	1.307	Ssa

## TIDAL OBSERVATIONS.

*Values of H's at Kidderpore—(Continued).*

TIDE	H						TIDE
	1886-87	1887-88	1888-89	1889-90	1890-91	1891-92	
	Feet	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0.082	0.077	0.091	0.087	0.081	0.086	S <sub>1</sub>
S <sub>2</sub>	1.482	1.490	1.496	1.520	1.498	1.541	S <sub>2</sub>
S <sub>3</sub>	0.093	0.093	0.094	0.099	0.093	0.108	S <sub>3</sub>
S <sub>4</sub>	.005	.004	.001	.002	.003	.003	S <sub>4</sub>
S <sub>5</sub>	.003	.002	.001	.001	.004	.002	S <sub>5</sub>
M <sub>1</sub>	.039	.030	.028	.033	.010	.011	M <sub>1</sub>
M <sub>2</sub>	3.521	3.568	3.720	3.638	3.572	3.645	M <sub>2</sub>
M <sub>3</sub>	0.056	0.055	0.046	0.030	0.024	0.016	M <sub>3</sub>
M <sub>4</sub>	.714	.735	.779	.742	.743	.755	M <sub>4</sub>
M <sub>5</sub>	.144	.156	.163	.145	.147	.154	M <sub>5</sub>
M <sub>6</sub>	.070	.073	.080	.056	.066	.064	M <sub>6</sub>
O	.194	.206	.213	.210	.200	.209	O
K <sub>1</sub>	.384	.383	.406	.390	.385	.383	K <sub>1</sub>
K <sub>2</sub>	.451	.474	.411	.413	.427	.502	K <sub>2</sub>
P	.136	.151	.120	.133	.120	.151	P
J	.004	.026	.044	.009	.005	.022	J
Q	.011	.027	.026	.034	.041	.022	Q
L	.210	.304	.152	.175	.172	.279	L
N	.649	.646	.737	.727	.690	.638	N
λ	...	...	...	...	...	...	λ
ν	.185	.133	.256	.341	.282	.133	ν
μ	.203	.231	.194	.222	.224	.275	μ
R	...	...	...	...	...	...	R
T	.127	.046	.176	.180	.115	.093	T
MS	.651	.653	.682	.694	.682	.706	MS
2SM	.089	.079	.071	.063	.071	.086	2SM
2N	.059	.100	.090	.145	.102	.041	2N
M <sub>2</sub> N	.146	.105	.068	.056	.149	.119	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	.123	.147	.099	.078	.135	.139	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	.028	.033	.032	.020	.032	.038	2M <sub>2</sub> K <sub>1</sub>
Mm	.287	.251	.314	.311	.404	.323	Mm
Mf	.263	.260	.243	.221	.260	.205	Mf
MSf	.979	.907	.901	.982	.893	.900	MSf
Sa	3.114	2.874	2.810	2.837	3.554	2.527	Sa
Ssa	1.092	0.711	1.289	0.900	1.177	0.751	Ssa

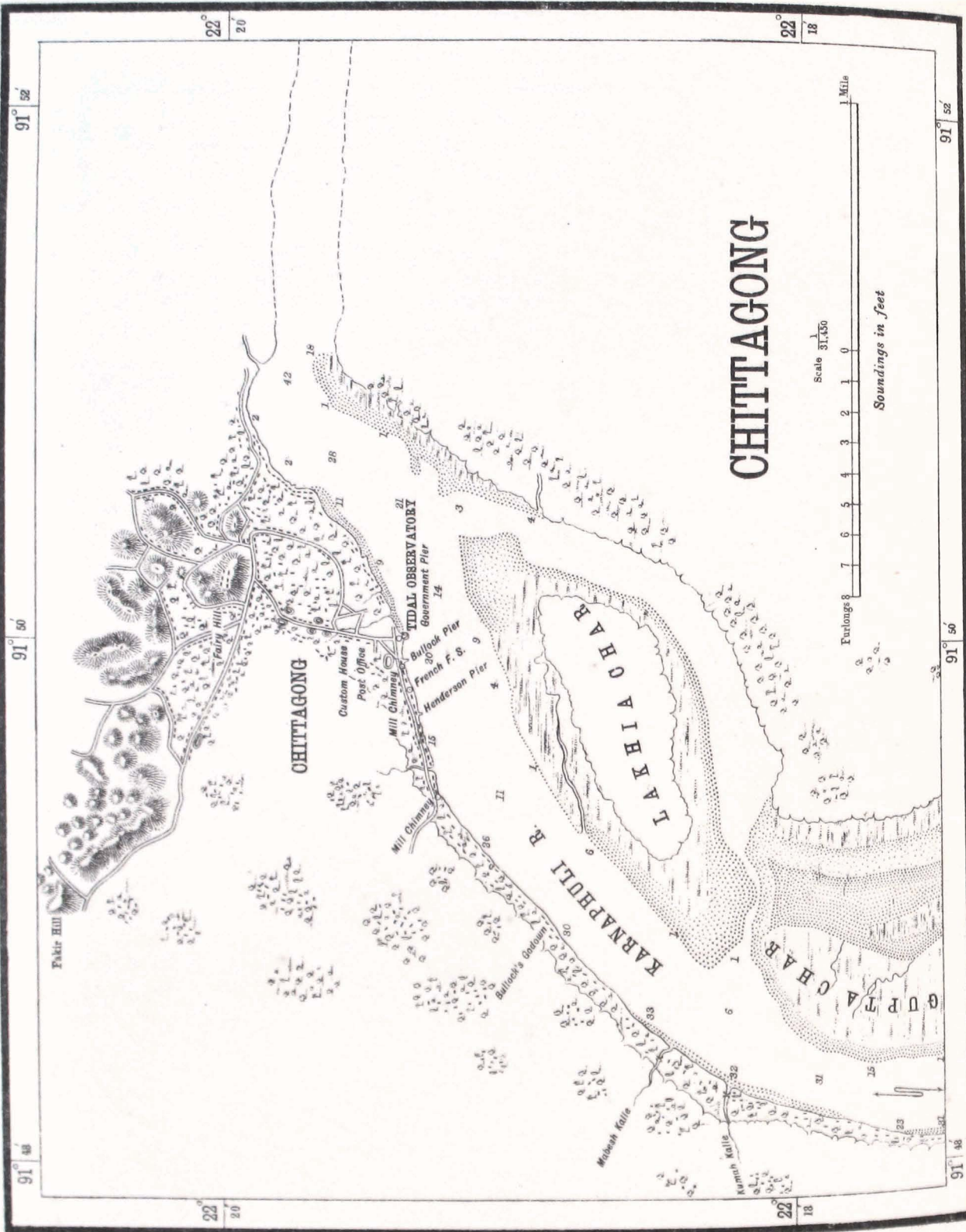
*Values of  $\kappa$ 's at Kidderpore.*

TIDE	$\kappa$					TIDE
	1881-82	1882-83	1883-84	1884-85	1885-86	
	°	°	°	°	°	
S <sub>1</sub>	196.96	189.51	193.42	200.48	204.50	S <sub>1</sub>
S <sub>2</sub>	101.81	100.52	102.95	103.66	102.45	S <sub>2</sub>
S <sub>4</sub>	126.45	110.68	124.12	118.10	116.88	S <sub>4</sub>
S <sub>6</sub>	266.37	331.70	58.67	194.04	340.40	S <sub>6</sub>
S <sub>8</sub>	297.76	323.26	227.29	235.01	285.35	S <sub>8</sub>
M <sub>1</sub>	112.04	201.79	177.81	260.29	334.75	M <sub>1</sub>
M <sub>2</sub>	58.53	57.64	57.88	59.87	60.35	M <sub>2</sub>
M <sub>3</sub>	334.89	327.72	350.26	343.98	332.75	M <sub>3</sub>
M <sub>4</sub>	38.59	35.49	36.03	40.34	42.07	M <sub>4</sub>
M <sub>6</sub>	322.56	314.87	310.40	325.37	330.81	M <sub>6</sub>
M <sub>8</sub>	275.82	263.27	267.59	273.46	284.33	M <sub>8</sub>
O	21.76	19.70	15.58	23.30	22.86	O
K <sub>1</sub>	57.53	53.51	55.31	55.02	56.90	K <sub>1</sub>
K <sub>2</sub>	90.28	100.73	103.14	98.13	94.88	K <sub>2</sub>
P	41.95	52.32	49.09	51.03	40.01	P
J	355.21	297.90	317.00	50.10	82.12	J
Q	357.58	19.74	349.87	350.28	14.40	Q
L	86.39	61.76	59.20	62.61	73.69	L
N	47.92	46.23	42.03	44.99	47.08	N
$\lambda$	130.99	83.53	43.54	72.92	134.35	$\lambda$
$\nu$	357.93	348.97	61.53	44.43	12.81	$\nu$
$\mu$	173.97	189.97	180.71	182.65	191.47	$\mu$
R	...	77.09	...	79.34	...	R
T	...	107.11	...	184.34	...	T
MS	82.01	80.29	82.46	84.92	85.00	MS
2SM	354.95	8.66	14.75	12.64	16.67	2SM
2N	25.71	103.53	354.88	34.36	8.24	2N
M <sub>2</sub> N	256.66	219.12	293.39	227.61	130.84	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	17.19	21.18	38.86	60.96	26.31	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	341.65	337.88	296.10	324.49	301.02	2M <sub>2</sub> K <sub>1</sub>
Mm	0.38	340.65	21.89	12.25	18.11	Mm
Mf	41.08	35.65	53.58	53.71	34.36	Mf
MSf	34.52	42.94	46.64	42.95	40.31	MSf
Sa	157.08	157.22	149.80	161.90	160.71	Sa
Ssa	204.56	333.63	321.58	353.22	328.33	Ssa

## TIDAL OBSERVATIONS.

Values of  $\kappa$ 's at Kidderpore—(Continued).

TIDE	$\kappa$						TIDE
	1886-87	1887-88	1888-89	1889-90	1890-91	1891-92	
	o	o	o	o	o	o	
S <sub>1</sub>	196.91	208.00	201.49	184.76	195.60	198.63	S <sub>1</sub>
S <sub>2</sub>	98.21	100.51	100.17	98.45	97.39	99.47	S <sub>2</sub>
S <sub>3</sub>	107.99	114.01	109.94	113.79	112.92	105.95	S <sub>3</sub>
S <sub>6</sub>	40.97	70.64	339.44	104.62	101.69	65.86	S <sub>6</sub>
S <sub>8</sub>	297.47	255.38	212.47	236.31	187.13	246.04	S <sub>8</sub>
M <sub>1</sub>	354.68	28.72	32.78	68.30	163.96	141.53	M <sub>1</sub>
M <sub>2</sub>	58.06	57.99	58.07	55.97	56.55	56.92	M <sub>2</sub>
M <sub>3</sub>	314.58	310.91	285.64	269.52	294.85	323.58	M <sub>3</sub>
M <sub>4</sub>	39.61	39.16	37.78	33.71	35.52	36.45	M <sub>4</sub>
M <sub>6</sub>	324.11	323.14	323.33	322.92	328.58	323.91	M <sub>6</sub>
M <sub>8</sub>	276.51	276.67	271.16	262.33	288.72	274.10	M <sub>8</sub>
O	22.65	18.41	24.16	25.17	23.86	21.55	O
K <sub>1</sub>	54.17	50.56	53.33	55.40	53.50	53.53	K <sub>1</sub>
K <sub>2</sub>	96.23	98.06	90.05	94.09	91.67	94.51	K <sub>2</sub>
P	40.22	46.03	40.19	42.32	43.34	40.60	P
J	274.02	351.01	31.10	58.00	62.25	348.89	J
Q	349.45	8.57	356.58	354.06	351.07	356.69	Q
L	65.45	65.84	55.41	74.15	71.21	97.67	L
N	44.84	41.97	39.83	42.81	49.27	43.83	N
$\lambda$	...	...	...	...	...	...	$\lambda$
$\nu$	2.68	28.59	56.79	20.07	1.87	4.68	$\nu$
$\mu$	203.07	190.99	186.34	186.12	190.44	189.20	$\mu$
R	...	...	...	...	...	...	R
T	87.49	176.27	167.03	115.26	75.49	179.74	T
MS	81.57	82.38	81.15	75.68	78.08	78.63	MS
2SM	17.17	26.51	25.64	12.52	7.22	15.61	2SM
2N	37.06	21.43	22.17	9.51	43.49	53.46	2N
M <sub>2</sub> N	235.19	257.44	245.27	172.93	255.57	262.21	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	20.98	32.09	49.42	18.67	20.94	38.41	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	262.16	286.98	292.51	341.63	317.92	335.63	2M <sub>2</sub> K <sub>1</sub>
Mm	353.10	359.79	5.28	354.27	355.98	9.20	Mm
Mf	19.21	13.37	37.49	21.49	18.68	27.23	Mf
MSf	40.73	45.72	41.49	44.24	41.37	43.94	MSf
Sa	162.83	149.00	153.53	159.25	153.49	152.69	Sa
Ssa	345.27	337.21	332.55	336.53	329.46	340.25	Ssa



Photos in photograph at the Office of the Trigonometrical Branch, Survey of India, Dacca Division, October, 1900.



## CHITTAGONG.

(*Tidal Observatory, Lat. 22° 20' N., Long. 91° 50' E.*)

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The tidal observatory at Chittagong, at the northern extremity of the eastern shore of the Bay of Bengal, was one of the minor observatories at which five years' observations are considered sufficient, and stood on the west side of the head of the iron jetty at the town of Chittagong, on the north or right bank of the river Karnaphuli, ten and three-quarter miles from its mouth, in the position shown on the accompanying chart. The observatory, which was that previously used at Diamond Harbour, was firmly bolted to the flooring of the jetty. The float-cylinder was of iron, twenty-four inches in diameter and thirty-two feet long. The top was two feet four inches above the floor of the observatory and about seven feet above the highest tides, and the bottom was three feet above the bed of the river and about six feet below the lowest tides. The cylinder was secured to the girders of the jetty by iron bands in four places, and by a chain about nine feet from the bottom; and chains were stretched from pile to pile under the jetty to defend the cylinder from damage by timber brought down the river by the ebb-tide which here flows with great strength. The communication was through a number of holes, about an inch in diameter, drilled just above the lowest flange and in the closed bottom of the cylinder.

The working scale of the tide-gauge was one-fourth.

Registrations were commenced on the 6th June, 1886, and continued satisfactorily until the observatory was dismantled on the 22nd July, 1891, on the completion of five years' observations. The only fault to be found with the tide-gauge apparatus was the somewhat variable rate of the driving clock, which occasionally led to small corrections having to be made on the diagrams.

Barometrical and anemometrical observations were carried on simultaneously with the tidal observations. The barometer was placed in the observatory and the anemometer on the top of the same building.

The bench-mark of reference is the Bench-mark A, which is indicated by a circle inscribed on the upper surface of a three-foot cube of masonry built near the S.E. corner of the Port and Customs Office. It is 22·702 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = 1<sup>h</sup> 12<sup>m</sup>.

The highest high water recorded was 19·3 feet above the zero of the gauge, and occurred in October, 1888.

The lowest low water recorded was 0·1 foot above the zero of the gauge, and occurred in February, 1887.

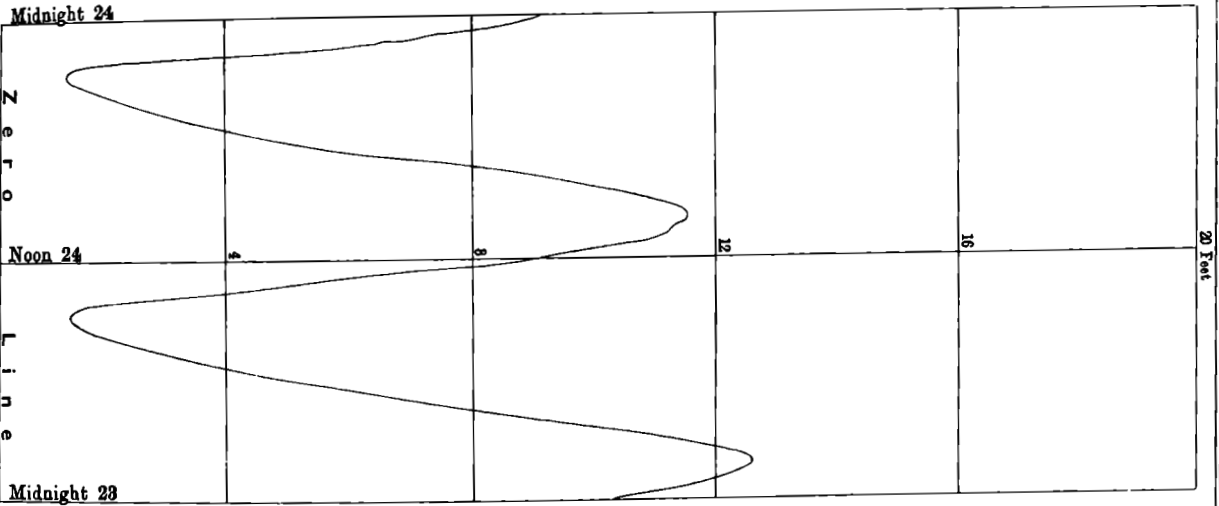
In 1889 the mean range of largest ordinary springs was found to be 13·3 feet.

The height of mean-water-level above the zero of the gauge had the following values:—

1886-87	...	...	...	8·251 feet.
1887-88	...	...	...	7·945 „
1888-89	...	...	...	7·923 „
1889-90	...	...	...	8·086 „
1890-91	...	...	...	7·977 „

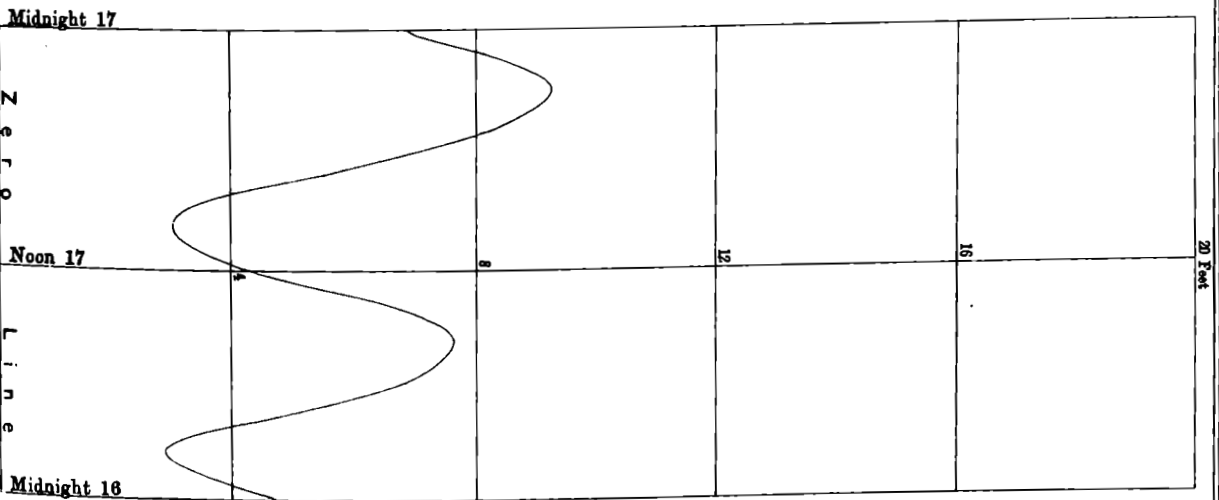
TIDAL CURVES  
at  
CHITTAGONG

Spring Tide — 24th February 1891



Full Moon — 23rd February 1891

Neap Tide — 17th February 1891



First Quarter — 15th February 1891

Photocnographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun. January 1900.

*Values of H's at Chittagong.*

TIDE	H					TIDE
	1886-87	1887-88	1888-89	1889-90	1890-91	
	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0.060	0.056	0.072	0.077	0.067	S <sub>1</sub>
S <sub>2</sub>	1.568	1.553	1.584	1.584	1.571	S <sub>2</sub>
S <sub>4</sub>	0.049	0.053	0.056	0.061	0.054	S <sub>4</sub>
S <sub>6</sub>	.010	.010	.006	.007	.010	S <sub>6</sub>
S <sub>8</sub>	.002	.002	.004	.004	.004	S <sub>8</sub>
M <sub>1</sub>	.025	.022	.048	.043	.006	M <sub>1</sub>
M <sub>2</sub>	4.428	4.440	4.424	4.485	4.445	M <sub>2</sub>
M <sub>3</sub>	0.039	0.044	0.040	0.031	0.012	M <sub>3</sub>
M <sub>4</sub>	.421	.395	.403	.391	.418	M <sub>4</sub>
M <sub>6</sub>	.143	.149	.124	.140	.143	M <sub>6</sub>
M <sub>8</sub>	.035	.034	.029	.027	.029	M <sub>8</sub>
O	.295	.289	.287	.289	.293	O
K <sub>1</sub>	.582	.576	.599	.596	.613	K <sub>1</sub>
K <sub>2</sub>	.438	.397	.389	.471	.458	K <sub>2</sub>
P	.192	.195	.188	.185	.219	P
J	.053	.027	.018	.038	.059	J
Q	.016	.025	.021	.019	.034	Q
L	.425	.399	.345	.181	.342	L
N	.869	.841	.847	.823	.824	N
λ	.207	...	...	...	...	λ
ν	.402	.295	.117	.314	.368	ν
μ	.268	.276	.304	.301	.300	μ
R	...	...	...	...	...	R
T	...	.139	.133	.074	.106	T
MS	.355	.344	.348	.345	.338	MS
2SM	.129	.138	.133	.123	.133	2SM
2N	.031	.080	.211	.334	.112	2N
M <sub>2</sub> N	.143	.088	.167	.056	.167	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	.131	.102	.039	.094	.134	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	.049	.043	.061	.071	.073	2M <sub>2</sub> K <sub>1</sub>
Mm	.075	.177	.230	.226	.253	Mm
Mf	.181	.173	.136	.029	.184	Mf
MSf	.432	.459	.450	.354	.443	MSf
Sa	1.666	1.435	1.637	1.221	1.877	Sa
Ssa	0.178	0.105	0.206	0.120	0.158	Ssa

## TIDAL OBSERVATIONS.

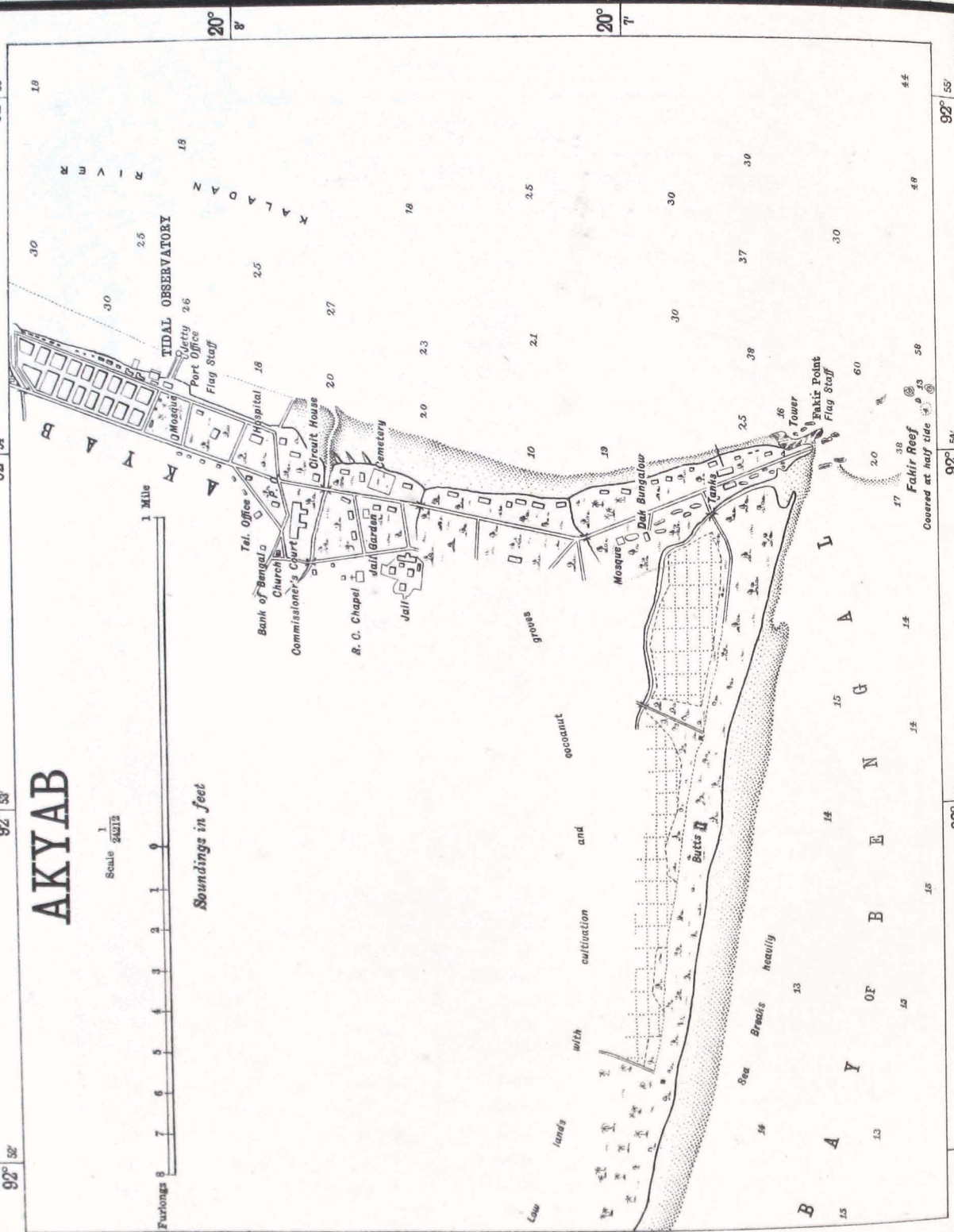
*Values of  $\kappa$ 's at Chittagong.*

TIDE	$\kappa$					TIDE
	1886-87	1887-88	1888-89	1889-90	1890-91	
	o	o	o	o	o	
S <sub>1</sub>	120.09	126.75	116.28	105.21	106.70	S <sub>1</sub>
S <sub>2</sub>	68.45	68.18	68.46	70.86	69.88	S <sub>2</sub>
S <sub>3</sub>	54.55	62.52	57.51	64.95	66.66	S <sub>3</sub>
S <sub>6</sub>	131.08	125.19	135.00	159.25	150.83	S <sub>6</sub>
S <sub>8</sub>	217.41	146.98	154.89	146.31	215.91	S <sub>8</sub>
M <sub>1</sub>	22.82	46.83	85.37	106.76	110.16	M <sub>1</sub>
M <sub>2</sub>	34.89	35.29	35.12	34.61	36.49	M <sub>2</sub>
M <sub>3</sub>	218.15	198.34	205.35	176.88	161.03	M <sub>3</sub>
M <sub>4</sub>	341.96	343.52	341.10	341.89	346.29	M <sub>4</sub>
M <sub>6</sub>	195.45	187.69	190.55	182.79	196.04	M <sub>6</sub>
M <sub>8</sub>	127.12	111.64	122.48	120.31	136.80	M <sub>8</sub>
O	11.55	16.13	10.79	9.00	11.72	O
K <sub>1</sub>	22.19	20.30	21.87	22.95	21.14	K <sub>1</sub>
K <sub>2</sub>	70.88	65.93	68.30	65.69	65.57	K <sub>2</sub>
P	26.00	31.21	31.32	34.19	32.52	P
J	51.47	98.88	17.75	33.91	59.94	J
Q	327.77	358.65	55.02	355.91	359.00	Q
L	60.30	39.17	39.71	65.96	70.35	L
N	23.51	24.78	24.48	28.77	22.81	N
$\lambda$	60.63	...	...	...	...	$\lambda$
$\nu$	24.23	1.67	19.39	50.28	38.03	$\nu$
$\mu$	200.14	205.60	196.43	203.80	197.41	$\mu$
R	...	...	...	...	...	R
T	...	246.33	164.75	83.50	302.21	T
MS	17.66	23.85	22.35	26.71	23.40	MS
2SM	299.41	303.05	306.54	295.83	296.42	2SM
2N	18.86	294.49	340.41	30.90	54.06	2N
M <sub>2</sub> N	246.35	274.99	237.45	203.82	257.10	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	310.32	337.51	326.90	289.07	308.63	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	262.97	262.93	279.85	266.22	273.24	2M <sub>2</sub> K <sub>1</sub>
Mm	338.70	8.64	11.13	0.18	341.66	Mm
Mf	39.64	343.44	22.07	21.36	19.53	Mf
MSf	39.14	42.31	39.61	38.90	38.82	MSf
Sa	136.59	131.74	132.62	135.87	134.51	Sa
Ssa	217.27	72.85	277.41	141.47	264.76	Ssa

# AKYAB

Scale  $\frac{1}{24113}$

*Soundings in feet*



Photostereographed at the Office of the Triangometrical Branch, Survey of India, Dibrud Dui, June 1899.

## A K Y A B .

(*Tidal Observatory, Lat. 20° 8' N., Long. 92° 54' E.*)

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The tidal observatory of Akyab, on the Burman coast at the mouth of the Kaladan River, was one of the minor observatories at which five years' observations are considered sufficient, and was situated at the north-west corner of the T-head of the iron pier opposite the Port Office, in the position shown on the accompanying chart. It was a very well constructed, substantial wooden cabin, twelve feet square, having its corner-posts let through the floor of the pier and bolted to the girders. The float-cylinder was of wrought iron, twenty-four inches in internal diameter and twenty-eight feet long. It was supported on stout cross beams resting on the iron frame-work of the pier, and its lower end was chained to the piles of the pier. The top of the cylinder was about a foot above the floor of the observatory and about ten feet above the highest tides, and the bottom was about seven feet below the lowest tides, and had deep water beneath it. The communication was through numerous perforations in a block of iron-wood that closed the bottom of the cylinder.

The working scale of the tide-gauge was one-third.

Registrations were commenced on the 9th May, 1887, and continued most satisfactorily until the observatory was closed on the 23rd May, 1892, at the end of five years' observations. At long intervals there were brief stoppages of the driving clock caused by steamers bumping against the pier, but these in no degree affected the value of the record; and the agreement between the predicted and the actually observed times and heights of the tides at this station has been extremely close.

Barometrical and anemometrical observations were taken simultaneously with the tidal observations. The barometer was placed in the observatory and the anemometer on the top of the same building.

## TIDAL OBSERVATIONS.

The bench-mark of reference is engraved <sup>G. T. S.</sup>  $\square$  B, and embedded in a block of masonry four-foot cube in the portico of the Port Office. It is 19·923 feet above the zero of the gauge. <sub>B. M. 1887.</sub>

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = IX<sup>h</sup> 37<sup>m</sup>.

The highest high water recorded was 13·9 feet above the zero of the gauge, and occurred in October, 1888.

The lowest low water recorded was 1·5 feet above the zero of the gauge, and occurred in March, 1892.

In 1890 the mean range of largest ordinary springs was found to be 8·3 feet.

The height of mean-sea-level above the zero of the gauge had the following values :—

1887-88	...	...	...	7·486 feet.
1888-89	...	...	...	7·430 „
1889-90	...	...	...	7·684 „
1890-91	...	...	...	7·535 „
1891-92	...	...	...	7·452 „



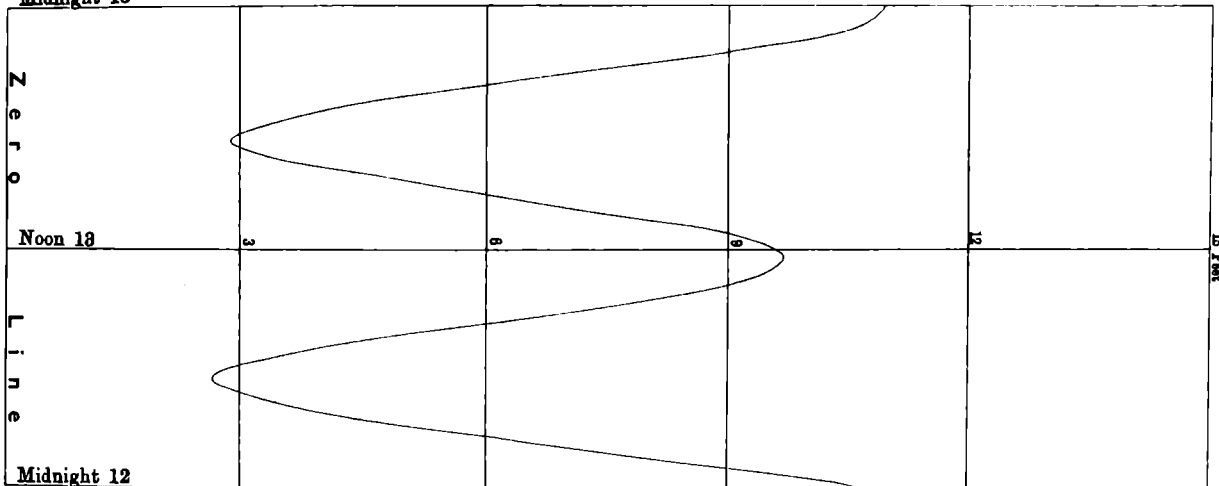
# TIDAL CURVES

at

## AKYAB

Spring Tide — 13th January 1891

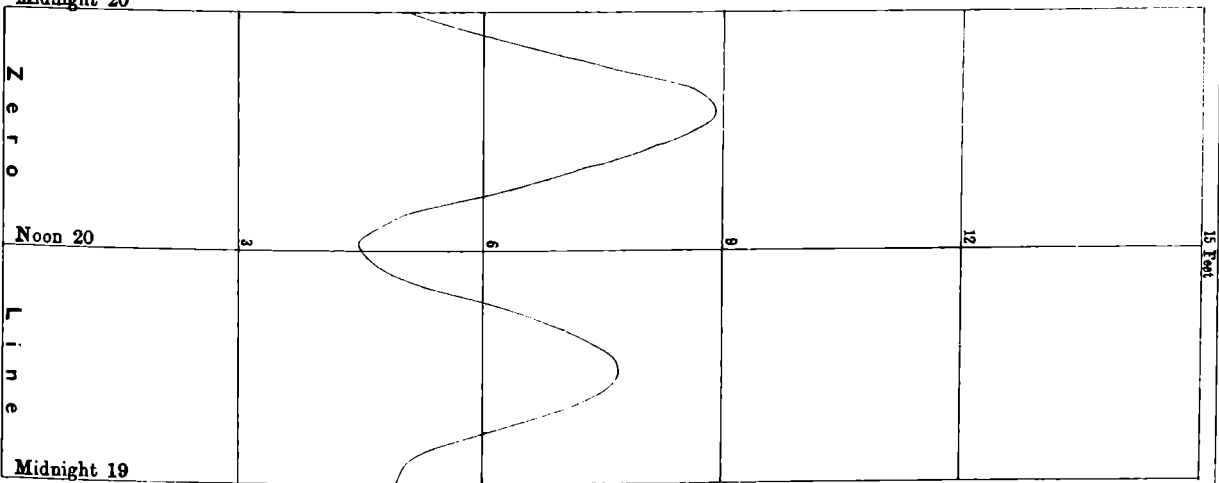
Midnight 13



New Moon — 10th January 1891

Neap Tide — 20th January 1891

Midnight 20



First Quarter — 17th January 1891

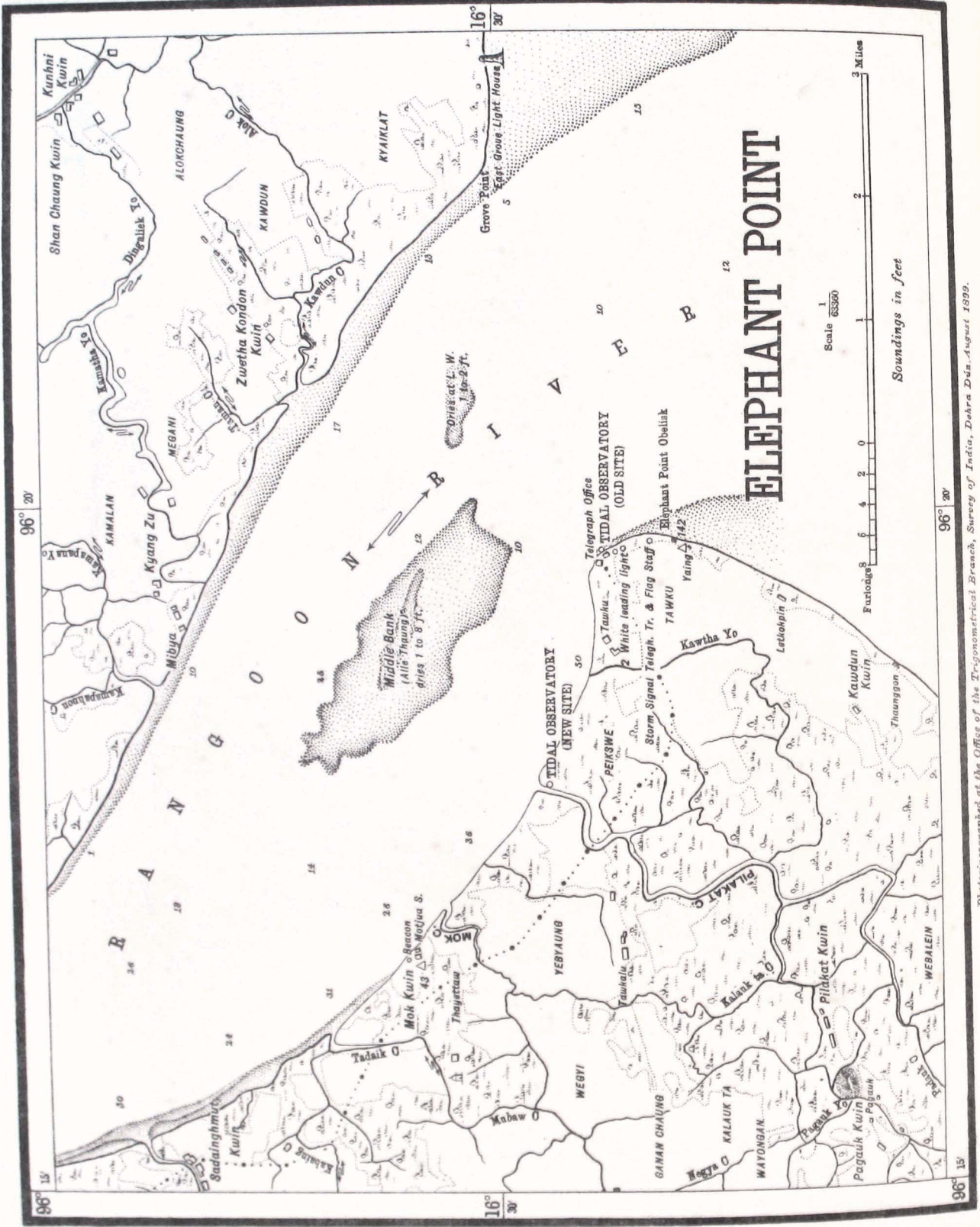
*Values of H's at Akyab.*

TIDE	H					TIDE
	1887-88	1888-89	1880-90	1890-91	1891-92	
	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0.042	0.042	0.048	0.049	0.050	S <sub>1</sub>
S <sub>2</sub>	1.118	1.126	1.126	1.146	1.142	S <sub>2</sub>
S <sub>4</sub>	0.006	0.007	0.011	0.007	0.005	S <sub>4</sub>
S <sub>6</sub>	.003	.002	.002	.003	.003	S <sub>6</sub>
S <sub>8</sub>	.003	.001	.002	.001	.002	S <sub>8</sub>
M <sub>1</sub>	.016	.027	.023	.003	.003	M <sub>1</sub>
M <sub>2</sub>	2.540	2.553	2.559	2.561	2.561	M <sub>2</sub>
M <sub>3</sub>	0.020	0.015	0.015	0.020	0.013	M <sub>3</sub>
M <sub>4</sub>	.006	.005	.004	.006	.015	M <sub>4</sub>
M <sub>6</sub>	.023	.023	.021	.023	.025	M <sub>6</sub>
M <sub>8</sub>	.006	.006	.006	.008	.010	M <sub>8</sub>
O	.183	.183	.186	.182	.182	O
K <sub>1</sub>	.443	.450	.442	.447	.448	K <sub>1</sub>
K <sub>2</sub>	.317	.316	.335	.328	.308	K <sub>2</sub>
P	.141	.142	.130	.137	.136	P
J	.021	.026	.038	.029	.009	J
Q	.002	.007	.011	.017	.012	Q
L	.103	.114	.077	.121	.119	L
N	.520	.506	.524	.533	.508	N
λ	...	...	...	...	...	λ
ν	.053	.070	.171	.197	.120	ν
μ	.017	.027	.028	.024	.019	μ
R	...	...	...	...	...	R
T	...	.020	.088	.109	.062	T
MS	.012	.015	.008	.019	.015	MS
2SM	.041	.030	.030	.031	.036	2SM
2N	.052	.078	.105	.091	.052	2N
M <sub>2</sub> N	.102	.095	.051	.041	.113	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	.016	.032	.044	.031	.013	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	.012	.010	.017	.011	.019	2M <sub>2</sub> K <sub>1</sub>
Mm	.026	.070	.027	.022	.081	Mm
Mf	.081	.079	.029	.090	.041	Mf
MSf	.046	.027	.036	.060	.063	MSf
Sa	.950	.980	.768	1.138	.883	Sa
Ssa	.252	.184	.234	0.112	.187	Ssa

## TIDAL OBSERVATIONS.

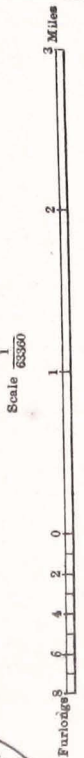
*Values of  $\kappa$ 's at Akyab.*

TIDE	$\kappa$					TIDE
	1887-88	1888-89	1889-90	1890-91	1891-92	
	o	o	o	o	o	
S <sub>1</sub>	84.17	91.23	71.79	75.32	74.69	S <sub>1</sub>
S <sub>2</sub>	310.28	308.79	307.03	307.38	306.90	S <sub>2</sub>
S <sub>4</sub>	208.77	210.43	201.00	179.13	178.78	S <sub>4</sub>
S <sub>6</sub>	107.10	55.31	123.69	53.97	103.50	S <sub>6</sub>
S <sub>8</sub>	113.43	108.44	46.85	85.60	59.93	S <sub>8</sub>
M <sub>1</sub>	342.06	22.87	18.16	324.04	297.20	M <sub>1</sub>
M <sub>2</sub>	280.12	277.58	277.58	277.86	277.33	M <sub>2</sub>
M <sub>3</sub>	11.31	13.44	27.67	21.52	39.46	M <sub>3</sub>
M <sub>4</sub>	289.81	282.87	228.46	274.66	295.04	M <sub>4</sub>
M <sub>6</sub>	132.41	114.72	116.11	123.84	126.87	M <sub>6</sub>
M <sub>8</sub>	142.66	130.36	162.09	156.20	146.08	M <sub>8</sub>
O	338.44	336.60	335.71	334.69	334.52	O
K <sub>1</sub>	344.23	343.45	343.28	343.30	342.97	K <sub>1</sub>
K <sub>2</sub>	304.41	309.49	308.83	304.48	305.31	K <sub>2</sub>
P	347.04	341.72	343.65	348.04	346.16	P
J	0.88	304.77	326.32	346.94	319.08	J
Q	168.98	33.94	303.24	268.24	279.28	Q
L	291.27	274.82	289.82	302.72	301.87	L
N	270.79	269.90	269.57	271.22	272.57	N
$\lambda$	...	...	...	...	...	$\lambda$
$\nu$	202.15	322.27	301.20	257.02	227.09	$\nu$
$\mu$	225.42	344.10	270.30	321.95	255.51	$\mu$
R	...	...	...	...	...	R
T	...	54.69	333.84	281.69	230.60	T
MS	313.20	252.77	260.79	237.13	307.32	MS
2SM	197.91	195.65	216.37	208.80	201.05	2SM
2N	250.28	224.80	264.53	253.72	275.85	2N
M <sub>2</sub> N	106.20	131.58	101.15	107.70	127.42	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	219.94	4.73	69.75	134.39	246.30	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	27.57	40.94	66.96	67.48	52.16	2M <sub>2</sub> K <sub>1</sub>
Mm	283.81	342.73	0.74	241.74	18.37	Mm
Mf	288.91	0.44	55.46	347.95	259.55	Mf
MSf	57.56	321.32	65.07	50.81	81.53	MSf
Sa	145.80	143.45	159.02	144.54	131.19	Sa
Ssa	128.72	190.58	140.94	165.70	172.43	Ssa



# ELEPHANT POINT

Soundings in feet



Photocopyographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun, August 1959.

## ELEPHANT POINT.

OPEN COAST STATION (AT OLD SITE).

*(Tidal Observatory, Lat. 16° 30' N., Long. 96° 20' E.)*

The minor tidal observatory at the open coast station of Elephant Point in Burma was just outside the mouth of the Rangoon river and was situated in front of the Telegraph Office, that existed there in 1880, and has since then been removed, on the right bank of the river and three quarters of a mile north-west of the Elephant Point Obelisk, in the position shown on the accompanying chart. It was a wooden cabin twelve feet square supported on the bank on piles driven well into the ground. The floor was about eleven feet above the ground and about three feet above the highest tides. The float-cylinder was of iron, twenty-two inches in diameter and thirty feet long. The top projected about two feet above the floor of the observatory and was five feet above the highest tides, and the bottom, which was closed, was sunk in the ground to a depth of two and a half feet below the lowest tides. The communication was through a two-inch iron pipe, one hundred and seventy feet long, bent into the form of a siphon and provided with a special contrivance for flushing it out. The short branch rose vertically from about eighteen inches above the bottom of the cylinder to about three feet above mean-sea-level: from this point, where there was a stop-cock, the pipe sloped gently downwards and ended in deep water.

The working scale of the tide-gauge was one-sixth.

Registrations were commenced on the 24th May, 1880, and continued without interruption for about two months, after which the communication pipe was continually getting clogged and damaged, and although a great deal of trouble was taken to have as few breaks as possible, there were sixty-six days' breaks in the observations up to the end of May, 1881, when, owing to the encroachment of the water, the observatory had to be dismantled. There are thus only one year's imperfect observations at this site.

Barometrical and anemometrical observations were carried on simultaneously with the tidal observations. The barometer was placed in the Telegraph Office and the anemometer on the roof of the observatory.

The bench-mark of reference used during the observations does not now exist, but in 1888, it was connected with the bench-mark cut on the lowest step (the fourth from the top) on the north-east side of the Elephant Point Obelisk, and subsequently inscribed  $\overset{\text{G. T. S.}}{\oplus}$ . This bench-mark, which still exists, has been adopted as the bench-mark of reference. It is 31.246 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = III<sup>h</sup> 30<sup>m</sup>.

The highest high water recorded was 27·8 feet above the zero of the gauge, and occurred in September, 1880.

The lowest low water recorded was 5·3 feet above the zero of the gauge, and occurred in January, 1881.

In 1880-81 the mean range of largest ordinary springs was found to be 18·6 feet.

The height of mean-sea-level above the zero of the gauge had the following value:—

1880-81      ...      ...      ...      16·554 feet.

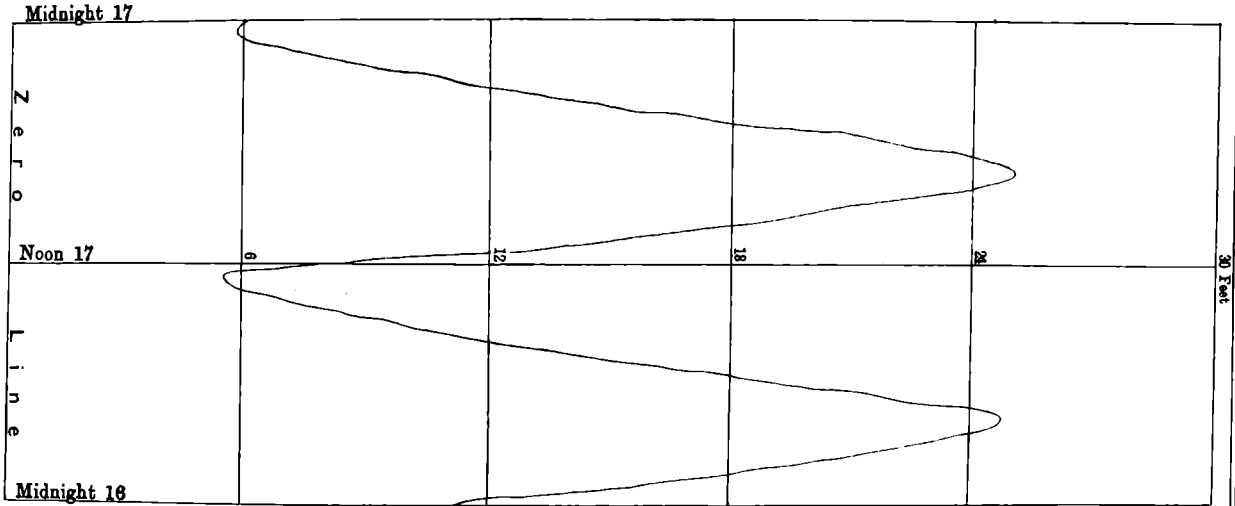
NOTE.—The zero of the gauge is 4·904 feet below the zero of the gauge at Elephant Point Riverain Station, and 7·182 feet below the zero of the gauge at Rangoon.

*Values of H's and κ's at Elephant Point.*

TIDE	H	κ	TIDE	H	κ
	1880-81	1880-81		1880-81	1880-81
	Feet	°		Feet	°
S <sub>1</sub>	0·113	79·37	N	1·545	77·89
S <sub>2</sub>	2·337	143·11	λ	0·660	323·14
S <sub>4</sub>	0·037	162·30	ν	·682	206·42
S <sub>6</sub>	·021	93·61	μ	·357	275·14
S <sub>8</sub>	·008	60·07	R	...	...
M <sub>1</sub>	·022	233·05	T	...	...
M <sub>2</sub>	5·876	100·99	MS	·135	64·45
M <sub>3</sub>	0·025	142·86	2SM	·042	86·57
M <sub>4</sub>	·079	41·90	2N	·520	67·11
M <sub>6</sub>	·206	342·71	M <sub>2</sub> N	·687	88·95
M <sub>8</sub>	·031	313·85	M <sub>2</sub> K <sub>1</sub>	·126	21·43
O	·356	277·14	2M <sub>2</sub> K <sub>1</sub>	·058	3·04
K <sub>1</sub>	·817	99·13	Mm	·145	5·85
K <sub>2</sub>	·405	73·24	Mf	·102	286·61
P	·199	302·52	MSf	·059	275·34
J	·113	137·78	Sa	·930	145·63
Q	·043	256·34	Ssa	·261	198·43
L	·413	278·75			

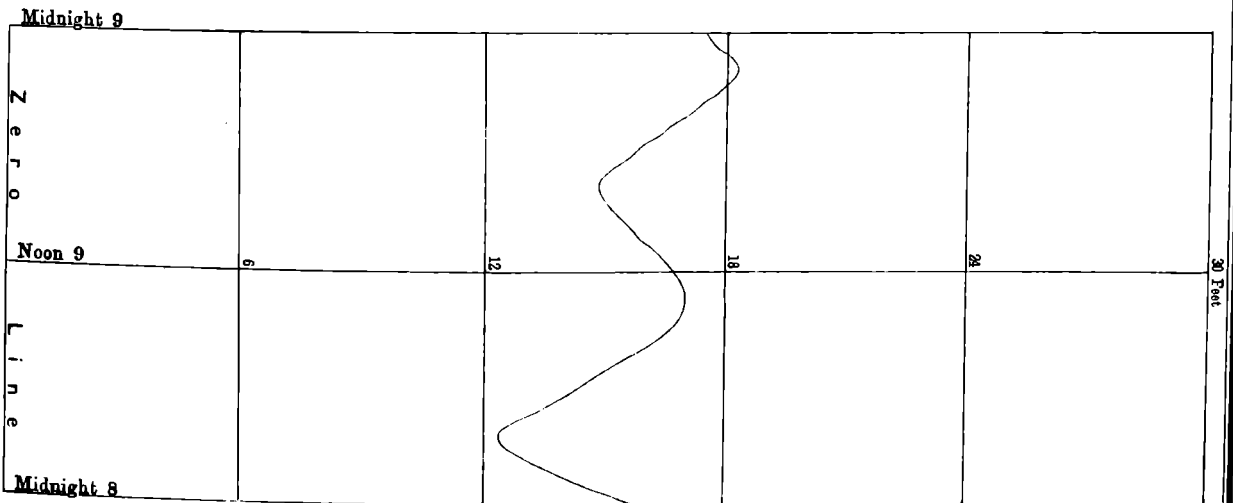
**TIDAL CURVES**  
at  
**ELEPHANT POINT (Open Coast Station)**

Spring Tide — 17th March 1881



Full Moon — 15th March 1881

Neap Tide — 9th March 1881



First Quarter — 7th March 1881

*Photocopyographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Ddn. September 1900.*

## ELEPHANT POINT.

ON THE RANGOON RIVER.

RIVERAIN STATION (AT NEW SITE).

*(Tidal Observatory, Lat. 16° 30' N., Long. 96° 18' E.)*

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The tidal observatory at the riverain station of Elephant Point in Burma, on the right bank of the Rangoon river a couple of miles above its mouth, was one of the minor observatories at which five years' observations are considered sufficient. It was situated on the right bank of Pilakat Creek, about three hundred and forty yards from its junction with the Rangoon river, two and a quarter miles north-west of the Elephant Point Obelisk, and one and a quarter miles north-west of the Telegraph Office, in the position shown on the accompanying chart. It was a wooden cabin twelve feet square, supported on piles driven into the bed of the creek, and connected with the bank by a wooden foot-bridge. Instead of the usual float-cylinder, a wooden casing two feet square in section and about twenty-five feet long was used. The top was level with the floor of the observatory and was about eighteen inches above the highest tides, and the bottom, which was fitted with a wooden grating, was about twelve inches below the lowest tides. The communication was through the wooden grating mentioned.

The working scale of the tide-gauge was one-sixth.

Registrations were commenced on the 1st January, 1884, and were continued without interruption to the 5th November of the same year, when the piles supporting the observatory sank and caused a suspension of the observations until the 8th of the following month, after which though there were some unimportant interruptions necessitated by the renewal of the float-casing, repairs to the cabin and piles, and accidents to the float-band and chain, the observations were practically continuous until the 18th June, 1888, when a heavy storm rendered the observatory unsafe, and it had to be dismantled. As four



and a half years' observations were completed, it was not thought necessary to reconstruct the observatory merely to extend them to the end of the customary five years.

Barometrical and anemometrical observations were carried on simultaneously with the tidal observations. The barometer was placed in the Telegraph Office and the anemometer on the neighbouring 'Look-out' house.

The bench-mark of reference is a stone engraved  $\begin{matrix} \text{G. T. S.} \\ \text{O} \\ \text{B. M.} \end{matrix}$  A, embedded in a block of masonry close to the site of the observatory on the right or eastern bank of Pilakat Creek. It is 24·000 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = III<sup>h</sup> 32<sup>m</sup>.

The highest high water recorded was 23·3 feet above the zero of the gauge, and occurred in May, 1884.

The lowest low water recorded was 0·4 foot above the zero of the gauge, and occurred in February, 1888.

In 1886 the mean range of largest ordinary springs was found to be 18·9 feet.

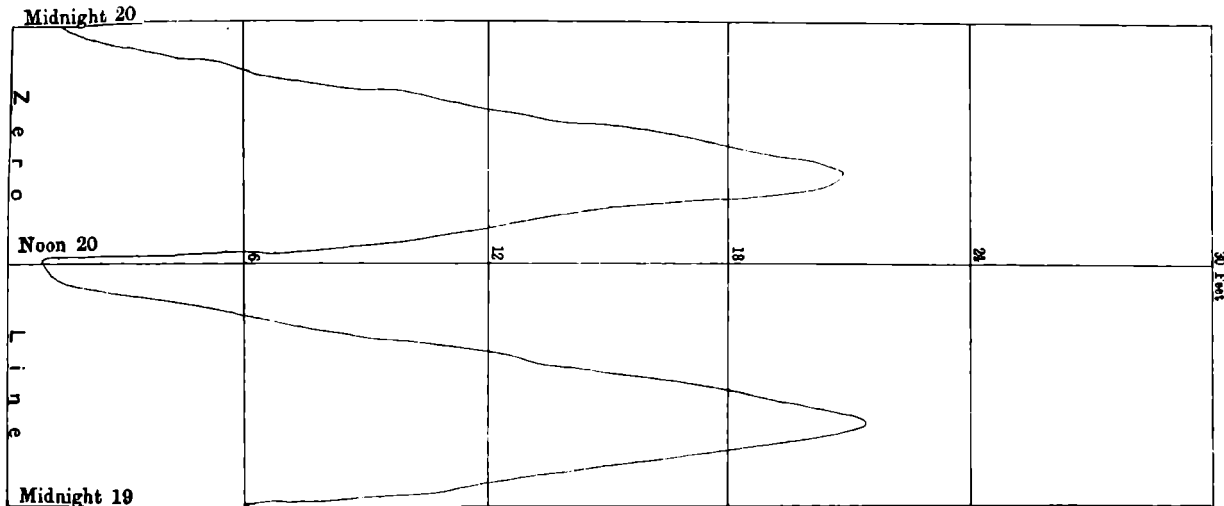
The height of mean-water-level above the zero of the gauge had the following values:—

1884	...	...	...	12·418 feet.
1885	...	...	...	11·745 „
1886	...	...	...	11·997 „
1887	...	...	...	11·982 „
1887-88	...	...	...	11·903 „

NOTE.—The zero of the gauge is 4·904 feet above the zero of the gauge at Elephant Point Open Coast Station, and is 2·278 feet below the zero of the gauge at Rangoon.

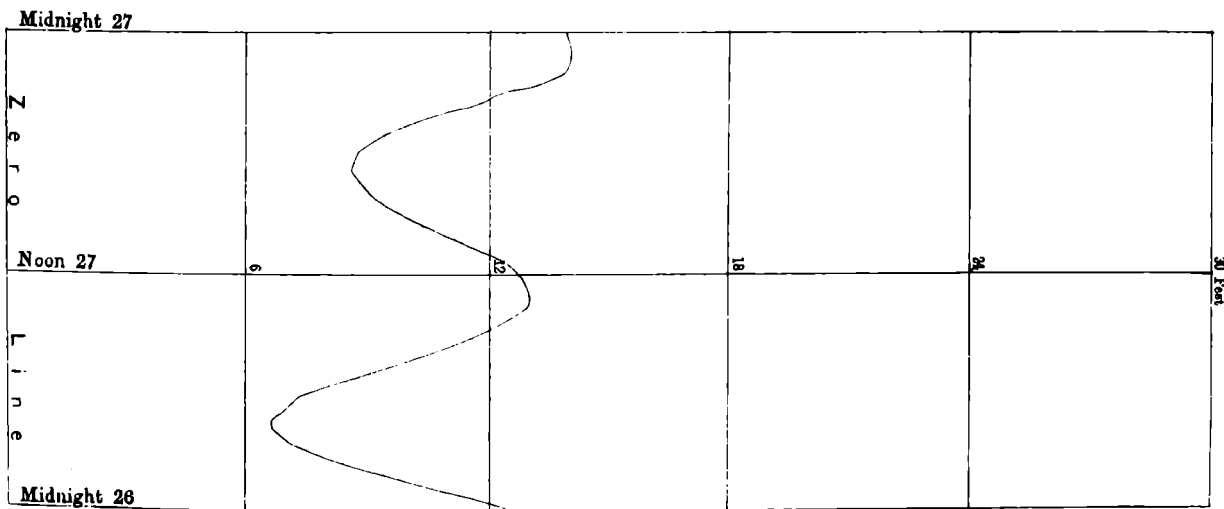
**TIDAL CURVES**  
at  
**ELEPHANT POINT (On the Rangoon River)**

Spring Tide — 20th February 1886



Full Moon — 18th February 1886

Neap Tide — 27th February 1886



Last Quarter — 25th February 1886

*Photoincographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun. April 1900.*

*Values of H's at Elephant Point.*

TIDE	H					TIDE
	1884	1885	1886	1887	1887-88	
	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0·140	0·082	0·082	0·075	0·101	S <sub>1</sub>
S <sub>2</sub>	2·384	2·397	2·365	2·366	2·395	S <sub>2</sub>
S <sub>4</sub>	0·092	0·088	0·078	0·081	0·081	S <sub>4</sub>
S <sub>6</sub>	·013	·007	·010	·011	·008	S <sub>6</sub>
S <sub>8</sub>	·009	·005	·002	·003	·001	S <sub>8</sub>
M <sub>1</sub>	·039	·009	·015	·039	·038	M <sub>1</sub>
M <sub>2</sub>	5·876	5·890	5·897	5·907	5·941	M <sub>2</sub>
M <sub>3</sub>	0·021	0·026	0·027	0·040	0·031	M <sub>3</sub>
M <sub>4</sub>	·270	·289	·275	·290	·280	M <sub>4</sub>
M <sub>6</sub>	·252	·241	·239	·242	·246	M <sub>6</sub>
M <sub>8</sub>	·107	·101	·104	·104	·104	M <sub>8</sub>
O	·344	·323	·323	·313	·312	O
K <sub>1</sub>	·723	·737	·751	·761	·760	K <sub>1</sub>
K <sub>2</sub>	·980	·716	·589	·710	·763	K <sub>2</sub>
P	·162	·189	·195	·223	·195	P
J	·029	·064	·011	·025	·023	J
Q	·043	·024	·004	·030	·029	Q
L	·440	·250	·412	·448	·423	L
N	·961	1·052	1·145	1·207	1·188	N
λ	·188	0·178	...	...	...	λ
ν	·132	·137	0·346	0·416	0·313	ν
μ	·346	·391	·342	·329	·382	μ
R	...	·077	...	...	...	R
T	...	·318	...	·142	...	T
MS	·310	·296	·292	·277	·281	MS
2SM	·163	·112	·131	·134	·138	2SM
2N	·281	·205	·102	·105	·197	2N
M <sub>2</sub> N	·235	·198	·126	·199	·196	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	·073	·055	·134	·151	·047	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	·069	·076	·069	·073	·032	2M <sub>2</sub> K <sub>1</sub>
Mm	·120	·120	·075	·056	·107	Mm
Mf	·190	·120	·148	·044	·037	Mf
MSf	·226	·245	·199	·221	·170	MSf
Sa	·812	·873	·918	·764	·845	Sa
Ssa	·134	·107	·141	·150	·115	Ssa

## TIDAL OBSERVATIONS.

*Values of  $\kappa$ 's at Elephant Point.*

TIDE	$\kappa$					TIDE
	1884	1885	1886	1887	1887-88	
	°	°	°	°	°	
S <sub>1</sub>	91°02	126°48	128°12	114°21	111°90	S <sub>1</sub>
S <sub>2</sub>	139°57	140°08	140°19	139°80	140°16	S <sub>2</sub>
S <sub>4</sub>	181°37	176°94	173°82	176°25	173°22	S <sub>4</sub>
S <sub>6</sub>	294°19	262°46	296°31	272°14	258°29	S <sub>6</sub>
S <sub>8</sub>	307°49	284°04	340°02	38°05	63°44	S <sub>8</sub>
M <sub>1</sub>	25°54	125°30	54°77	64°38	72°76	M <sub>1</sub>
M <sub>2</sub>	101°88	103°95	103°42	103°44	104°14	M <sub>2</sub>
M <sub>3</sub>	15°16	337°43	322°80	305°24	286°28	M <sub>3</sub>
M <sub>4</sub>	78°58	87°74	90°74	90°42	91°44	M <sub>4</sub>
M <sub>6</sub>	338°65	337°74	337°71	332°21	333°61	M <sub>6</sub>
M <sub>8</sub>	323°75	333°93	335°01	325°89	322°78	M <sub>8</sub>
O	5°59	8°36	6°88	4°84	5°79	O
K <sub>1</sub>	19°52	19°47	19°40	17°66	18°28	K <sub>1</sub>
K <sub>2</sub>	120°49	135°16	135°87	144°43	147°24	K <sub>2</sub>
P	17°86	31°59	35°58	30°86	32°83	P
J	77°32	102°82	106°70	61°00	89°33	J
Q	23°11	328°93	279°48	4°11	38°76	Q
L	116°82	131°54	138°95	125°85	120°21	L
N	90°24	85°62	86°28	87°73	90°70	N
$\lambda$	161°97	144°48	...	...	...	$\lambda$
$\nu$	67°51	122°10	122°77	94°95	66°62	$\nu$
$\mu$	273°33	293°47	288°44	302°38	302°13	$\mu$
R	...	104°07	...	...	...	R
T	...	92°67	...	184°87	...	T
MS	121°72	127°73	125°77	129°08	130°57	MS
2SM	42°16	34°57	35°28	39°19	40°39	2SM
2N	87°44	84°96	143°73	326°54	13°74	2N
M <sub>2</sub> N	33°75	44°75	36°31	79°77	136°10	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	66°26	344°26	3°22	36°12	46°99	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	350°60	353°03	353°55	357°12	349°82	2M <sub>2</sub> K <sub>1</sub>
Mm	348°88	6°96	359°60	347°45	350°89	Mm
Mf	9°87	24°28	12°62	107°55	20°33	Mf
MSf	56°23	52°78	27°22	37°25	30°36	MSf
Sa	117°21	141°07	152°24	141°20	148°88	Sa
Ssa	204°09	219°26	121°94	88°91	113°58	Ssa

96° 9'

96° 10'

96° 11'

# RANGOON

Scale  $\frac{1}{21670}$

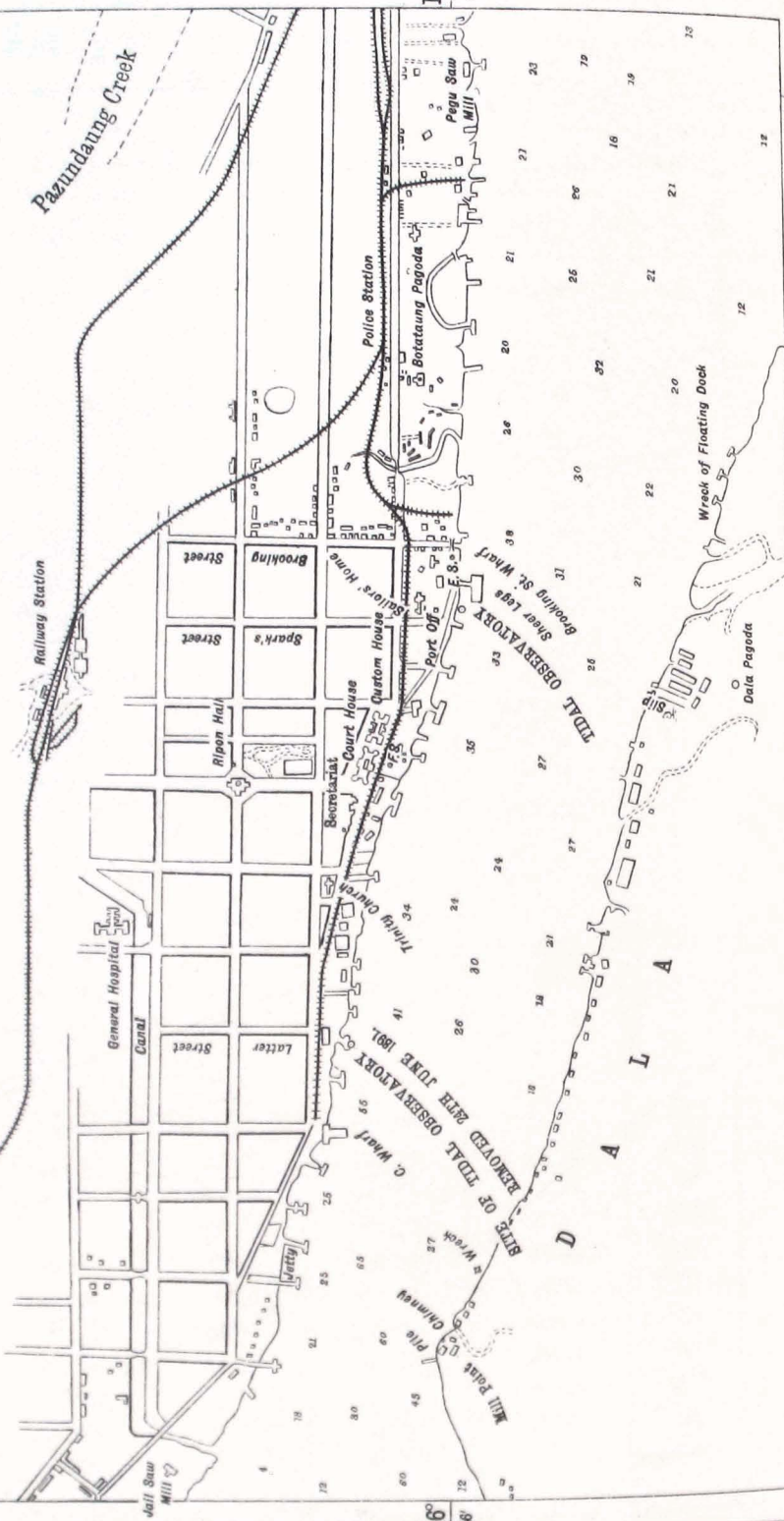


*Soundings in Feet*

*Railway to Proms 163 miles*

16° 47'

16° 47'



96° 9'

96° 10'

96° 11'

Photographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun, January 1908.

## R A N G O O N .

## ON THE RANGOON RIVER.

(*Tidal Observatory, Lat. 16° 46' N., Long. 96° 10' E.*)

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Rangoon is the one permanent tidal station in Burma. The tidal observations there have been taken in the town of Rangoon on the left bank of the Rangoon River at two sites at which the mean-water-level has been found by Spirit-levelling to be the same. The first observatory was erected in 1880 on the Latter Street Wharf, near the centre of its length and about three feet within its edge, in the position shown on the accompanying chart. It was a wooden structure fixed to the flooring of the wharf. In place of a float-cylinder a teak-wood casing two feet square in section and twenty-nine feet long was let down through the floor of the observatory and secured by iron braces, ties, and chains. The bottom of the casing was about six feet below the lowest tides and the top about two feet above the highest. The communication was through a wooden grating fastened across the bottom of the casing. In January, 1888, the casing was replaced exactly by an iron float-cylinder twenty-four inches in diameter and twenty-nine feet long, with an iron grating across the bottom of it through which communication was effected. The site of the observatory was objectionable, owing to the great traffic, and its liability to accidents caused by the shipping. On the 14th April, 1891, the work of extending the wharf necessitated the temporary shifting of the observatory a distance of fifteen yards, and this was effected in two days. On the 24th June of the same year, the observatory was dismantled and the instruments and float-cylinder were taken to Brooking Street Wharf, about a mile further down the river, and placed in the present observatory which is far less exposed to accidents than the old one, and is conveniently situated in the river opposite the Port Engineer's Office, in the position shown on the accompanying chart. It is a substantial wooden structure supported on four iron screw piles braced together by iron tie-rods, and is connected with the bank by a wooden bridge one hundred feet long and four and a half feet wide. The iron float-cylinder from Latter Street Wharf was placed in the same position as regards high and low tides as before, and with its top on a level with the floor of the observatory, and was secured by iron tie-rods to the piles.

The working scale of the tide-gauge in its present position is one-sixth, and at Latter Street Wharf it was the same.

Registrations were commenced at Latter Street Wharf on the 1st March, 1880, and were fairly continuous until the 24th June, 1886, when a steamer coming alongside damaged the observatory and its various instruments. Registrations were resumed on the 5th of the following month, and were tolerably uninterrupted until the 28th of the following December, when the float-casing was swept away by a strong ebb-tide, and a gap ensued until the 18th January, 1887. Between the 29th June and the 1st July, 1889, a two days' gap was caused by a steamer smashing in the roof of the observatory. Throughout the period of the registrations at Latter Street Wharf, there were also frequent unimportant breaks in the tidal curves due to stoppages of the driving clock caused by vibration, and by heavy shocks received by the wharf. At Brooking Street Wharf registrations were commenced on the 4th July, 1891, and have been practically continuous and most satisfactory up to the present.

Barometrical and anemometrical observations have been carried on simultaneously with the tidal observations. The barometer has been in the observatory both at Latter Street and Brooking Street wharves. The anemometer was on the top of a galvanised iron shed at the former wharf until the 24th February, 1893, when it was transferred to the roof of the observatory at Brooking Street Wharf.

The bench-mark of reference is Graham Smith's Bench-mark, a flat stone just outside the S.E. corner of the walled enclosure of the Sailors' Home, bearing the inscription "G. S. Datum 23·27  $\circ$  below this B. M." Graham Smith's Bench-mark is 23·270 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India =  $IV^h 36^m$ .

The highest high water recorded was 21·3 feet above the zero of the gauge, and occurred in September, 1882.

The lowest low water recorded was 0·2 foot *below* the zero of the gauge, and occurred in February, 1893.

In 1880-81 the mean range of largest ordinary springs was found to be 16·4 feet.

The height of mean-water-level above the zero of the gauge had the following values:—

1880-81	...	...	...	10·508 feet.
1881-82	...	...	...	10·414 „
1882-83	...	...	...	10·387 „
1883-84	...	...	...	10·359 „
1884-85	...	...	...	10·173 „
1885-86	...	...	...	10·077 „
1886-87	...	...	...	10·407 „
1887-88	...	...	...	10·194 „
1888-89	...	...	...	10·161 „
1889-90	...	...	...	10·299 „
1890-91	...	...	...	10·374 „
1891-92	...	...	...	9·991 „

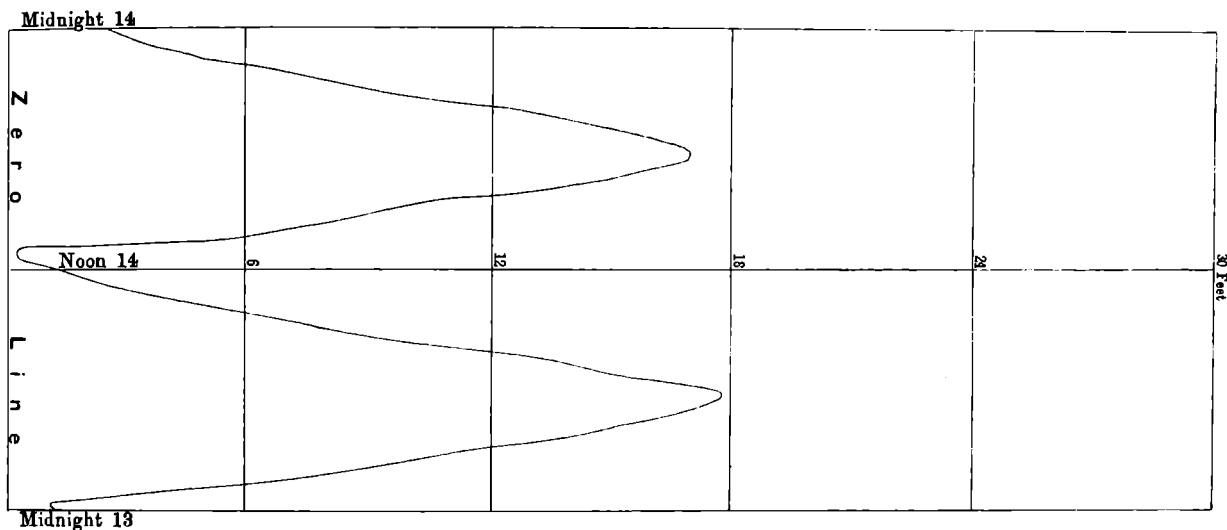
NOTE.—The zero of the gauge is 2·278 feet above the zero of the gauge at Elephant Point Riverain Station, and 7·182 feet above the zero of the gauge at Elephant Point Open Coast Station.

# TIDAL CURVES

at

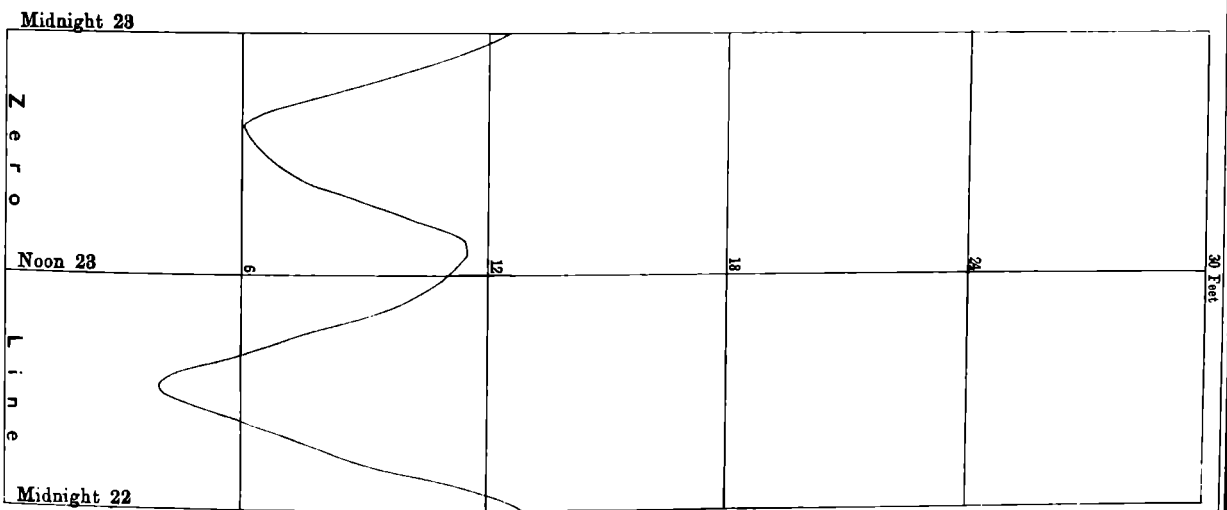
## RANGOON

Spring Tide — 14th February 1892



Full Moon — 12th February 1892

Neap Tide — 23rd February 1892



Last Quarter — 21st February 1892

*Photostereographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun, February 1900.*



*Values of H's at Rangoon.*

TIDE	H						TIDE
	1880-81	1881-82	1882-83	1883-84	1884-85	1885-86	
	Feet	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0·120	0·123	0·097	0·118	0·105	0·106	S <sub>1</sub>
S <sub>2</sub>	2·009	2·003	2·025	1·995	2·021	1·922	S <sub>2</sub>
S <sub>4</sub>	0·076	0·088	0·079	0·083	0·088	0·083	S <sub>4</sub>
S <sub>6</sub>	·011	·009	·011	·007	·011	·011	S <sub>6</sub>
S <sub>8</sub>	·006	·003	·005	·002	·007	·005	S <sub>8</sub>
M <sub>1</sub>	·049	·037	·013	·029	·031	·017	M <sub>1</sub>
M <sub>2</sub>	5·539	5·519	5·577	5·588	5·635	5·609	M <sub>2</sub>
M <sub>3</sub>	0·009	0·016	0·038	0·024	0·031	0·030	M <sub>3</sub>
M <sub>4</sub>	·388	·424	·418	·441	·419	·405	M <sub>4</sub>
M <sub>6</sub>	·236	·227	·235	·228	·226	·228	M <sub>6</sub>
M <sub>8</sub>	·074	·083	·087	·094	·089	·091	M <sub>8</sub>
O	·289	·294	·300	·297	·287	·283	O
K <sub>1</sub>	·674	·682	·653	·666	·668	·669	K <sub>1</sub>
K <sub>2</sub>	·535	·576	·598	·543	·578	·699	K <sub>2</sub>
P	·134	·148	·166	·134	·167	·139	P
J	·049	·023	·018	·034	·039	·033	J
Q	·028	·024	·028	·045	·036	·021	Q
L	·368	·327	·525	·426	·444	·283	L
N	1·045	·949	·977	1·006	1·050	1·074	N
λ	0·299	·290	·181	0·203	0·320	0·228	λ
ν	·479	·288	·184	·383	·508	·455	ν
μ	·497	·508	·536	·478	·506	·566	μ
R	...	·117	...	·096	...	·112	R
T	...	·290	...	·222	...	·289	T
MS	·349	·415	·394	·421	·386	·393	MS
2SM	·173	·155	·153	·175	·154	·187	2SM
2N	·261	·097	·079	·108	·233	·118	2N
M <sub>2</sub> N	·123	·198	·164	·154	·096	·275	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	·095	·169	·193	·118	·099	·166	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	·122	·117	·113	·124	·116	·121	2M <sub>2</sub> K <sub>1</sub>
Mm	·296	·230	·182	·279	·171	·206	Mm
Mf	·168	·223	·233	·228	·270	·171	Mf
MSf	·515	·559	·588	·541	·530	·542	MSf
Sa	1·600	1·415	1·444	1·405	1·201	1·184	Sa
Ssa	0·193	0·012	0·174	0·174	0·071	0·228	Ssa

## TIDAL OBSERVATIONS.

Values of H's at Rangoon—(Continued).

TIDE	H						TIDE
	1886-87	1887-88	1888-89	1889-90	1890-91	1891-92	
	Feet	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0.098	0.111	0.114	0.125	0.114	0.114	S <sub>1</sub>
S <sub>2</sub>	2.068	2.048	2.070	2.102	2.144	2.209	S <sub>2</sub>
S <sub>4</sub>	0.083	0.089	0.086	0.086	0.079	0.091	S <sub>4</sub>
S <sub>6</sub>	.012	.015	.008	.012	.012	.014	S <sub>6</sub>
S <sub>8</sub>	.005	.001	.002	.005	.003	.006	S <sub>8</sub>
M <sub>1</sub>	.022	.040	.035	.074	.032	.013	M <sub>1</sub>
M <sub>2</sub>	5.597	5.821	5.870	5.816	5.832	6.081	M <sub>2</sub>
M <sub>3</sub>	0.049	0.066	0.046	0.023	0.016	0.029	M <sub>3</sub>
M <sub>4</sub>	.441	.436	.462	.430	.455	.413	M <sub>4</sub>
M <sub>6</sub>	.189	.221	.196	.200	.197	.244	M <sub>6</sub>
M <sub>8</sub>	.081	.102	.090	.077	.076	.099	M <sub>8</sub>
O	.298	.291	.264	.289	.283	.278	O
K <sub>1</sub>	.655	.682	.676	.661	.674	.701	K <sub>1</sub>
K <sub>2</sub>	.769	.570	.630	.686	.611	.617	K <sub>2</sub>
P	.142	.178	.161	.165	.174	.163	P
J	.023	.022	.045	.037	.014	.009	J
Q	.031	.042	.010	.017	.024	.029	Q
L	.611	.551	.517	.368	.369	.657	L
N	1.044	1.073	1.135	1.077	1.067	1.061	N
λ	...	...	...	...	...	...	λ
ν	0.236	0.297	0.510	0.461	0.256	0.220	ν
μ	.594	.483	.526	.524	.585	.537	μ
R	...	...	...	...	...	...	R
T	.135	.245	.380	.254	.136	.324	T
MS	.421	.408	.400	.407	.429	.383	MS
2SM	.192	.189	.184	.174	.192	.204	2SM
2N	.055	.059	.257	.225	.225	.091	2N
M <sub>2</sub> N	.209	.163	.072	.244	.113	.172	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	.194	.130	.084	.173	.187	.099	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	.110	.121	.109	.131	.125	.135	2M <sub>2</sub> K <sub>1</sub>
Mm	.176	.164	.209	.191	.214	.202	Mm
Mf	.328	.147	.192	.170	.116	.145	Mf
MSf	.489	.533	.488	.492	.526	.454	MSf
Sa	1.344	1.189	1.258	1.130	1.535	1.131	Sa
Ssa	0.099	0.120	0.206	0.159	0.370	0.141	Ssa

*Values of  $\kappa$ 's at Rangoon.*

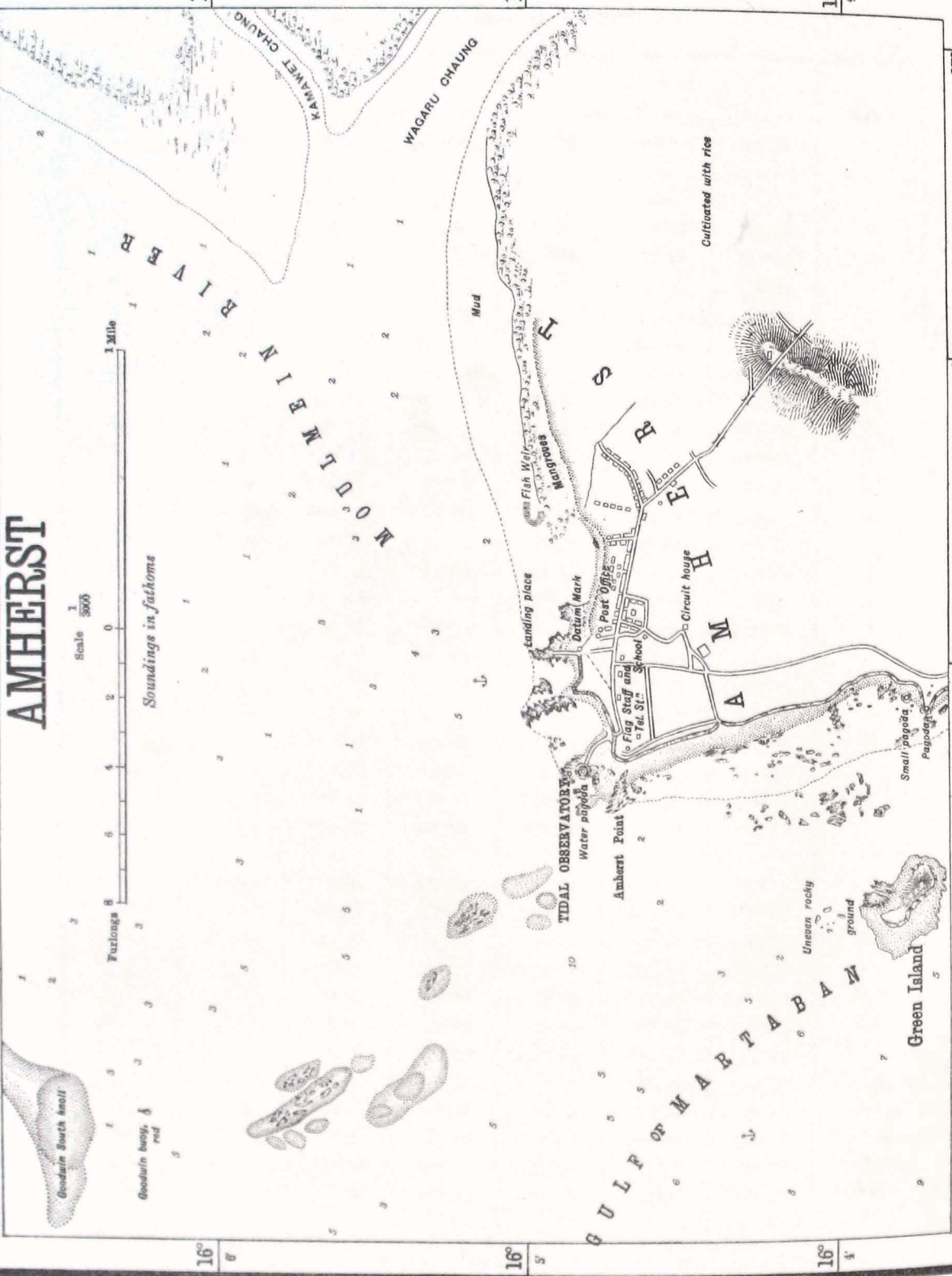
TIDE	$\kappa$						TIDE
	1880-81	1881-82	1882-83	1883-84	1884-85	1885-86	
	°	°	°	°	°	°	
S <sub>1</sub>	140° 83	128° 72	128° 78	129° 60	128° 52	139° 21	S <sub>1</sub>
S <sub>2</sub>	169° 39	170° 37	171° 20	170° 17	171° 70	171° 93	S <sub>2</sub>
S <sub>4</sub>	262° 16	256° 12	258° 12	257° 46	264° 56	261° 38	S <sub>4</sub>
S <sub>6</sub>	41° 80	39° 29	62° 97	58° 34	32° 12	47° 62	S <sub>6</sub>
S <sub>8</sub>	118° 77	117° 47	122° 47	115° 20	96° 71	133° 41	S <sub>8</sub>
M <sub>1</sub>	150° 55	235° 54	162° 58	125° 52	51° 58	143° 52	M <sub>1</sub>
M <sub>2</sub>	130° 48	131° 89	131° 09	130° 82	132° 10	133° 13	M <sub>2</sub>
M <sub>3</sub>	238° 20	154° 47	142° 09	151° 33	69° 69	14° 63	M <sub>3</sub>
M <sub>4</sub>	166° 69	171° 26	168° 30	168° 54	171° 13	175° 31	M <sub>4</sub>
M <sub>6</sub>	84° 86	88° 65	86° 69	87° 27	88° 72	91° 81	M <sub>6</sub>
M <sub>8</sub>	91° 95	103° 13	95° 68	95° 09	99° 20	108° 69	M <sub>8</sub>
O	29° 68	27° 37	28° 13	33° 14	31° 36	32° 04	O
K <sub>1</sub>	34° 53	34° 72	36° 18	37° 34	37° 90	37° 18	K <sub>1</sub>
K <sub>2</sub>	168° 02	173° 05	165° 46	162° 77	172° 65	189° 98	K <sub>2</sub>
P	61° 30	51° 68	53° 08	49° 33	54° 70	57° 14	P
J	69° 75	91° 49	297° 86	37° 70	89° 93	135° 30	J
Q	9° 29	28° 75	55° 57	67° 76	38° 76	39° 94	Q
L	152° 91	158° 13	159° 85	142° 50	150° 31	131° 20	L
N	117° 18	119° 56	115° 34	114° 89	116° 01	117° 51	N
$\lambda$	174° 15	183° 82	151° 97	142° 95	168° 65	197° 05	$\lambda$
$\nu$	94° 18	74° 94	130° 39	137° 99	109° 09	97° 55	$\nu$
$\mu$	288° 74	294° 73	285° 91	288° 18	287° 99	292° 09	$\mu$
R	...	66° 36	...	125° 23	...	45° 30	R
T	...	128° 26	...	182° 87	...	123° 75	T
MS	207° 15	212° 18	209° 99	212° 97	214° 23	217° 50	MS
2SM	46° 10	54° 28	60° 52	60° 69	49° 64	55° 72	2SM
2N	89° 56	147° 94	63° 38	82° 29	74° 36	125° 24	2N
M <sub>2</sub> N	35° 36	343° 28	56° 98	36° 21	31° 18	11° 28	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	48° 54	68° 13	86° 17	102° 46	63° 43	66° 43	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	55° 73	52° 49	53° 99	56° 06	60° 56	49° 04	2M <sub>2</sub> K <sub>1</sub>
Mm	20° 53	8° 83	38° 79	14° 88	4° 62	11° 74	Mm
Mf	35° 39	26° 84	39° 13	45° 75	28° 91	37° 21	Mf
MSf	45° 49	52° 16	49° 10	46° 21	51° 37	50° 89	MSf
Sa	144° 06	153° 23	152° 48	157° 04	145° 83	150° 43	Sa
Ssa	305° 64	314° 51	3° 33	0° 53	263° 27	298° 27	Ssa

## TIDAL OBSERVATIONS.

Values of  $\kappa$ 's at Rangoon—(Continued).

TIDE	$\kappa$						TIDE
	1886-87	1887-88	1888-89	1889-90	1890-91	1891-92	
	°	°	°	°	°	°	
S <sub>1</sub>	121.88	119.64	132.30	126.34	137.45	126.04	S <sub>1</sub>
S <sub>2</sub>	170.84	172.56	172.62	170.60	169.40	170.22	S <sub>2</sub>
S <sub>4</sub>	256.96	260.31	262.17	259.37	252.46	264.44	S <sub>4</sub>
S <sub>6</sub>	50.88	45.27	25.59	46.41	25.71	42.11	S <sub>6</sub>
S <sub>8</sub>	122.23	78.69	254.48	138.01	100.89	93.07	S <sub>8</sub>
M <sub>1</sub>	2.97	87.83	65.03	156.85	178.15	112.37	M <sub>1</sub>
M <sub>2</sub>	133.86	132.94	133.45	131.81	131.06	130.23	M <sub>2</sub>
M <sub>3</sub>	357.80	350.53	328.35	335.69	185.22	181.02	M <sub>3</sub>
M <sub>4</sub>	179.30	171.35	174.30	171.51	172.31	168.27	M <sub>4</sub>
M <sub>6</sub>	94.05	89.40	91.25	84.99	85.94	79.73	M <sub>6</sub>
M <sub>8</sub>	112.55	104.53	92.65	89.56	93.49	85.23	M <sub>8</sub>
O	26.79	30.62	31.39	26.75	26.88	21.72	O
K <sub>1</sub>	36.91	35.55	35.69	35.36	32.86	34.55	K <sub>1</sub>
K <sub>2</sub>	177.68	170.38	172.68	168.73	163.16	168.30	K <sub>2</sub>
P	72.28	51.88	55.94	56.31	54.39	59.00	P
J	132.47	73.28	78.62	82.92	359.48	344.21	J
Q	59.13	77.63	69.38	66.41	72.56	56.13	Q
L	138.85	146.32	145.64	131.28	161.75	161.19	L
N	102.23	116.39	116.94	120.15	118.71	116.51	N
$\lambda$	...	...	...	...	...	...	$\lambda$
$\nu$	254.30	147.48	120.70	98.24	79.59	149.01	$\nu$
$\mu$	286.52	292.07	291.94	292.54	291.94	285.85	$\mu$
R	...	...	...	...	...	...	R
T	120.15	170.63	150.23	122.74	172.90	176.35	T
MS	217.21	216.72	218.24	212.55	214.15	212.65	MS
2SM	62.90	59.37	53.11	51.56	53.90	47.95	2SM
2N	115.97	129.09	48.77	93.71	125.88	184.71	2N
M <sub>2</sub> N	80.69	50.09	15.88	26.29	38.56	69.02	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	90.38	106.00	59.49	64.09	87.29	108.95	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	60.57	53.28	64.67	53.79	54.47	51.83	2M <sub>2</sub> K <sub>1</sub>
Mm	3.22	3.77	10.67	22.94	348.34	23.70	Mm
Mf	27.57	50.79	13.14	23.52	18.51	22.09	Mf
MSf	45.99	48.50	43.20	44.08	47.32	47.29	MSf
Sa	153.96	142.91	143.83	157.36	143.07	134.28	Sa
Ssa	348.52	24.36	323.75	42.17	335.38	267.66	Ssa

# AMHERST



## AMHERST.

## ON THE MOULMEIN RIVER.

(*Tidal Observatory, Lat. 16° 5' N., Long. 97° 34' E.*)

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The tidal observatory at Amherst, at the mouth of the Moulmein River on the coast of Burma, was one of the minor observatories at which five years' observations are generally considered sufficient, and was situated about twenty feet north of the Water Pagoda in the position shown on the accompanying chart. It was a substantial wooden cabin built on posts let into the rock, with its flooring about four feet above the highest tides. The iron float-cylinder was twenty-two inches in diameter and about twenty-six feet long. It had to be sunk in a well excavated in the rock, at first only ten feet deep; but as this depth did not embrace the lowest tides, the well was sunk lower to a depth of fifteen feet in 1881. The cylinder was held firmly by cross-beams to the bracing of the posts. The communication was by a pipe bent so as to form a syphon about ninety feet long which terminated in a rose. An air-cock protected by a box and worked by a rod was provided at the upper bend of the syphon, and a groove was cut in the rock for the reception of the pipe.

The working scale of the tide-gauge was one-sixth.

Registrations were commenced on the 30th July, 1880. The great quantity of mud held in suspension by the water necessitated frequent flushing of the communication pipe. The deepening of the well caused a cessation of the observations which lasted from the 10th April to the 18th July, 1881, and in October, 1882, a gap of twenty-four days occurred while the communication pipe was being repaired. The observatory was on three or four occasions broken into by mischievous persons who tampered with the instruments, but who fortunately never caused serious interruption to the observations, which were fairly continuous until the dismantling of the observatory in August, 1886, when an extra year's observations, taken to compensate for the break of four months in 1880-81, were completed.

Barometrical and anemometrical observations were carried on simultaneously with the tidal observations. The barometer was set up in the Telegraph Office, and the anemometer was placed sixteen feet above the ground on a small wooden house fifty yards south of the Telegraph Office.

The bench-mark of reference is Bench-mark A, placed on the north-eastern post supporting the Water Pagoda. It is 26·883 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = 11<sup>h</sup> 21<sup>m</sup>.

The highest high water recorded was 26·0 feet above the zero of the gauge, and occurred in August, 1882.

The lowest low water recorded was 0·8 foot above the zero of the gauge, and occurred in February, 1886.

In 1881-82 the mean range of largest ordinary springs was found to be 19·2 feet.

The height of mean-sea-level above the zero of the gauge had the following values:—

1880-81	...	...	...	13·591 feet.
1881-82	...	...	...	13·974 „
1882-83	...	...	...	13·701 „
1883-84	...	...	...	13·757 „
1884-85	...	...	...	13·588 „
1885-86	...	...	...	13·311 „

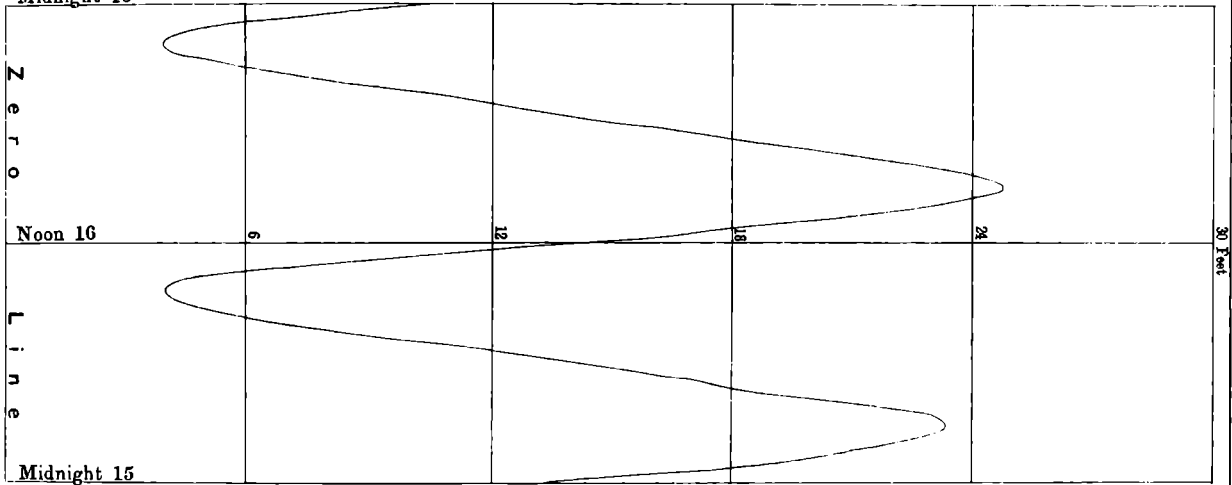
# TIDAL CURVES

at

## AMHERST

Spring Tide — 16th May 1885

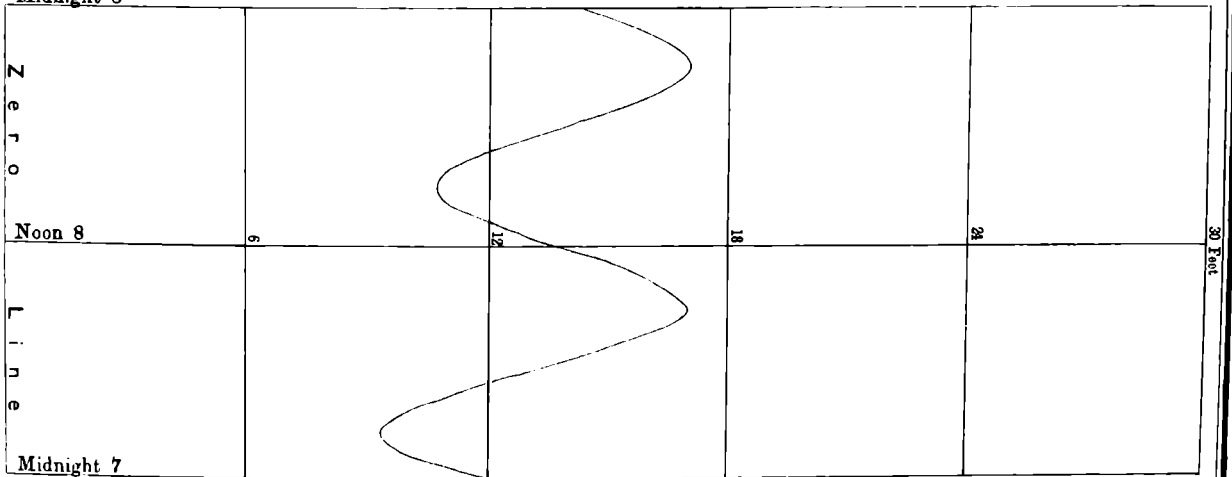
Midnight 16



New Moon — 14th May 1885

Neap Tide — 8th May 1885

Midnight 8



Last Quarter — 7th May 1885

*Photostereographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dún. February 1900.*



*Values of H's at Amherst.*

TIDE	H						TIDE
	1880-81	1881-82	1882-83	1883-84	1884-85	1885-86	
	Feet	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0.426	0.143	0.096	0.124	0.137	0.131	S <sub>1</sub>
S <sub>2</sub>	2.851	2.705	2.750	2.680	2.700	2.563	S <sub>2</sub>
S <sub>4</sub>	0.095	0.118	0.104	0.080	0.099	0.075	S <sub>4</sub>
S <sub>6</sub>	.022	.004	.009	.008	.002	.002	S <sub>6</sub>
S <sub>8</sub>	.009	.006	.009	.003	.002	.003	S <sub>8</sub>
M <sub>1</sub>	.041	.021	.035	.014	.038	.045	M <sub>1</sub>
M <sub>2</sub>	6.230	6.081	6.389	6.376	6.427	6.415	M <sub>2</sub>
M <sub>3</sub>	0.034	0.003	0.019	0.021	0.033	0.031	M <sub>3</sub>
M <sub>4</sub>	.273	.423	.355	.303	.315	.273	M <sub>4</sub>
M <sub>6</sub>	.070	.146	.139	.138	.142	.151	M <sub>6</sub>
M <sub>8</sub>	.006	.014	.021	.016	.021	.023	M <sub>8</sub>
O	.310	.319	.323	.339	.335	.310	O
K <sub>1</sub>	.668	.686	.744	.714	.702	.738	K <sub>1</sub>
K <sub>2</sub>	1.771	.858	.682	.883	.973	.752	K <sub>2</sub>
P	0.132	.193	.207	.207	.195	.212	P
J	.109	.083	.031	.022	.028	.045	J
Q	.064	.060	.039	.018	.020	.035	Q
L	.226	.303	.348	.362	.373	.314	L
N	1.374	1.248	1.343	1.230	1.194	1.312	N
λ	0.393	0.280	0.226	0.185	0.178	0.216	λ
ν	.426	.283	.566	.428	.232	.099	ν
μ	.443	.247	.220	.274	.202	.326	μ
R	...	.451	...	.033	...	.174	R
T	...	.841	...	.074	...	.352	T
MS	.285	.406	.350	.291	.300	.275	MS
2SM	.188	.150	.115	.176	.181	.176	2SM
2N	.325	.239	.258	.271	.204	.173	2N
M <sub>2</sub> N	.293	.320	.164	.271	.198	.035	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	.105	.135	.071	.011	.102	.122	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	.066	.054	.063	.039	.044	.037	2M <sub>2</sub> K <sub>1</sub>
Mm	...	.152	.038	.109	.049	.006	Mm
Mf	...	.062	.132	.083	.107	.017	Mf
MSf	...	.080	.029	.052	.067	.068	MSf
Sa	...	.638	.814	.739	.713	.886	Sa
Ssa	...	.188	.124	.161	.119	.154	Ssa

## TIDAL OBSERVATIONS.

*Values of  $\kappa$ 's at Amherst.*

TIDE	$\kappa$						TIDE
	1880-81	1881-82	1882-83	1883-84	1884-85	1885-86	
	°	°	°	°	°	°	
S <sub>1</sub>	178.00	148.53	97.13	120.19	132.64	121.86	S <sub>1</sub>
S <sub>2</sub>	108.69	101.22	104.70	100.39	95.11	102.09	S <sub>2</sub>
S <sub>4</sub>	146.81	102.23	116.81	108.12	101.27	107.59	S <sub>4</sub>
S <sub>6</sub>	221.61	221.06	118.99	327.53	164.48	341.57	S <sub>6</sub>
S <sub>8</sub>	209.25	348.16	269.33	301.83	266.99	244.36	S <sub>8</sub>
M <sub>1</sub>	191.71	273.03	300.37	88.34	92.93	28.99	M <sub>1</sub>
M <sub>2</sub>	69.94	67.60	68.46	66.06	65.09	67.26	M <sub>2</sub>
M <sub>3</sub>	287.00	224.23	273.03	274.63	237.32	259.81	M <sub>3</sub>
M <sub>4</sub>	60.32	51.34	41.49	37.02	35.73	32.03	M <sub>4</sub>
M <sub>6</sub>	256.69	248.25	250.72	254.39	250.34	248.96	M <sub>6</sub>
M <sub>8</sub>	282.25	243.79	220.09	218.83	222.19	239.89	M <sub>8</sub>
O	327.71	338.50	351.90	344.72	347.32	349.30	O
K <sub>1</sub>	3.47	6.29	6.27	2.90	1.12	3.88	K <sub>1</sub>
K <sub>2</sub>	91.39	81.38	96.78	100.63	96.40	111.49	K <sub>2</sub>
P	307.74	348.07	353.68	2.59	5.61	12.27	P
J	13.16	6.52	82.46	10.63	58.60	72.50	J
Q	324.60	320.88	321.97	10.61	7.37	347.19	Q
L	112.34	119.89	103.28	81.05	89.84	78.07	L
N	59.61	51.10	51.00	52.12	50.50	47.65	N
$\lambda$	112.83	65.29	177.83	91.65	132.83	183.97	$\lambda$
$\nu$	185.52	267.18	78.79	48.67	25.41	55.06	$\nu$
$\mu$	278.05	298.94	325.59	309.99	281.13	292.90	$\mu$
R	...	252.46	...	346.62	...	316.23	R
T	...	143.90	...	284.28	...	78.55	T
MS	89.98	79.93	75.70	72.76	65.55	64.14	MS
2SM	345.09	28.36	15.96	5.22	13.44	327.91	2SM
2N	14.86	40.12	355.07	23.10	72.32	61.11	2N
M <sub>2</sub> N	217.41	305.68	115.16	215.64	243.84	159.45	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	331.42	2.14	25.48	280.38	301.65	347.95	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	293.53	325.25	329.61	309.06	319.85	313.14	2M <sub>2</sub> K <sub>1</sub>
Mm	...	43.45	51.63	341.86	3.52	290.22	Mm
Mf	...	315.34	23.66	327.64	33.68	212.82	Mf
MSf	...	76.43	65.67	134.29	69.31	306.24	MSf
Sa	...	149.83	129.63	149.27	146.54	106.54	Sa
Ssa	...	138.72	331.92	107.36	180.74	153.91	Ssa

97° 33'

# MOULMEIN

Scale 1:2500

Chains 10 5 0 1 2 3 Furlongs

*Soundings in feet*



16° 27'

16° 27'

97° 33'

## MOULMEIN.

## ON THE MOULMEIN RIVER.

(*Tidal Observatory, Lat. 16° 29' N., Long. 97° 37' E.*)

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The tidal observatory at Moulmein in Burma was one of the minor observatories, at which five years' observations are generally considered sufficient. The town of Moulmein stands at the mouth of the river Salween on the left bank, and at the commencement of the channel known as the Moulmein River which separates the main land from a large island, named Bheologyun, lying off it to the west. A portion of the waters of the Salween escapes to sea to the west, through a shallow channel round the north of Bheologyun; the rest flows south, down the Moulmein River for about twenty-eight and a half miles, to Amherst, and there falls into the Gulf of Martaban. The observatory was situated on the T head of the main wharf opposite the Port Office in the position shown on the accompanying chart. It was a wooden cabin fixed on the flooring of the wharf. The floor of the observatory, on which the trestle of the tide-gauge at first rested, was about a foot and a half above the flooring of the wharf; but as the latter was found after a few months' trial to be the more rigid, the trestle was then made to rest upon it. In place of an iron float-cylinder, a stout teak-wood casing was employed; it was two feet square in section and twenty-six feet long, giving ample range for extreme tides, and was well secured to the flooring and supports of the wharf. The communication was through a number of holes in an iron plate which closed the bottom of the casing.

The working scale of the tide-gauge was one-fourth.

Registrations were commenced on the 18th April, 1880. Throughout the period of the observations there were frequent insignificant breaks in the curves due to the stoppage of the clock by vibrations caused by shocks given to the wharf. On the 7th September, 1884, the greater part of the stout teak-wood float-case was carried away, it was supposed by some heavy log coming down the stream. This caused a month's gap in the observations, but otherwise the record was practically continuous until the 24th April, 1886, when, after six years' observations, the observatory was dismantled. The configuration

of the land, described above, has a remarkable effect on the tides, and in consequence of their peculiarity it was thought well to take an extra year's observations. Throughout the period of the observations, it was found that at the wharf where they were taken, the water, although rising higher at spring tides than at neaps, falls lower at neaps than at springs. Strange to say, this remarkable peculiarity of the Moulmein tides does not appear to have been noticed until these observations brought it to light.

Barometrical and anemometrical observations were carried on simultaneously with the tidal observations. The barometer was placed in the Port Office and the anemometer on the top of the same building.

The bench-mark of reference is Bench-mark A, cut on a block of Portland cement let into the flooring of the Port Office. It is 24·295 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = III<sup>h</sup> 41<sup>m</sup>.

The highest high water recorded was 19·3 feet above the zero of the gauge, and occurred in August, 1883.

The lowest low water recorded was 1·1 feet above the zero of the gauge, and occurred in March, 1881.

In 1880-81 the mean range of largest ordinary springs was found to be 12·7 feet.

The height of mean-water-level above the zero of the gauge had the following values:—

1880-81	...	...	...	8·453 feet.
1881-82	...	...	...	8·659 „
1882-83	...	...	...	8·658 „
1883-84	...	...	...	8·737 „
1884-85	...	...	...	8·146 „
1885-86	...	...	...	8·388 „

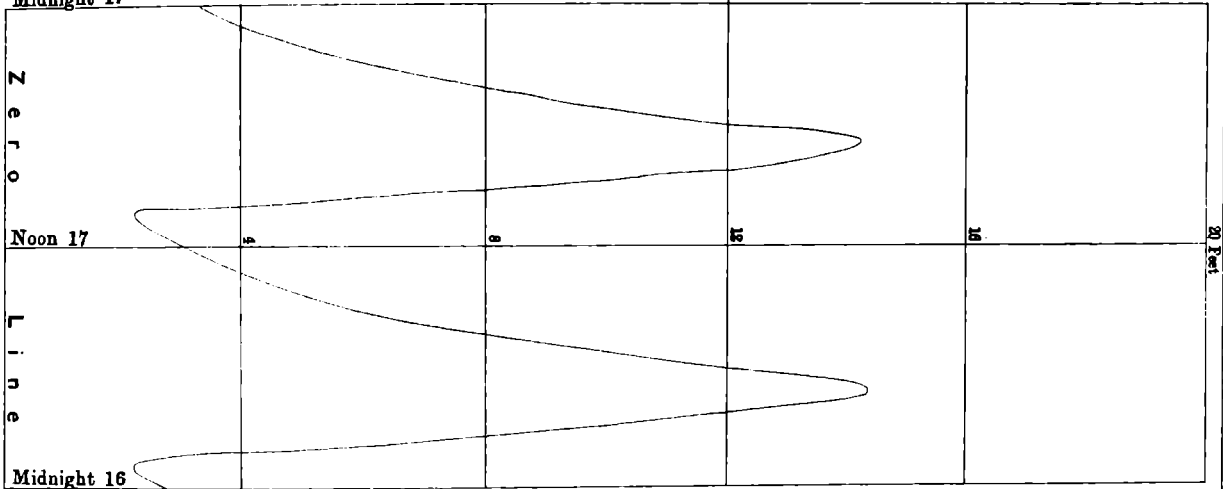
# TIDAL CURVES

at

## MOULMEIN

Spring Tide — 17th February 1885

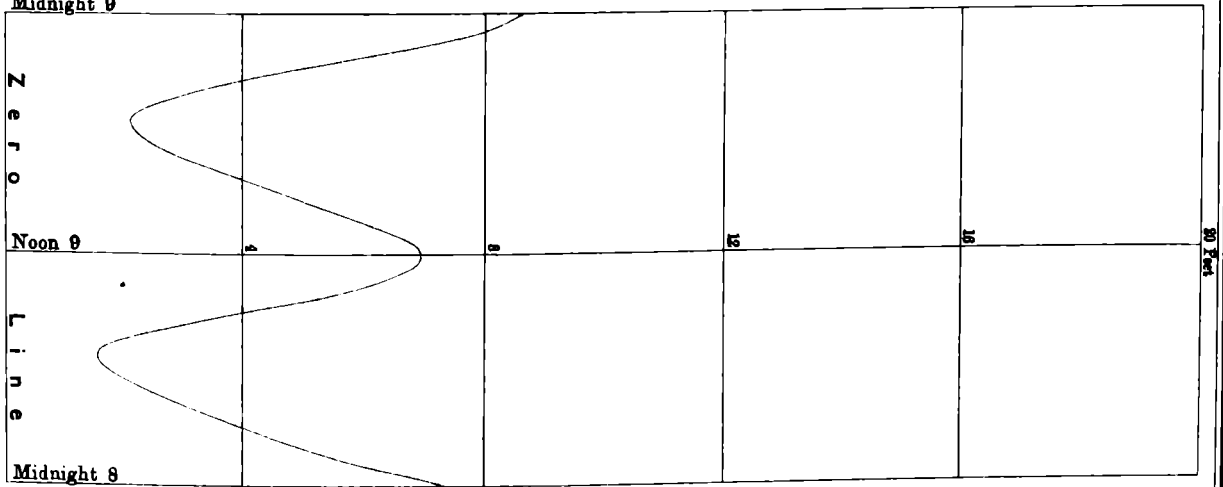
Midnight 17



New Moon — 16th February 1885

Neap Tide — 9th February 1885

Midnight 9



Last Quarter — 6th February 1885

*Photoincographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dún, September 1889.*

*Values of H's at Moulmein.*

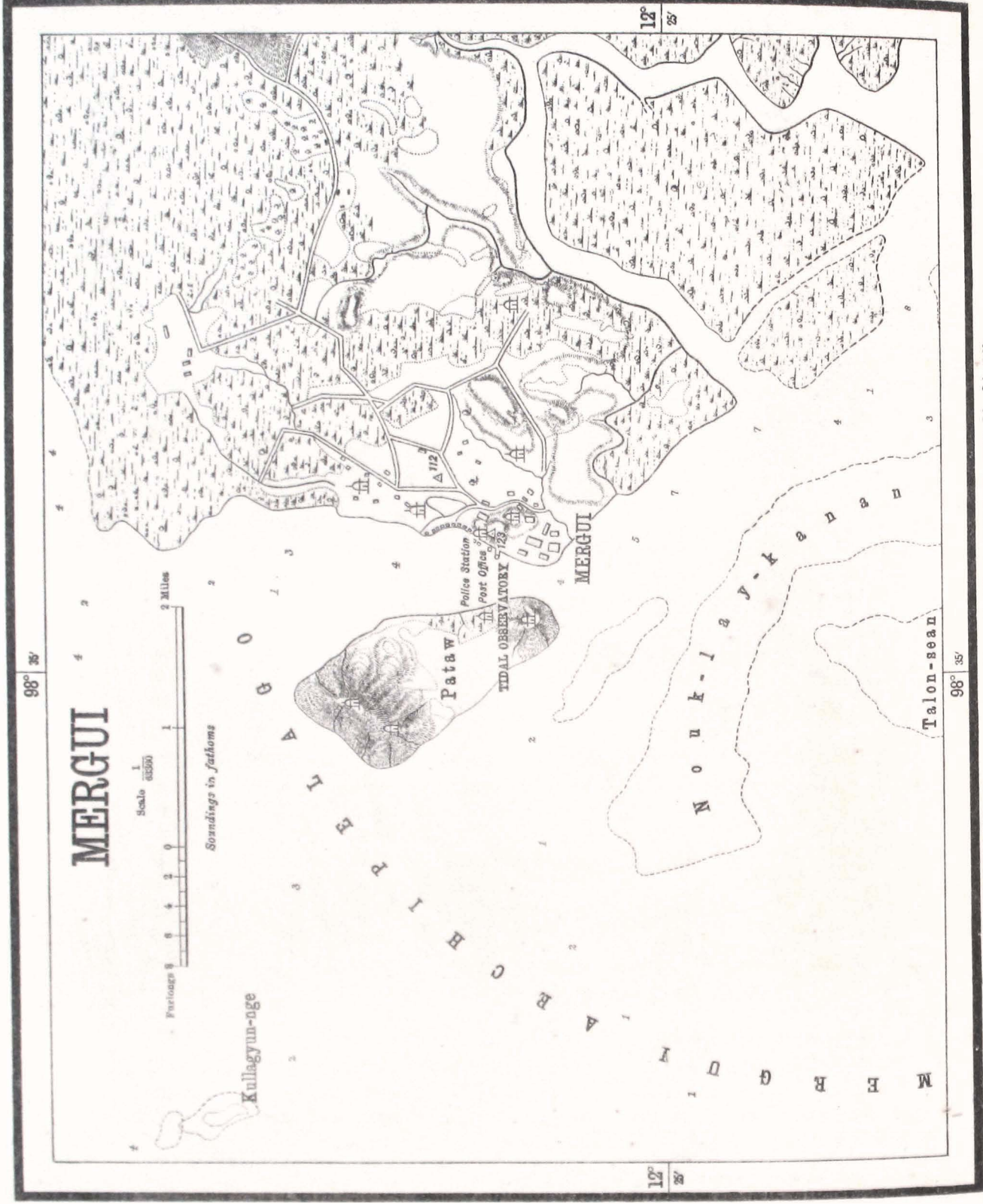
TIDE	H						TIDE
	1880-81	1881-82	1882-83	1883-84	1884-85	1885-86	
	Feet	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0.095	0.099	0.095	0.099	0.114	0.074	S <sub>1</sub>
S <sub>2</sub>	1.400	1.344	1.343	1.349	1.364	1.364	S <sub>2</sub>
S <sub>4</sub>	0.068	0.069	0.065	0.062	0.071	0.073	S <sub>4</sub>
S <sub>6</sub>	.006	.006	.004	.005	.007	.007	S <sub>6</sub>
S <sub>8</sub>	.002	.001	.002	.002	.002	.000	S <sub>8</sub>
M <sub>1</sub>	.034	.019	.002	.029	.019	.026	M <sub>1</sub>
M <sub>2</sub>	3.884	3.698	3.756	3.720	3.887	3.803	M <sub>2</sub>
M <sub>3</sub>	0.023	0.031	0.020	0.020	0.019	0.028	M <sub>3</sub>
M <sub>4</sub>	.926	.880	.897	.869	.906	.897	M <sub>4</sub>
M <sub>6</sub>	.105	.107	.095	.093	.077	.084	M <sub>6</sub>
M <sub>8</sub>	.034	.036	.044	.040	.043	.036	M <sub>8</sub>
O	.256	.252	.252	.275	.273	.245	O
K <sub>1</sub>	.452	.447	.414	.425	.456	.429	K <sub>1</sub>
K <sub>2</sub>	.409	.282	.316	.371	.275	.309	K <sub>2</sub>
P	.113	.144	.144	.119	.145	.116	P
J	.038	.018	.009	.022	.016	.015	J
Q	.043	.054	.039	.042	.056	.046	Q
L	.204	.390	.242	.320	.330	.297	L
N	.735	.672	.630	.654	.620	.713	N
λ	.161	.249	.118	.104	.183	.165	λ
ν	.314	.215	.169	.173	.435	.331	ν
μ	.308	.314	.316	.347	.320	.339	μ
R	...	.097	...	.133	...	.204	R
T	...	.200	...	.151	...	.264	T
MS	.741	.701	.693	.685	.714	.715	MS
2SM	.127	.137	.109	.123	.155	.118	2SM
2N	.117	.050	.067	.120	.082	.120	2N
M <sub>2</sub> N	.134	.100	.158	.126	.203	.086	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	.158	.154	.181	.197	.162	.133	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	.118	.122	.108	.111	.099	.111	2M <sub>2</sub> K <sub>1</sub>
Mm	.409	.441	.229	.407	.344	.369	Mm
Mf	.282	.379	.342	.377	.217	.371	Mf
MSf	1.088	1.097	1.146	1.091	1.050	1.063	MSf
Sa	2.460	2.389	2.453	2.519	2.032	2.128	Sa
Ssa	0.563	0.653	0.593	0.653	0.501	0.730	Ssa

## TIDAL OBSERVATIONS.

*Values of  $\kappa$ 's at Moulmein.*

TIDE	$\kappa$						TIDE
	1880-81	1881-82	1882-83	1883-84	1884-85	1885-86	
	°	°	°	°	°	°	
S <sub>1</sub>	145.51	154.60	147.70	150.78	143.69	154.09	S <sub>1</sub>
S <sub>2</sub>	148.32	145.31	150.01	149.26	150.10	151.41	S <sub>2</sub>
S <sub>4</sub>	230.06	225.18	231.29	227.80	222.67	228.02	S <sub>4</sub>
S <sub>6</sub>	177.99	187.13	185.32	261.42	246.37	222.05	S <sub>6</sub>
S <sub>8</sub>	164.48	251.57	218.29	319.76	120.96	198.44	S <sub>8</sub>
M <sub>1</sub>	128.32	101.26	183.42	144.52	121.57	71.05	M <sub>1</sub>
M <sub>2</sub>	111.89	112.36	114.99	113.24	113.66	115.25	M <sub>2</sub>
M <sub>3</sub>	273.89	214.84	138.86	164.54	117.12	42.02	M <sub>3</sub>
M <sub>4</sub>	168.90	169.67	174.13	171.08	172.78	176.01	M <sub>4</sub>
M <sub>6</sub>	200.19	198.05	200.97	197.15	208.07	218.47	M <sub>6</sub>
M <sub>8</sub>	125.48	140.90	134.00	135.54	119.40	123.01	M <sub>8</sub>
O	44.11	49.17	49.96	51.38	55.47	53.58	O
K <sub>1</sub>	39.41	40.42	41.51	41.17	43.96	42.60	K <sub>1</sub>
K <sub>2</sub>	150.55	152.49	161.82	163.73	158.46	158.63	K <sub>2</sub>
P	62.00	61.19	56.84	54.02	52.59	54.42	P
J	51.90	47.53	221.74	22.11	62.95	71.92	J
Q	52.63	54.80	52.88	57.16	79.36	57.33	Q
L	133.82	155.27	129.10	135.71	123.33	144.17	L
N	97.22	106.41	102.12	95.13	92.37	99.45	N
$\lambda$	152.00	182.20	162.23	106.79	153.28	170.32	$\lambda$
$\nu$	101.46	91.35	58.12	125.65	127.76	84.25	$\nu$
$\mu$	272.43	258.84	279.64	274.02	260.17	279.08	$\mu$
R	...	69.59	...	78.67	...	71.57	R
T	...	110.28	...	173.75	...	100.22	T
MS	209.92	208.62	214.47	213.33	215.44	217.96	MS
2SM	37.64	40.25	37.43	38.79	49.97	40.30	2SM
2N	110.84	75.87	30.18	79.06	144.78	73.56	2N
M <sub>2</sub> N	33.22	327.26	41.67	30.32	35.75	4.24	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	95.03	77.83	79.19	92.78	103.41	87.40	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	56.27	62.13	64.43	69.66	57.40	60.91	2M <sub>2</sub> K <sub>1</sub>
Mm	3.00	17.43	21.38	18.72	5.08	9.33	Mm
Mf	42.25	40.10	40.47	49.27	31.98	32.04	Mf
MSf	43.24	47.84	45.68	45.23	42.49	45.30	MSf
Sa	144.56	152.84	148.89	151.86	143.52	150.71	Sa
Ssa	282.51	283.89	295.13	298.36	267.69	287.80	Ssa





Photostereographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun, July 1939.

Reg. No. D. 112. S. I. D. - May 99 - 500

## M E R G U I .

(*Tidal Observatory, Lat. 12° 26' N., Long. 98° 36' E.*)

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The tidal observatory at Mergui in Burma, on the coast of Tenasserim, is one of the minor observatories at which five years' observations are considered sufficient, and is situated twenty-three feet beyond the T-head of the Mergui Pier, in the position shown on the accompanying chart. It is a wooden cabin, twelve feet square, resting on four piles driven sixteen feet into the bed of the anchorage. Its flooring is about three feet above the highest tides, and four feet above the level of the head of the pier with which it is connected by a wooden bridge having a movable piece at the end to isolate it. The float-cylinder is of wrought iron, twenty-four inches in internal diameter and thirty feet long. Its top is two feet three inches above the observatory floor, and the bottom, which is closed, rests on the bed of the anchorage, and being close in to shore is only two and a half feet below the lowest tides. The cylinder is supported by cross beams under its flanges, and its lowest length is guyed to the piles by four chains. The communication is through three sets of holes bored in the lowest length of the cylinder.

The working scale of the tide-gauge is one-sixth.

Registrations were commenced on the 24th March, 1889, and have been practically continuous up to the present. At first there were several insignificant breaks in the curve from stoppages of the driving clock due to cargo boats bumping against the piles; but the construction at the end of 1891 of an outer barrier, consisting of horizontal beams connecting four stout piles, has removed this source of interruption. In 1891, the clerk allowed a time error to accumulate until it reached seventeen minutes, thus involving correction of the diagrams.

Barometrical and anemometrical observations are carried on simultaneously with the tidal observations. The barometer was set up in the observatory, and the anemometer was placed on the roof of the Court House on the top of the hill.

The bench-mark of reference is a stone engraved  $\overset{\text{A}}{\underset{\text{B. M.}}{\text{O.}}}$  G. T. S. and embedded in a block of masonry about five feet from the S.E. corner of the Post Office. It is 26·488 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = X<sup>h</sup> 29<sup>m</sup>.

The highest high water recorded was 24·2 feet above the zero of the gauge, and occurred in September, 1891.

The lowest low water recorded was 1·4 feet above the zero of the gauge, and occurred in March, 1891.

In 1890 the mean range of largest ordinary springs was found to be 18·1 feet.

The height of mean-sea-level above the zero of the gauge had the following values :—

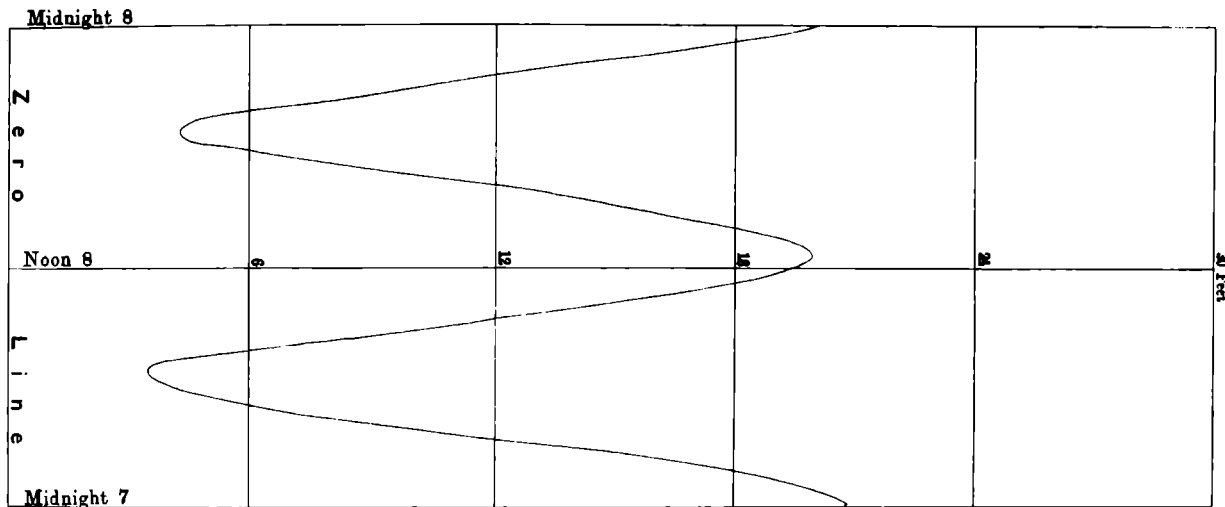
1889-90	...	...	...	13·084 feet.
1890-91	...	...	...	12·983 ,,
1891-92	...	...	...	12·902 ,,
1892-93	...	...	...	12·999 ,,

# TIDAL CURVES

at

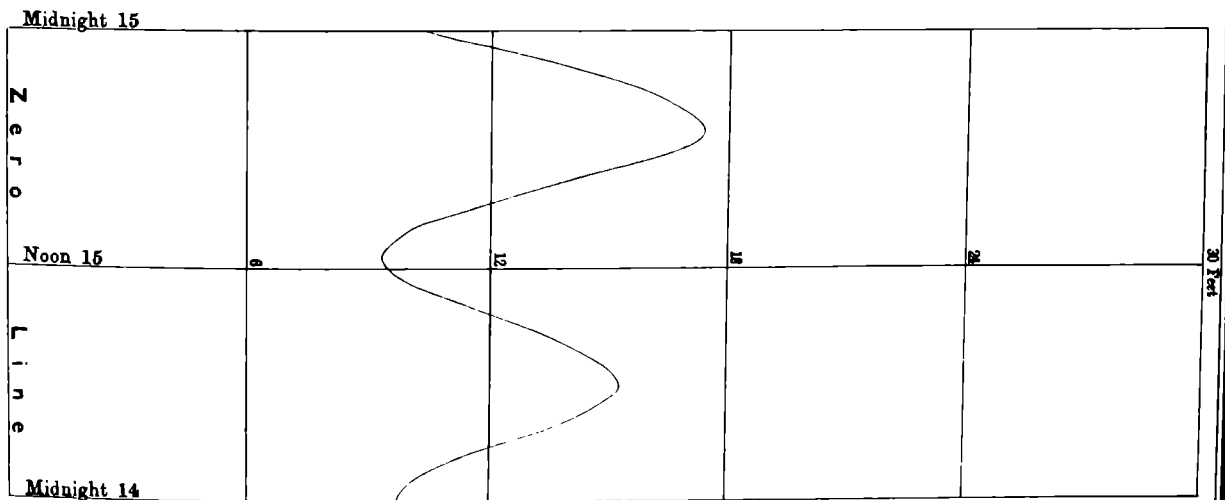
## MERGUI

Spring Tide — 8th February 1890



Full Moon — 5th February 1890

Neap Tide — 15th February 1890



Last Quarter — 12th February 1890

*Photoincographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun. September 1890.*

*Values of H's at Mergui.*

TIDE	H				TIDE
	1880-90	1890-91	1891-92	1892-93	
	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0.083	0.073	0.065	0.076	S <sub>1</sub>
S <sub>2</sub>	2.903	2.912	2.946	2.921	S <sub>2</sub>
S <sub>4</sub>	0.042	0.046	0.050	0.043	S <sub>4</sub>
S <sub>6</sub>	.022	.018	.017	.015	S <sub>6</sub>
S <sub>8</sub>	.003	.001	.002	.004	S <sub>8</sub>
M <sub>1</sub>	.028	.015	.004	.011	M <sub>1</sub>
M <sub>2</sub>	5.506	5.486	5.505	5.495	M <sub>2</sub>
M <sub>3</sub>	0.040	0.051	0.064	0.064	M <sub>3</sub>
M <sub>4</sub>	.120	.120	.122	.125	M <sub>4</sub>
M <sub>6</sub>	.070	.070	.081	.067	M <sub>6</sub>
M <sub>8</sub>	.023	.017	.013	.016	M <sub>8</sub>
O	.211	.208	.210	.208	O
K <sub>1</sub>	.524	.518	.521	.530	K <sub>1</sub>
K <sub>2</sub>	.792	.848	.880	.854	K <sub>2</sub>
P	.150	.160	.151	.151	P
J	.046	.024	.024	.031	J
Q	.031	.026	.025	.033	Q
L	.205	.240	.340	.210	L
N	1.068	1.068	1.019	.994	N
λ	...	...	...	...	λ
ν	0.327	0.262	0.051	.224	ν
μ	.437	.441	.425	.462	μ
R	...	...	...	...	R
T	...	.240	.163	.306	T
MS	.167	.144	.161	.155	MS
2SM	.176	.206	.157	.167	2SM
2N	.196	.162	.164	.120	2N
M <sub>2</sub> N	.117	.226	.141	.113	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	.078	.069	.037	.044	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	.011	.004	.006	.020	2M <sub>2</sub> K <sub>1</sub>
Mm	.034	.048	.084	.071	Mm
Mf	.043	.010	.043	.063	Mf
MSf	.055	.023	.043	.044	MSf
Sa	.492	.645	.528	.645	Sa
Ssa	.220	.108	.125	.200	Ssa

## TIDAL OBSERVATIONS.

*Values of  $\kappa$ 's at Mergui.*

TIDE	$\kappa$				TIDE
	1880-90	1890-91	1891-92	1892-93	
	°	°	°	°	
S <sub>1</sub>	73·14	72·64	69·92	60·09	S <sub>1</sub>
S <sub>2</sub>	349·79	350·45	347·90	349·18	S <sub>2</sub>
S <sub>4</sub>	226·84	243·10	236·47	222·36	S <sub>4</sub>
S <sub>6</sub>	108·68	94·55	92·39	123·58	S <sub>6</sub>
S <sub>8</sub>	236·31	114·78	148·00	226·08	S <sub>8</sub>
M <sub>1</sub>	20·78	131·89	15·86	337·68	M <sub>1</sub>
M <sub>2</sub>	309·78	311·57	308·38	310·35	M <sub>2</sub>
M <sub>3</sub>	132·11	137·98	134·91	131·60	M <sub>3</sub>
M <sub>4</sub>	128·91	136·56	132·11	131·32	M <sub>4</sub>
M <sub>6</sub>	217·41	232·72	236·69	234·78	M <sub>6</sub>
M <sub>8</sub>	59·67	67·26	45·69	58·90	M <sub>8</sub>
O	317·67	315·18	312·72	312·78	O
K <sub>1</sub>	333·48	334·53	334·70	333·76	K <sub>1</sub>
K <sub>2</sub>	344·76	347·58	343·82	341·10	K <sub>2</sub>
P	334·94	336·74	331·81	336·82	P
J	343·83	335·68	289·96	321·18	J
Q	274·33	265·00	281·53	300·24	Q
L	300·94	278·28	306·04	247·46	L
N	306·57	311·75	307·68	306·22	N
$\lambda$	...	...	...	...	$\lambda$
$\nu$	294·53	256·21	240·88	348·04	$\nu$
$\mu$	347·36	344·51	349·65	344·54	$\mu$
R	...	...	...	...	R
T	...	313·34	16·51	5·16	T
MS	173·88	181·77	178·00	165·33	MS
2SM	138·60	130·21	124·17	129·62	2SM
2N	265·41	306·09	312·73	329·11	2N
M <sub>2</sub> N	184·51	179·80	242·86	154·50	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	132·63	206·40	301·57	73·36	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	336·15	104·69	227·39	157·81	2M <sub>2</sub> K <sub>1</sub>
Mm	31·50	350·51	27·49	339·50	Mm
Mf	350·69	357·34	37·27	44·91	Mf
MSf	0·72	346·94	48·99	37·66	MSf
Sa	167·56	139·00	140·92	141·34	Sa
Ssa	109·29	99·00	158·25	75·71	Ssa

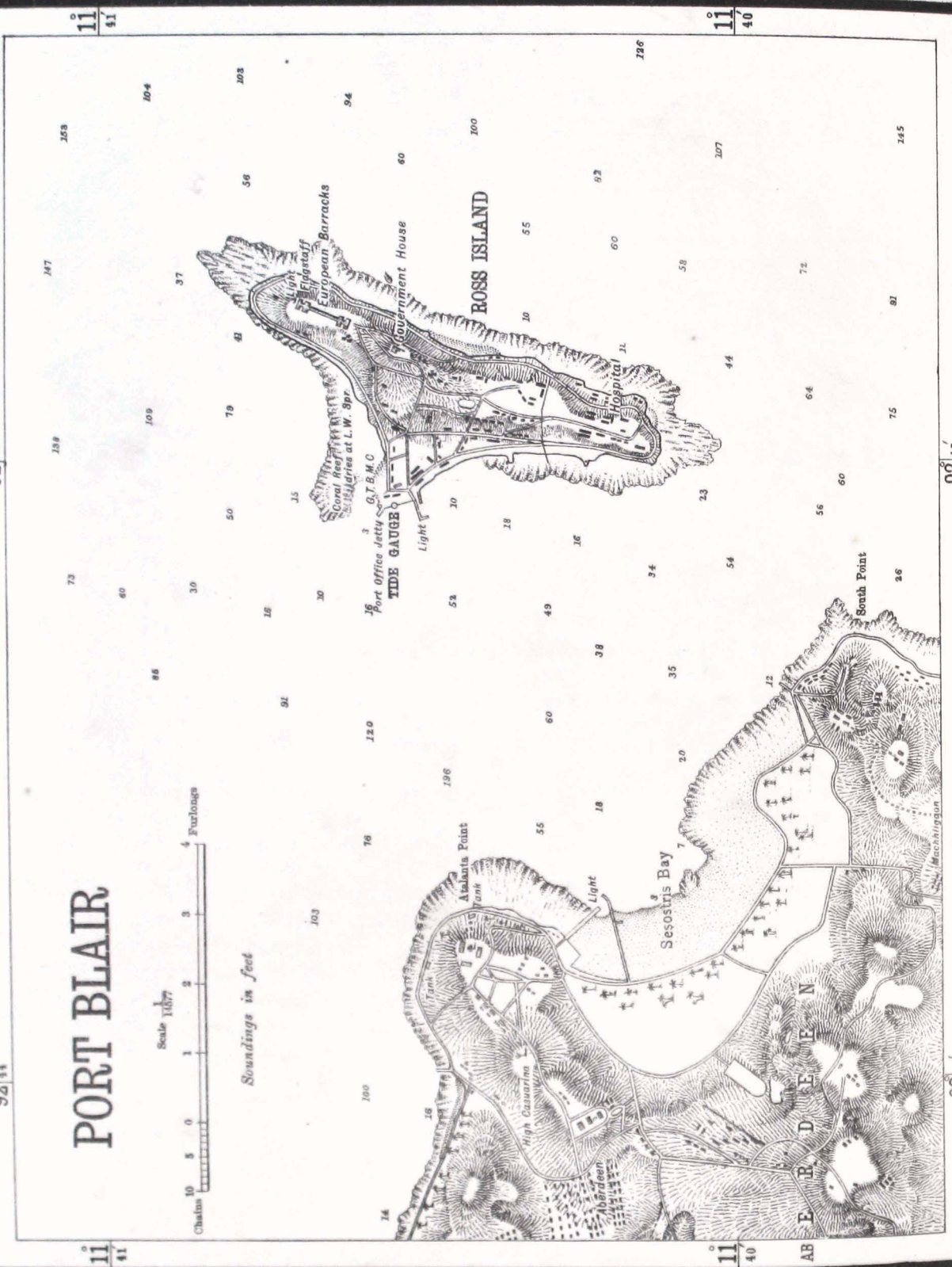
92 44

# PORT BLAIR

Scale 1:1877



Soundings in feet



92 44

Photocopy made at the Office of the Topographical Branch, Survey of India, Dabra, Dist July 1954.



## PORT BLAIR.

(*Tidal Observatory, Lat. 11° 41' N., Long. 92° 45' E.*)

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The tidal observatory at Port Blair, in the Andaman Islands, is one of the permanent observatories, and is situated two hundred feet north of the pier, on the sea wall adjoining the Port Officer's house on the west side of Ross Island, in the position shown on the accompanying chart. The present observatory was erected in January, 1892, on the same site as had been occupied by the original observatory from 1880 till the 1st November, 1891, when it was destroyed together with all the instruments, &c., by a most violent cyclone which caused serious damage and loss of life at Port Blair. The original observatory was a substantial wooden structure resting partly on the sea wall and partly on piles. The float-cylinder was twenty-two inches in internal diameter and sixteen and a half feet long: its lower end was sunk two and a half feet into the bed of the sea, giving nearly four feet of water in the cylinder at extreme low tides; and its mouth was about three and a half feet above highest tides. The communication was at first by a two and three quarter inch pipe, sixty feet long, leading from the bottom of the cylinder into deep water; but this arrangement was found superfluous, and communication by small holes near the bottom of the cylinder was substituted for it in December, 1884. In 1889 a masonry wall was built round the cylinder so as to enclose it in a well and protect it the better, and communication with the sea was obtained by means of small zinc tubes passed through the wall.

The working scale of the tide-gauge was one-half.

Registrations commenced in April, 1880, and were practically continuous until the 10th September, 1884, when a gap occurred until the 1st November following, while the cylinder was being repaired. At long intervals the tidal curves were impaired by short breaks due to renewals of and repairs to the cylinder, and by occasional retardation caused by obstruction of the communication; but the record was practically continuous and satisfactory till the cyclone destroyed the observatory. The new observatory was erected, and observations were resumed, by the 30th January, 1892. It is very similar to the old observatory, and the tide-gauge has the same working scale, namely one-half. The float-cylinder is thirty-six inches in internal diameter and fourteen feet long: its upper flange rests on the floor of the observatory and its bottom is supported about two feet below the lowest tides on a



flat circular stone thirty-eight inches in diameter. The communication is by three holes, each half an inch in diameter, nine inches above the bottom of the cylinder. The water immediately under the observatory, enclosed by the supporting piles and the sea wall, has been strongly planked in (about an inch of water way being left between the planks), thus protecting the cylinder from the roughness of the external water. The registrations have been highly satisfactory up to the present. The disturbances of the surface of the ocean, caused by an earthquake whose centre lay between Port Blair and Car Nicobar, were recorded at this station by the self-registering tide-gauge on the 31st December, 1881, and those caused by the Krakatoa volcanic eruptions were similarly recorded on the 27th August, 1883.

Barometrical and anemometrical observations have been carried on simultaneously with the tidal observations. The barometer is placed in the observatory and the anemometer on the top of the European Barracks on the ridge at the north-eastern extremity of Ross Island. They were similarly situated before the cyclone of 1891.

The bench-mark of reference is the Bench-mark A situated in the verandah of the Port Officer's house. It is 11·24 feet above the zero of the gauge.

The establishment of the Port, calculated according to the method employed by the Marine Survey of India = IX<sup>h</sup> 36<sup>m</sup>.

The highest high water recorded was 9·2 feet above the zero of the gauge, and occurred in December, 1892, (the record during the cyclone of the 1st November, 1891, perished with the observatory).

The lowest low water recorded was 0·4 foot above the zero of the gauge, and occurred in March, 1888.

In 1880-81 the mean range of largest ordinary springs was found to be 6·6 feet.

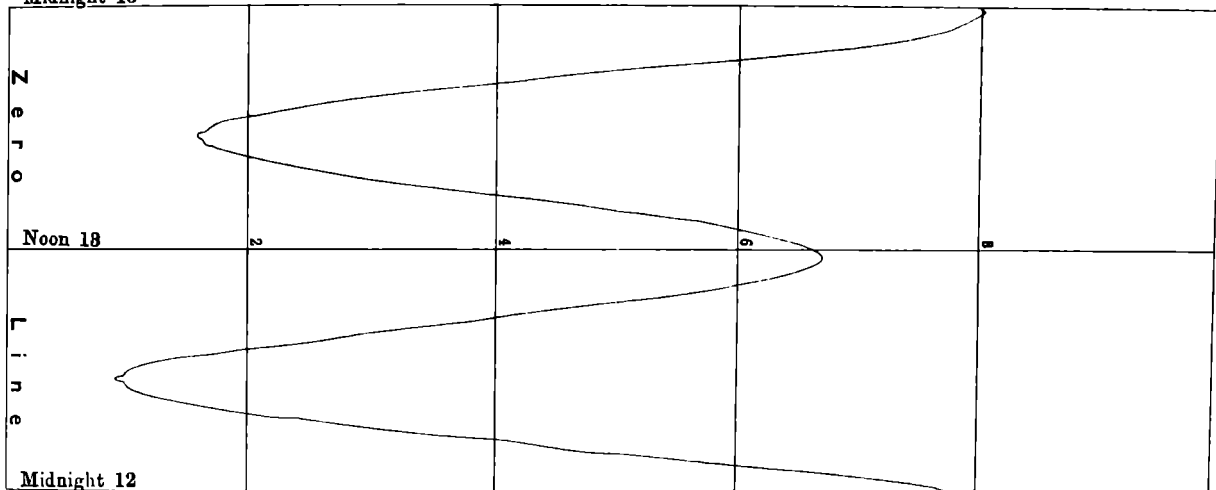
The height of mean-sea-level above the zero of the gauge had the following values :—

1880-81	...	...	...	4·792 feet.
1881-82	...	...	...	4·718 „
1882-83	...	...	...	4·710 „
1883-84	...	...	...	4·726 „
1884-85	...	...	...	4·689 „
1885-86	...	...	...	4·612 „
1886-87	...	...	...	4·506 „
1887-88	...	...	...	4·709 „
1888-89	...	...	...	4·625 „
1889-90	...	...	...	4·586 „
{ 1890-91 (ending 24th April, 1891)	...	...	...	4·605 „
{ 1890-91 (ending 29th October, 1891)	...	...	...	4·606 „
1892-93	...	...	...	4·811 „

TIDAL CURVES  
at  
PORT BLAIR

Spring Tide — 13th January 1891

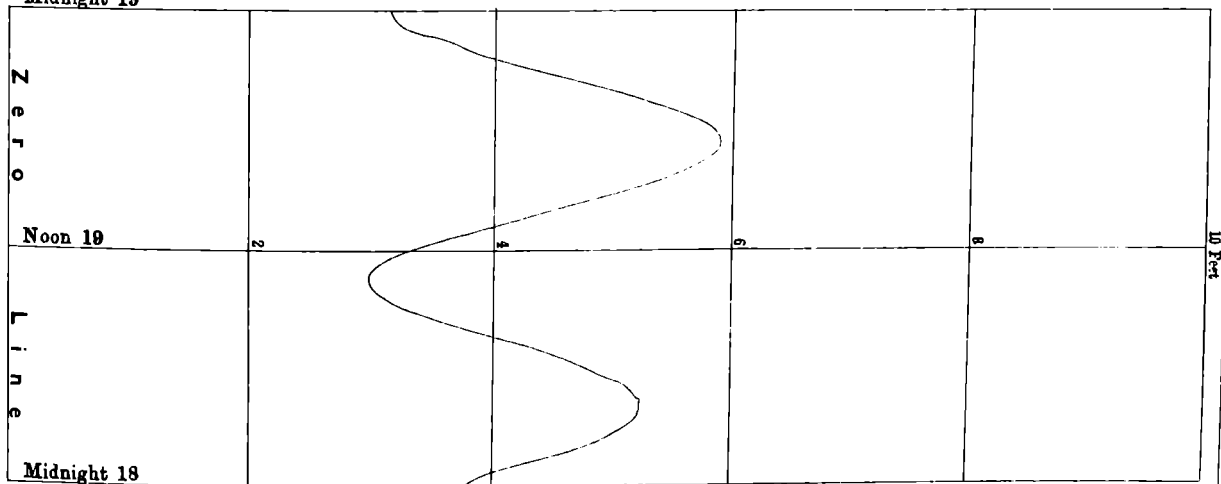
Midnight 13



New Moon — 10th January 1891

Neap Tide — 19th January 1891

Midnight 19



First Quarter — 17th January 1891

Photostereographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dun, September 1899.

*Values of H's at Port Blair.*

TIDE	H						TIDE
	1880-81	1881-82	1882-83	1883-84	1884-85	1885-86	
	Feet	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0.028	0.018	0.016	0.015	0.051	0.006	S <sub>1</sub>
S <sub>2</sub>	.966	.978	.959	.975	.963	.933	S <sub>2</sub>
S <sub>4</sub>	.003	.001	.004	.004	.004	.004	S <sub>4</sub>
S <sub>6</sub>	.002	.002	.002	.003	.001	.002	S <sub>6</sub>
S <sub>8</sub>	.002	.002	.001	.001	.000	.002	S <sub>8</sub>
M <sub>1</sub>	.016	.007	.008	.004	.028	.032	M <sub>1</sub>
M <sub>2</sub>	2.042	2.014	2.010	2.013	2.029	1.951	M <sub>2</sub>
M <sub>3</sub>	0.004	0.011	0.007	0.009	0.005	0.004	M <sub>3</sub>
M <sub>4</sub>	.003	.011	.011	.013	.017	.016	M <sub>4</sub>
M <sub>6</sub>	.004	.002	.000	.007	.002	.008	M <sub>6</sub>
M <sub>8</sub>	.003	.002	.002	.001	.001	.002	M <sub>8</sub>
O	.153	.162	.166	.159	.155	.162	O
K <sub>1</sub>	.403	.397	.391	.393	.417	.397	K <sub>1</sub>
K <sub>2</sub>	.286	.296	.264	.277	.179	.233	K <sub>2</sub>
P	.130	.137	.134	.132	.176	.129	P
J	.038	.030	.014	.021	.033	.032	J
Q	.023	.027	.023	.011	.022	.020	Q
L	.059	.098	.046	.093	.049	.087	L
N	.413	.392	.391	.382	.423	.391	N
λ	.035	.046	.047	.036	.087	...	λ
ν	.148	.137	.079	.020	.179	.139	ν
μ	.094	.089	.074	.074	.121	.071	μ
R	...	.020	...	.022	...	...	R
T	...	.099	...	.037	...	.112	T
MS	.004	.016	.007	.004	.007	.006	MS
2SM	.021	.020	.028	.017	.022	.021	2SM
2N	...	.072	.048	.044	.094	.066	2N
M <sub>2</sub> N	...	.038	.099	.037	.105	.024	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	...	.015	.016	.025	.026	.025	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	...	.008	.003	.003	.004	.005	2M <sub>2</sub> K <sub>1</sub>
Mm	.020	.017	.005	.010	.001	.034	Mm
Mf	.056	.067	.048	.053	.036	.048	Mf
MSf	.019	.007	.018	.014	.018	.036	MSf
Sa	.299	.062	.251	.218	.165	.255	Sa
Ssa	.106	.134	.110	.153	.157	.201	Ssa

## TIDAL OBSERVATIONS.

*Values of H's at Port Blair—(Continued).*

TIDE	H						TIDE
	1886-87	1887-88	1888-89	1889-90	1890-91*	1890-91†	
	Feet	Feet	Feet	Feet	Feet	Feet	
S <sub>1</sub>	0.024	0.022	0.018	0.010	0.017	0.013	S <sub>1</sub>
S <sub>2</sub>	.953	.914	.961	.924	.966	.974	S <sub>2</sub>
S <sub>4</sub>	.002	.007	.004	.002	.002	.001	S <sub>4</sub>
S <sub>6</sub>	.003	.002	.001	.001	.001	.001	S <sub>6</sub>
S <sub>8</sub>	.002	.002	.001	.001	.002	.002	S <sub>8</sub>
M <sub>1</sub>	.017	.024	.021	.006	.006	.007	M <sub>1</sub>
M <sub>2</sub>	1.986	1.911	2.052	1.917	1.990	2.021	M <sub>2</sub>
M <sub>3</sub>	0.007	0.003	0.005	0.009	0.005	0.008	M <sub>3</sub>
M <sub>4</sub>	.008	.022	.008	.008	.006	.006	M <sub>4</sub>
M <sub>6</sub>	.006	.006	.002	.002	.001	.007	M <sub>6</sub>
M <sub>8</sub>	.002	.003	.001	.001	.002	.003	M <sub>8</sub>
O	.152	.160	.155	.149	.157	.157	O
K <sub>1</sub>	.397	.388	.400	.387	.393	.397	K <sub>1</sub>
K <sub>2</sub>	.234	.346	.287	.284	.268	.296	K <sub>2</sub>
P	.131	.141	.119	.131	.121	.122	P
J	.015	.024	.037	.036	.015	.023	J
Q	.014	.011	.018	.021	.024	.023	Q
L	.083	.112	.065	.084	.068	.102	L
N	.405	.399	.414	.401	.417	.415	N
λ	...	...	...	...	...	...	λ
ν	.100	.050	.079	.114	.127	.088	ν
μ	.080	.069	.086	.069	.090	.094	μ
R	...	...	...	...	...	...	R
T	...	.022	.099	.093	.024	...	T
MS	.003	.020	.006	.008	.013	.011	MS
2SM	.030	.018	.018	.024	.028	.027	2SM
2N	.070	.043	.076	.074	.075	.052	2N
M <sub>3</sub> N	.078	.032	.045	.060	.083	.041	M <sub>3</sub> N
M <sub>1</sub> K <sub>1</sub>	.021	.021	.023	.020	.016	.025	M <sub>1</sub> K <sub>1</sub>
2M <sub>1</sub> K <sub>1</sub>	.005	.007	.007	.008	.007	.005	2M <sub>1</sub> K <sub>1</sub>
Mm	.023	.027	.027	.049	.020	.038	Mm
Mf	.025	.063	.037	.056	.043	.053	Mf
MSf	.027	.036	.011	.025	.012	.013	MSf
Sa	.048	.203	.183	.079	.277	.241	Sa
Ssa	.105	.136	.143	.016	.027	.136	Ssa

\* Commencing 19th April, 1890.

† Commencing 24th October, 1890.

*Values of  $\kappa$ 's at Port Blair.*

TIDE	$\kappa$						TIDE
	1880-81	1881-82	1882-83	1883-84	1884-85	1885-86	
	°	°	°	°	°	°	
S <sub>1</sub>	49'42	34'84	31'03	85'49	28'34	124'99	S <sub>1</sub>
S <sub>2</sub>	315'51	313'49	314'82	316'24	320'21	321'75	S <sub>2</sub>
S <sub>4</sub>	106'86	85'60	59'04	108'44	126'03	67'89	S <sub>4</sub>
S <sub>6</sub>	152'35	98'53	142'13	175'60	167'01	99'46	S <sub>6</sub>
S <sub>8</sub>	97'77	87'61	53'13	220'60	277'60	113'63	S <sub>8</sub>
M <sub>1</sub>	22'59	253'83	238'04	312'86	288'03	314'58	M <sub>1</sub>
M <sub>2</sub>	279'22	277'40	278'45	278'81	282'02	285'19	M <sub>2</sub>
M <sub>3</sub>	20'38	11'20	15'58	24'52	27'53	41'13	M <sub>3</sub>
M <sub>4</sub>	167'28	128'16	157'93	98'75	112'31	108'16	M <sub>4</sub>
M <sub>6</sub>	342'30	206'41	42'24	165'55	133'46	232'71	M <sub>6</sub>
M <sub>8</sub>	19'00	70'00	119'77	80'27	63'87	55'82	M <sub>8</sub>
O	299'12	303'55	302'45	302'20	300'18	304'28	O
K <sub>1</sub>	326'43	327'14	326'80	327'52	330'20	332'29	K <sub>1</sub>
K <sub>2</sub>	313'96	307'82	309'73	315'28	278'59	321'64	K <sub>2</sub>
P	324'37	326'79	325'58	323'81	319'02	327'47	P
J	316'27	324'16	333'49	296'85	305'32	347'53	J
Q	236'28	241'86	232'57	255'88	254'77	250'40	Q
L	268'51	290'35	257'87	287'72	327'41	290'85	L
N	273'04	273'00	276'69	271'57	273'67	277'04	N
$\lambda$	229'02	311'02	300'96	216'41	175'94	...	$\lambda$
$\nu$	294'33	254'46	213'52	332'49	297'56	281'26	$\nu$
$\mu$	288'19	298'00	291'23	315'01	280'13	312'44	$\mu$
R	...	326'15	...	260'54	...	...	R
T	...	312'65	...	354'65	...	290'74	T
MS	153'31	206'39	284'12	183'44	107'15	173'32	MS
2SM	148'67	168'34	145'59	140'06	330'05	181'67	2SM
2N	...	254'35	301'12	240'90	281'89	239'95	2N
M <sub>2</sub> N	...	134'86	122'84	166'15	96'96	123'75	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	...	156'87	242'07	324'89	56'62	154'45	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	...	197'07	237'12	229'46	165'88	259'61	2M <sub>2</sub> K <sub>1</sub>
Mm	12'95	25'71	20'70	34'68	129'34	340'86	Mm
Mf	355'64	14'84	16'61	13'41	31'97	32'17	Mf
MSf	168'31	4'24	9'48	32'70	17'70	354'44	MSf
Sa	162'50	132'87	155'76	179'84	162'47	146'54	Sa
Ssa	165'14	196'96	169'63	176'54	176'25	180'82	Ssa

## TIDAL OBSERVATIONS.

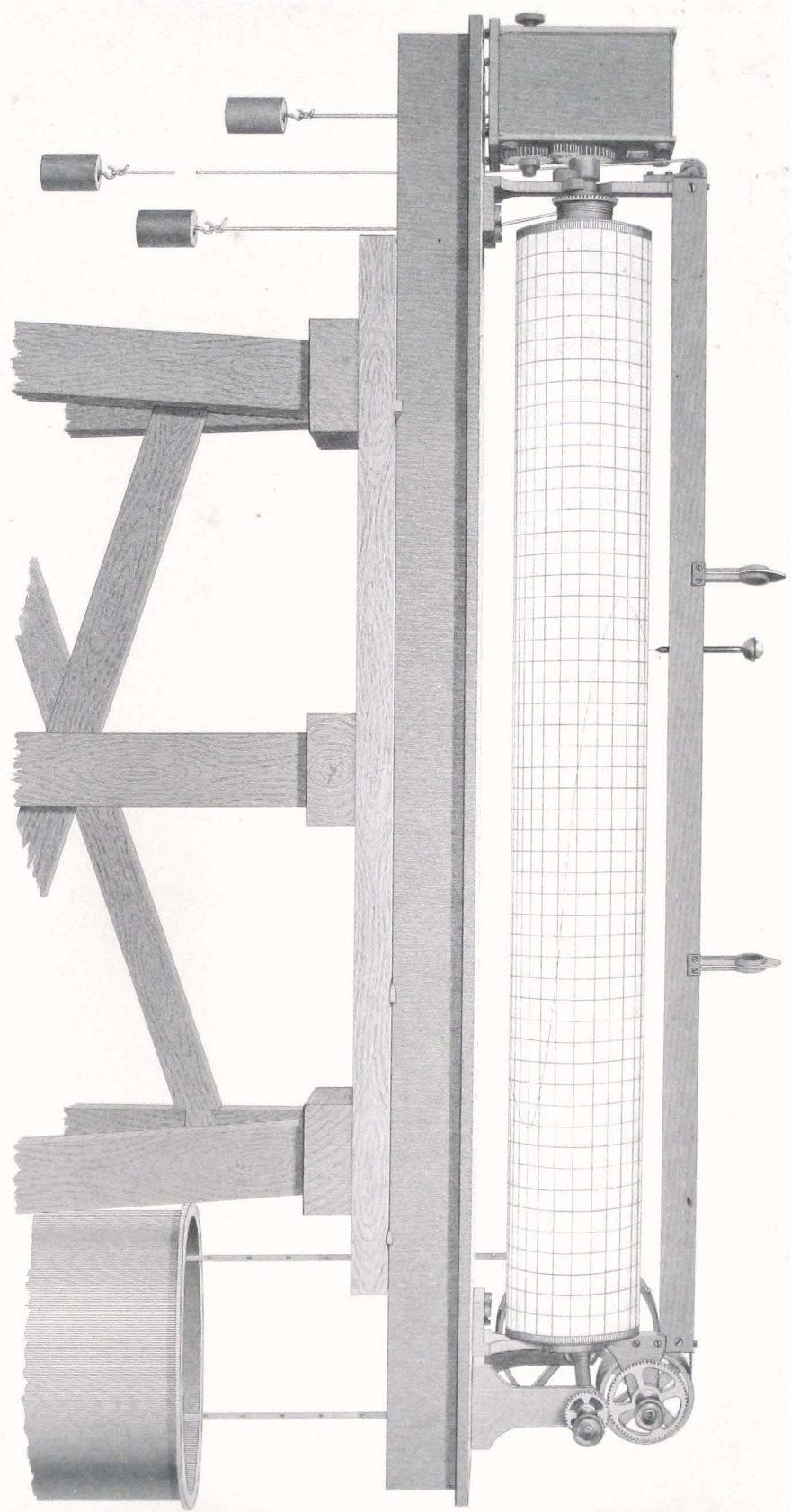
Values of  $\kappa$ 's at Port Blair—(Continued).

TIDE	$\kappa$						TIDE
	1886-87	1887-88	1888-89	1889-90	1890-91*	1890-91†	
	°	°	°	°	°	°	
S <sub>1</sub>	79.12	56.60	45.00	26.06	58.87	51.34	S <sub>1</sub>
S <sub>2</sub>	316.73	321.92	313.84	318.57	311.93	312.00	S <sub>2</sub>
S <sub>4</sub>	256.76	220.14	79.46	83.66	239.93	331.39	S <sub>4</sub>
S <sub>6</sub>	117.55	203.96	51.34	63.44	138.81	233.13	S <sub>6</sub>
S <sub>8</sub>	49.76	71.57	100.31	111.80	36.25	43.15	S <sub>8</sub>
M <sub>1</sub>	321.50	348.45	336.77	22.43	175.37	248.67	M <sub>1</sub>
M <sub>2</sub>	280.88	286.04	277.55	283.16	276.85	277.04	M <sub>2</sub>
M <sub>3</sub>	14.03	60.43	32.80	22.79	39.51	40.77	M <sub>3</sub>
M <sub>4</sub>	76.09	134.02	137.46	121.85	93.20	105.65	M <sub>4</sub>
M <sub>6</sub>	190.35	114.58	138.00	226.38	240.62	170.98	M <sub>6</sub>
M <sub>8</sub>	94.94	348.06	14.04	305.31	316.36	319.88	M <sub>8</sub>
O	301.63	306.16	302.34	304.72	299.89	299.21	O
K <sub>1</sub>	328.49	331.92	326.92	328.62	326.10	326.60	K <sub>1</sub>
K <sub>2</sub>	311.48	314.60	310.03	319.46	312.03	311.59	K <sub>2</sub>
P	325.84	335.56	328.12	327.29	325.82	327.74	P
J	329.82	301.63	318.04	335.45	299.62	308.32	J
Q	213.89	238.50	244.16	219.41	227.32	232.47	Q
L	268.61	293.50	252.96	290.87	268.71	271.09	L
N	272.52	278.97	268.56	278.72	272.04	275.74	N
$\lambda$	...	...	...	...	...	...	$\lambda$
$\nu$	232.64	228.30	317.12	285.73	241.76	223.89	$\nu$
$\mu$	285.46	313.43	294.64	307.98	284.69	290.99	$\mu$
R	...	...	...	...	...	...	R
T	...	338.63	328.56	308.84	287.40	...	T
MS	345.31	197.76	312.60	236.56	261.49	289.84	MS
2SM	145.85	155.22	176.27	140.97	144.44	135.16	2SM
2N	282.10	244.10	257.91	245.80	273.09	267.46	2N
M <sub>2</sub> N	138.41	206.94	130.13	84.54	160.20	291.15	M <sub>2</sub> N
M <sub>2</sub> K <sub>1</sub>	234.58	314.84	48.15	165.21	250.32	352.48	M <sub>2</sub> K <sub>1</sub>
2M <sub>2</sub> K <sub>1</sub>	264.40	188.01	207.80	214.88	215.84	231.48	2M <sub>2</sub> K <sub>1</sub>
Mm	9.53	34.18	20.73	46.83	260.77	289.62	Mm
Mf	294.35	352.80	6.57	359.02	14.16	358.23	Mf
MSf	73.51	17.27	281.43	47.90	94.40	111.59	MSf
Sa	124.85	172.94	125.79	347.63	152.77	130.92	Sa
Ssa	236.55	171.73	180.38	217.56	234.66	163.71	Ssa

\* Commencing 19th April, 1890.

† Commencing 24th October, 1890.

SELF-REGISTERING TIDE GAUGE,  
Constructed for the Government of India.



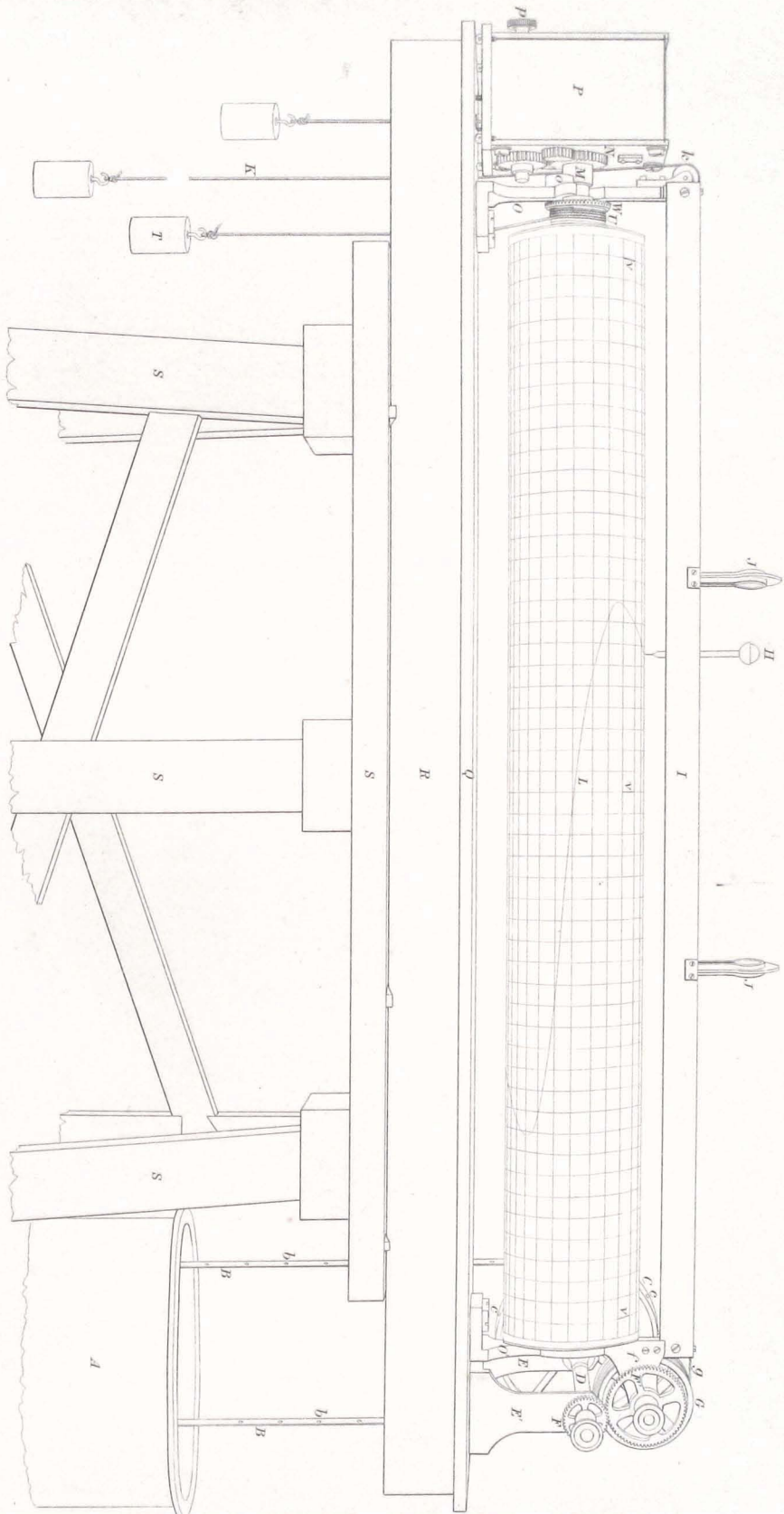
Approved at the Survey of India Office, Calcutta, December, 1891.

S. H. Gould & Co.





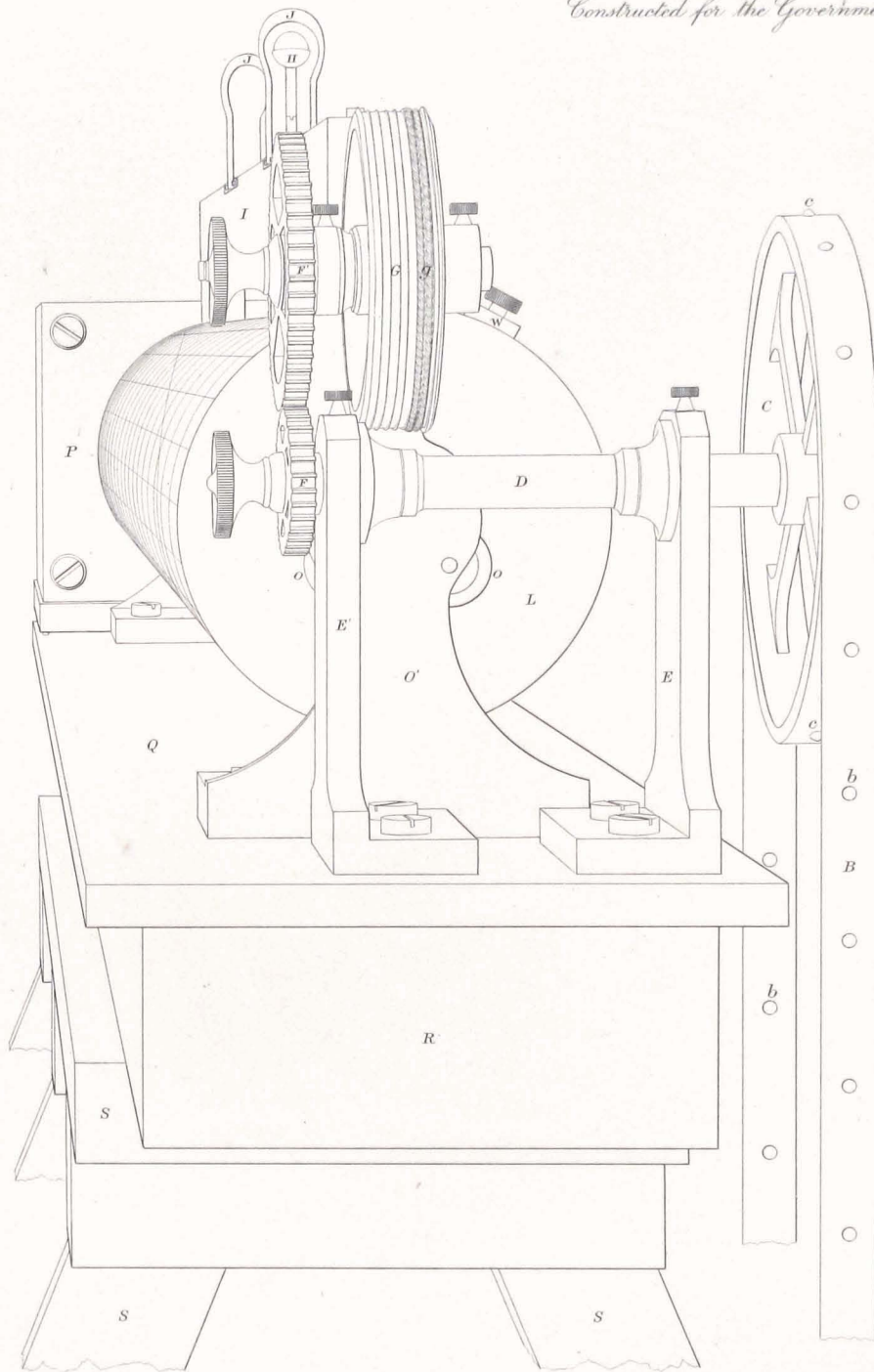
SELF-REGISTERING TIDE GAUGE,  
Constructed for the Government of India.



Figured in the Survey of India Office, Calcutta, September 1891.

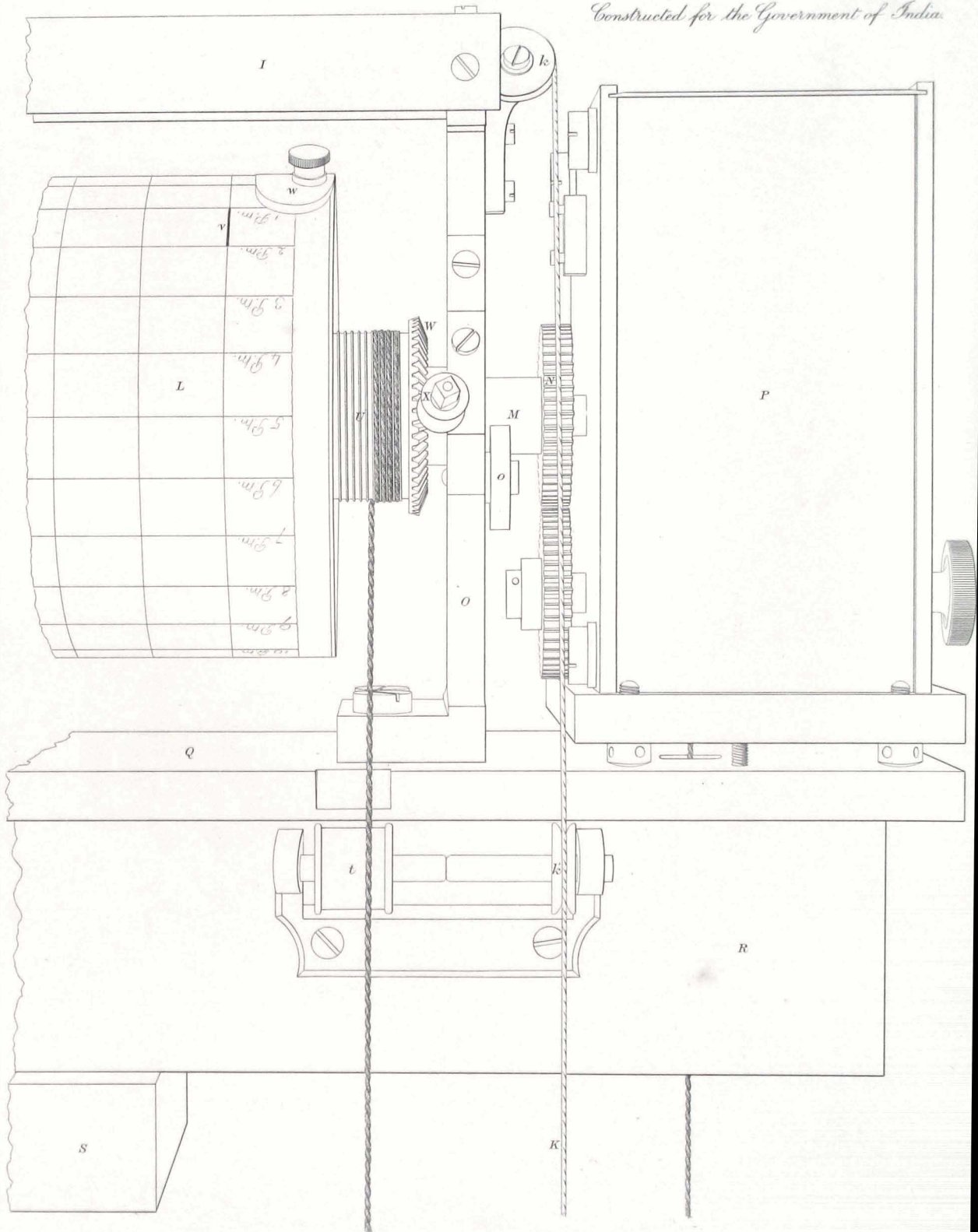


SELF-REGISTERING TIDE GAUGE,  
*Constructed for the Government of India.*





SELF-REGISTERING TIDE GAUGE,  
*Constructed for the Government of India.*





SELF-REGISTERING TIDE GAUGE,  
Constructed for the Government of India.

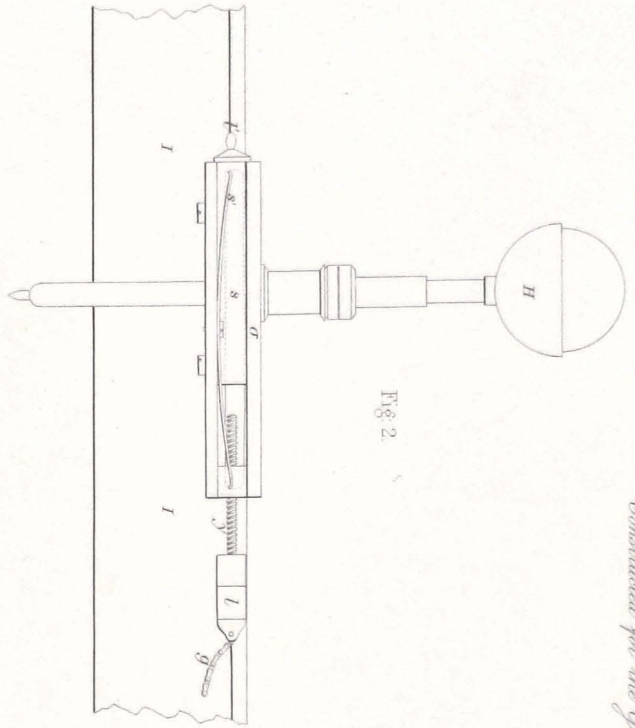


Fig. 2.

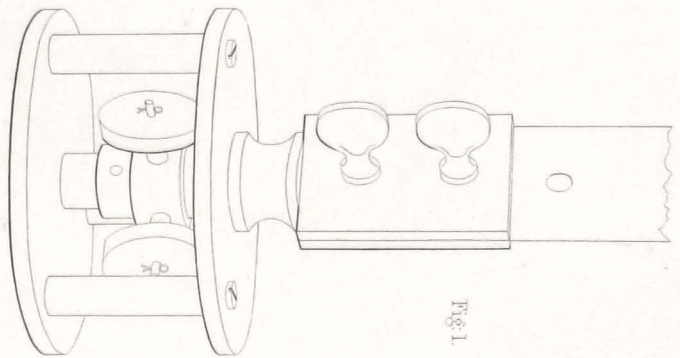


Fig. 1.

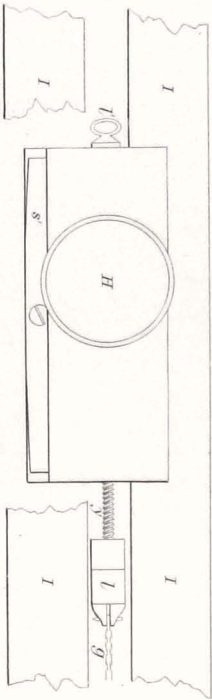


Fig. 3.

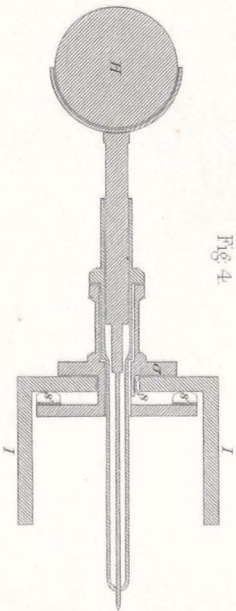


Fig. 4.

Approved at the Survey of India Office, Calcutta, March, 1892.

S.M. Dawson, Secy.

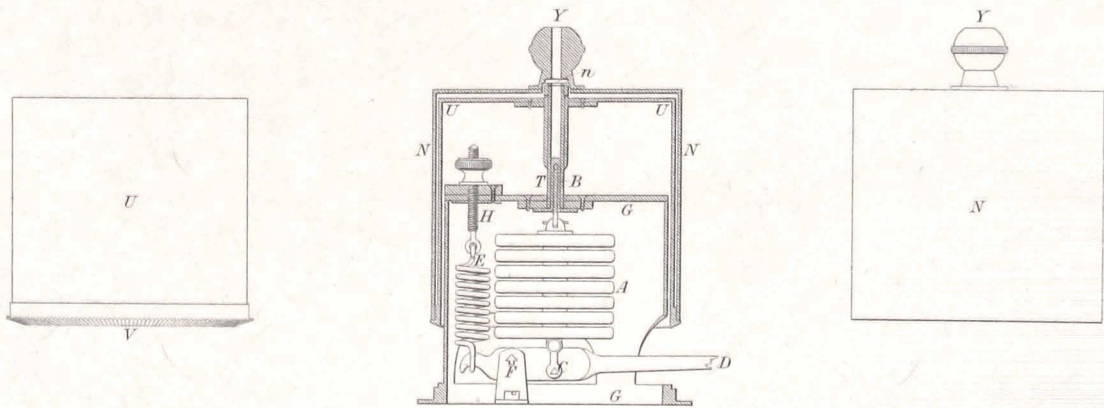
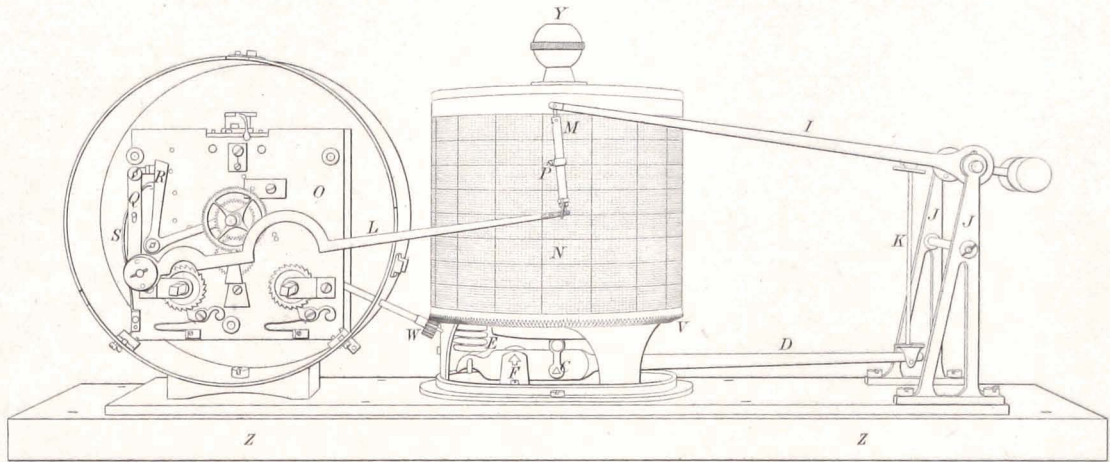




SELF-REGISTERING ANEROID,

BY MESSRS. A. LÉVÉ & C<sup>o</sup>

*Constructed for the Government of India.*



S. M. Courd. Sc.



SELF-REGISTERING ANEMOMETER,  
*Constructed for the Government of India.*

Plate VI.

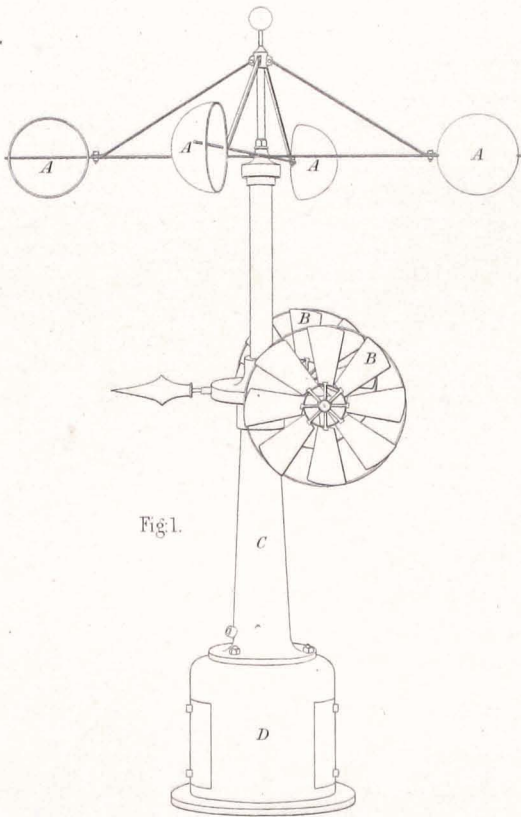


Fig. 1.

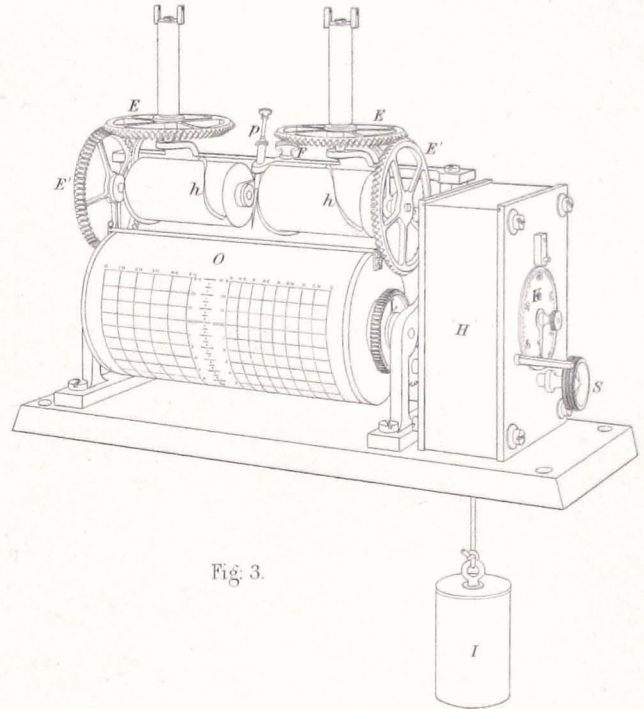


Fig. 3.

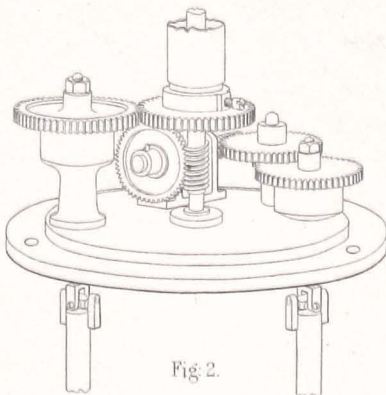


Fig. 2.

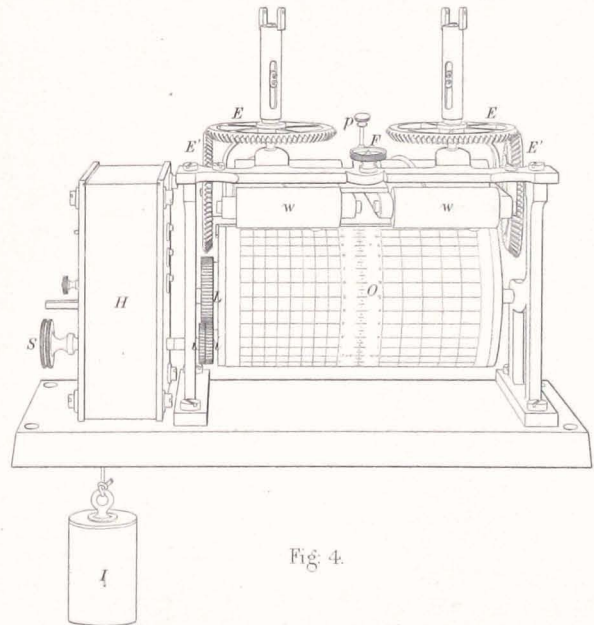
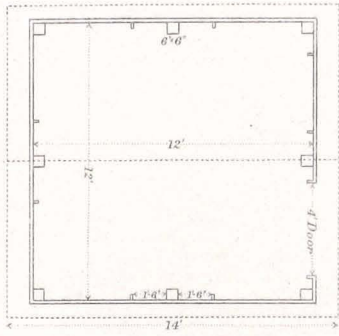


Fig. 4.

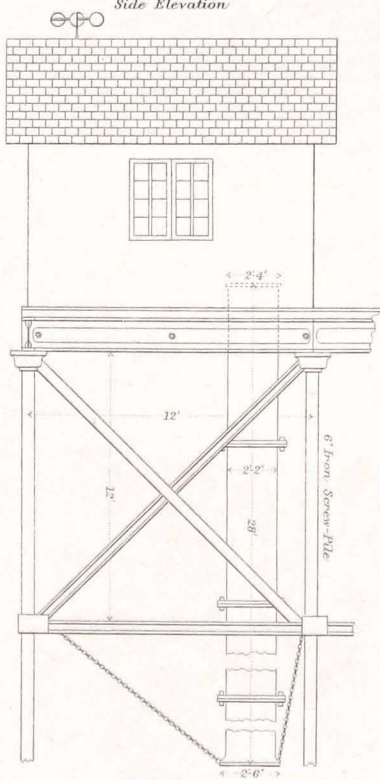
S.M. Coard, Sc.



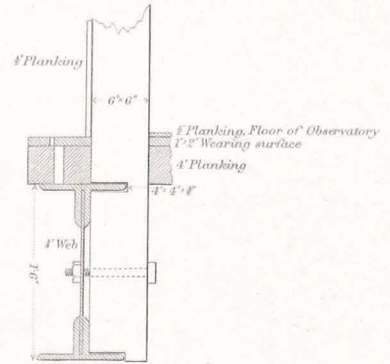


# AKYAB TIDAL OBSERVATORY.

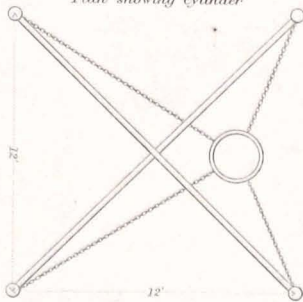
Side Elevation



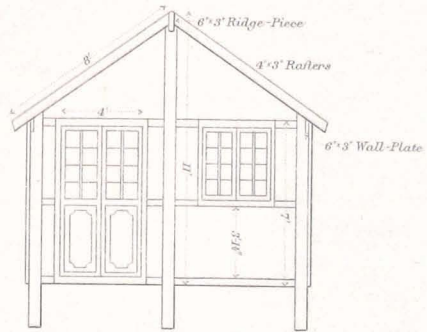
Details of fixture of Posts  
to Girders of Pier



Plan showing Cylinder



End Elevation

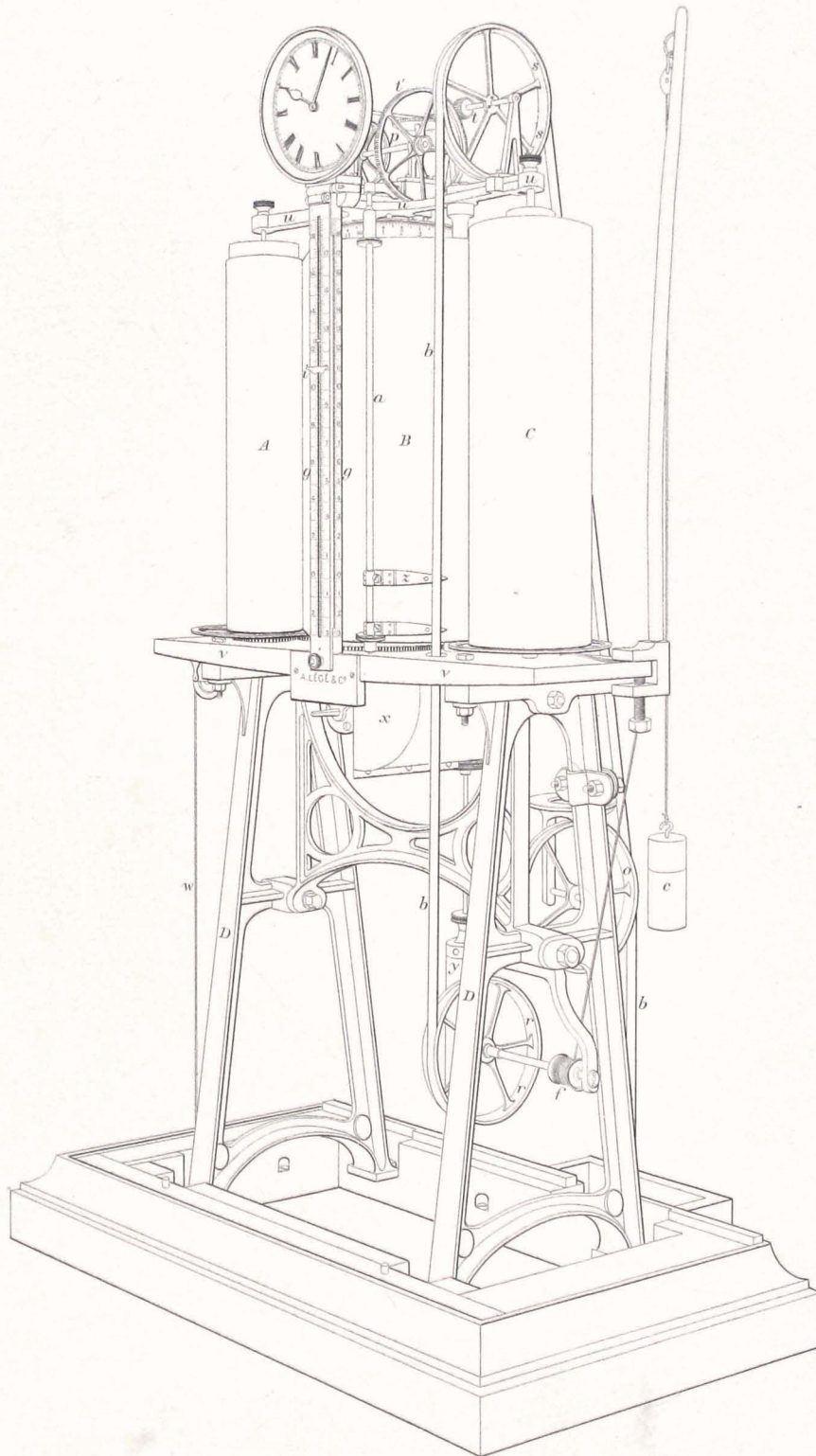






VERTICAL SELF-REGISTERING TIDE GAUGE.

BY  
A. LEGG & CO



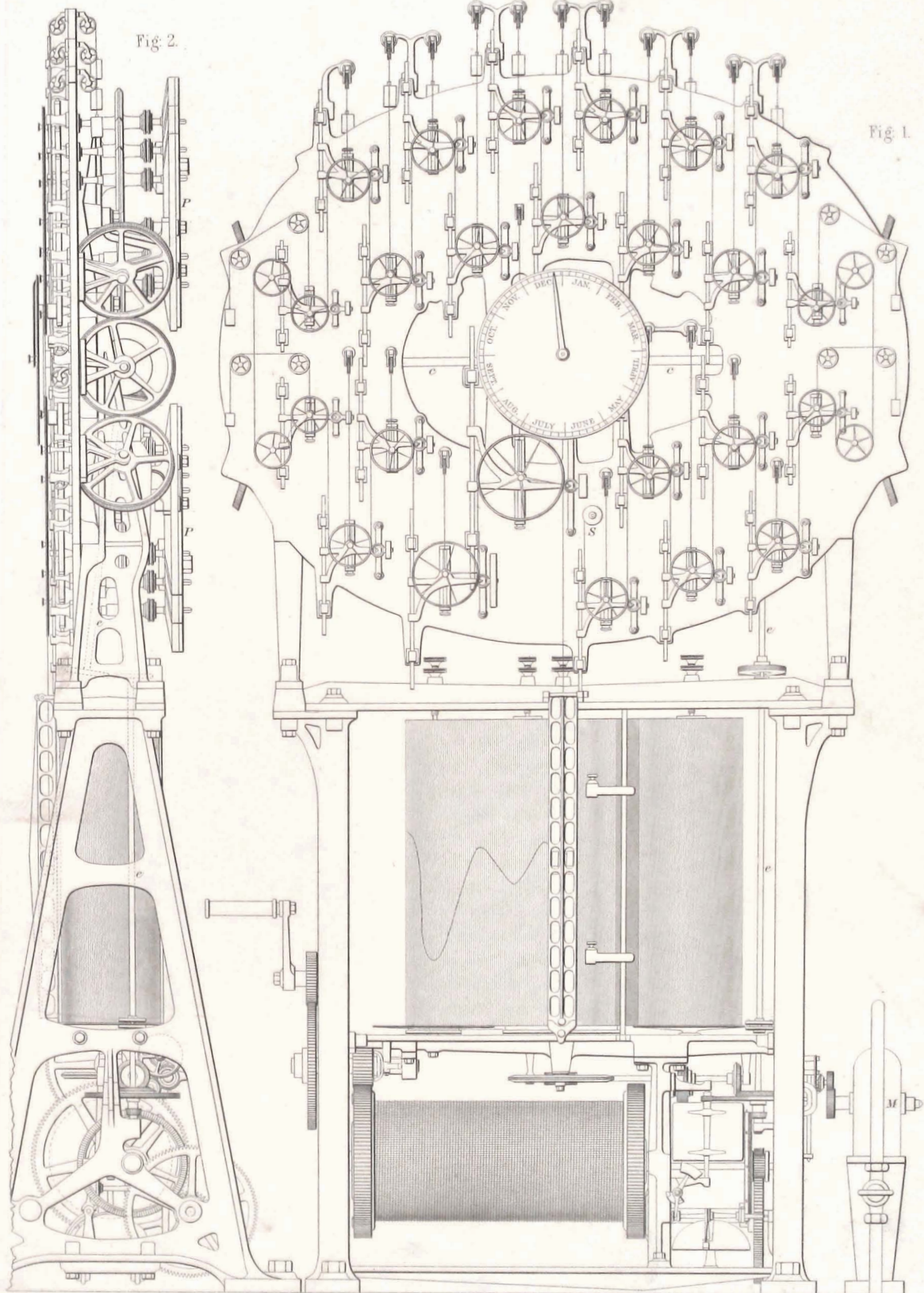




TIDE-PREDICTING MACHINE

BY

A. LÉON & C<sup>Y</sup>





TIDE-PREDICTING MACHINE.

BY

A. LÉGÉ & C<sup>o</sup>

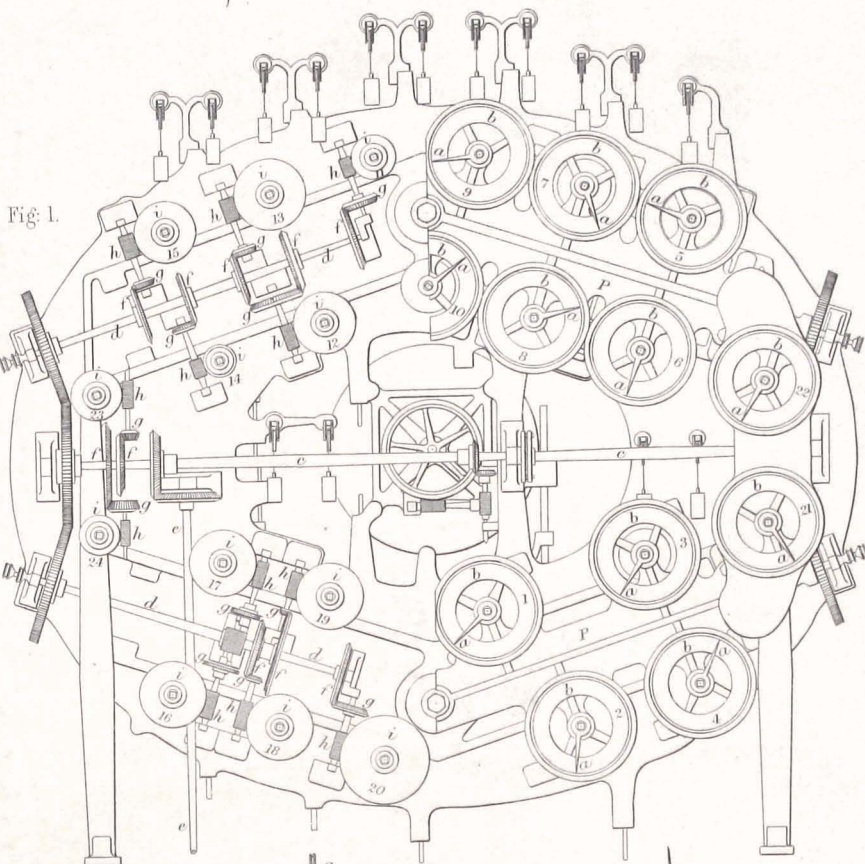


Fig. 1.

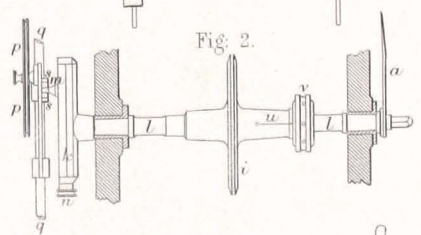


Fig. 2.

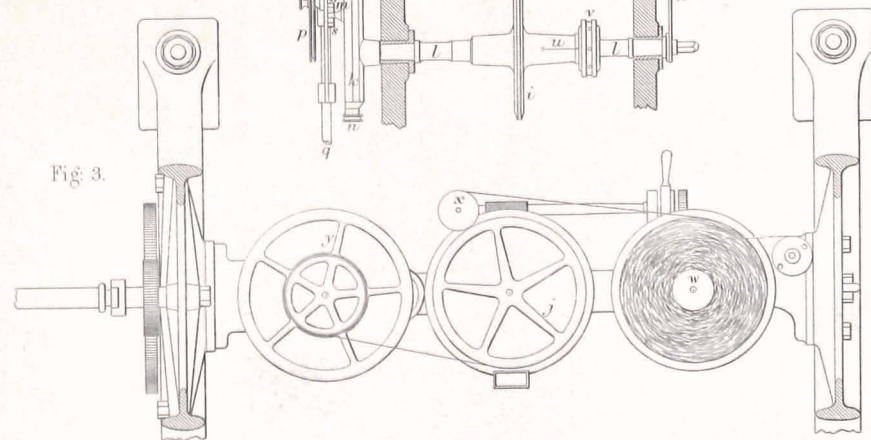


Fig. 3.





TIDE-PREDICTING MACHINE.

BY

A. LÉGER & C<sup>T</sup>

